

1 **An urban module coupled with the Variable Infiltration Capacity**  
2 **model to improve hydrothermal simulations in urban systems**

3 **Yibing Wang<sup>1</sup>, Xianhong Xie<sup>1\*</sup>, Bowen Zhu<sup>2</sup>, Arken Tursun<sup>1</sup>, Fuxiao Jiang<sup>3</sup>, Yao Liu<sup>1</sup>,**  
4 **Dawei Peng<sup>1</sup>, Buyun Zheng<sup>1</sup>**

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6 1. State Key Laboratory of Remote Sensing Science, Faculty of Geographical Science, Beijing  
7 Normal University, Beijing 100875, China

8 2. College of Water Science and Engineering, Taiyuan University of Technology, Taiyuan  
9 030024, China

10 3. Institute of Earth Surface Dynamics, University of Lausanne, 1015 Lausanne, Switzerland

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13 \*Corresponding author:

14 Xianhong Xie (Beijing Normal University, [xianhong@bnu.edu.cn](mailto:xianhong@bnu.edu.cn))

15

16 **Abstract**

17 Global urban expansion has altered surface aerodynamics and hydrothermal dynamics, aggravating  
18 environmental challenges such as urban heat/dry islands. To identify such environmental responses,  
19 various physical models, including urban canyon models (UCMs) and land surface models (LSMs),  
20 have been developed to represent surface hydrothermal processes. However, UCMs often treat a city as  
21 a unified entity and overlook subcity heterogeneity. LSMs are generally designed for natural land covers  
22 and lack the capability to capture urban characteristics. To address these limitations, the aim of this study  
23 is to couple an urban module with a sophisticated LSM, i.e., the Variable Infiltration Capacity (VIC)  
24 model. This coupled model, i.e., the VIC-urban model, is characterized by its ability to coordinate certain  
25 critical urban features, including the urban geometry, radiative interactions, and human impacts.  
26 Adopting Beijing as an evaluation site, the VIC-urban model shows higher performance than the original  
27 version, with excellent accuracy in simulating sensible heat, latent heat, runoff, and land surface  
28 temperature (LST). The absolute error is smaller than 25% for the sensible heat and latent heat, and  
29 smaller than 12% and 30% for the LST and runoff, respectively, which indicates that VIC-urban can  
30 effectively simulate hydrological and thermal fluxes in urban systems. Sensitivity analysis reveals that  
31 the roof emissivity and interception capacity exert the greatest impact on the roof temperature and  
32 evaporation, and the height-width ratio has the greatest influence on the canyon. Our work introduces a  
33 reliable option for large-scale land surface simulations that accounts for urban environments, and is  
34 among the first attempts to establish a systematic urban modelling framework of the VIC model. The  
35 VIC-urban model enables the analysis of urbanization-induced environmental changes and  
36 quantification of environmental variations among different urban configurations. The proposed model  
37 can thus offer invaluable insights for urban planners and landscape designers.

38 **Key words:** Urban canyon models; VIC model; Hydrothermal processes; Urban system; Sensitivity  
39 analysis

## 40 **1. Introduction**

41 Urban areas have been expanding globally and are characterized by increasing impervious surfaces  
42 and decreasing natural land coverage. This land cover change has led to alterations in surface  
43 aerodynamics and hydrothermal dynamics, resulting in decreased local evaporation and an exacerbation  
44 of temperature and extreme precipitation events (Yang et al., 2021). It has caused numerous  
45 environmental issues, such as urban heat islands (Morabito et al., 2021; Yao et al., 2021), urban dry  
46 islands (Meili et al., 2022; Li et al., 2021) and inundation problems (Huang et al., 2022b; Mu et al.,  
47 2020). Moreover, cities encompass unique land surface processes, which differ from those of natural  
48 land surfaces. The difference results from the diverse urban configurations, varied building materials,  
49 and human interventions (Oh and Sushama, 2021). Therefore, it is necessary to accurately quantify the  
50 impacts of urbanization and develop proper mitigation strategies (Yao et al., 2021).

51 As efficient tools, various land surface models (LSMs) have been rapidly developed in recent  
52 decades, providing unprecedented opportunities to obtain detailed information on the storage and  
53 movement of surface energy and water cycles (Bierkens et al., 2015). LSMs have been used for various  
54 applications, such as land-climate interactions (Zhong et al., 2020; Wang et al., 2020), hydrothermal  
55 environment quantifications (Zhao et al., 2019; Huang et al., 2022a), and dataset productions (Hersbach  
56 et al., 2020; Rodell et al., 2004). However, LSMs are generally formulated for natural land surfaces  
57 (Best and Grimmond, 2015), and often overlook the unique characteristics (e.g., urban configurations  
58 and buildings) of urban systems. Specific models should be developed or improved by considering the  
59 complexity and uniqueness within cities.

60 The existing urban parameterization schemes in LSMs mainly involve the bulk approach and  
61 coupling with urban canopy models (UCMs) (Ji et al., 2021; Meng, 2015). The bulk approach treats

62 urban surfaces as a regular land cover category with modified thermal and hydrological parameters (e.g.,  
63 albedo and infiltration) (Wang et al., 2020; Yang et al., 2010), but still lacks consideration of urban-  
64 specific characteristics, such as building blocking, radiative interactions (Salvadore et al., 2015),  
65 artificial heating and irrigation (Chen et al., 2022). Coupling LSMs with UCMs (hereafter referred to as  
66 LSM-UCMs) is also a popular strategy for capturing land surface processes in urban systems. Various  
67 LSM-UCMs have been favorably applied in studies (Meng, 2015; Mcnorton et al., 2021; Yang et al.,  
68 2010), including the Met Office–Reading Urban Surface Exchange Scheme (MORUSES) (Simón-  
69 Moral et al., 2019), Community Land Model-Urban (CLMU) (Oleson and Feddema, 2020), and  
70 Geophysical Fluid Dynamics Laboratory land model LM3 (LM3-UCM) (Li et al., 2016b). However,  
71 there remains a shortage of LSM-UCM models, typically oversimplifying the dynamics of land cover  
72 and climate change by using constant parameters in simulations (Kusaka et al., 2001).

73 To better represent urban environments, more suitable methodologies are needed (Yao et al., 2021).  
74 Among the various LSM models, the Variable Infiltration Capacity (VIC) model is widely used for  
75 identifying thermal and hydrological processes on land surfaces (Meng et al., 2019; Meng et al., 2020;  
76 Zhu et al., 2020). VIC is characterized by grid-independent calculation and favorable consideration of  
77 multiple layers along both horizontal (i.e., land cover types) and vertical (i.e., soil layers) directions  
78 (Liang and Xie, 2001; Liang et al., 1996). The model can be coupled with multiple remote sensing data  
79 (e.g., shortwave/longwave radiation, albedo, and leaf area index [LAI]) (Jiang et al., 2022; Meng et al.,  
80 2020; Wang et al., 2022), to consider the realistic dynamics in land surface properties and atmospheric  
81 conditions. The VIC model has been implemented in several urban-related studies based on the bulk  
82 approach, and has provided an acceptable performance in simulating energy and hydrological fluxes  
83 (Yang et al., 2010; Mishra et al., 2010; Wang et al., 2020). Yet a systematic urban calculation method

84 that considers the unique urban characteristics within VIC is still lacking.

85 In this study, we developed an urban module within the VIC model based on the Urban Tethys-  
86 Chloris model (UT&C) (Meili et al., 2020), namely, the VIC-urban model. The coupled model can  
87 efficiently identify urban hydrothermal processes when solving the water and energy balance and  
88 consider unique urban characteristics, including urban geometry, radiative interactions among urban  
89 surfaces (i.e., roof, canyon, walls, and ground), and human interference (e.g., irrigation and indoor  
90 temperature). VIC-urban can facilitate multiple urban-related researches, such as identifying long-term  
91 hydrothermal processes in urban systems, quantifying environmental changes resulting from urban  
92 expansion, and comparing environmental variations among different urban configurations. In this article,  
93 we first provide a technical description of the model coupling, process and evaluate the model in Beijing  
94 regarding the land surface temperature (LST), turbulent heat fluxes, and runoff. Further, we examine the  
95 sensitivity of the urban model input parameters to the urban environment (i.e., roof evaporation and  
96 temperature, canyon evaporation and temperature).

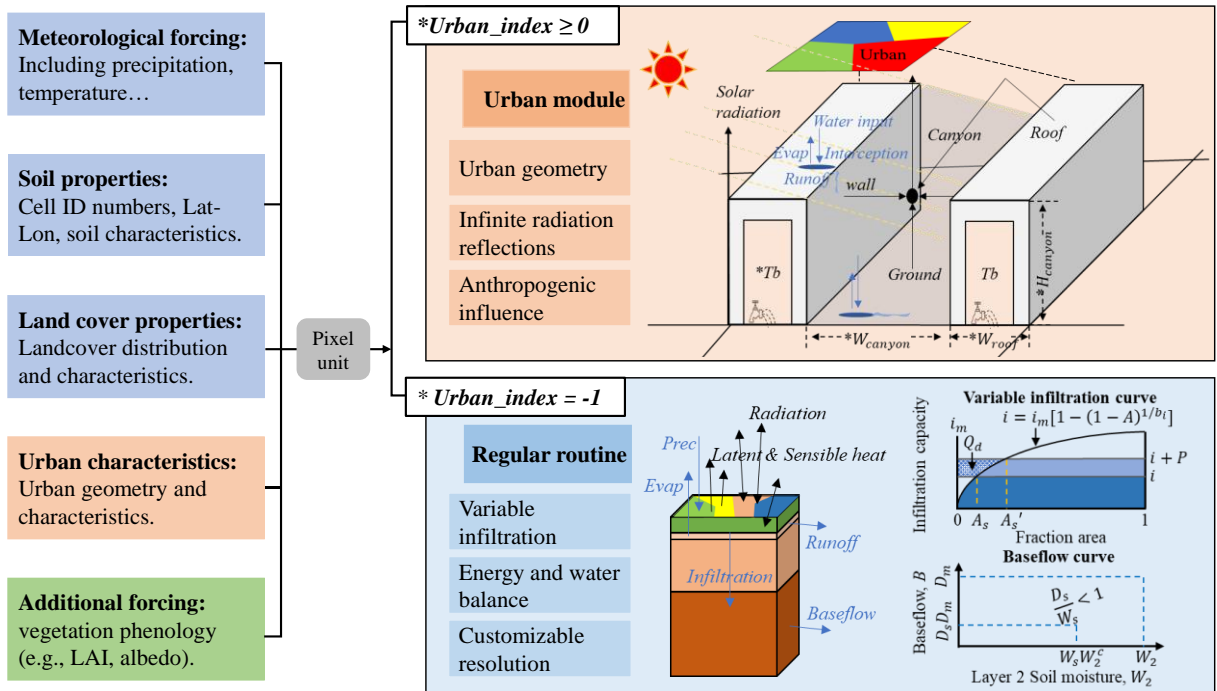
## 97 **2. Methodology**

### 98 **2.1 Urban module coupled with VIC**

99 The VIC model divides a study area into Latitude-Longitude grids, with each grid representing  
100 multiple land cover types and soil layers. It estimates hydrological and thermal processes for each  
101 subgrid land cover type in the solution of water and energy balance (Liang et al., 1994; Liang et al.,  
102 1996). However, the existing parameterization scheme ignores the unique characteristics of urban areas, such  
103 as building blockage and human influence (e.g., indoor temperature, anthropogenic heat and water inputs).  
104 Fortunately, VIC assigns a unique ID number to each grid, and labels each vegetation type within the target  
105 grid. This enables VIC to identify and compute the subgrid land cover with individual parameters, offering

116 advantages for establishing the urban module channel.

117 We integrate an urban module into the VIC model (VIC-urban). It executes the urban module for  
 118 urban tiles, and follows the same calculation routine as the original VIC model for the other land cover  
 119 tiles. Specifically, the model uses two parameters (i.e., Gridcell and Urban\_index) to identify urban tiles,  
 120 as shown in Figure 1. Gridcell is the ID number of the target grid. Urban\_index serves as an index to  
 121 ascertain the presence of an urban tile, and to identify the urban tile label in the target grid. Urban\_index  
 122 is equal to  $n-1$  if the urban tile is the  $n$ th land cover type of the target grid, and equal to  $-1$  if there is no  
 123 urban tile in the grid. The VIC-urban model can thus identify the target grid and urban tile, and obtain  
 124 the parameters of the urban tile (i.e., the parameters of the  $[Urban\_index+1]$ th land cover type in the  
 125 target grid).



116  
 117 **Figure 1.** Diagram of the urban module coupled with the VIC model.  $*W_{canyon}$ ,  $*W_{roof}$ ,  $*H_{canyon}$  are  
 118 parameters that describe the urban geometry (canyon width, roof width, and canyon height).  $*T_b$  is the indoor  
 119 temperature. The parameters including  $A_s$  and  $D_s$  are defined by the original VIC model, and detailed  
 120 information can be found on the VIC website.

121 The urban module implemented in our study is based on the methods described in Meili et al.  
 122 (2020). The urban tile is parameterized by three urban geometry parameters (canyon height, canyon

123 width, and roof width) and four urban surfaces (roof, impervious ground, sunlit and shaded walls). The  
124 hydrothermal fluxes and states (e.g., turbulent heat fluxes and land surface temperature) are individually  
125 calculated for each urban surface, considering the urban geometry, radiative interaction, and water and  
126 energy budgets. In addition, the urban module accounts for human impacts, including indoor  
127 temperature, and artificial heating and irrigation. We present core formulations of the urban processes  
128 and related parameters in Subsections 2.2-2.5. A more detailed explanation is included in the  
129 Supplementary Document and Meili et al. (2020).

## 130 **2.2 Energy balance in the urban module**

131 The newly developed urban module in VIC-urban treats the energy balance differently between  
132 the upper (i.e., roof) and lower canyon surfaces (i.e., ground and walls). For the roof surface, both short-  
133 and longwave radiation values are calculated similar to those on bare soil, as the model assumes no  
134 obstruction or radiative interaction on roofs (Supplementary Section 1.1). For the ground and walls, the  
135 model first computes the incoming direct shortwave radiation as a function of the urban geometry, solar  
136 position, and grid location (Supplementary Section 1.2). Then, it estimates the temperature, net absorbed  
137 radiation, and turbulent fluxes of each surface according to the sky-view factor (Supplementary Section  
138 1.5) and infinite radiation reflections among the various surfaces (i.e., ground, sunlit and shaded walls,  
139 and sky) based on energy and water budgets. The detailed calculation method for the radiation can be  
140 found in Supplementary Section 1, and that for the turbulent fluxes can be found in Supplementary  
141 Section 2.

142 The energy balance of the roof, ground and wall can be calculated as:

$$143 \quad EB_i = S_{abs,i} + L_{abs,i} - G_i - H_i - LE_i, \quad (1)$$

144 where  $EB_i$  is the energy balance of surface  $i$ , and  $S_{abs,i}$  and  $L_{abs,i}$  [ $\text{W m}^{-2}$ ] are the net absorbed short-

145 and longwave radiation values, respectively, of surface  $i$  (roof, ground, and wall).  $G_i$ ,  $H_i$ , and  $LE_i$  are  
 146 the conductive heat, sensible heat and latent heat fluxes, respectively, of surface  $i$ , and they can be  
 147 calculated as:

$$148 \quad H_i = \rho_a C_p \frac{T_i - T_a}{r}, \quad (2)$$

$$149 \quad LE_i = \lambda \rho_a \frac{q_{sat,T_i} - q_a}{r}, \quad (3)$$

$$150 \quad G = -\lambda g \frac{(T_{int} - T_i)}{z}, \quad (4)$$

151 where  $\rho_a$  [ $\text{kg m}^{-3}$ ] is the air density,  $C_p$  [ $\text{J kg}^{-1} \text{K}^{-1}$ ] is the specific heat capacity of air at a constant pressure,  
 152  $T_i$  [K] is the temperature of surface  $i$ , [ $\text{s m}^{-1}$ ] is the sum of the resistance values,  $\lambda$  [ $\text{J kg}^{-1}$ ] is the latent heat  
 153 of vaporization, and  $q_{sat,T_i}$  [-] is the saturation specific humidity at temperature  $T_i$ . Notably, for the surface  
 154 above the canyon (i.e., canyon roof),  $T_a$  [K] and  $q_a$  [-] are the air temperature and specific humidity,  
 155 respectively, and for the ground and walls,  $T_a$  [K] and  $q_a$  [-] are the canyon temperature and specific  
 156 humidity at the canyon reference height, respectively (Supplementary Section 2.5). Moreover,  $\lambda g$  [ $\text{J K}^{-1}$   
 157  $\text{m}^{-1} \text{s}^{-1}$ ] is the heat conductivity, and  $z$  is the thickness of the layer.  $T_{int}$  is the interior building temperature,  
 158 which can be calculated from the outdoor and indoor temperatures based on the thermal conductivity  
 159 parameters (Supplementary Section 2.2).

160 The energy balance of an urban canyon can be expressed as:

$$161 \quad EB_{can} = Q_{can} + H_g + h_{can} (H_{wsun} + H_{wshd}) + LE_g - H_{can} - LE_{can}, \quad (5)$$

162 where  $EB_{can}$  is the energy balance of the canyon,  $Q_{can}$  is anthropogenic heat, which can be prescribed  
 163 according to associated observations or estimated from other formulations.  $H$  and  $LE$  are the sensible  
 164 heat and latent heat fluxes, respectively, and the subscripts  $g$ ,  $can$ ,  $wsun$ , and  $wshd$  denote the ground,  
 165 canyon, sunlit wall, and shaded wall, respectively.  $h_{can}$  [-] is the canyon height normalized by the canyon  
 166 width ( $H_{can} / W_{can}$ ).

167 The turbulent heat fluxes of canyon can be calculated as the area-weighted average of the walls and



168 ground and directly include the anthropogenic heat input (Equation 6), and the total turbulent fluxes of  
 169 an urban tile can be calculated as the area-weighted average of the roof and urban canyon (Equation 7):

$$170 \quad X_{can} = w_{can} X_g + h_{can} (X_{wsun} + X_{wshd}) + Q_{can}, \quad (6)$$

$$171 \quad X_{urban} = f_{roof} X_{roof} + f_{can} X_{can}, \quad (7)$$

172 where  $X$  [ $\text{W m}^{-2}$ ] denotes the turbulent heat fluxes (i.e., latent or sensible heat fluxes),  $f_{roof}$  and  $f_{can}$   
 173 [-] are the roof and canyon fractions, respectively, and  $Q_{can}$  [ $\text{W m}^{-2}$ ] is the anthropogenic heat input.  
 174 The subscripts  $g$ ,  $can$ ,  $wsun$ , and  $wshd$  denote the ground, canyon, sunlit wall, and shaded wall,  
 175 respectively.

### 176 **2.3 Water balance in the urban module**

177 The urban module computes the water mass balance for the roof and ground individually. For the  
 178 roof, the incoming water is initially consumed by evaporation. Subsequently, runoff occurs when the  
 179 remaining water exceeds the maximum water interception capacity. Runoff can be further divided into  
 180 outflow runoff and runon according to a certain ratio defined by experience. Outflow runoff flows off  
 181 the roof and turns into incoming water for the ground, while runon remains on the roof as the incoming  
 182 water for the roof at the next time step. Therefore, the incoming water is equal to the precipitation and  
 183 runon of the previous time step.

$$184 \quad Int_t - Int_{t-1} = P_t + Runon_{t-1} - E_t - Runoff_t - Runon_t, \quad (8)$$

185 where  $Int$  [ $\text{mm h}^{-1}$ ] is the interception water,  $P$  [ $\text{mm h}^{-1}$ ] is the precipitation, and  $E$  [ $\text{mm h}^{-1}$ ] is the  
 186 evaporation.

187 For the ground, the incoming water flux includes precipitation, roof runoff, anthropogenic water  
 188 input, and runoff of the previous time step. The incoming water is first consumed by evaporation and  
 189 leakage and then by runoff and runon. Outflow runoff leaves the current cell, while runon remains in  
 190 the cell as incoming water of the next time step. Notably, the model does not consider subsurface

191 hydrological fluxes within urban tiles, such as soil moisture and baseflow, since impermeable surfaces  
 192 impede vertical hydrological interactions. Therefore, the grid-scale subsurface water fluxes are assumed  
 193 to be equal to the areal-weighted mean value of the fluxes of the other land cover types in the grid.

$$194 \quad Int_t - Int_{t-1} = P_t + Runon_{t-1} + Runoff_{t,roof} + Q - E_t - Leak_t - Runoff_t - Runon_t, \quad (9)$$

195 where  $Q$  [mm h<sup>-1</sup>] is the anthropogenic water input, and currently can be prescribed by user-defined 12  
 196 monthly-cycle values, but this prescription can be improved with dynamic values according to  
 197 observations.

## 198 2.4 Parameters for the urban module

199 **Table 1.**  
 200 Overview of datasets for urban module in VIC model

Parameter	Unit	Description
Gridcell	N/A	<b>Grid cell number</b>
Urban_index	N/A	<b>Index of the veg tile containing the urban</b> , with respect to the list of veg tiles given in the veg param file for the current grid cell. Ranges 0~(Nveg-1) for a grid cell that contain urban, and set to -1 to denote the grid cell exclude urban.
Theta_canyon	°	<b>Canyon orientation</b>
Zatm	m	<b>Atmospheric forcing/reference height</b>
Qf_canyon	W/m <sup>2</sup>	<b>Human interference:</b> Anthropogenic heat input
Waterf_canyon	mm/h	<b>Human interference:</b> Anthropogenic water input
Height_canyon	m	<b>Urban geometry:</b> Height of urban canyon
Width_canyon	m	<b>Urban geometry:</b> Ground width of urban canyon
Width_roof	m	<b>Urban geometry:</b> Roof width of urban canyon
Perrunoff_R/G	N/A	<b>Water budget:</b> Percentage of excess water that leaves the roof/ground as runoff
In_max_R/G	mm	<b>Water budget:</b> Maximum interception capacity of roof/ground
Kimp_R/G	mm/h	<b>Water budget:</b> Hydraulic conductivity of roof/ground
Albedo_R/G/W	N/A	<b>Energy budget:</b> Albedo roof/ground/walls
Emissivity_R/G/W	N/A	<b>Energy budget:</b> Emissivity roof/ground/walls
Lan_dry_R/G/W	W/(m*K)	<b>Energy budget:</b> Thermal conductivity of roof/ground/walls
Cv_s_R/G/W	J/(m <sup>3</sup> *K)	<b>Energy budget:</b> Volumetric heat capacity of roof/ground/walls
Dz1_R/W	m	<b>Energy budget:</b> Thickness of first roof/wall layer
Dz2_R/W	m	<b>Energy budget:</b> Thickness of second roof/wall layer

201 For the urban module, the input data include land cover maps and urban-related parameters. The  
 202 land cover maps represent the locations of urban areas. The urban-related parameters are summarized  
 203 in Table 1. Specifically, the Gridcell and Urban\_index parameters are used to identify urban tiles,  
 204 Qf\_canyon and Waterf\_canyon denote anthropogenic forcings, and the Theta\_canyon, Zatm,

205 Height\_canyon, Width\_canyon, and Width\_roof parameters define the urban geometry. Parameters such  
206 as the hydraulic conductivity and maximum interception capacity albedo (i.e., Perrunoff, In\_max, and  
207 Kimp) are used for water budget calculation, while the other parameters (e.g., albedo, emissivity,  
208 Lan\_dry, Cv\_s, and Dz) are used for energy budget calculation.

## 209 **2.5 Input data for VIC-urban**

210 In addition to the urban-related parameters listed in Table 1, the other needed input data of the VIC-  
211 urban model are similar to those of the original VIC model, referring to Liang et al. (1994), Liang et al.  
212 (1996), and Liang and Xie (2001). In general, the input data include topographical, meteorological  
213 forcing, soil and land cover (i.e., vegetation) properties. The topographical dataset is used to delineate  
214 river networks and interpolate meteorological data. Meteorological forcings provide information on  
215 precipitation, maximum and minimum air temperatures, wind speed, and humidity. Soil data define the  
216 initial soil moisture conditions, including variable infiltration curve and saturated hydrologic  
217 conductivity, and land cover data provide vegetation conditions such as the root zone thickness and the  
218 root fraction of each vegetation type.

219 In addition to the needed forcing files, the VIC model can incorporate vegetation and radiation time  
220 series data (e.g., LAI, albedo, and shortwave/longwave radiation), which are particularly useful because  
221 they provide dynamic information on vegetation and radiation variables. By incorporating these data,  
222 the VIC model can better capture realistic land surface dynamics and energy budgets.

## 223 **3. Case description**

### 224 **3.1. Study area and data input**

225 The performance of the VIC-urban model was evaluated in simulating sensible and latent heat  
226 fluxes, runoff, and land surface temperature (LST) observations in Beijing from 2005 to 2020. Beijing

227 is the capital of China, located between 39.43-41.05°N and 115.42-117.50°E. The city has experienced  
228 rapid urbanization since 1980, with extensive urban coverage since 2000 (Wang et al., 2020). Beijing  
229 can be divided into four functional zones with varying degrees of urbanization: the Core Functional  
230 Zone (Core-Zone, with an urban fraction of ~90%), the Urban Functional Extended Zone (Extended-  
231 Zone, ~70%), the New Urban Development Zone (NewDev-Zone, ~30%), and the Ecological  
232 Conservation Zone (Eco-Zone, ~5%) (Figure 2). This evaluation primarily focused on the three highly  
233 urbanized zones (Core-Zone, Extended-Zone, and NewDev-Zone) to demonstrate the performance of  
234 VIC-urban.

235 The parameters used in the urban module were based on those reported by Jackson et al. (2010),  
236 with manual calibration of the height-to-width ratio and the wall layer thickness based on MODIS LST  
237 and runoff observation data. The height-to-width ratio is a highly sensitive parameter in LST modelling  
238 and ranges from 0.5 to 1.1 according to the MODIS LST product. The prescribed wall layer thickness  
239 ranged from 0.2 to 0.6. The values of these parameters are generally consistent with previous research  
240 (Mcnorton et al., 2021; Li et al., 2016a), where the height-to-width ratio ranges from 0.75 to 1.5 and the  
241 wall layer thickness ranges from 0.3 to 0.5. Supplementary Figure 2 illustrates the spatial distribution  
242 maps of the urban parameters.

243 Regarding the model input data of Beijing, topographical data (i.e., the digital elevation model)  
244 were obtained from the USGS with a 90-m resolution. Meteorological forcing data were produced by  
245 interpolating the data obtained from observation stations of the China Meteorological Administration  
246 (CMA) (Xie et al., 2015; Zhu et al., 2021). A soil map was obtained based on a 30 arc-second-resolution  
247 soil characteristics dataset. The soil parameters were derived based on a Chinese soil dataset (Shangguan  
248 et al., 2013; Zhu et al., 2020) and Food and Agriculture Organization (FAO) (Nijssen et al., 2001). The

249 land cover maps included base maps and urban maps. The base maps were obtained from Liu et al.  
250 (2010), which were created by merging Landsat TM digital images with a spatial resolution of 1 km and  
251 12 land cover types. The urban maps were obtained from Wang et al. (2020), which were created by the  
252 Classification Regression Tree (CART) method using Landsat images with a spatial resolution of 30 m.  
253 The land cover parameters were obtained from Zhu et al. (2020). To better reasonably reflect the land  
254 cover changes in modeling, our study updated land cover maps and related parameters (e.g., the thermal  
255 conductivity, volumetric heat capacity) every five years. Moreover, four satellite datasets, namely,  
256 Downward Shortwave Radiation (DSR), albedo, LAI, and Fraction of Vegetation Cover (FVC), were  
257 incorporated in the modelling process (Zhang et al., 2019; Liang et al., 2021) to better identify land  
258 conditions and calculate turbulent heat fluxes. The four datasets used in this study are at 0.05° spatial  
259 resolution. The DSR dataset is at daily temporal resolution, while the other three datasets are at 8-day  
260 temporal resolution. The four datasets were obtained from Global Land Surface Satellite (GLASS)  
261 products (<http://www.geodata.cn/thematicView/GLASS.html>) (Liang et al., 2021). The spatial/temporal  
262 resolution of the VIC modelling is defined as 0.0625°/3 hours in this study. To ensure consistency, all  
263 model input data were adjusted to match the same spatial resolution through a linear interpolation.

### 264 **3.2 Evaluation data and method**

265 The VIC-urban model underwent calibration using streamflow data from two watersheds and  
266 MODIS-based LST data. Then, it was validated against observations retrieved from gauge stations and  
267 MODIS data regarding sensible and latent heat, runoff, and LST. The locations of the gauge stations are  
268 shown in Figure 2, and detailed information is listed in Table 2. Four measures, namely, the Nash–  
269 Sutcliffe efficiency (*NSE*), Root Mean Squared Error (*RMSE*), relative bias (*Er*), and correlation  
270 coefficient (*R*) were used to evaluate the performance of VIC-urban.

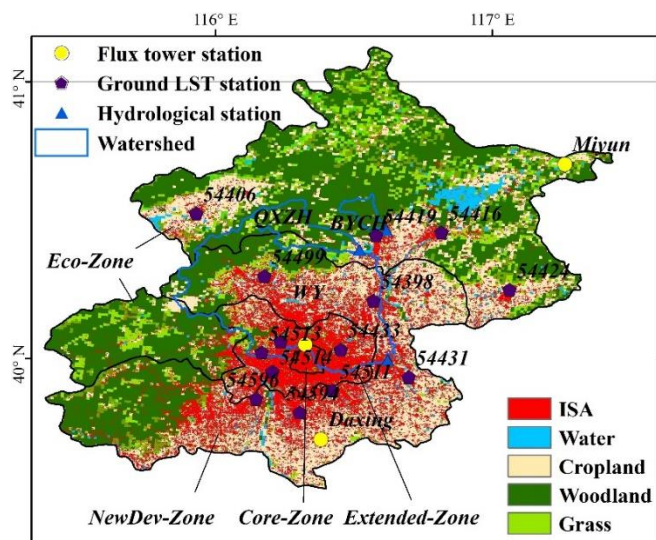
271 In regard to sensible and latent heat evaluation, three flux towers were used, namely, the Beijing,  
 272 Daxing, and Miyun stations. In particular, the Beijing station is located in the central part of Beijing and  
 273 is widely used to investigate urban turbulence characteristics (Liu et al., 2020b; Ji et al., 2021). To  
 274 calibrate and validate the simulated runoff, streamflow data from three stations were used, namely,  
 275 Boyachang (BYCH), Qianxinzhuang (QXZH), and Wenyu (WY). Their corresponding watersheds are  
 276 located in the northern part of Beijing and contain various land cover types, including urban, forest, crop,  
 277 and grass (Figure 2). The observed discharge data of the QXZH and BYCH stations were separated into  
 278 two periods for model calibration and validation, whereas the observed discharge of the WY station was  
 279 compared to the simulated runoff for the entire period due to the availability of only yearly data.

280 **Table 2.**

281 Validation data used in this work

Name	Source	Detailed information
Sensible heat	NCDDC, IAP	Beijing, 2011-2013, daily
Latent heat	NCDDC, IAP	Miyun, 2018-2010, daily Daxing, 2018-2010, daily
Runoff	AHRPR	QXZH, 2006-2009, monthly BYCH, 2006-2014, monthly
LST	CMA, MODIS	WY, 2005-2017, yearly 14 ground stations, daily MOD11A2, eight-days

NCDDC, National Cryosphere Desert Data Center; IAP, Institute of Atmospheric Physics; AHRPRC, Annual Hydrological Report for the P.R. China, CMA, China Meteorological Administration; MODIS, MODerate-resolution Imaging Spectroradiometer; QXZH, Qianxinzhuang; BYCH, Boyachang; WY, Wenyu.



282  
 283 **Figure 2.** Location of Beijing and the flux tower stations, hydrological stations and watersheds, and ground  
 284 LST stations, with the 2015 land cover map as the background.

285           Regarding LST evaluation, we obtained data from fourteen ground-based stations and one satellite-  
286 based product. At the ground-based stations of the CMA, platinum resistance sensors are used that are  
287 semi-buried in soil to measure the daily temperature at the skin surface. Among the stations, three  
288 stations provide long-term coverage data for the 2005 to 2020 period, while the remaining stations  
289 provide data covering the 2016 and 2020 period. The satellite-based LST product of the Terra Moderate  
290 Resolution Imaging Spectroradiometer (MODIS) was adopted, i.e., MOD11A2 v006  
291 (<https://modis.gsfc.nasa.gov/>). MODIS LST data constitute one of the most widely used data for LST  
292 studies (Bounoua et al., 2015; Zhou et al., 2010; Liu et al., 2020a; Morabito et al., 2021; Zhou et al.,  
293 2018). The MODIS has provided two instantaneous LST estimates (10:30 and 22:30 local solar time)  
294 every eight days since 2000, with a spatial resolution of 1 km. In our work, the simulated LST was  
295 averaged every eight days for comparison with the MODIS data. The simulated LSTs from 9:00-12:00  
296 and 21:00-24:00 were compared with the MODIS data for 10:30 and 22:30, assumed to represent the  
297 morning and evening times, respectively. Notably, the gauge-based measurements were obtained at the  
298 point scale, which is smaller than the model output resolution. To resolve the mismatch in the spatial  
299 scale, the evaluation was conducted at the subgrid scale with the same land cover type in the  
300 corresponding grid.

### 301 **3.3 Sensitivity analysis**

302           To examine the sensitivity of the model parameters to changes in the urban environment. Four  
303 fluxes, namely, roof temperature, roof evaporation, canyon temperature, and canyon evaporation, were  
304 used as indicators of the urban environment. A single grid cell with high urban coverage was selected,  
305 and its input values were used as default values. The urban input parameters range from 70% to 130%  
306 of the default values in 6% change steps. The specific parameters and their values are listed in

307 Supplementary Table 1.

308 The sensitivity analysis covered 6 years (2015-2020) and was conducted at the annual scale, as  
309 well as for the winter (December to February of the next year) and summer (June to August) seasons.

310 The sensitivity coefficient  $Sc$  can be calculated as (Beven, 1979):

$$311 \quad Sc = \lim_{X \rightarrow 0} \frac{\Delta Y / Y}{\Delta X / X} \times 100\%, \quad (10)$$

312 where  $X$  is the input parameter that affects the urban environment ( $Y$ ). A positive (or negative)  $Sc$  value  
313 suggest that  $Y$  is enhanced (or reduced) with increasing  $X$ .

## 314 **4. Results**

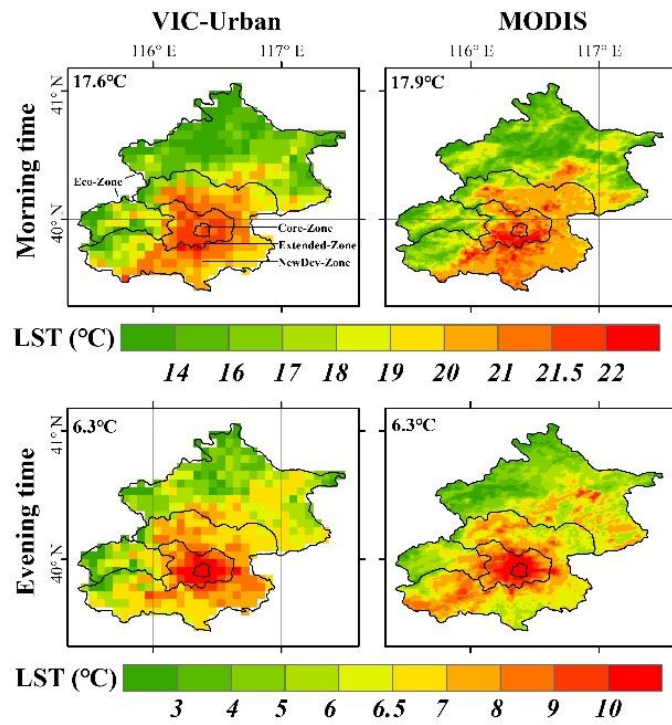
### 315 **4.1 Land surface temperature**

316 The simulated LST was calibrated against the MODIS LST and evaluated using two ground  
317 observations and the MODIS LST dataset. As shown in Figure 3, the simulated LST exhibited similar  
318 spatial patterns to those of the MODIS estimates for both the morning and evening times at the city  
319 center. At the morning time, both the VIC-urban model and MODIS data exhibited high LST values in  
320 Core-Zone and the southern part of Extended-Zone. At the evening time, the VIC-urban model  
321 simulations failed to capture the scattered LST patterns in Eco-Zone and the southwestern part of  
322 NewDev-Zone. This disagreement may be attributed to the relatively low urban fraction in these areas,  
323 given that our work mainly focused on the calculation of urban-related processes. Other than in these  
324 areas, the model could accurately produce a similar LST distribution relative to the MODIS LST data  
325 in Core-Zone and Extended-Zone.

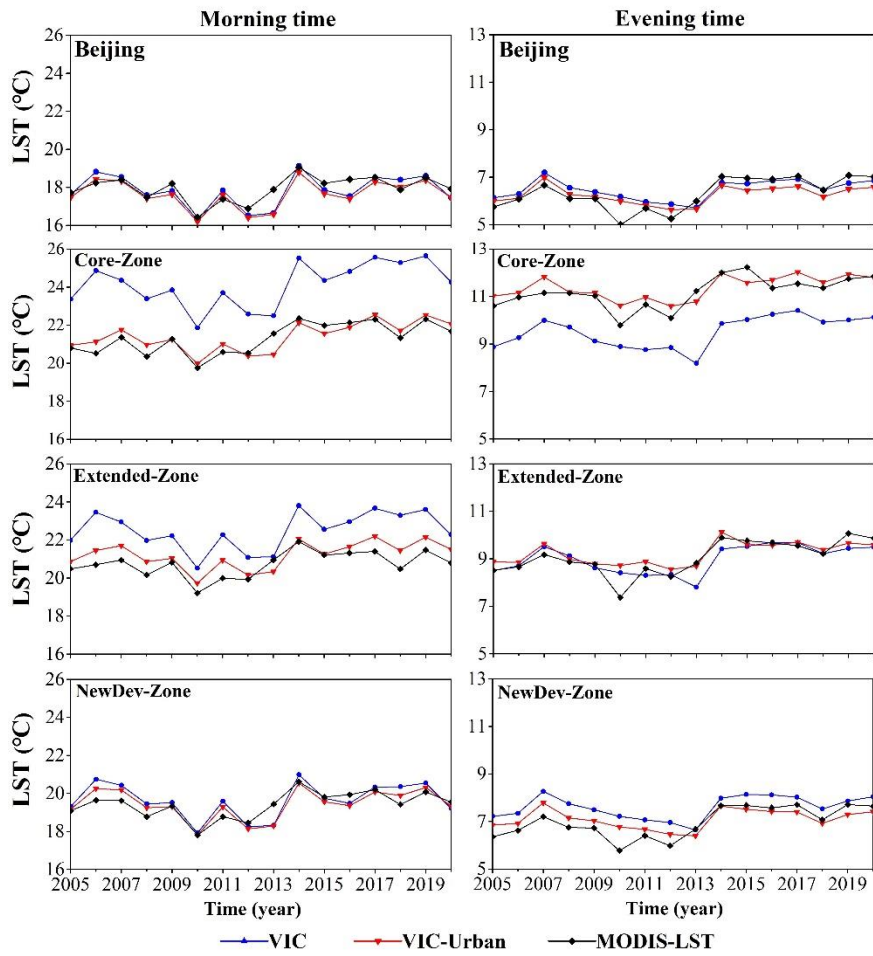
326 In terms of temporal comparison, the simulated LST exhibited a high performance in all of Beijing  
327 and the three subzones (Core-Zone, Extended-Zone, and NewDev-Zone). As shown in Figures 4 and 5,  
328 the simulated LST indicated similar yearly dynamics and mean monthly cycles relative to the MODIS



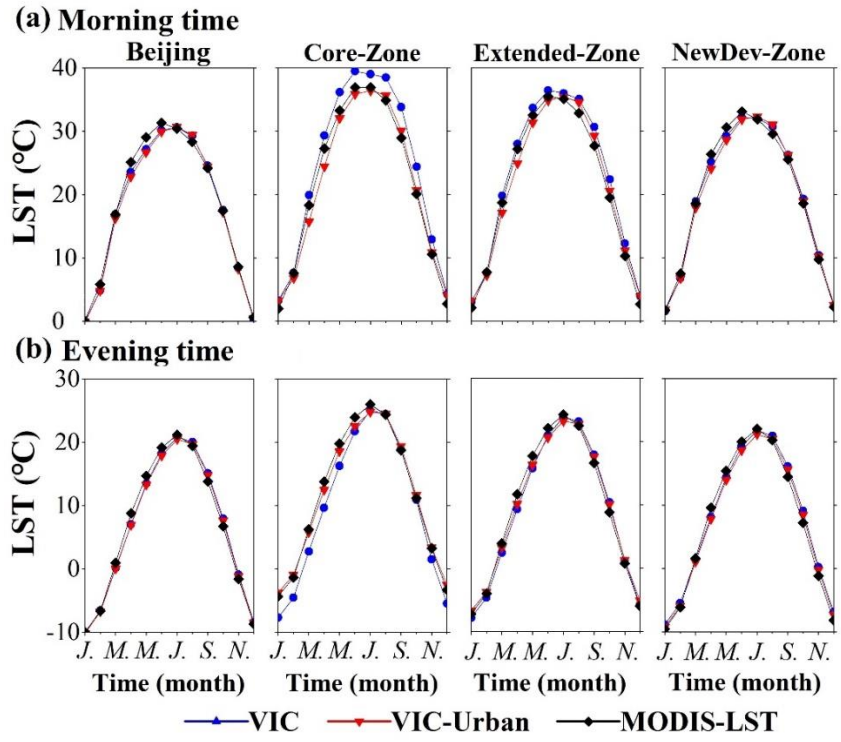
329 LST data. The  $R$  values were over 0.8, and the  $RMSE$  and  $Er$  values were lower than  $0.5^{\circ}\text{C}$  and 2.3%  
 330 for the morning and evening times, respectively. These results indicated that the simulated LST values  
 331 closely captured the temporal variations and spatial patterns of the MODIS LST data for Beijing and the  
 332 three subzones.



333  
 334 **Figure 3.** Spatial distribution of the simulated LST compared to the MOD11A2 product, with the average  
 335 LST shown in the upper left of the figure.



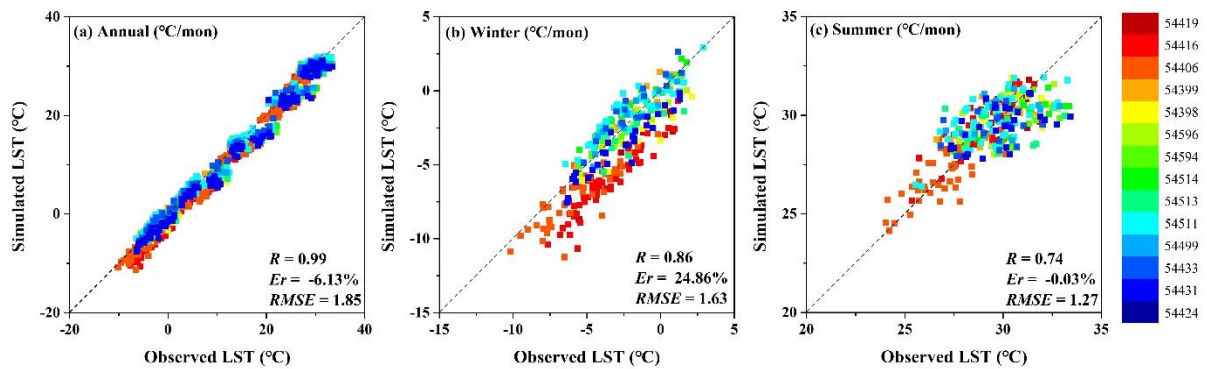
336  
 337 **Figure 4.** Yearly dynamics of the simulated LST compared to the MOD11A2 product for Beijing and the  
 338 three functional zones (i.e., Core-Zone, Extended-Zone, and NewDev-Zone).



339  
 340 **Figure 5.** Mean monthly cycle of the simulated LST compared to the MOD11A2 product for Beijing and the

341 three functional zones (Core-Zone, Extended-Zone, and NewDev-Zone).

342 In regard to station-scale comparison, the model produced satisfactory LST estimates for the annual  
 343 dynamics and during the winter and summer seasons (Figure 6). Specifically, the overall *RMSE* was  
 344 lower than 1.9 °C, *R* was higher than 0.9, and *Er* was lower than 7% at the annual scale. During the  
 345 winter and summer seasons, the *RMSE* values were lower than 1.7 °C, the *R* values were higher than  
 346 0.7, and *Er* was approximately 24.9% in winter and -0.2% in summer. The high *Er* value during the  
 347 winter season could be attributed to the low average winter LST. The comparison at each site also  
 348 indicated promising results (Table 3), with all *Er* values lower than 12% and all *RMSE* values below  
 349 1.8 °C. It is important to note that the stations generally provided only five available values, i.e., annual  
 350 data for the 2016 to 2020 period. Nevertheless, the *R* values for all the stations consistently exceeded  
 351 0.4, indicating the satisfactory performance of the VIC-urban model.



352  
 353 **Figure 6.** Monthly simulated LST validated against 14 ground-based observation stations, which are marked  
 354 in different colours.

355 **Table 3.**

356 The simulated LSTs from VIC-urban and VIC models are validated by 14 ground-based observations at an  
 357 annual scale. The results of three indexes (*Er*, *R* and *RMSE*) are shown in the table, with the better results  
 358 underlined.

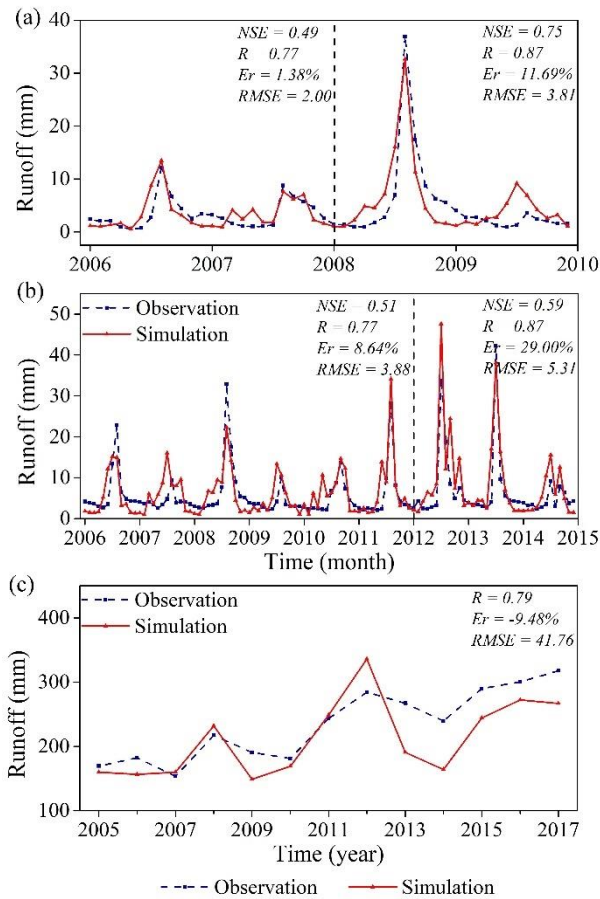
Station	<i>Er</i> (%)		<i>R</i>		<i>RMSE</i>	
	VIC-urban	VIC	VIC-urban	VIC	VIC-urban	VIC
54419	<u>-7.78</u>	-9.56	<u>0.64</u>	0.15	<u>1.19</u>	1.47
54416	-11.28	-10.58	0.79	0.89	1.63	1.52
54406	<u>-8.37</u>	-12.75	<u>0.87</u>	0.65	<u>1.06</u>	1.64
54399	<u>0.29</u>	8.61	<u>0.92</u>	0.69	<u>0.12</u>	1.28
54398	<u>-8.24</u>	-13.54	<u>0.61</u>	0.56	<u>1.34</u>	2.17
54596	-6.54	-5.29	0.63	0.68	1.07	0.88
54594	-7.10	-3.77	0.48	0.92	1.13	0.60

54514	-5.21	1.18	<u>0.92</u>	0.73	0.84	0.28
54513	-5.46	-3.54	<u>0.80</u>	0.51	0.85	0.67
54511	<u>-1.38</u>	-3.97	<u>0.73</u>	0.34	<u>0.61</u>	2.00
54499	-1.88	-1.71	<u>0.88</u>	0.72	<u>0.37</u>	0.40
54433	<u>-0.87</u>	3.09	<u>0.40</u>	0.38	<u>0.35</u>	0.58
54431	<u>-5.24</u>	-7.59	<u>0.85</u>	0.01	<u>0.85</u>	1.24
54424	<u>-11.74</u>	-12.44	<u>0.77</u>	0.46	<u>1.76</u>	1.88

359 **4.2 Runoff**

360 The model was further calibrated using the streamflow data for the QXZH and BYCH watersheds  
361 and validated against the streamflow data for the WY, QXZH, and BYCH watersheds (Figure 7). During  
362 the calibration period, the *NSE* and *R* values for the QXZH and BYCH watersheds were approximately  
363 0.5 and 0.8, respectively, and the *Er* and *RMSE* values were below 10% and 4 mm/month, respectively,  
364 for both watersheds. During the validation period, the simulated runoff showed a high correlation with  
365 the observed data of the three watersheds, with *R* ranging from 0.8 to 0.9 and *NSE* ranging from 0.6 to  
366 0.8. The *RMSE* reached approximately 4 mm/month at QXZH, 5 mm/month at BYCH, and 42 mm/yr  
367 at WY. The *Er* values were approximately 12% (QXZH), 29% (BYCH), and -9.5% (WY), respectively.

368 The overestimations at QXZH and BYCH and the underestimation at WY could likely be attributed  
369 to the limitations of the VIC-urban model in considering human activities. Specifically, the model did  
370 not consider water allocation for industrial use in the upstream region of the city (QXZH and BYCH)  
371 or the impact of industrial and domestic wastewater at the city center (WY). *Er* of the WY watershed  
372 showed an increasing trend, particularly after 2013, which could be attributed to the increasing  
373 wastewater discharge. Despite these limitations, the VIC-urban model demonstrated an acceptable  
374 performance in simulating runoff.

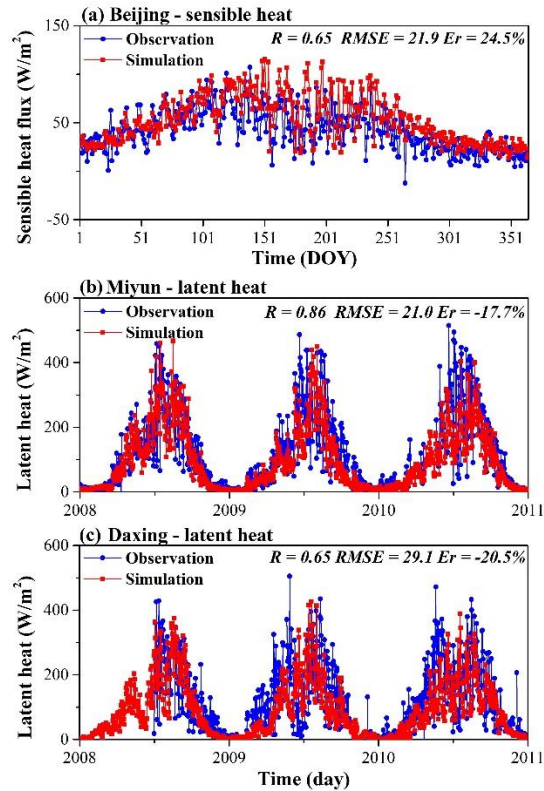


**Figure 7.** Evaluation of the simulated runoff. (a) QXZH; (b) BYCH; and (c) WY. The dark dotted line divides the data into the calibration period (before) and validation period (after).

375  
376  
377

### 378 4.3 Turbulent heat fluxes

379 The VIC-urban model was evaluated regarding the sensible and latent heat using the observed  
380 data of three stations: Beijing, Miyun, and Daxing. As shown in Figure 8a, the simulated sensible heat  
381 flux agrees well with the observed value at the Beijing station.  $R$  is approximately 0.65, and the  $RMSE$   
382 and  $Er$  are below  $22 \text{ W/m}^2$  and 25%, respectively. Regarding the latent heat (Figure 8b, c), the  
383 simulated values exhibit high correlation ( $R$ ) with the observed data at the Miyun station ( $\sim 0.86$ ), and  
384  $R$  at the Daxing station is approximately 0.65. Additionally, the  $RMSE$  values are below  $30 \text{ W/m}^2$  for  
385 all stations, and the  $Er$  values vary between  $-21\%$  and  $-17\%$ .



386

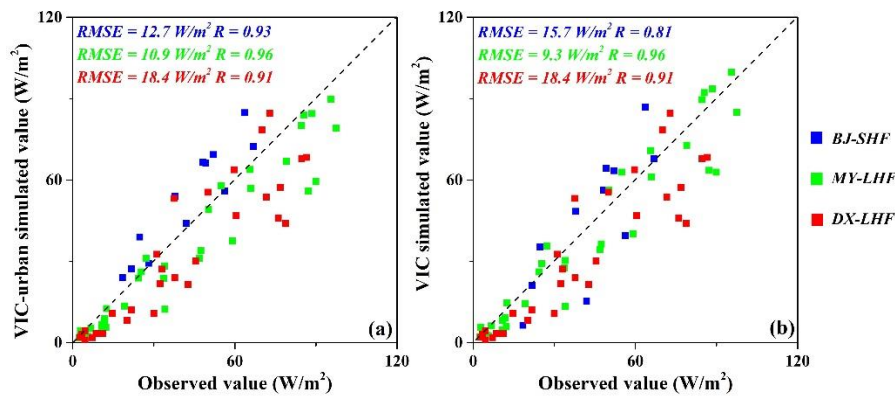
387 **Figure 8.** Evaluation of the sensible and latent heat flux simulations. (a) sensible heat flux at the Beijing flux  
 388 tower; (b) latent heat flux at the Miyun flux tower; (c) latent heat flux at the Daxing flux tower.

389 **4.4 Comparison with the original VIC**

390 The performance of the VIC-urban model and the original VIC model were compared in terms of  
 391 the simulated turbulent heat fluxes, LST, and runoff. As shown in Figure 9, the simulation results of the  
 392 VIC-urban and VIC models showed similar patterns at the Miyun and Daxing stations. However, at the  
 393 Beijing station, with a high degree of urbanization, the VIC-urban model provided a better performance.  
 394 Specifically, the VIC-urban model yielded a smaller  $RMSE$  ( $\sim 12.7 \text{ W/m}^2$ ) for the sensible heat flux than  
 395 that of the VIC model ( $\sim 15.7 \text{ W/m}^2$ ), and attained a higher correlation ( $\sim 0.93$ ) than the VIC model  
 396 ( $\sim 0.81$ ).

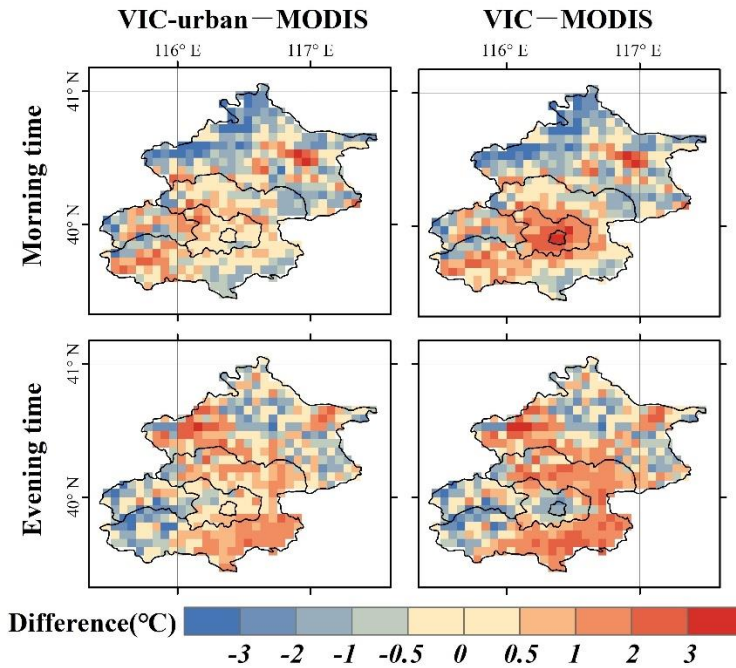
397 In terms of the LST, the VIC-urban model simulations show a lower discrepancy from the MODIS  
 398 product, especially at the city center, and the average LST difference is less than  $0.5 \text{ }^\circ\text{C}$  for both the  
 399 morning and evening times (Figure 10). However, the average LST difference is larger than  $1.8 \text{ }^\circ\text{C}$  when

400 using the VIC model. Regarding temporal comparison (Figures 3 and 4), the VIC-urban model  
 401 simulations show similar patterns to those in the MODIS data, while the VIC model simulations tend to  
 402 overestimate the LST at the morning time and underestimate the LST at the evening time in Extended-  
 403 Zone. The VIC-urban model also outperforms the VIC model at the station scale, as indicated by the  
 404 higher  $R$  and lower  $Er$  and  $RMSE$  values (Table 3).



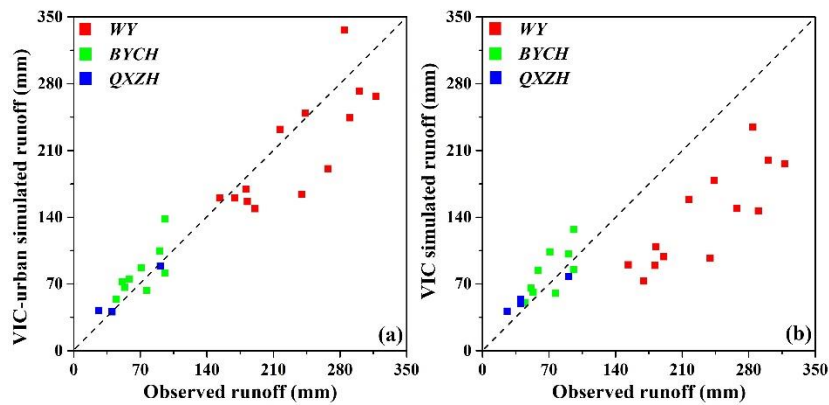
405  
 406 **Figure 9.** Simulated yearly turbulence heat fluxes of the VIC-urban and VIC models compared to the  
 407 observed data. The blue points denote the comparison of the sensible heat flux at the Beijing station, and the  
 408 green and red points denote the comparisons of the latent heat flux at the Miyun and Daxing stations,  
 409 respectively.

410 Regarding runoff (Figure 11), the VIC-urban and VIC models exhibit similar performance levels  
 411 for both the BYCH and QXZH watersheds. However, the VIC model obviously underestimates runoff  
 412 in the WY watershed, which has a high urban coverage. The  $RMSE$  values of the VIC and VIC-urban  
 413 model simulations for WY are 98.3 and 41.8 mm/yr, respectively. Based on the comparisons above, it is  
 414 evident that the VIC-urban model outperforms the original VIC model in analyzing urban-related  
 415 processes and can capture more realistic hydrological and thermal processes in cities.



416

417 **Figure 10.** Spatial distribution of the LST differences between the MODIS LST and the simulated LST of  
 418 the VIC-urban model (left), and between MODIS LST and the simulated LST of the VIC model.



419

420 **Figure 11.** Simulated yearly runoff of the VIC-urban and VIC models compared to the observed data. The  
 421 red, green, and blue points denote the comparisons in the WY, BYCH, and QXZH watersheds, respectively.

#### 422 4.5 Sensitivity analysis

423 We further calculated the sensitivity of the hydrothermal process-related urban input parameters,

424 that is, we calculated the impact on four indicators (i.e., roof temperature and evaporation and canyon

425 temperature and evaporation). Regarding the roof (Figure 12 a, b), Emissivity\_R and Albedo\_R

426 generally exhibited high sensitivity to the roof temperature, with sensitivity coefficients of  $-21\%$  and

427  $-11\%$ , respectively. The changes in In\_max\_R, Perrunoff\_R, Emissivity\_R and Albedo\_R exerted

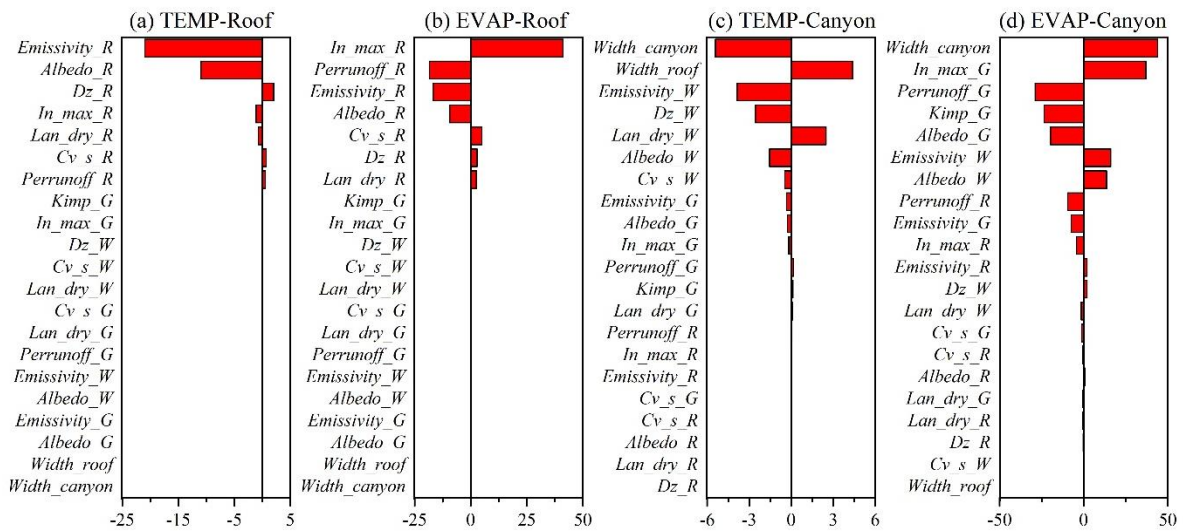


428 obvious impacts on roof evaporation, with values of 41%, -19%, -10%, and -8%, respectively.

429       Regarding the sensitivity of the canyon environment (Figure 12 c, d), Width\_canyon (-5%) and  
430 Width\_roof (4%) imposed the greatest impact on the canyon temperature, followed by Emissivity\_W  
431 (-4%), Dz\_W (-3%), Lan\_dry\_W (3%), and Albedo\_W (-2%). In terms of canyon evaporation,  
432 Width\_canyon (44%) and In\_max\_G (37%) yielded the highest impact, followed by Perrunoff\_G  
433 (-29%), Kimp\_G (-23%), Albedo\_G (-20%), Emissivity\_W (16%) and Albedo\_W (14%). An  
434 interesting finding is that the wall parameters (e.g., Emissivity\_W, Albedo\_W) generally imposed a  
435 greater influence on the canyon temperature, while the ground parameters exerted a higher influence on  
436 canyon evaporation. The sensitivity coefficients of all parameters are listed in Supplementary Table 2.

437       Supplementary Figures 3 and 4 show the urban environment (roof and canyon temperature and  
438 evaporation) changes with increasing parameter value during the summer and winter seasons. The urban  
439 environment exhibited diverse patterns under parameter increase, rather than simply following linear  
440 trajectories. An interesting discovery is that the Dz\_R and Lan\_dry\_R parameters showed opposite  
441 impacts on the roof temperature during the summer and winter seasons. This inconsistency could be  
442 attributed to their role in regulating heat transfer between indoor and outdoor environments. Specifically,  
443 indoor temperatures are higher than outdoor temperatures in winter and lower in summer. A higher  
444 thermal conductivity (i.e., higher Lan\_dry\_R and lower Dz\_R values) will increase the outdoor surface  
445 temperature in winter and decrease it in summer. Similarly, the parameters related to heat conduction  
446 (e.g., Dz\_W and Lan\_dry\_G) in canyon exerted contrasting impacts on the canyon environment during  
447 the summer and winter seasons. Moreover, parameters such as albedo and emissivity directly exerted  
448 negative impacts on both the roof and canyon temperatures and evaporation levels. Their effects on roofs  
449 are generally similar between winter and summer, and their impact on canyons is more pronounced in

450 summer than in winter.



451  
 452 **Figure 12.** Sensitivity coefficients of the parameters to the urban environment: (a) Roof temperature; (b) roof  
 453 evaporation; (c) canyon temperature; and (d) canyon evaporation.

454 **5. Discussion**

455 **5.1. Enhanced performance of VIC-urban in urban systems**

456 The urban module described above is among the first attempts to establish a systematic urban  
 457 environment in the solution of the energy and water budget in the VIC model. The VIC-urban model  
 458 incorporates detailed representations of urban canyons, urban geometry, and human influences. The  
 459 model therefore provides favorable estimates of various components of the energy and water balance  
 460 (e.g., surface runoff, evaporation, and LST) of each urban surface (i.e., roof, canyon, ground, and sunlit  
 461 and shaded walls).

462 In each urban tile, the VIC-urban model calculates the incoming radiation of each surface based on  
 463 geographic information, solar time, and geometric parameters. It then estimates energy budgets using  
 464 an iterative approach that considers radiative interactions and energy balance principles (Meili et al.,  
 465 2020). In water balance calculation, the model simulates the hydrological processes of the ground and  
 466 roof individually and assumes that roof runoff contributes to the groundwater input. Additionally, given

467 the distinct characteristics of urban areas, where excess water on a given surface tends to remain in place  
468 rather than immediately exiting the system (e.g., flat roofs and ground), the model includes a runoff  
469 component to more comprehensively represent water movement in urban environments.

470 The VIC-urban model was assessed based on the data of multiple gauge stations and MODIS LST  
471 data and compared to the original VIC model in Beijing urban areas. The results indicated that the VIC-  
472 urban model achieves excellent performance, with *RMSE* values below 0.5 and 1.8 °C relative to the  
473 MODIS LST and gauge station data, respectively, and lower than 30 W/m<sup>2</sup> and 6 mm/month in turbulent  
474 heat and runoff evaluation, respectively. Importantly, the VIC-urban model outperforms the original VIC  
475 model in urban areas. It largely reduces the discrepancy between the simulated and observed values,  
476 successfully capturing higher LST and runoff values at the urban center. These findings suggest that the  
477 VIC-urban model is a valuable tool for reliable analysis of urban areas.

## 478 **5.2 Advantages of the VIC-urban model**

479 The development of the VIC-urban model provides a new urban modelling option. It employs the  
480 canyon concept, which has been widely used in UCMs and coupled models (Oleson and Feddema, 2020;  
481 Li et al., 2016a; Sun and Grimmond, 2019). Most UCMs, such as the Surface Urban Energy and Water  
482 Balance Scheme (SUEWS) (Järvi et al., 2011), are primarily focus on water and energy balances on  
483 urban impervious surface, and generally applied at small spatial scale, such as a single city. Moreover,  
484 UCMs often neglect heterogeneity within urban areas (Kusaka et al., 2001; Meili et al., 2020). In contrast,  
485 the VIC-urban model is able to simulate hydrothermal processes for multiple land cover types, and has  
486 the strength for large-scale applications beyond urban areas (e.g., regional and global scales). The VIC-  
487 urban offers high customizability with urban configurations and simulates hydrothermal processes at  
488 the grid cell scale. It can merge hydrothermal inputs at the subcity scale to enhance its potential for

489 predicting water and energy balances in complex urban systems.

490 Large-scale urban models provide advantages in detecting hydrothermal dynamics in urban  
491 environments due to their consideration of surface heterogeneity within a city. For instance, the CLMU  
492 model incorporates a building energy model that considers convection and longwave radiation exchange  
493 with interior building surfaces (Oleson and Feddema, 2020). The LM3-UCM model can simulate carbon  
494 exchange and considers dynamic transitions between urban, agricultural, and unmanaged tiles (Li et al.,  
495 2016a). However, these models often use constant land cover and radiation parameters over time. The  
496 VIC-urban model can continuously capture land cover and radiation dynamics by integrating remote  
497 sensing products. Furthermore, it incorporates a comprehensive thermally conductive framework that  
498 considers three distinct layers (i.e., outdoor environment, interior building, and indoor environment) and  
499 two vertical wall layers. These features are crucial for identifying long-term urban-induced  
500 environmental changes and providing a comprehensive understanding of the urban environment.

### 501 **5.3 Limitations**

502 The current version of the VIC-urban model still has certain limitations. First, the model lacks the  
503 water and energy balance related to snow melting, as well as certain anthropogenic disturbances (e.g.,  
504 drainage systems, air conditioning, and car exhaust) (Liu et al., 2021). The model also simplifies  
505 anthropogenic heat and water impacts, which are user-defined and represented by a constant setting and  
506 12-month cycle values, respectively. However, these anthropogenic influences fluctuate over time, such  
507 as anthropogenic heat input in office areas varying between weekdays and weekends. These factors may  
508 impose a significant impact on the urban environment, and need to be further studied given the  
509 availability and accuracy of data and the feasibility of methods. Second, the model does not consider  
510 horizontal interactions between land cover types and water and energy transfer in the subsoil beneath

511 impervious surfaces due to impermeable characteristics.

512 Third, the module does not explicitly formulate the type of urban vegetation (i.e., vegetation or  
513 trees in cities), which may play an important role in the hydrology and energy cycle of cities (Meili et  
514 al., 2020; Wang et al., 2018). Nevertheless, the VIC-urban model divides the study area of interest into  
515 grids and categorizes urban vegetation as forests and/or grasslands, thus estimating the water and energy  
516 balance. Moreover, the VIC-urban model introduces new parameters (Table 1) that should be estimated  
517 or calibrated before the simulation, and these parameters may cause substantial uncertainties. Notably,  
518 parameters such as `In_max_R` (maximum infiltration rate) and height-to-width ratio are influential on  
519 estimating urban temperature and evaporation patterns, as illustrated in Subsection 4.5. Cities worldwide  
520 exhibit diverse configurations and various human influences, leading to differing empirical parameters  
521 of influence. The VIC-urban model therefore requires more evaluations in cities with diverse urban  
522 environments.

## 523 **6. Conclusion**

524 In this study, we developed a new urban module in the VIC model, demonstrated its reliability and  
525 estimated the sensitivity of the model parameters. Adopting Beijing as an evaluation site, the VIC-urban  
526 model showed promising performance regarding the simulation of sensible heat, latent heat, runoff, and  
527 LST. Moreover, the VIC-urban model could better capture the LST and runoff patterns at the city center  
528 than the original VIC model. The sensitivity analysis revealed that the parameters of emissivity (i.e.,  
529 `Emissivity_R`) and maximum interception capacity of the roof (i.e., `In_max_R`) generally exert the  
530 greatest impacts on the roof temperature and evaporation, respectively, and the height-to-width ratio  
531 imposed the highest impact on the canyon temperature and evaporation.

532 The current version of the VIC-urban model still holds substantial uncertainties due to its

533 parameters and related processes and the lack of consideration of human disturbances (anthropogenic  
534 heat and water inputs), horizontal interactions, and snow dynamics. However, our work is among the  
535 first attempts to establish a systematic urban estimation within the VIC model, and the model is suitably  
536 formulated with detailed subcity configurations, human influences, and radiative balance and  
537 interactions. By considering the unique characteristics of urban areas and land cover and radiation  
538 dynamics, the VIC-urban model provides a more realistic representation of urban hydrology and thermal  
539 dynamics. Therefore, the model can be a valuable tool for detecting and understanding water and energy  
540 processes in urban areas, and for improving the prediction of hydrothermal fluxes and states of the urban  
541 environment.

#### 542 **Code and data availability**

543 The codes of the VIC-urban, and example file for urban parameters are available at  
544 <https://doi.org/10.5281/zenodo.10258321>. The original VIC model is available at  
545 <https://vic.readthedocs.io/en/master/Overview/ModelOverview/>, and the urban module refers to  
546 <https://doi.org/10.5194/gmd-13-335-2020> (Meili et al., 2020). The MODerate-resolution Imaging  
547 Spectroradiometer (MODIS) datasets used in this study are available at <https://modis.gsfc.nasa.gov/>. The  
548 Global LAnd Surface Satellite (GLASS) products are available at [www.glass.umd.edu](http://www.glass.umd.edu).

#### 549 **Author contributions**

550 Yibing Wang designed and implemented the model, performed the analysis, and wrote the manuscript.  
551 Xianhong Xie proposed and supervised the study, wrote and revised the manuscript. Bowen Zhu, Arken  
552 Tursun, Fuxiao Jiang created the figures and wrote Supplementary Section 1. Yao Liu, Dawei Peng, Buyun  
553 Zheng wrote Supplementary Section 2. All authors gave comments and discussions to the study.

#### 554 **Competing interests**

555 The contact author has declared that neither of the authors has any competing interests.

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558 42271021) and Open Fund of State Key Laboratory of Remote Sensing Science and Beijing Engineering  
559 Research Center for Global Land Remote Sensing Products (No. OF202204).

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