An urban module coupled with the Variable Infiltration Capacity model to improve hydrothermal simulations in urban systems

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Abstract

Global urban expansion has altered surface aerodynamics and hydrothermal dynamics, aggravating environmental challenges such as urban heat/dry islands. To identify such environmental responses, various physical models, including urban canyon models (UCMs) and land surface models (LSMs), have been developed to represent surface hydrothermal processes. However, UCMs often treat a city as a unified entity and overlook subcity heterogeneity. LSMs are generally designed for natural land covers and lack the capability to capture urban characteristics. To address these limitations, the aim of this study is to couple an urban module with a sophisticated LSM, i.e., the Variable Infiltration Capacity (VIC) model. This coupled model, i.e., the VIC-urban model, is characterized by its ability to coordinate certain critical urban features, including the urban geometry, radiative interactions, and human impacts. Adopting Beijing as an evaluation site, the VIC-urban model shows higher performance than the original version, with excellent accuracy in simulating sensible heat, latent heat, runoff, and land surface temperature (LST). The absolute error is smaller than 25% for the sensible heat and latent heat, and smaller than 12% and 30% for the LST and runoff, respectively, which indicates that VIC-urban can effectively simulate hydrological and thermal fluxes in urban systems. Sensitivity analysis reveals that the roof emissivity and interception capacity exert the greatest impact on the roof temperature and evaporation, and the height-width ratio has the greatest influence on the canyon. Our work introduces a reliable option for large-scale land surface simulations that accounts for urban environments, and is among the first attempts to establish a systematic urban modelling framework of the VIC model. The VIC-urban model enables the analysis of urbanization-induced environmental changes and quantification of environmental variations among different urban configurations. The proposed model can thus offer invaluable insights for urban planners and landscape designers.

Key words: Urban canyon models; VIC model; Hydrothermal processes; Urban system; Sensitivity analysis

1. Introduction

Urban areas have been expanding globally and are characterized by increasing impervious surfaces and decreasing natural land coverage. This land cover change has led to alterations in surface aerodynamics and hydrothermal dynamics, resulting in decreased local evaporation and an exacerbation of temperature and extreme precipitation events (Yang et al., 2021). It has caused numerous environmental issues, such as urban heat islands (Morabito et al., 2021; Yao et al., 2021), urban dry islands (Meili et al., 2022; Li et al., 2021) and inundation problems (Huang et al., 2022a; Mu et al., 2020). Moreover, cities encompass unique land surface processes, which differ from those of natural land surfaces. The difference results from the diverse urban configurations, varied building materials, and human interventions (Oh and Sushama, 2021). Therefore, it is necessary to accurately quantify the impacts of urbanization and develop proper mitigation strategies (Yao et al., 2021).

As efficient tools, various land surface models (LSMs) have been rapidly developed in recent decades, providing unprecedented opportunities to obtain detailed information on the storage and movement of surface energy and water cycles (Bierkens et al., 2015). LSMs have been used for various applications, such as land-climate interactions (Zhong et al., 2020; Wang et al., 2020), hydrothermal environment quantifications (Zhao et al., 2019; Huang et al., 2022b), and dataset productions (Hersbach et al., 2020; Rodell et al., 2004). However, LSMs are generally formulated for natural land surfaces (Best and Grimmond, 2015), and often overlook the unique characteristics (e.g., urban configurations and buildings) of urban systems. Specific models should be developed or improved by considering the complexity and uniqueness within cities.

The existing urban parameterization schemes in LSMs mainly involve the bulk approach and coupling with urban canopy models (UCMs) (Ji et al., 2021; Meng, 2015). The bulk approach treats

62 urban surfaces as a regular land cover category with modified thermal and hydrological parameters (e.g.,

63 albedo and infiltration) (Wang et al., 2020; Yang et al., 2010), but still lacks consideration of urban-

64 specific characteristics, such as building blocking, radiative interactions (Salvadore et al., 2015),

65 artificial heating and irrigation (Chen et al., 2022). Coupling LSMs with UCMs (hereafter referred to as

66 LSM-UCMs) is also a popular strategy for capturing land surface processes in urban systems. Various

67 LSM-UCMs have been favorably applied in studies (Meng, 2015; Mcnorton et al., 2021; Yang et al.,

68 2010), including the Met Office–Reading Urban Surface Exchange Scheme (MORUSES) (Simón-

69 Moral et al., 2019), Community Land Model-Urban (CLMU) (Oleson and Feddema, 2020), and

70 Geophysical Fluid Dynamics Laboratory land model LM3 (LM3-UCM) (Li et al., 2016a). However,

71 there remains a shortage of LSM-UCM models, typically oversimplifying the dynamics of land cover

72 and climate change by using constant parameters in simulations (Kusaka et al., 2001).

73   To better represent urban environments, more suitable methodologies are needed (Yao et al., 2021).

74 Among the various LSM models, the Variable Infiltration Capacity (VIC) model is widely used for

75 identifying thermal and hydrological processes on land surfaces (Meng et al., 2019; Meng et al., 2020;

76 Zhu et al., 2020). VIC is characterized by grid-independent calculation and favorable consideration of

77 multiple layers along both horizontal (i.e., land cover types) and vertical (i.e., soil layers) directions

78 (Liang and Xie, 2001; Liang et al., 1996). The model can be coupled with multiple remote sensing data

79 (e.g., shortwave/longwave radiation, albedo, and leaf area index [LAI]) (Jiang et al., 2022; Meng et al.,

80 2020; Wang et al., 2022), to consider the realistic dynamics in land surface properties and atmospheric

81 conditions. The VIC model has been implemented in several urban-related studies based on the bulk

82 approach, and has provided an acceptable performance in simulating energy and hydrological fluxes

83 (Yang et al., 2010; Mishra et al., 2010; Wang et al., 2020). Yet a systematic urban calculation method

84 that considers the unique urban characteristics within VIC is still lacking.

85   In this study, we developed an urban module within the VIC model based on the Urban Tethys-

86 Chloris model (UT&C) (Meili et al., 2020), namely, the VIC-urban model. The coupled model can

87 efficiently identify urban hydrothermal processes when solving the water and energy balance and

88 consider unique urban characteristics, including urban geometry, radiative interactions among urban

89 surfaces (i.e., roof, canyon, walls, and ground), and human interference (e.g., irrigation and indoor

90 temperature). VIC-urban can facilitate multiple urban-related researches, such as identifying long-term

91 hydrothermal processes in urban systems, quantifying environmental changes resulting from urban

92 expansion, and comparing environmental variations among different urban configurations. In this article,

93 we first provide a technical description of the model coupling, process and evaluate the model in Beijing

94 regarding the land surface temperature (LST), turbulent heat fluxes, and runoff. Further, we examine the

95 sensitivity of the urban model input parameters to the urban environment (i.e., roof evaporation and

96 temperature, canyon evaporation and temperature).

2. Methodology

2.1 Urban module coupled with VIC

99   The VIC model divides a study area into Latitude-Longitude grids, with each grid representing

100 multiple land cover types and soil layers. It estimates hydrological and thermal processes for each

101 subgrid land cover type in the solution of water and energy balance (Liang et al., 1994; Liang et al.,

102 1996). However, the existing parameterization scheme ignores the unique characteristics of urban areas, such

103 as building blockage and human influence (e.g., indoor temperature, anthropogenic heat and water inputs).

104 Fortunately, VIC assigns a unique ID number to each grid, and labels each vegetation type within the target

105 grid. This enables VIC to identify and compute the subgrid land cover with individual parameters, offering

106   advantages for establishing the urban module channel.

107   We integrate an urban module into the VIC model (VIC-urban). It executes the urban module for

108   urban tiles, and follows the same calculation routine as the original VIC model for the other land cover

109   tiles. Specifically, the model uses two parameters (i.e., Gridcell and Urban_index) to identify urban tiles,

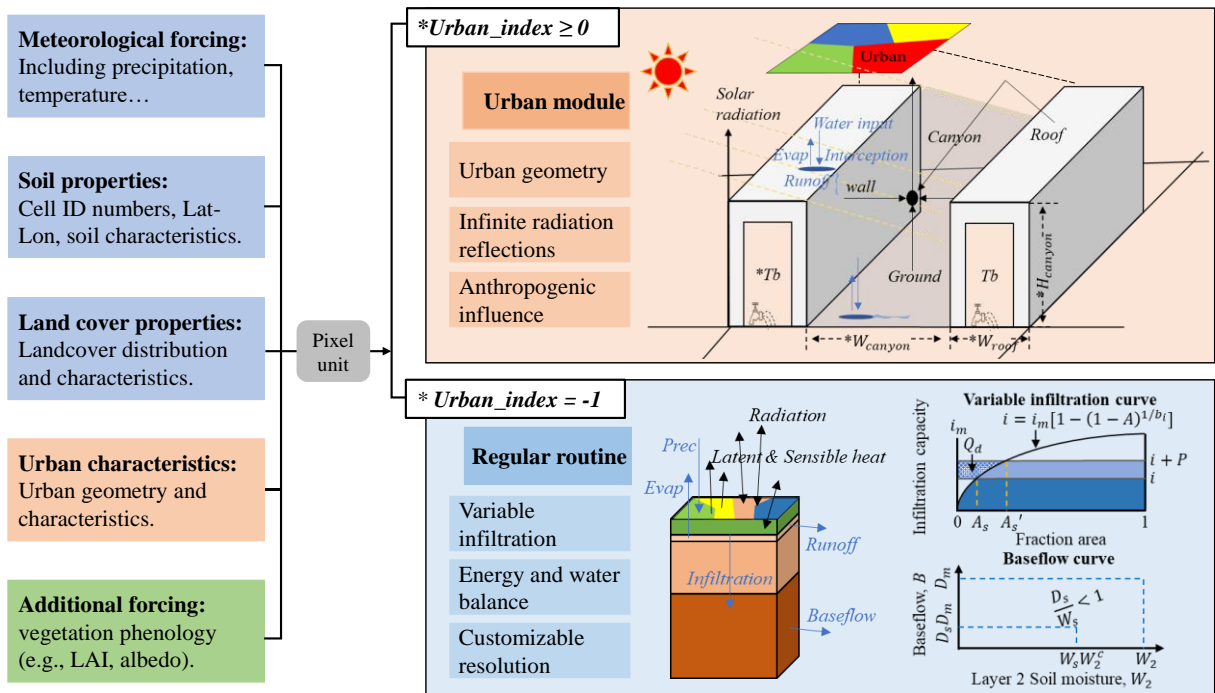
110   as shown in Figure 1. Gridcell is the ID number of the target grid. Urban_index serves as an index to

111   ascertain the presence of an urban tile, and to identify the urban tile label in the target grid. Urban_index

112   is equal to n-1 if the urban tile is the n_{th} land cover type of the target grid, and equal to -1 if there is no

113   urban tile in the grid. The VIC-urban model can thus identify the target grid and urban tile, and obtain

114   the parameters of the urban tile (i.e., the parameters of the [Urban_index+1]$_{th}$ land cover type in the

115   target grid).

116
117 **Figure 1.** Diagram of the urban module coupled with the VIC model. *Wcanyon, *Wroof, *Hcanyon* are
118 parameters that describe the urban geometry (canyon width, roof width, and canyon height). *Tb* is the indoor
119 temperature. The parameters including *As* and *Ds* are defined by the original VIC model, and detailed
120 information can be found on the VIC website.

121   The urban module implemented in our study is based on the methods described in Meili et al.

122   (2020). The urban tile is parameterized by three urban geometry parameters (canyon height, canyon

123   width, and roof width) and four urban surfaces (roof, impervious ground, sunlit and shaded walls). The

124   hydrothermal fluxes and states (e.g., turbulent heat fluxes and land surface temperature) are individually

125   calculated for each urban surface, considering the urban geometry, radiative interaction, and water and

126   energy budgets. In addition, the urban module accounts for human impacts, including indoor

127   temperature, and artificial heating and irrigation. We present core formulations of the urban processes

128   and related parameters in Subsections 2.2-2.5. A more detailed explanation is included in the

129   Supplementary Document and Meili et al. (2020).

130   **2.2 Energy balance in the urban module**

131   The newly developed urban module in VIC-urban treats the energy balance differently between

132   the upper (i.e., roof) and lower canyon surfaces (i.e., ground and walls). For the roof surface, both short-

133   and longwave radiation values are calculated similar to those on bare soil, as the model assumes no

134   obstruction or radiative interaction on roofs (Supplementary Section 1.1). For the ground and walls, the

135   model first computes the incoming direct shortwave radiation as a function of the urban geometry, solar

136   position, and grid location (Supplementary Section 1.2). Then, it estimates the temperature, net absorbed

137   radiation, and turbulent fluxes of each surface according to the sky-view factor (Supplementary Section

138   1.5) and infinite radiation reflections among the various surfaces (i.e., ground, sunlit and shaded walls,

139   and sky) based on energy and water budgets. The detailed calculation method for the radiation can be

140   found in Supplementary Section 1, and that for the turbulent fluxes can be found in Supplementary

141   Section 2.

142   The energy balance of the roof, ground and wall can be calculated as:

143        $$EB_i = S_{abs,i} + L_{abs,i} - G_i - H_i - LE_i, \tag{1}$$

144   where EB_i is the energy balance of surface i, and $S_{abs,i}$ and $L_{abs,i}$ [W m^{-2}] are the net absorbed short-

145 and longwave radiation values, respectively, of surface i (roof, ground, and wall). G_i, H_i, and LE_i are

146 the conductive heat, sensible heat and latent heat fluxes, respectively, of surface i, and they can be

147 calculated as:

148
$$H_i = \rho_a C_p \frac{T_i - T_a}{r},$$
(2)

149
$$LE_i = \lambda \rho_a \frac{q_{sat,T_i} - q_a}{r},$$
(3)

150
$$G = -\lambda g \frac{(T_{int} - T_i)}{z},$$
(4)

151 where ρ_a [kg m^{-3}] is the air density, C_p [J kg^{-1} K^{-1}] is the specific heat capacity of air at a constant pressure,

152 T_i [K] is the temperature of surface i, [s m^{-1}] is the sum of the resistance values, λ [J kg^{-1}] is the latent heat

153 of vaporization, and q_{sat,T_i} [-] is the saturation specific humidity at temperature T_i. Notably, for the surface

154 above the canyon (i.e., canyon roof), T_a [K] and q_a [-] are the air temperature and specific humidity,

155 respectively, and for the ground and walls, T_a [K] and q_a [-] are the canyon temperature and specific

156 humidity at the canyon reference height, respectively (Supplementary Section 2.5). Moreover, λg [J K^{-1}

157 m^{-1} s^{-1}] is the heat conductivity, and z is the thickness of the layer. T_{int} is the interior building temperature,

158 which can be calculated from the outdoor and indoor temperatures based on the thermal conductivity

159 parameters (Supplementary Section 2.2).

160   The energy balance of an urban canyon can be expressed as:

161
$$EB_{can} = Q_{can} + H_g + h_{can}(H_{wsun} + H_{wshd}) + LE_g - H_{can} - LE_{can},$$
(5)

162 where EB_{can} is the energy balance of the canyon, Q_{can} is anthropogenic heat, which can be prescribed

163 according to associated observations or estimated from other formulations. H and LE are the sensible

164 heat and latent heat fluxes, respectively, and the subscripts g, can, $wsun$, and $wshd$ denote the ground,

165 canyon, sunlit wall, and shaded wall, respectively. h_{can} [-] is the canyon height normalized by the canyon

166 width (H_{can} / W_{can}).

167   The turbulent heat fluxes of canyon can be calculated as the area-weighted average of the walls and

168   ground and directly include the anthropogenic heat input (Equation 6), and the total turbulent fluxes of

169   an urban tile can be calculated as the area-weighted average of the roof and urban canyon (Equation 7):

170 $$X_{can} = w_{can} X_g + h_{can}(X_{wsun} + X_{wshd}) + Q_{can},$$ (6)

171 $$X_{urban} = f_{roof} X_{roof} + f_{can} X_{can},$$ (7)

172   where X [W m^{-2}] denotes the turbulent heat fluxes (i.e., latent or sensible heat fluxes), f_{roof} and f_{can}

173   [-] are the roof and canyon fractions, respectively, and Q_{can} [W m^{-2}] is the anthropogenic heat input.

174   The subscripts *g, can, wsun*, and *wshd* denote the ground, canyon, sunlit wall, and shaded wall,

175   respectively.

176   **2.3 Water balance in the urban module**

177   The urban module computes the water mass balance for the roof and ground individually. For the

178   roof, the incoming water is initially consumed by evaporation. Subsequently, runoff occurs when the

179   remaining water exceeds the maximum water interception capacity. Runoff can be further divided into

180   outflow runoff and runon according to a certain ratio defined by experience. Outflow runoff flows off

181   the roof and turns into incoming water for the ground, while runon remains on the roof as the incoming

182   water for the roof at the next time step. Therefore, the incoming water is equal to the precipitation and

183   runon of the previous time step.

184 $$Int_t - Int_{t-1} = P_t + Runon_{t-1} - E_t - Runoff_t - Runon_t,$$ (8)

185   where Int [mm h^{-1}] is the interception water, P [mm h^{-1}] is the precipitation, and E [mm h^{-1}] is the

186   evaporation.

187   For the ground, the incoming water flux includes precipitation, roof runoff, anthropogenic water

188   input, and runoff of the previous time step. The incoming water is first consumed by evaporation and

189   leakage and then by runoff and runon. Outflow runoff leaves the current cell, while runon remains in

190   the cell as incoming water of the next time step. Notably, the model does not consider subsurface

191 hydrological fluxes within urban tiles, such as soil moisture and baseflow, since impermeable surfaces

192 impede vertical hydrological interactions. Therefore, the grid-scale subsurface water fluxes are assumed

193 to be equal to the areal-weighted mean value of the fluxes of the other land cover types in the grid.

194 $$Int_t - Int_{t-1} = P_t + Runon_{t-1} + Runoff_{t,roof} + Q - E_t - Leak_t - Runoff_t - Runon_t, \qquad (9)$$

195 where Q [mm h^{-1}] is the anthropogenic water input, and currently can be prescribed by user-defined 12

196 monthly-cycle values, but this prescription can be improved with dynamic values according to

197 observations.

2.4 Parameters for the urban module

199 **Table 1.**
200 Overview of datasets for urban module in VIC model

Parameter	Unit	Description
Gridcell	N/A	**Grid cell number**
Urban_index	N/A	**Index of the veg tile containing the urban**, with respect to the list of veg tiles given in the veg param file for the current grid cell. Ranges 0~(Nveg-1) for a grid cell that contain urban, and set to -1 to denote the gird cell exclude urban.
Theta_canyon	°	**Canyon orientation**
Zatm	m	**Atmospheric forcing/reference height**
Qf_canyon	W/m^2	**Human interference:** Anthropogenic heat input
Waterf_canyon	mm/h	**Human interference:** Anthropogenic water input
Height_canyon	m	**Urban geometry:** Height of urban canyon
Width_canyon	m	**Urban geometry:** Ground width of urban canyon
Width_roof	m	**Urban geometry:** Roof width of urban canyon
Perrunoff_R/G	N/A	**Water budget:** Percentage of excess water that leaves the roof/ground as runoff
In_max_R/G	mm	**Water budget:** Maximum interception capacity of roof/ground
Kimp_R/G	mm/h	**Water budget:** Hydraulic conductivity of roof/ground
Albedo_R/G/W	N/A	**Energy budget:** Albedo roof/ground/walls
Emissivity_R/G/W	N/A	**Energy budget:** Emissivity roof/ground/walls
Lan_dry_R/G/W	W/(m*K)	**Energy budget:** Thermal conductivity of roof/ground/walls
Cv_s_R/G/W	J/(m^3*K)	**Energy budget:** Volumetric heat capacity of roof/ground/walls
Dz1_R/W	m	**Energy budget:** Thickness of first roof/wall layer
Dz2_R/W	m	**Energy budget:** Thickness of second roof/wall layer

201   For the urban module, the input data include land cover maps and urban-related parameters. The

202 land cover maps represent the locations of urban areas. The urban-related parameters are summarized

203 in Table 1. Specifically, the Gridcell and Urban_index parameters are used to identify urban tiles,

204 Qf_canyon and Waterf_canyon denote anthropogenic forcings, and the Theta_canyon, Zatm,

205 Height_canyon, Width_canyon, and Width_roof parameters define the urban geometry. Parameters such

206 as the hydraulic conductivity and maximum interception capacity albedo (i.e., Perrunoff, In_max, and

207 Kimp) are used for water budget calculation, while the other parameters (e.g., albedo, emissivity,

208 Lan_dry, Cv_s, and Dz) are used for energy budget calculation.

209 **2.5 Input data for VIC-urban**

210 In addition to the urban-related parameters listed in Table 1, the other needed input data of the VIC-

211 urban model are similar to those of the original VIC model, referring to Liang et al. (1994), Liang et al.

212 (1996), and Liang and Xie (2001). In general, the input data include topographical, meteorological

213 forcing, soil and land cover (i.e., vegetation) properties. The topographical dataset is used to delineate

214 river networks and interpolate meteorological data. Meteorological forcings provide information on

215 precipitation, maximum and minimum air temperatures, wind speed, and humidity. Soil data define the

216 initial soil moisture conditions, including variable infiltration curve and saturated hydrologic

217 conductivity, and land cover data provide vegetation conditions such as the root zone thickness and the

218 root fraction of each vegetation type.

219 In addition to the needed forcing files, the VIC model can incorporate vegetation and radiation time

220 series data (e.g., LAI, albedo, and shortwave/longwave radiation), which are particularly useful because

221 they provide dynamic information on vegetation and radiation variables. By incorporating these data,

222 the VIC model can better capture realistic land surface dynamics and energy budgets.

223 **3. Case description**

224 **3.1. Study area and data input**

225 The performance of the VIC-urban model was evaluated in simulating sensible and latent heat

226 fluxes, runoff, and land surface temperature (LST) observations in Beijing from 2005 to 2020. Beijing

227 is the capital of China, located between 39.43-41.05°N and 115.42-117.50°E. The city has experienced

228 rapid urbanization since 1980, with extensive urban coverage since 2000 (Wang et al., 2020). Beijing

229 can be divided into four functional zones with varying degrees of urbanization: the Core Functional

230 Zone (Core-Zone, with an urban fraction of ~90%), the Urban Functional Extended Zone (Extended-

231 Zone, ~70%), the New Urban Development Zone (NewDev-Zone, ~30%), and the Ecological

232 Conservation Zone (Eco-Zone, ~5%) (Figure 2). This evaluation primarily focused on the three highly

233 urbanized zones (Core-Zone, Extended-Zone, and NewDev-Zone) to demonstrate the performance of

234 VIC-urban.

235   The parameters used in the urban module were based on those reported by Jackson et al. (2010),

236 with manual calibration of the height-to-width ratio and the wall layer thickness based on MODIS LST

237 and runoff observation data. The height-to-width ratio is a highly sensitive parameter in LST modelling

238 and ranges from 0.5 to 1.1 according to the MODIS LST product. The prescribed wall layer thickness

239 ranged from 0.2 to 0.6. The values of these parameters are generally consistent with previous research

240 (Mcnorton et al., 2021; Li et al., 2016b), where the height-to-width ratio ranges from 0.75 to 1.5 and the

241 wall layer thickness ranges from 0.3 to 0.5. Supplementary Figure 2 illustrates the spatial distribution

242 maps of the urban parameters.

243   Regarding the model input data of Beijing, topographical data (i.e., the digital elevation model)

244 were obtained from the USGS with a 90-m resolution. Meteorological forcing data were produced by

245 interpolating the data obtained from observation stations of the China Meteorological Administration

246 (CMA) (Xie et al., 2015; Zhu et al., 2021). A soil map was obtained based on a 30 arc-second-resolution

247 soil characteristics dataset. The soil parameters were derived based on a Chinese soil dataset (Shangguan

248 et al., 2013; Zhu et al., 2020) and Food and Agriculture Organization (FAO) (Nijssen et al., 2001). The

249   land cover maps included base maps and urban maps. The base maps were obtained from Liu et al.

250   (2010), which were created by merging Landsat TM digital images with a spatial resolution of 1 km and

251   12 land cover types. The urban maps were obtained from Wang et al. (2020), which were created by the

252   Classification Regression Tree (CART) method using Landsat images with a spatial resolution of 30 m.

253   The land cover parameters were obtained from Zhu et al. (2020). To better reasonably reflect the land

254   cover changes in modeling, our study updated land cover maps and related parameters (e.g., the thermal

255   conductivity, volumetric heat capacity) every five years. Moreover, four satellite datasets, namely,

256   Downward Shortwave Radiation (DSR), albedo, LAI, and Fraction of Vegetation Cover (FVC), were

257   incorporated in the modelling process (Zhang et al., 2019; Liang et al., 2021) to better identify land

258   conditions and calculate turbulent heat fluxes. The four datasets used in this study are at 0.05° spatial

259   resolution. The DSR dataset is at daily temporal resolution, while the other three datasets are at 8-day

260   temporal resolution. The four datasets were obtained from Global Land Surface Satellite (GLASS)

261   products (http://www.geodata.cn/thematicView/GLASS.html) (Liang et al., 2021). The spatial/temporal

262   resolution of the VIC modelling is defined as 0.0625°/3 hours in this study. To ensure consistency, all

263   model input data were adjusted to match the same spatial resolution through a linear interpolation.

264   **3.2 Evaluation data and method**

265   The VIC-urban model underwent calibration using streamflow data from two watersheds and

266   MODIS-based LST data. Then, it was validated against observations retrieved from gauge stations and

267   MODIS data regarding sensible and latent heat, runoff, and LST. The locations of the gauge stations are

268   shown in Figure 2, and detailed information is listed in Table 2. Four measures, namely, the Nash–

269   Sutcliffe efficiency (*NSE*), Root Mean Squared Error (*RMSE*), relative bias (*Er*), and correlation

270   coefficient (*R*) were used to evaluate the performance of VIC-urban.

271   In regard to sensible and latent heat evaluation, three flux towers were used, namely, the Beijing,

272   Daxing, and Miyun stations. In particular, the Beijing station is located in the central part of Beijing and

273   is widely used to investigate urban turbulence characteristics (Liu et al., 2020b; Ji et al., 2021). To

274   calibrate and validate the simulated runoff, streamflow data from three stations were used, namely,

275   Boyachang (BYCH), Qianxinzhuang (QXZH), and Wenyu (WY). Their corresponding watersheds are

276   located in the northern part of Beijing and contain various land cover types, including urban, forest, crop,

277   and grass (Figure 2). The observed discharge data of the QXZH and BYCH stations were separated into

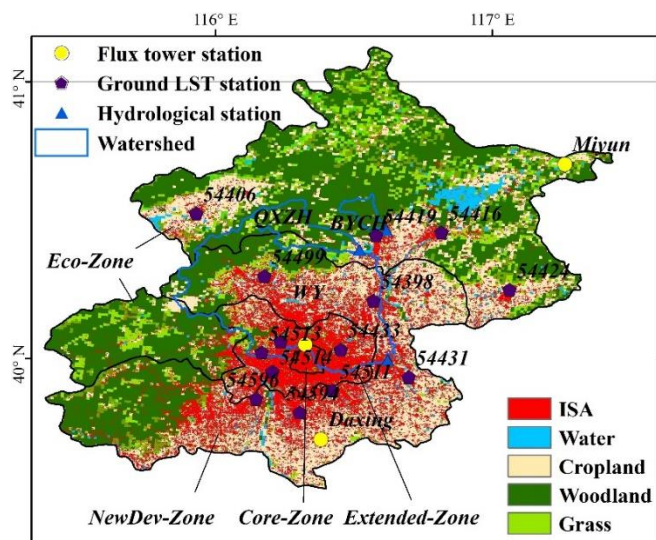
278   two periods for model calibration and validation, whereas the observed discharge of the WY station was

279   compared to the simulated runoff for the entire period due to the availability of only yearly data.

280   **Table 2.**

281   Validation data used in this work

Name	Source	Detailed information
Sensible heat	NCDDC, IAP	Beijing, 2011-2013, daily
Latent heat	NCDDC, IAP	Miyun, 2018-2010, daily
		Daxing, 2018-2010, daily
Runoff	AHRPR	QXZH, 2006-2009, monthly
		BYCH, 2006-2014, monthly
		WY, 2005-2017, yearly
LST	CMA, MODIS	14 ground stations, daily
		MOD11A2, eight-days

NCDDC, National Cryosphere Desert Data Center; IAP, Institute of Atmospheric Physics; AHRPRC, Annual Hydrological Report for the P.R. China, CMA, China Meteorological Administration; MODIS, MODerate-resolution Imaging Spectroradiometer; QXZH, Qianxinzhuang; BYCH, Boyachang; WY, Wenyu.

282

283   **Figure 2.** Location of Beijing and the flux tower stations, hydrological stations and watersheds, and ground
284   LST stations, with the 2015 land cover map as the background.

285   Regarding LST evaluation, we obtained data from fourteen ground-based stations and one satellite-

286   based product. At the ground-based stations of the CMA, platinum resistance sensors are used that are

287   semi-buried in soil to measure the daily temperature at the skin surface. Among the stations, three

288   stations provide long-term coverage data for the 2005 to 2020 period, while the remaining stations

289   provide data covering the 2016 and 2020 period. The satellite-based LST product of the Terra Moderate

290   Resolution Imaging Spectroradiometer (MODIS) was adopted, i.e., MOD11A2 v006

291   (https://modis.gsfc.nasa.gov/). MODIS LST data constitute one of the most widely used data for LST

292   studies (Bounoua et al., 2015; Zhou et al., 2010; Liu et al., 2020a; Morabito et al., 2021; Zhou et al.,

293   2018). The MODIS has provided two instantaneous LST estimates (10:30 and 22:30 local solar time)

294   every eight days since 2000, with a spatial resolution of 1 km. In our work, the simulated LST was

295   averaged every eight days for comparison with the MODIS data. The simulated LSTs from 9:00-12:00

296   and 21:00-24:00 were compared with the MODIS data for 10:30 and 22:30, assumed to represent the

297   morning and evening times, respectively. Notably, the gauge-based measurements were obtained at the

298   point scale, which is smaller than the model output resolution. To resolve the mismatch in the spatial

299   scale, the evaluation was conducted at the subgrid scale with the same land cover type in the

300   corresponding grid.

301   **3.3 Sensitivity analysis**

302   To examine the sensitivity of the model parameters to changes in the urban environment. Four

303   fluxes, namely, roof temperature, roof evaporation, canyon temperature, and canyon evaporation, were

304   used as indicators of the urban environment. A single grid cell with high urban coverage was selected,

305   and its input values were used as default values. The urban input parameters range from 70% to 130%

306   of the default values in 6% change steps. The specific parameters and their values are listed in

307   Supplementary Table 1.

308   The sensitivity analysis covered 6 years (2015-2020) and was conducted at the annual scale, as

309   well as for the winter (December to February of the next year) and summer (June to August) seasons.

310   The sensitivity coefficient Sc can be calculated as (Beven, 1979):

311   $$Sc = \lim_{X \to 0} \frac{\Delta Y / Y}{\Delta X / X} \times 100\%, \tag{10}$$

312   where X is the input parameter that affects the urban environment (Y). A positive (or negative) Sc value

313   suggest that Y is enhanced (or reduced) with increasing X.

4. Results

4.1 Land surface temperature

316   The simulated LST was calibrated against the MODIS LST and evaluated using two ground

317   observations and the MODIS LST dataset. As shown in Figure 3, the simulated LST exhibited similar

318   spatial patterns to those of the MODIS estimates for both the morning and evening times at the city

319   center. At the morning time, both the VIC-urban model and MODIS data exhibited high LST values in

320   Core-Zone and the southern part of Extended-Zone. At the evening time, the VIC-urban model

321   simulations failed to capture the scattered LST patterns in Eco-Zone and the southwestern part of

322   NewDev-Zone. This disagreement may be attributed to the relatively low urban fraction in these areas,

323   given that our work mainly focused on the calculation of urban-related processes. Other than in these

324   areas, the model could accurately produce a similar LST distribution relative to the MODIS LST data

325   in Core-Zone and Extended-Zone.

326   In terms of temporal comparison, the simulated LST exhibited a high performance in all of Beijing

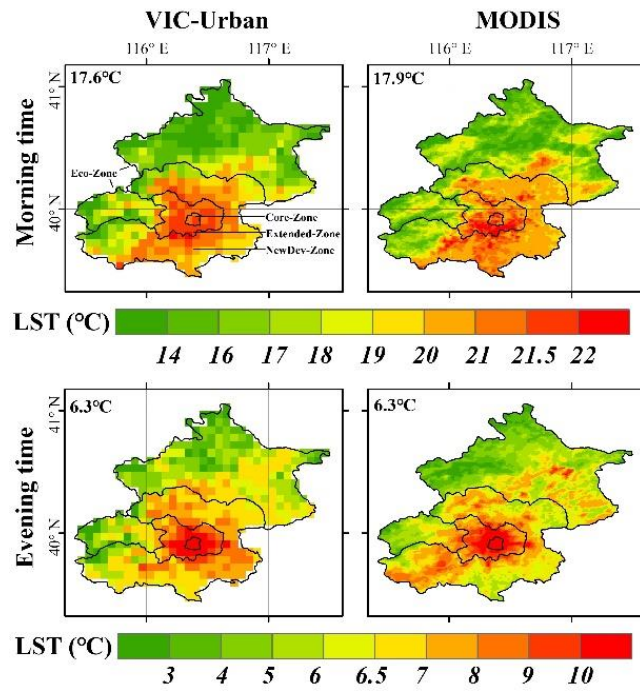
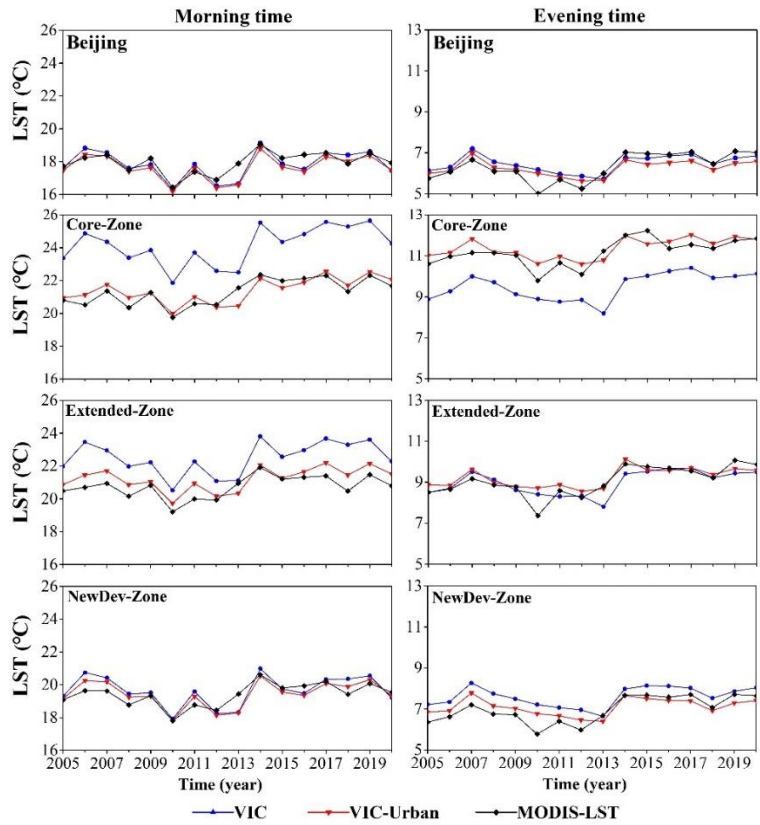
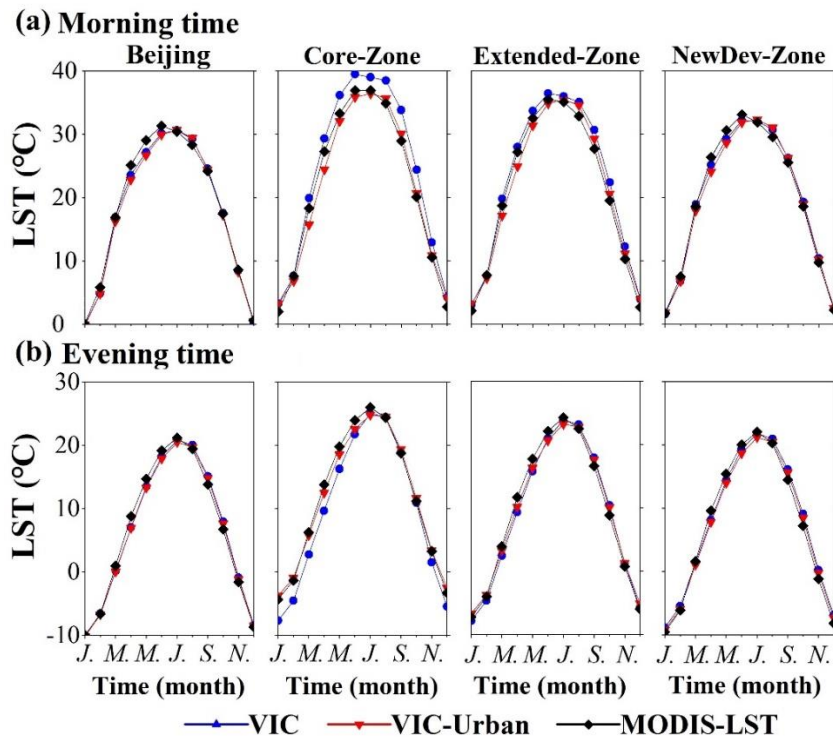
327   and the three subzones (Core-Zone, Extended-Zone, and NewDev-Zone). As shown in Figures 4 and 5,

328   the simulated LST indicated similar yearly dynamics and mean monthly cycles relative to the MODIS

329   LST data. The *R* values were over 0.8, and the *RMSE* and *Er* values were lower than 0.5°C and 2.3%

330   for the morning and evening times, respectively. These results indicated that the simulated LST values

331   closely captured the temporal variations and spatial patterns of the MODIS LST data ~~for Beijing and the~~

332   ~~three subzones~~.

333
334   **Figure 3.** Spatial distribution of the simulated LST compared to the MOD11A2 product, with the average
335   LST shown in the upper left of the figure.

336
337 **Figure 4.** Yearly dynamics of the simulated LST compared to the MOD11A2 product for Beijing and the
338 three functional zones (i.e., Core-Zone, Extended-Zone, and NewDev-Zone).

339

340 **Figure 5.** Mean monthly cycle of the simulated LST compared to the MOD11A2 product for Beijing and the
341 three functional zones (Core-Zone, Extended-Zone, and NewDev-Zone).

342   In regard to station-scale comparison, the model produced satisfactory LST estimates for the annual

343   dynamics and during the winter and summer seasons (Figure 6). Specifically, the overall *RMSE* was

344   lower than 1.9 °C, *R* was higher than 0.9, and *Er* was lower than 7% at the annual scale. During the

345   winter and summer seasons, the *RMSE* values were lower than 1.7 °C, the *R* values were higher than

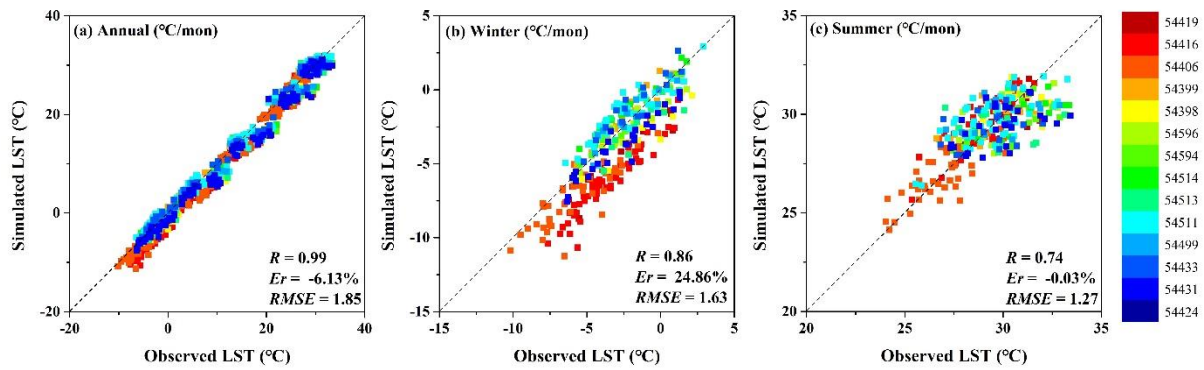
346   0.7, and *Er* was approximately 24.9% in winter and −0.2% in summer. The high *Er* value during the

347   winter season could be attributed to the low average winter LST. The comparison at each site also

348   indicated promising results (Table 3), with all *Er*s values lower than 12% and all *RMSE* values below

349   1.8 °C. It is important to note that the stations generally provided only five available values, i.e., annual

350   data for the 2016 to 2020 period. Nevertheless, the *R* values for all the stations consistently exceeded

351   0.4, indicating the satisfactory performance of the VIC-urban model.

353   **Figure 6.** Monthly simulated LST validated against 14 ground-based observation stations, which are marked
354   in different colours.

355   **Table 3.**
356   The simulated LSTs from VIC-urban and VIC models are validated by 14 ground-based observations at an
357   annual scale. The results of three indexes (*Er*, *R* and *RMSE*) are shown in the table, with the better results
358   underlined.

Station	*Er (%)*		*R*		*RMSE*	
	VIC-urban	VIC	VIC-urban	VIC	VIC-urban	VIC
54419	−7.78	-9.56	0.64	0.15	1.19	1.47
54416	−11.28	-10.58	0.79	0.89	1.63	1.52
54406	−8.37	-12.75	0.87	0.65	1.06	1.64
54399	0.29	8.61	0.92	0.69	0.12	1.28
54398	−8.24	-13.54	0.61	0.56	1.34	2.17
54596	−6.54	-5.29	0.63	0.68	1.07	0.88
54594	−7.10	-3.77	0.48	0.92	1.13	0.60
54514	−5.21	1.18	0.92	0.73	0.84	0.28
54513	−5.46	-3.54	0.80	0.51	0.85	0.67
54511	−1.38	-3.97	0.73	0.34	0.61	2.00
54499	−1.88	-1.71	0.88	0.72	0.37	0.40

54433	−0.87	3.09	0.40	0.38	0.35	0.58
54431	−5.24	-7.59	0.85	0.01	0.85	1.24
54424	−11.74	-12.44	0.77	0.46	1.76	1.88

4.2 Runoff

The model was further calibrated using the streamflow data for the QXZH and BYCH watersheds and validated against the streamflow data for the WY, QXZH, and BYCH watersheds (Figure 7). During the calibration period, the *NSE* and *R* values for the QXZH and BYCH watersheds were approximately 0.5 and 0.8, respectively, and the *Er* and *RMSE* values were below 10% and 4 mm/month, respectively, for both watersheds. During the validation period, the simulated runoff showed a high correlation with the observed data of the three watersheds, with *R* ranging from 0.8 to 0.9 and *NSE* ranging from 0.6 to 0.8. The *RMSE* reached approximately 4 mm/month at QXZH, 5 mm/month at BYCH, and 42 mm/yr at WY. The *Er* values were approximately 12% (QXZH), 29% (BYCH), and −9.5% (WY), respectively.

The overestimations at QXZH and BYCH and the underestimation at WY could likely be attributed to the limitations of the VIC-urban model in considering human activities. Specifically, the model did not consider water allocation for industrial use in the upstream region of the city (QXZH and BYCH) or the impact of industrial and domestic wastewater at the city centre (WY). *Er* of the WY watershed showed an increasing trend, particularly after 2013, which could be attributed to the increasing wastewater discharge. Despite these limitations, the VIC-urban model demonstrated an acceptable performance in simulating runoff.

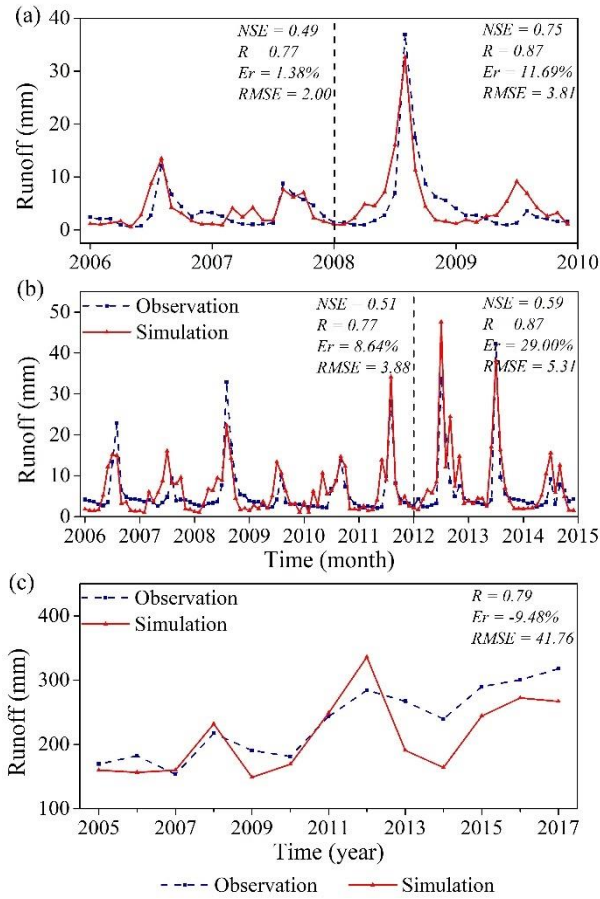
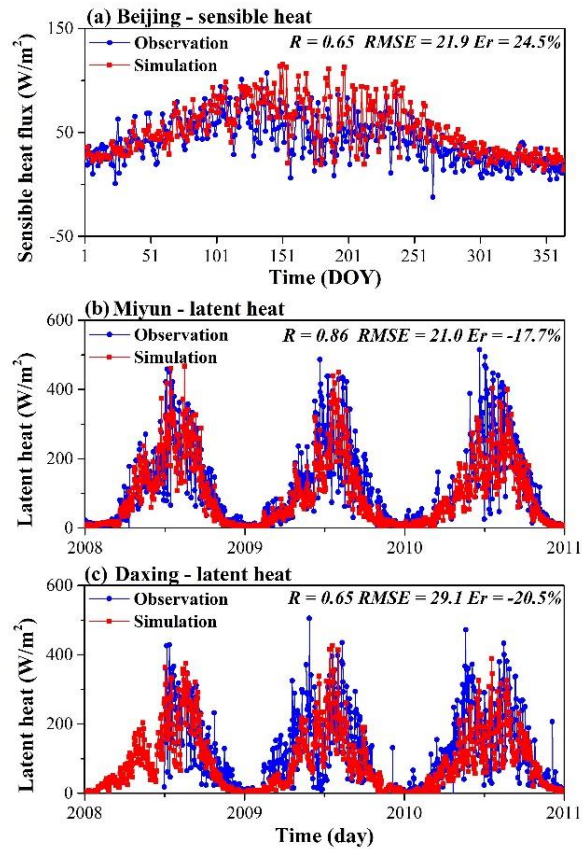



Figure 7. Evaluation of the simulated runoff. (a) QXZH; (b) BYCH; and (c) WY. The dark dotted line divides the data into the calibration period (before) and validation period (after).

4.3 Turbulent heat fluxes

The VIC-urban model was evaluated regarding the sensible and latent heat using the observed data of three stations: Beijing, Miyun, and Daxing. As shown in Figure 8a, the simulated sensible heat flux agrees well with the observed value at the Beijing station. R is approximately 0.65, and the $RMSE$ and Er are below 22 W/m^2 and 25%, respectively. Regarding the latent heat (Figure 8c, d), the simulated values exhibit high correlations (Rs) with the observed data at the Miyun stations (~ 0.86), and R at the Daxing station is approximately 0.65. Additionally, the $RMSE$ values are below 30 W/m^2 for all stations, and the Er values vary between -21% and -17%.

386

387 **Figure 8.** Evaluation of the sensible and latent heat flux simulations. (a) sensible heat flux at the Beijing flux
388 tower; (b) latent heat flux at the Miyun flux tower; (c) latent heat flux at the Daxing flux tower.

4.4 Comparison with the original VIC

390   The performance of the VIC-urban model and the original VIC model were compared in terms of

391 the simulated turbulent heat fluxes, LST, and runoff. As shown in Figure 9, the simulation results of the

392 VIC-urban and the VIC models showed similar patterns at the Miyun and Daxing stations, as the two

393 stations are located in suburban areas. The VIC-urban model mainly focuses on improving the model

394 performance in urban areas rather than suburban areas. However, atFor the Beijing station, which is

395 located at the site with a high degree of urbanization, the VIC-urban model provided a better

396 performance. Specifically, the VIC-urban model yielded a smaller *RMSE* (~12.7 W/m^2) for the sensible

397 heat flux than that of the VIC model (~15.7 W/m^2), and attained a higher correlation (~0.93) than the

398 VIC model (~0.81).

399   In terms of the LST, the VIC-urban model simulations show a lower discrepancy from the MODIS

400   product, especially at the city centre, and the average LST difference is less than 0.5 °C for both the

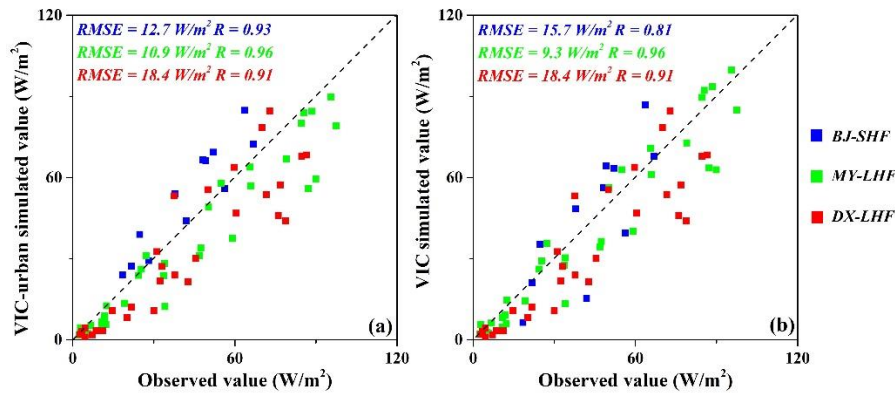
401   morning and evening times (Figure 10). However, the average LST difference is larger than 1.8 °C when

402   using the VIC model. Regarding temporal comparison (Figures 3 and 4), the VIC-urban model

403   simulations show similar patterns to those in the MODIS data, while the VIC model simulations tend to

404   overestimate the LST at the morning time and underestimate the LST at the evening time in Extended-

405   Zone. The VIC-urban model also outperforms the VIC model at the station scale, as indicated by the

406   higher *R* and lower *Er* and *RMSE* values (Table 3).

407
408   **Figure 9.** Simulated yearly turbulence heat fluxes of the VIC-urban and VIC models compared to the
409   observed data. The blue points denote the comparison of the sensible heat flux at the Beijing station, and the
410   green and red points denote the comparisons of the latent heat flux at the Miyun and Daxing stations,
411   respectively.

412   Regarding runoff (Figure 11), the VIC-urban and VIC models exhibit similar performance levels

413   for both the BYCH and QXZH watersheds. However, the VIC model obviously underestimates runoff

414   in the WY watershed, which has a high urban coverage. The *RMSE* values of the VIC and VIC-urban

415   model simulations for WY are 98.3 and 41.8 mm/yr, respectively. Based on the comparisons above, it is

416   evident that the VIC-urban model outperforms the original VIC model in analyzing urban-related

417   processes and can capture more realistic hydrological and thermal processes in cities.

418

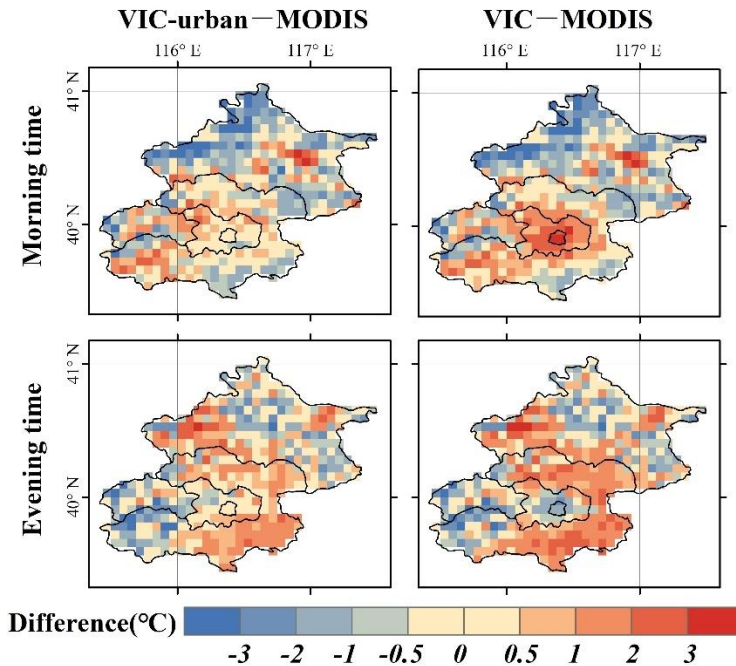



Figure 10. Spatial distribution of the LST differences between the MODIS LST and the simulated LST of the VIC-urban model (left), and between MODIS LST and the simulated LST of the VIC model.

421

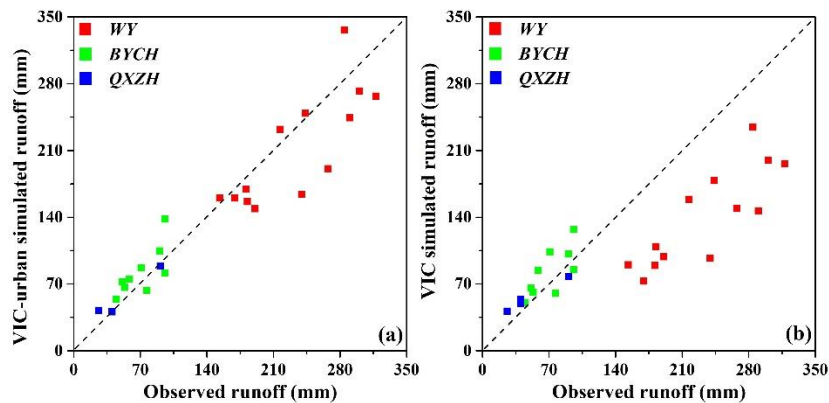



Figure 11. Simulated yearly runoff of the VIC-urban and VIC models compared to the observed data. The red, green, and blue points denote the comparisons in the WY, BYCH, and QXZH watersheds, respectively.

4.5 Sensitivity analysis

We further calculated the sensitivity of the hydrothermal process-related urban input parameters, that is, we calculated the impact on four indicators (i.e., roof temperature and evaporation and canyon temperature and evaporation). Regarding the roof (Figure 12 a, b), Emissivity_R and Albedo_R generally exhibited high sensitivity to the roof temperature, with sensitivity coefficients of −21% and −11%, respectively. The changes in In_max_R, Perrunoff_R, Emissivity_R and Albedo_R exerted

430 obvious impacts on roof evaporation, with values of 41%, −19%, −10%, and −8%, respectively.

431  Regarding the sensitivity of the canyon environment (Figure 12 c, d), Width_canyon (−5%) and

432 Width_roof (4%) imposed the greatest impact on the canyon temperature, followed by Emissivity_W

433 (−4%), Dz_W (−3%), Lan_dry_W (3%), and Albedo_W (−2%). In terms of canyon evaporation,

434 Width_canyon (44%) and In_max_G (37%) yielded the highest impact, followed by Perrunoff_G

435 (−29%), Kimp_G (−23%), Albedo_G (−20%), Emissivity_W (16%) and Albedo_W (14%). An

436 interesting finding is that the wall parameters (e.g., Emissivity_W, Albedo_W) generally imposed a

437 greater influence on the canyon temperature, while the ground parameters exerted a higher influence on

438 canyon evaporation. The sensitivity coefficients of all parameters are listed in Supplementary Table 2.

439  Supplementary Figures 3 and 4 show the urban environment (roof and canyon temperature and

440 evaporation) changes with increasing parameter value during the summer and winter seasons. The urban

441 environment exhibited diverse patterns under parameter increase, rather than simply following linear

442 trajectories. An interesting discovery is that the Dz_R and Lan_dry_R parameters showed opposite

443 impacts on the roof temperature during the summer and winter seasons. This inconsistency could be

444 attributed to their role in regulating heat transfer between indoor and outdoor environments. Specifically,

445 indoor temperatures are higher than outdoor temperatures in winter and lower in summer. A higher

446 thermal conductivity (i.e., higher Lan_dry_R and lower Dz_R values) will increase the outdoor surface

447 temperature in winter and decrease it in summer. Similarly, the parameters related to heat conduction

448 (e.g., Dz_W and Lan_dry_G) in canyon exerted contrasting impacts on the canyon environment during

449 the summer and winter seasons. Moreover, parameters such as albedo and emissivity directly exerted

450 negative impacts on both the roof and canyon temperatures and evaporation levels. Their effects on roofs

451 are generally similar between winter and summer, and their impact on canyons is more pronounced in

452 summer than in winter.

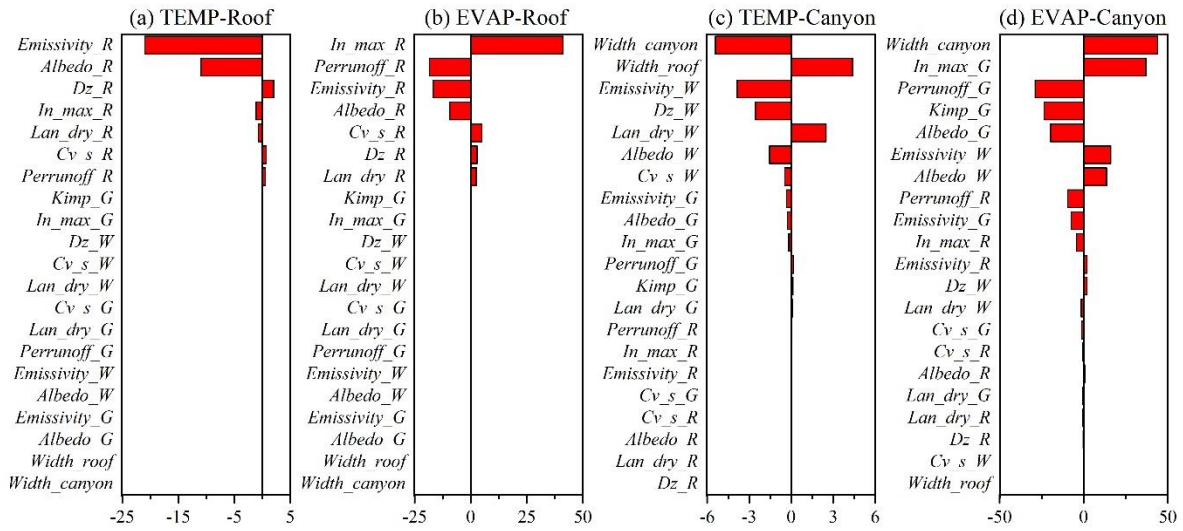



Figure 12. Sensitivity coefficients of the parameters to the urban environment: (a) Roof temperature; (b) roof evaporation; (c) canyon temperature; and (d) canyon evaporation.

5. Discussion

5.1. Enhanced performance of VIC-urban in urban systems

The urban module described above is among the first attempts to establish a systematic urban environment in the solution of the energy and water budget in the VIC model. The VIC-urban model incorporates detailed representations of urban canyons, urban geometry, and human influences. The model therefore provides favourable estimates of various components of the energy and water balance (e.g., surface runoff, evaporation, and LST) of each urban surface (i.e., roof, canyon, ground, and sunlit and shaded walls).

In each urban tile, the VIC-urban model calculates the incoming radiation of each surface based on geographic information, solar time, and geometric parameters. It then estimates energy budgets using an iterative approach that considers radiative interactions and energy balance principles(Meili et al., 2020). In water balance calculation, the model simulates the hydrological processes of the ground and roof individually and assumes that roof runoff contributes to the groundwater input. Additionally, given

469   the distinct characteristics of urban areas, where excess water on a given surface tends to remain in place

470   rather than immediately exiting the system (e.g., flat roofs and ground), the model includes a runon

471   component to more comprehensively represent water movement in urban environments.

472   The VIC-urban model was assessed based on the data of multiple gauge stations and MODIS LST

473   data and compared to the original VIC model in Beijing urban areas. The results indicated that the VIC-

474   urban model achieves excellent performance, with *RMSE* values below 0.5 and 1.8 ℃ relative to the

475   MODIS LST and gauge station data, respectively, and lower than 30 W/m^2 and 6 mm/month in turbulent

476   heat and runoff evaluation, respectively. Importantly, the VIC-urban model outperforms the original VIC

477   model in urban areas. It largely reduces the discrepancy between the simulated and observed values,

478   successfully capturing higher LST and runoff values at the urban center. These findings suggest that the

479   VIC-urban model is a valuable tool for reliable analysis of urban areas.

480   **5.2 Advantages of the VIC-urban model**

481   The development of the VIC-urban model provides a new urban modelling option. It employs the

482   canyon concept, which has been widely used in UCMs and coupled models (Oleson and Feddema, 2020;

483   Li et al., 2016b; Sun and Grimmond, 2019). Most UCMs, such as the Surface Urban Energy and Water

484   Balance Scheme (SUEWS) (Järvi et al., 2011), are primarily focus on water and energy balances on

485   urban impervious surface, and generally applied at small spatial scale, such as a single city. Moreover,

486   UCMs often neglect heterogeneity within urban areas (Kusaka et al., 2001; Meili et al., 2020). In contrast,

487   the VIC-urban model is able to simulate hydrothermal processes for multiple land cover types, and has

488   the strength for large-scale applications beyond urban areas (e.g., regional and global scales). The VIC-

489   urban offers high customizability with urban configurations and simulates hydrothermal processes at

490   the grid cell scale. It can merge hydrothermal inputs at the subcity scale to enhance its potential for

491   predicting water and energy balances in complex urban systems.

492   Large-scale urban models provide advantages in detecting hydrothermal dynamics in urban

493   environments due to their consideration of surface heterogeneity within a city. For instance, the CLMU

494   model incorporates a building energy model that considers convection and longwave radiation exchange

495   with interior building surfaces (Oleson and Feddema, 2020). The LM3-UCM model can simulate carbon

496   exchange and considers dynamic transitions between urban, agricultural, and unmanaged tiles (Li et al.,

497   2016b). However, these models often use constant land cover and radiation parameters over time. The

498   VIC-urban model can continuously capture land cover and radiation dynamics by integrating remote

499   sensing products. Furthermore, it incorporates a comprehensive thermally conductive framework that

500   considers three distinct layers (i.e., outdoor environment, interior building, and indoor environment) and

501   two vertical wall layers. These features are crucial for identifying long-term urban-induced

502   environmental changes and providing a comprehensive understanding of the urban environment.

503   **5.3 Limitations**

504   The current version of the VIC-urban model ~~still~~ has certain limitations. First, the model lacks the

505   water and energy balance related to snow melting, as well as certain anthropogenic disturbances (e.g.,

506   drainage systems, air conditioning, and car exhaust) (Liu et al., 2021). The model also simplifies

507   anthropogenic heat and water impacts, which are user-defined and represented by a constant setting and

508   12-month cycle values, respectively. However, these anthropogenic influences fluctuate over time, such

509   as anthropogenic heat input in office areas varying between weekdays and weekends. These factors may

510   impose a significant impact on the urban environment, and need to be further studied given the

511   availability and accuracy of data and the feasibility of methods (Yousefi Sohi et al., 2024). Second, the

512   model does not consider horizontal interactions between land cover types and water and energy transfer

513 in the subsoil beneath impervious surfaces due to impermeable characteristics. Third, the module does

514 not explicitly formulate the type of urban vegetation (i.e., vegetation or trees in cities), which may play

515 an important role in the hydrology and energy cycle of cities (Meili et al., 2020; Wang et al., 2018).

516 Nevertheless, the VIC-urban model divides the study area of interest into grids and categorises urban

517 vegetation as forests and/or grasslands, thus estimating the water and energy balance.

518 The validation of the turbulent heat flues was not sufficient to reflect the model performance due

519 to the scarcity of station data. However, the model was further validated using runoff and LST data

520 obtained from gauge stations and the MODIS product. These hydrothermal fluxes and states can be

521 cross-verified based on the principles of water and energy balance, proving the reliability of VIC-urban

522 in representing the complexity of urban environments. In addition, the VIC-urban model introduces new

523 parameters (Table 1) that should be estimated or calibrated before the simulation, and these parameters

524 may cause substantial uncertainties. Notably, parameters such as In_max_R (maximum infiltration rate)

525 and height-to-width ratio are influential on estimating urban temperature and evaporation patterns, as

526 illustrated in Subsection 4.5. Cities worldwide exhibit diverse configurations and various human

527 influences, leading to differing empirical parameters of influence. The VIC-urban model therefore

528 requires more evaluations in cities with diverse urban environments.

6. Conclusion

530 In this study, we developed a new urban module in the VIC model, demonstrated its reliability and

531 estimated the sensitivity of the model parameters. Adopting Beijing as an evaluation site, the VIC-urban

532 model showed promising performance regarding the simulation of sensible heat, latent heat, runoff, and

533 LST. Moreover, the VIC-urban model could better capture the LST and runoff patterns at the city centre

534 than the original VIC model. The sensitivity analysis revealed that the parameters of emissivity (i.e.,

Emissivity_R) and maximum interception capacity of the roof (i.e., In_max_R) generally exert the greatest impacts on the roof temperature and evaporation, respectively, and the height-to-width ratio imposed the highest impact on the canyon temperature and evaporation.

The current version of the VIC-urban model still holds substantial uncertainties due to its parameters and related processes and the lack of consideration of human disturbances (anthropogenic heat and water inputs), horizontal interactions, and snow dynamics. However, our work is among the first attempts to establish a systematic urban estimation within the VIC model, and the model is suitably formulated with detailed subcity configurations, human influences, and radiative balance and interactions. By considering the unique characteristics of urban areas and land cover and radiation dynamics, the VIC-urban model provides a more realistic representation of urban hydrology and thermal dynamics. Therefore, the model can be a valuable tool for detecting and understanding water and energy processes in urban areas, and for improving the prediction of hydrothermal fluxes and states of the urban environment.

Code and data availability

The codes of ~~the~~ VIC-urban, and example file for urban parameters are available at https://doi.org/10.5281/zenodo.10258321. The original VIC model is available at https://vic.readthedocs.io/en/master/Overview/ModelOverview/, and the urban module refers to https://doi.org/10.5194/gmd-13-335-2020 (Meili et al., 2020). The MODerate-resolution Imaging Spectroradiometer (MODIS) datasets used in this study are available at https://modis.gsfc.nasa.gov/. The Global LAnd Surface Satellite (GLASS) products are available at www.glass.umd.edu.

Author contributions

Yibing Wang designed and implemented the model, performed the analysis, and wrote the manuscript.

557 Xianhong Xie proposed and supervised the study, wrote and revised the manuscript. Bowen Zhu, Arken

558 Tursun, Fuxiao Jiang created the figures and wrote Supplementary Section 1. Yao Liu, Dawei Peng, Buyun

559 Zheng wrote Supplementary Section 2. All authors gave comments and discussions to the study.

Competing interests

561 The contact author has declared that neither of the authors has any competing interests.

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