# Development of the tangent linear and adjoint models of the global online chemical transport model MPAS-CO<sub>2</sub> v7.3

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Abstract. We describe the development of the tangent linear (TL) and adjoint models of the MPAS- $CO_2$  transport model, which is a global online chemical transport model developed upon the non-hydrostatic Model for Prediction Across Scales-Atmosphere (MPAS-A). The primary goal is to make the model system a valuable research tool for investigating atmospheric carbon transport and inverse modeling. First, we develop the TL code, encompassing all  $CO_2$  transport processes within the

- 5 MPAS- $CO_2$  forward model. Then, we construct the adjoint model using a combined strategy involving re-calculation and storage of the essential meteorological variables needed for  $CO_2$  transport. This strategy allows the adjoint model to undertake long-period integration with moderate memory demands. To ensure accuracy, the TL and adjoint models undergo vigorous verifications through a series of standard tests. The adjoint model, through backward-in-time integration, calculates the sensitivity of atmospheric  $CO_2$  observations to surface  $CO_2$  fluxes and the initial atmospheric  $CO_2$  mixing ratio. To demonstrate the
- 10 utility of the newly-developed adjoint model, we conduct simulations for two types of atmospheric  $CO_2$  observations: towerbased *in situ*  $CO_2$  mixing ratio and satellite-derived column-averaged  $CO_2$  mixing ratio  $(X_{CO_2})$ . A comparison between the sensitivity to surface flux calculated by the MPAS- $CO_2$  adjoint model with its counterpart from Carbon Tracker-Lagrange (CT-L) reveals spatial agreement but notable magnitude differences. These differences, particularly evident for  $X_{CO_2}$ , likely arise from differences in vertical mixing between the two systems might be attributed to the two model systems' differences in
- 15 simulation configuration, spatial resolution, and treatment of vertical mixing processes. Moreover, this comparison highlights the substantial loss of information in the atmospheric  $CO_2$  observations due to CT-L's simulation length and spatial domain limitationsspatial domain limitation. Furthermore, the adjoint sensitivity analysis demonstrates that the sensitivities to both surface flux and initial  $CO_2$  conditions spread out throughout the entire northern hemisphere within a month. MPAS- $CO_2$ forward, TL, and adjoint models stand out for their calculation efficiency and variable-resolution capability, making them
- 20 competitive in computational cost. In conclusion, the successful development of the MPAS- $CO_2$  TL and adjoint models, and their integration into the MPAS- $CO_2$  system, establish the possibility of using MPAS's unique features in atmospheric  $CO_2$ transport sensitivity studies and in inverse modeling with advanced methods such as variational data assimilation.

## 1 Introduction

Estimating CO2 fluxes through inverse modeling, using atmospheric chemical transport models and atmospheric CO2 mea-

- surements, is an important approach for understanding the global carbon budget. Beyond providing seasonal flux estimates that are useful for understanding the magnitude and phase of photosynthesis and respiration, it provides annual mean flux estimates that shed light on the key processes driving the response to climate change. When these annual mean  $CO_2$  estimates are adjusted to account for lateral fluxes (e.g., due to rivers, or the transport of crops and wood products), it gives an independent means of validating carbon stock change estimates from the terrestrial biogeochemical models and inventories (Byrne
- 30 et al., 2023). However, atmospheric transport models, which play a key role in inverse modeling, remain a significant source of uncertainty on both regional and global scales (Hurtt et al., 2022)(Schuh et al., 2019, 2022; Hurtt et al., 2022).

Two classes of chemical transport models – online and offline – are commonly used for simulating atmospheric  $CO_2$  transport. Offline models, such as TM5 (Krol et al., 2005; Meirink et al., 2006), PCTM (Kawa et al., 2004; Baker et al., 2006) and

- 35 GEOS-Chem (Kopacz et al., 2009), solve the tracer continuity equation using winds and vertical mixing fields computed from an independent run of a meteorological model or from a meteorological analysis. Online models, such as WRF-Chem (Grell et al., 2011), OLAM (Walko and Avissar, 2008; Schuh et al., 2021), and MPAS-CO<sub>2</sub> (Skamarock et al., 2012; Zheng et al., 2021), integrate chemistry, transport and meteorology simultaneously. Although offline models typically have lower computational costs, the separation of chemistry/transport from meteorology leads to a loss of information regarding atmospheric
- 40 processes occurring at time scales shorter than the meteorological model output frequency (Grell et al., 2005). In comparison, online models, owing to their simultaneous integration of meteorology and chemistry, have the potential to improve transport accuracy, particularly for vertical transport of chemistry. Recent advances in computer power and parallelization have greatly reduced the computational cost of online transport models, making them increasingly more accessible and practical for atmospheric  $CO_2$  research.
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A number of studies have demonstrated that transport model accuracy can be improved by increasing the model's horizontal resolution (Feng et al., 2016; Agusti-Panareda et al., 2019). Because global high-resolution  $CO_2$  transport simulations are computationally demanding, limited-area models (regional models) are often used instead (Pillai et al., 2012; Lauvaux et al., 2012; Zheng et al., 2018). However, regional models introduce the lateral boundary condition, posing challenges for  $CO_2$  inverse

- 50 modeling (Zheng et al., 2019; Rayner et al., 2019). As a global online chemical transport model, MPAS-(Zheng et al., 2021) addresses this limitation by being an online global transport model based on the compressible non-hydrostatic Model for Prediction Across Scales-Atmosphere (MPAS-A) (Skamarock et al., 2012). CO2 (Zheng et al., 2021) avoids the lateral boundary condition problem. Like OLAM (Schuh et al., 2021), MPAS-CO<sub>2</sub> uses a global variable-resolution mesh to facilitate local grid refinement for high-resolution simulations in specific regions without incurring prohibitively high computational costs and
- 55 avoiding the disadvantages of lateral boundary conditions.

The primary objective of this study is to develop the tangent linear (TL) and adjoint (AD) models associated with the global online transport model MPAS-CO<sub>2</sub> (Zheng et al., 2021). Adjoint model techniques have been widely used in both meteorological and atmospheric greenhouse gas research (Errico, 1997; Courtier et al., 1994; Giering et al., 2006; Meirink et al., 2008; Henze et al.,

- 60 (Errico, 1997; Courtier et al., 1994; Giering et al., 2006; Meirink et al., 2008; Henze et al., 2007; Tian and Zou, 2021), and play critical roles in variational data assimilation and sensitivity analyses (Baker et al., 2006; Zheng et al., 2018; Tian and Zou, 2020).
- The subsequent sections of this paper provide an overview of the MPAS-CO<sub>2</sub> forward model developed in Zheng et al. (2021) (Section 2), and the development and verification of the TL and AD models based on the forward model (Sections 3 & 4). The utility of the newly developed AD model is demonstrated with adjoint sensitivity analyses in Section 5. Finally, a summary and <u>conclusion\_conclusions</u> are given in Section 6.

## 2 MPAS-CO<sub>2</sub> forward model

Zheng et al. (2021) documented the development of MPAS-CO<sub>2</sub>, verifying its mass conservation and assessing its accuracy.
Hereafter, we refer to MPAS-CO<sub>2</sub> as the forward model, whose TL and AD model counterparts we develop in the present paper. A brief description of the forward model is provided here; see Zheng et al. (2021) for comprehensive details. The forward model characterizes CO<sub>2</sub> transport through the continuity equation:

$$\frac{\partial(\tilde{\rho}q_{co_2})}{\partial t} = -(\nabla \cdot \tilde{\rho}q_{co_2}\mathbf{V})_{\zeta} + F_{bl} + F_{cu}$$
(1)

where  $q_{co_2}$  is CO<sub>2</sub> dry air mixing ratio,  $\tilde{\rho} = \rho_d / (\partial \zeta / \partial z)$ ,  $\rho_d$  is dry air density,  $\zeta$  is the vertical coordinate, z is geometric 75 height, t is time, and  $\mathbf{V} = (u, v, w)$  is the velocity vector (u, v), and w are the zonal, meridional, and vertical wind components, respectively). The meteorological variables, such as wind velocity and dry air density, are updated simultaneously with CO<sub>2</sub> by the model's dynamical core and physics parameterizations. The left-hand side (LHS) of Eq. (1) is the total CO<sub>2</sub> time tendency  $(\partial (\tilde{\rho}q_{co_2}) / \partial t)$ . The first term on the righ-hand side (HRSright-hand side (RHS) represents the contributions to CO<sub>2</sub> time tendency from the advection, and the first, second, and third terms on the right-hand side (RHS) represent. The second

80  $(F_{bl})$  and third  $(F_{cu})$  terms of RHS represent the contribution from the contributions from advection, vertical mixing by the planetary boundary layer (PBL) parameterization, and convective transport and cumulus convective transport parameterizations, respectively. Advection of CO<sub>2</sub> in MPAS-CO<sub>2</sub> is handled in the model's dynamical core and can be expressed as Eq. (2), where the first two terms on the RHS represent the horizontal advection, and the third term represents the vertical advection:

$$(\nabla \cdot \tilde{\rho} q_{co_2} \mathbf{V})_{\zeta} = \left[\frac{\partial (\tilde{\rho} u q_{co_2})}{\partial x} + \frac{\partial (\tilde{\rho} v q_{co_2})}{\partial y}\right]_{\zeta} + \frac{\partial (\tilde{\rho} w q_{co_2})}{\partial \zeta}$$
(2)

85 CO<sub>2</sub> vertical mixing in the PBL by the PBL parameterization is implemented based on the YSU PBL scheme (Hong et al., 2006) and can be expressed as:

$$\underline{F_{bl}} = \left[\frac{\partial q_{co_2}}{\partial t}\right]_{\underline{bl}} = \frac{\partial}{\partial z} \left[K_h(\frac{\partial q_{co_2}}{\partial z}) - \overline{(w'q'_{co_2})_h}(\frac{z}{h})^3\right]$$
(3)

where z is the vertical distance to the surface, h is the boundary layer top height, and  $K_h$  is the vertical eddy diffusivity. The second term of the RHS in the square bracket of Eq. (3) represents the contribution from CO<sub>2</sub> entrainment flux at the inversion layer. The term  $[\partial q_{cos}/\partial t]_{\mu}$  from Eq. (3) is coupled with dry-air density  $\tilde{\rho}$  to form the term  $F_{bl}$  of Eq. (1).

Convective transport of  $CO_2$  is implemented based on the Kain-Fristch convection scheme (Kain, 2004) and it can be expressed as Eq. (4)

$$\frac{F_{cu}}{\partial t} = \left[\frac{\partial q_{co_2}}{\partial t}\right]_{cu} = \frac{(M_u + M_d)}{\rho A} \frac{\partial q_{co_2}}{\partial z} + \frac{M_{ud}}{M}(q^u_{co_2} - q_{co_2}) + \frac{M_{dd}}{M}(q^d_{co_2} - q_{co_2})$$
(4)

95 where  $q_{co_2}$ ,  $q_{co_2}^u$ , and  $q_{co_2}^d$  are the CO<sub>2</sub> mixing ratio in the environment, updraft, and downdraft, respectively,  $M_u$  and  $M_d$  are the updraft and downdraft mass, respectively,  $\rho$  is the environment air density, A is the horizontal area of a cell,  $M = \rho A \delta z$  is the mass of environmental air in a grid box, and  $M_{ud}$  and  $M_{dd}$  are the detrainment from the updraft and downdraft, respectively. The term  $\left[\partial q_{co_2}/\partial t\right]_{res}$  of Eq. (4) is coupled with dry-air density  $\tilde{\rho}$  to form the term  $F_{cu}$  of Eq. (1).

## 100 3 Development of the MPAS-CO<sub>2</sub> TL model

## 3.1 TL model development

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The CO<sub>2</sub> advective transport process described in Eq. (2) is implemented by two two-different numerical schemes in the forward model: (1) a monotonic scheme with hyperviscosity ( $\beta$ ) set to 0.25; and (2) a non-monotonic scheme with  $\beta = 1.0$  (Skamarock et al., 2012). The monotonicity in the first scheme is achieved by applying a flux limiter in the last step of the third-order Runge-Kutta solver (Wang et al., 2009; Skamarock and Gassmann, 2011). While the second scheme is linear in CO<sub>2</sub>, the first scheme is nonlinear due to the application of the flux limiter. Because both the YSU PBL and Kain-Fristch convection schemes are linear in CO<sub>2</sub>, using the linear advective scheme makes the forward model a linear model in CO<sub>2</sub>. In this paper, we develop the TL and adjoint models based on the linear version of the MPAS-CO<sub>2</sub> forward model, which can be symbolically expressed as:

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$$\mathbf{x}_t = \mathcal{M}(\mathbf{x}_0, \mathbf{e}),$$
 (5)

where  $\mathbf{x}_0$  and  $\mathbf{x}_t$  are the CO<sub>2</sub> dry air mixing ratio at the initial and forecast time (*t*), respectively.  $\mathcal{M}()$  represents the MPAS-CO<sub>2</sub> forward model and e represents a timeseries of CO<sub>2</sub> fluxes between times 0 and *t*. While both  $\mathbf{x}_0$  and  $\mathbf{x}_t$  are 3-dimensional vectors in space, e is 2-dimensional in space, indicating that CO<sub>2</sub> flux is applied only to the model's surface cells. Eq.(5) indicates that CO<sub>2</sub> mixing ratio at a forecast time ( $\mathbf{x}_t$ ) is determined by the CO<sub>2</sub> mixing ratio at an initial time ( $\mathbf{x}_0$ ) and the CO<sub>2</sub> flux (e) through the forward model.

The TL and adjoint models are designed to calculate the sensitivity of X<sub>t</sub> x<sub>t</sub> with respect to x<sub>0</sub> and e. This is achieved by introducing the TL and adjoint variables of their counterparts in the forward model (Giles and Pierce, 2000). While the introduction of the TL and adjoint variables for the initial CO<sub>2</sub> mixing ratio (x<sub>0</sub>) is straightforward, it is a bit more complex
for the CO<sub>2</sub> fluxes (e). This complexity arises from the fact that CO<sub>2</sub> flux, at each surface cell of the model, varies with time throughout the model's entire simulation period. Depending on the underlying biosphere model and emission inventory used, CO<sub>2</sub> flux varies at a certain temporal frequency, ranging from hourly to monthly. Although it is possible to introduce TL and adjoint variables for CO<sub>2</sub> flux at the flux's temporal frequency, it is neither practical nor necessary to do so. Instead, a common approach is to introduce flux scaling factors (Henze et al., 2007; Zheng et al., 2018) as follows:

$$125 \quad \mathbf{e} = \mathbf{S}(\mathbf{k})\tilde{\mathbf{e}},\tag{6}$$

where  $\tilde{\mathbf{e}}$  are time-variant  $CO_2$  fluxes, typically from a process model or inventory, and  $\mathbf{S}(\mathbf{k})$  is a generic scaling function. Eq. (6) means that at each surface cell, the magnitude of the  $CO_2$  flux ( $\tilde{\mathbf{e}}$ ) is adjusted using a flux scaling factor before it is used to modify the cell's  $CO_2$  mixing ratio. We implemented Eq. (6) in an emission driver of the forward model in a way that allows the flexibility of choosing the temporal frequency of the flux scaling factor. For instance, for a 24-hour forward model

- simulation forced by 3-hourly CO<sub>2</sub> flux, one can choose to have eight scaling factors at each surface cell (one for each of the eight 3-hour segments), or just one scaling factor for the entire time period. All the MPAS-CO<sub>2</sub> model runs used in the remainder of this paper are conducted using a single scaling factor for each surface cell that is repeated for each flux timestep in the entire simulation period. In this case, the scaling function S(k) in Eq. (6) is a function of a scaling vector k that has the same dimension as the model's surface mesh. The introduction of the flux scaling factors turns CO<sub>2</sub> flux from active variables to parameters, and the impacts of their variation on CO<sub>2</sub> mixing ratio are calculated through their corresponding scaling factors
  - **k**. Accordingly, the MPAS- $CO_2$  forward model can be symbolically expressed as

$$\mathbf{x}_t = \mathcal{M}(\mathbf{x}_0, \mathbf{k}) \tag{7}$$

Eq. (7) shows that for a given set of  $CO_2$  flux ( $\tilde{\mathbf{e}}$ ), the forecast time  $CO_2$  mixing ratio ( $\mathbf{x}_t$ ) is a function of the initial time  $CO_2$  mixing ratio ( $\mathbf{x}_0$ ) and the flux scaling factor ( $\mathbf{k}$ ).

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The TL counterpart of the MPAS- $CO_2$  forward model represented by Eq. (7) can be symbolically expressed as the first derivative of the forward model:

$$\Delta \mathbf{x}_t = \mathbf{M}(\Delta \mathbf{x}_0, \Delta \mathbf{k}) \tag{8}$$

where  $\mathbf{M}()$  represents the MPAS-CO<sub>2</sub> TL model,  $\Delta \mathbf{x}_0$  and  $\Delta \mathbf{x}_t$  are the TL variable of CO<sub>2</sub> mixing ratio at the initial and forecast time, respectively, and  $\Delta \mathbf{k}$  is the TL variable of the flux scaling factor  $\mathbf{k}$ . In essence, Eq. (8) shows that the TL model computes the perturbation in the forecast time CO<sub>2</sub> mixing ratio ( $\Delta \mathbf{x}_t$ ), given the perturbation in the flux scaling factor ( $\Delta \mathbf{k}$ ) and/or perturbation in the initial time CO<sub>2</sub> mixing ratio ( $\Delta \mathbf{x}_0$ ).

Based on the source code of the forward model, we developed the TL code by differentiating each process relevant to CO<sub>2</sub>
flux and transport, including advection, vertical mixing by the YSU PBL scheme, convective transport by the Kain-Fritsch scheme, and the CO<sub>2</sub> emission driver that implements Eq. (6). Automatic differentiation tools, such as Tapenade (Hascoet and Pascual, 2013) and Tangent and Adjoint Model Compiler (Giering and Kaminski, 1998), can be used to assist TL and adjoint code generation. However, the code these tools generate typically contains redundancies and is difficult to read, particularly for the adjoint code. To optimize the computation efficiency and facilitate future code upgrading, we manually developed the TL and adjoint code for MPAS-CO<sub>2</sub> with some minor assistance from Tapenade.

## 3.2 TL model validation

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After the TL model is completed, a thorough examination of its correctness was undertaken. As indicated in Eq. (8), the TL model can calculate the sensitivity of  $\mathbf{x}_t$  with respect to both  $\mathbf{x}_0$  and  $\mathbf{k}$ . The calculation of the sensitivity of  $\mathbf{x}_t$  with respect to  $\mathbf{x}_0$  involves the TL code of all the CO<sub>2</sub> transport processes, including advection, PBL, and convective transport. In comparison, the calculation of the sensitivity of  $\mathbf{x}_t$  with respect to the flux scaling factor  $\mathbf{k}$  involves the TL code of the CO<sub>2</sub> emission driver in addition to the TL code of all the CO<sub>2</sub> transport processes. Because the calculation of sensitivity to  $\mathbf{k}$  includes the TL code of all the processes in the TL model, and because both the transport processes and emission driver are linear, the correctness of the entire MPAS-CO<sub>2</sub> TL model can be verified by checking whether the following equation is satisfied (Errico, 1997; Tian and Zou, 2020):

$$\Phi(\alpha) = \frac{\parallel \mathcal{M}(\mathbf{x}_0, (1+\alpha)\mathbf{k}) - \mathcal{M}(\mathbf{x}_0, \mathbf{k}) \parallel}{\parallel \mathbf{M}(0, \alpha \mathbf{k}) \parallel} = 1,$$
(9)

where  $\mathbf{M}()$  is the TL model,  $\mathcal{M}()$  is the forward model and  $\alpha$  is a scalar. The second item in the numerator of Eq. (9),  $\mathcal{M}(\mathbf{x_0}, \mathbf{k})$ , is a forward model run. The first item in the numerator,  $\mathcal{M}(\mathbf{x_0}, (1+\alpha)\mathbf{k})$  is an identical forward model run except that its flux scaling factor at each surface cell is adjusted by multiplying  $1 + \alpha$ . In the denominator,  $\mathbf{M}(0, \alpha \mathbf{k})$  is a TL model run with its perturbation in initial time CO<sub>2</sub> mixing ratio set to zero ( $\Delta \mathbf{x}_0 = 0$ ) and perturbation in flux scaling factor  $\Delta \mathbf{k} = \alpha \mathbf{k}$ , which is the difference in the flux scaling factors between the two forward model runs.

If the TL model is correctly coded with regard to the forward model, Eq. (9) should be satisfied to the extent of machine accuracy until α is too small that the result is affected by round-off errors and drifts away from unity. To verify using Eq. (9), we ran a series of simulations using the forward model and newly developed tangent linear model with the scale factor α ranging from 1.0 × 10<sup>3</sup> to 1.0 × 10<sup>-4</sup> (Table 1). All the simulations start at 2018-10-01 00:00 UTC, run for 1 month, and end at 2018-11-01 00:00 UTC. The meteorological initial condition is from the ERA5 reanalysis (Hoffmann et al., 2019) and the CO<sub>2</sub> initial condition (x<sub>0</sub>) is from the Carbon Tracker (Jacobson et al., 2020) v2022 (CT2022) posterior CO<sub>2</sub> mole fraction at this time. Three-hourly CO<sub>2</sub> fluxes for the biogenic, fire, fossil fuel, and oceanic components from the CT2022 posterior

- are applied throughout the 1-month simulation period for each model run. Flux scaling factors of  $\mathbf{k} = \mathbf{1}$  were used in all our simulations here, with 1 being a vector the same length as  $\mathbf{k}$  with ones in every element. The model simulations are conducted using the global variable-resolution (VR) mesh shown in Fig. 1. This VR mesh has a total of 15,898 cells, which range from 120 km over most of the land regions to 480 km over oceans. Table 1 shows that the magnitudes of both the numerator and the denominator in Eq. (9) decrease as  $\alpha$  decreases. Moreover, the table also shows that the ratio remains close to unity until  $\alpha$
- 185 decreases to  $1.0 \times 10^{-1}$ , beyond which round-off errors lead to a deviation from unity. These results confirm that the MPAS-CO<sub>2</sub> TL model has been correctly developed with regard to the forward model. In the next section, we proceed to develop the MPAS-CO<sub>2</sub> adjoint model.

## 4 Development of the MPAS-CO<sub>2</sub> adjoint model

## 190 4.1 Adjoint model development

An adjoint model is an essential component of a variational data assimilation system and is very useful for adjoint sensitivity analysis (<u>Tian and Zou</u>, 2021; <u>Zheng et al.</u>, 2018; <u>Bosman and Krol</u>, 2023). Symbolically, the MPAS-CO<sub>2</sub> adjoint model can be expressed as:

$$(\Delta \hat{\mathbf{x}}_0, \Delta \hat{\mathbf{k}}) = \mathbf{M}^T (\Delta \hat{\mathbf{x}}_t), \tag{10}$$

195 where  $\mathbf{M}^{T}()$  is the MPAS-CO<sub>2</sub> adjoint model,  $\Delta \hat{\mathbf{k}}$  is the adjoint variable of the flux scaling factor, and  $\Delta \hat{\mathbf{x}}_{0}$  and  $\Delta \hat{\mathbf{x}}_{t}$  are the adjoint variables of CO<sub>2</sub> mixing ratio at the initial and forecast time, respectively. Eq. (10) demonstrates shows that starting with  $\Delta \hat{\mathbf{x}}_{t}$  at the forecast time, the MPAS-CO<sub>2</sub> adjoint model runs backward in time to the initial time while ingesting CO<sub>2</sub> observations along the way, resulting in the adjoint variable of CO<sub>2</sub> mixing ratio at the initial time ( $\Delta \hat{\mathbf{x}}_{0}$ ), and the adjoint variable of the flux scaling factor ( $\Delta \hat{\mathbf{k}}$ ).

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Similar to its TL model counterpart, the development of the MPAS- $CO_2$  adjoint model was carried out through manual implementation to avoid redundancy and optimize computational efficiency. However, unlike the forward and TL models, the adjoint model faces the challenge of accessing The calculation of the  $CO_2$  transport needs access to the meteorological fields at every time stepduring its model integration. This challenge arises due to the fact each time step. Since the forward

- 205 and TL model both run forward in time, this access is straightforward. However, because the adjoint model runs backward in time, making accessing the meteorological fields unavailable more challenging. One approach to this problem is saving meteorological fields in memory during the adjoint model's forward sweep, enabling accessing during the subsequent backward sweep (Guerrette and Henze, 2015; Zheng et al., 2018). However, since the MPAS-CO<sub>2</sub> adjoint model is intended for long simulations, this approach becomes impractical due to the excessive memory it demands. As an alternative strategy, we
- 210 adopt an approach that combines both recalculation and storage of the meteorological fields. This strategy effectively divides a long simulation into segments, and the forward and backward sweeps are carried out sequentially for each segment, requiring internal memory only large enough to accommodate one segment's worth of meteorological fields. This internal manipulation is handled seamlessly by the adjoint model, enabling it to run as long as needed without overburdening memory resources. Another strategy we adopted for developing the adjoint code is to have the forward sweep save some immediate variables that
- 215 are needed by the subsequent backward sweep so that they do not need to be recalculated. For instance, the values of some variables related to mass fluxes in the Kain-Fristch convection scheme Kain (2004) are saved by the forward sweep in the memory to speed up the subsequent backward sweep execution. This strategy not only increases the adjoint model efficiency but also simplifies some of its code development.

## 220 4.2 Adjoint model validation

The correctness of the newly developed MPAS- $CO_2$  adjoint model can be verified using the following equation (Tian and Zou, 2020):

$$\langle \Delta \mathbf{x}, \mathbf{M}(0, \Delta \mathbf{k}) \rangle = \langle \mathbf{M}^T(\Delta \mathbf{x}), \Delta \mathbf{k} \rangle, \tag{11}$$

where () represents the inner product operator, Δx is a perturbation of CO<sub>2</sub> mixing ratio and Δk is a perturbation of CO<sub>2</sub>
flux scaling factor. If the adjoint model is correctly coded with respect to the TL model, Eq. (11) should be satisfied for any choice of Δx and Δk. M(0, Δk) on the LHS of the equation is the perturbation in forecast CO<sub>2</sub> mixing ratio resulting from a TL model run whose perturbation in initial CO<sub>2</sub> mixing ratio is set to zero and perturbation to flux scaling factor is set to Δk. The first item of the RHS, M<sup>T</sup>(Δx), represents the adjoint variable of flux scaling factor, which is an output from the adjoint model integration from the forecast time backward to the initial time. The TL and adjoint model runs on the two sides of Eq.
(11) have the same simulation time period, but the latter runs backward in time.

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- We conducted two sets of experiments using the TL and adjoint models following Eq. (11) to verify the correctness of the newly developed adjoint model. In the first set of experiments, we set  $\Delta \mathbf{k} = 10^{-1}\mathbf{1}$ , and  $\Delta \mathbf{x} = \mathbf{M}(0, \Delta \mathbf{k})$ . The experiments were carried out in two steps: First, the TL model was integrated 7 days from the initial time (2018-10-01 00:00 UTC) to the end time (2018-10-08 00:00 UTC), with  $\Delta \mathbf{k} = 10^{-1}\mathbf{1}$ , resulting in  $\mathbf{M}(0, \Delta \mathbf{k})$  which is the perturbation in forecast time  $CO_2$  mixing ratio; Second, the adjoint model is initialized at 2018-10-08 00:00 UTC with its adjoint variable for  $CO_2$  mixing ratio set to  $M(0, \Delta k)$ . The adjoint model is then integrated backward in time for 7 days to 2018-10-01 00:00 UTC, resulting in  $\mathbf{M}^T(\Delta \mathbf{x})$ . The LHS and RHS of Eq. (11) are then calculated using the above results (Table 2). The table shows that the agreement between the LHS and RHS of Eq. (11) is about  $\frac{-5.15 \times 10^{-15}}{-5.16 \times 10^{-15}}$ . We note that this value is not exactly 240 zero due to the machine rounding errors. This experiment is repeated with the same configuration but the simulation length is increased to 31 days, ending at 2018-11-01 00:00 UTC. As expected, the magnitude of both the LHS and RHS increased, and they agree agreed to about  $-2.55 \times 10^{-16}$ . In the second set of the experiment,  $\Delta \mathbf{k} = 10^{-11}$  (same as the first set of experiments), but  $\Delta \mathbf{x} = \mathcal{M}_{14d}(\mathbf{x}_0, \mathbf{k})$ , which is the CO<sub>2</sub> mixing ratio at the end of 14-day forward model run (2018-10-01 00:00
- UTC to 2018-10-15 00:00 UTC). We note that this forward model run uses  $x_0$  from CT2022 posterior CO<sub>2</sub> mole fraction, and 245 k = 1. However, however, Eq. (911) should satisfy for any configurations configuration and simulation period of the forward model. The resulting LHS and RHS of Eq. (11) from the second set of experiments are about 2 orders of magnitude larger than their counterpart of the first experiments. This is caused by the much larger  $\Delta x$  of the second set of experiments. The LHS and RHS agree to to about  $-3.42 \times 10^{-15}$  for the 7-day simulation and about  $2.66 \times 10^{-15}$  for the 31-day simulation (Table 2).
- 250 The results shown in Table 2 obtained from the experiments based on Eq. (11) confirm that the MPAS-CO<sub>2</sub> adjoint model has been correctly developed with regard to the TL model. As the TL model has already been confirmed correct with respect to the forward model, it follows that both TL and adjoint models are correct with respect to the forward model of MPAS-CO<sub>2</sub>. This validation ensures the reliability and integrity of the entire MPAS-CO<sub>2</sub> system, including the forward, TL, and adjoint models, as described in this paper and model system since the forward model has already been validated in Zheng et al. (2021). It allows MPAS-CO<sub>2</sub> to be used as the basis of a variational assimilation system for carbon flux estimation and as a platform 255
- for conducting sensitivity analyses in atmospheric carbon research.

Table 3 presents the computational cost of model simulations using the MPAS-CO<sub>2</sub> system. Using the global 120-480 km VR mesh (Fig. 1; 15898 cells), the 1-month forward model simulation completes in 20 minutes when using 128 processors. 260 Both the TL and adjoint model simulations using the same configuration take approximately 10% longer, indicating that the majority of the computation time is used for integrating the meteorological fields, than the forward model. This extra computation time for the TL/adjoint model is incurred by the execution of the TL/adjoint code of the CO<sub>2</sub> transport processes. Furthermore, we conducted another set of 1-month simulations using the models on a global quasi-uniform resolution (UR) mesh of about 120 km, consisting of a total of 40,962 cells. Table 3 demonstrates that the simulations with the VR mesh 265 reduce the computational cost by over 50% for all three models, primarily due to its substantially smaller number of cells. This reduction in computation cost, while preserving the high resolution over areas of interest, should prove advantageous when the models are applied in variational assimilation problems, which typically require many iterations of forward and adjoint model runs.

#### 5 Adjoint sensitivity analysis 270

#### 5.1 **Comparison with CT-L footprints**

In addition to forming a key component of variational assimilation systems (Baker et al., 2006; Zheng et al., 2018; Tian and Zou, 2021), adjoint models are powerful tools for sensitivity analysis (Errico and Vukicevic, 1992; Errico, 1997; Zou et al., 1997; Tian and Zou, 2020). Studies focused on carbon flux estimation are often interested in exploring the sensitivity of atmospheric  $CO_2$  measurements to surface  $CO_2$  fluxes; these maps are. This sensitivity is commonly referred to as observation influence functions or footprints (Cui et al., 2022). The computation of observation footprints using forward models requires a

- large number of model runs, making it impractical, except for optimizing state vector elements at coarse horizontal resolutions. In contrast, adjoint models can calculate observation footprints much more efficiently. For point measurements, such as those from tower data, Lagrangian dispersion models offer an efficient alternative for obtaining footprints (Lin et al., 2003; Stohl
- 280 et al., 2005). For an example of this, see the publicly available  $CO_2$  observation footprints from Carbon Tracker-Lagrange (CT-L) (Hu et al., 2019), which are generated using the Lagrangian particle dispersion model STILT (Lin et al., 2003), driven by meteorology generated by the Weather Research and Forecast (WRF) model (Skamarock et al., 2008). This approach involves releasing a certain number of particles from the observation location/height and tracing their backward transport in time. Note that CT-L is a regional modeling system that only provides observation footprints within the latitude range  $10^{\circ}$ - $80^{\circ}$  N and longitude 0°-180° W for up to 10 days backward in time. 285

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In this section, we perform sensitivity analyses using the MPAS-CO<sub>2</sub> adjoint model, which employs backward-in-time integration to calculate two quantities: (1) the sensitivity of atmospheric  $CO_2$  to the model's initial  $CO_2$  mixing ratio, and (2) the sensitivity to the surface flux scaling factor. When a spatially uniform time-invariant surface flux is used of unity value is 290 used and  $S(\mathbf{k}) = \mathbf{k}$  in Eq. (6), the sensitivity to the surface flux scaling factor calculated by the MPAS-CO<sub>2</sub> adjoint model is the observation footprint. To facilitate comparison compare with CT-L footprints, the all MPAS-CO<sub>2</sub> adjoint model simulations conducted in this section use uniform a time-invariant  $CO_2$  surface fluxes of 1.0  $\mu$ mol/(m<sup>2</sup> s) for all surface cells, including both land and ocean cells. Because S(k) = k is used, Eq. (6) takes the form of  $e = k\tilde{e}$ . The units of the CO<sub>2</sub> flux ( $\mu$ mol m<sup>-2</sup> s<sup>-1</sup>) and the multiplicative nature of the flux scaling factor k determine the units of the adjoint variable  $\Delta \hat{\mathbf{k}}$  (which represents observation footprints) to be ppm/( $\mu$ mol m<sup>-2</sup> s<sup>-1</sup>). Meteorological initial conditions for MPAS-CO2 295 model simulations conducted in this section are from the ERA5 reanalysis (Hoffmann et al., 2019). Footprints calculated by the MPAS-CO<sub>2</sub> adjoint model are of the 120-480km variable resolution grid while the CT-L footprints are of  $1^{\circ} \times 1^{\circ}$ .

First, we conduct MPAS-CO<sub>2</sub> adjoint model simulations for *in situ* CO<sub>2</sub> observations at two towers in the United States:
WKT, located at Moody, Texas (31.31° N, 97.33° W), and WGC, located at Walnut Grove, California (38.26° N, 121.49° W). For each tower, the adjoint model is initialized at 00:00 UTC on March 31, 2018. We add an adjoint forcing of 1 ppm CO<sub>2</sub> at that time to the model grid cell closest to the tower location and the intake height (475m-457m at WKT and 483m at WGC). The forcing is turned off for subsequent time steps and the adjoint model is run backward in time for 30 days, ending at 00:00 UTC on March 1, 2018. The resulting sensitivity of CO<sub>2</sub> at the WKT tower to the model's CO<sub>2</sub> mixing ratio, which is

- 305 3-dimensional, is shown as a column average in the left panel of Fig. 2. The right panel of Fig. 2 shows the observation footprint (sensitivity to the surface flux scaling factor) at the corresponding times. The figures figure panels show that the sensitivity to the initial  $CO_2$  is highest and concentrated closest to the tower site at the time closest to the measurement: 5-days. With the increasing length of the backward-in-time integration, the sensitivity spreads over a larger area and its magnitude decreases. After 30 days, the sensitivity to the initial condition has propagated across most of the northern hemisphere. Figure 2 also
- 310 indicates that the <u>spatial</u> variation in the sensitivity magnitude decreases with time. To examine this, we calculated the standard deviation ( $\sigma$ ) of sensitivity for each day of the <del>30-day period (Figure 30 days (Fig. 3)</del>. The triangles in Fig. 3 show that the magnitude of the standard deviation of <u>the</u> sensitivity to the <u>initial</u> CO<sub>2</sub> mixing ratio decreases rapidly with <u>time the increasing</u> <u>length of the adjoint model simulation</u> for both towers. On the other hand, the sensitivity to the surface flux scaling factor (footprint) exhibits a different pattern from the sensitivity to the initial CO<sub>2</sub> mixing ratio. As shown in Fig. 2, the footprint
- 315 spread spreads spatially but the near field to the tower maintains a much higher magnitude than the far fields. By the end of 30 days, the footprint of the WKT tower covers almost the entire northern hemisphere, with the area north and northwest of the tower within the conterminous United States exhibiting a much higher magnitude than the more distant area. The circles in Fig. 3 indicate that the standard deviation of the footprint increase increases with time, but the rate of increase diminishes substantially after about 10 to 15 days. The finding suggests that extending the adjoint model integration further backward in
- 320 time will still result in changes to the footprint , but with a much-reduced change rate.

For comparison, in FigureFig. 4 we plot the MPAS-CO<sub>2</sub> adjoint model-calculated 10-day footprints in the CT-L geographic domain. The figure reveals that the MPAS-CO<sub>2</sub> adjoint model-calculated WKT tower footprint spans most of the western and northwestern United States, with the highest sensitivity in Texas, Missouri, Iowa, Kansas, and Nebraska. Additionally, the footprint extends to a substantial area over the northeastern Pacific Ocean. The spatial pattern of the CT-L calculated footprint (Fig. 4c) is similar to that from the MPAS-CO<sub>2</sub> adjoint model, but it is visibly less continuous. Fig. 4 also shows that the MPAS-CO2 adjoint model-calculated footprint for the WGC tower covers northern California, southwestern WashingtonOregon, west Nevada, and a portion of the northeastern Pacific Ocean. The CT-L-calculated footprint exhibits a similar spatial pattern and magnitude. Overall, both the MPAS-CO2 adjoint model and CT-L provide valuable information on the sensitivity of atmospheric.

spheric  $CO_2$  measurements to the surface flux: similar spatial patterns although with some differences due to resolution and the Lagrangian/Eulerian framework difference. In the second set of experiments, we compare CT-L and MPAS- $CO_2$  adjoint model footprints for a swath of OCO-2  $X_{CO_2}$  measurements. The ground track of the OCO-2 orbit used in the experiments is indicated by the blue color line in Fig. 1. This

- 335 orbit crosses North America from the Caribbean Sea to Canada's Northwest Territories in a northward direction between 18:31 UTC and 18:48 UTC on June 30, 2106. 2016. Since OCO-2  $X_{CO_2}$  represents the column average of atmospheric CO<sub>2</sub>, CT-L calculates  $X_{CO_2}$  footprints at 14 discrete height levels, ranging from 50 to 14,000 meters above the ground. For each height level, footprints are computed by placing a number of particles at that specific height. To ensure consistency with the CT-L approach, the MPAS-CO<sub>2</sub> adjoint model is configured to apply the adjoint forcing at the corresponding vertical levels within
- 340 the model. This is done by interpolating the CT-L's 14 height levels to MPAS-CO2 model's 55 vertical levels. This configuration allows for a direct comparison between the footprints calculated by the MPAS-CO<sub>2</sub> adjoint model and the CT-L footprints.

In the top panel of Fig. Figure 5, we present shows the footprints of a point located south of Jamaica in the Caribbean Sea (17.82°N, 77.88°W) at 500 m above the surface. Both four different height levels: 500m, 2,000m, 4,500m, and 10,000m.

- 345 The top three rows of Fig. 5 shows that both the MPAS- $CO_2$  adjoint model and CT-L footprints largely extend eastward over the Atlantic Ocean, indicating transport from the surface due to the influence of the easterly trade winds. Additionally, the MPAS- $CO_2$  adjoint model-calculated footprint includes a branch that crosses the equator and extends southeastward to the southern hemisphere between  $30^{\circ}$ W and  $40^{\circ}$ W longitude. This feature is not shown in the CT-L footprint due to its limitedarea domain. In the lower The bottom panel of Fig. 5, we present the footprint of the same location but at shows the footprints
- of 10,000 m above the surface. Both calculated by both the MPAS-CO<sub>2</sub> adjoint and CT-L footprints show feature a primarily counterclockwise extension, covering the Gulf of Mexico and Texas. Moreover, there is a second segment extending westward from Texas toward the west coast. Upon closer examination, we observe that the CT-L-calculated footprint has a higher lower magnitude than the MPAS-CO<sub>2</sub> adjoint model over the Gulf of Mexico, but a lower magnitude over the mid-Atlantic regions of the United States, including from Kentucky to the Carolinasat the 500m, 2,000m, and 4,500m height levels, but not at the 10,000m height level. The distinct patterns in both systems' footprints at different vertical levels (500m and 10,000m) height

levels indicate significant differences in horizontal and vertical transport patterns.

Figure 6 shows the corresponding footprints for an OCO-2  $X_{CO_2}$  sounding location in eastern Kentucky (36.8°N,82.9°W) for particles released at 2,000 and 4, the same four height levels as shown in Fig. 5. The figure shows that the footprints of 500m

above the ground, respectively. The footprint of and 2,000m extends extend predominantly northward, covering the Great Lakes region and part of the Canadian Shield. In comparison, the footprint for 4,500m is mostly directed to the west. Another notable difference is that the highest magnitude portion of the 500m and 2,000m footprint is footprints are in close proximity to the pointsounding location, while the 4,500m footprint is not in proximity to the point at all. These differences between the two among the height levels are evident in both the MPAS-CO<sub>2</sub> adjoint model and CT-L calculated footprints. In Fig. Figure 7,

365 we show the footprint shows the footprints of an OCO-2 sounding location on the southwest coast of Hudson Bay, Canada (56.96°N, 91.89°W) at 500m and 4,500m altitude for the four height levels. Both the MPAS-CO<sub>2</sub> adjoint and CT-L footprints for 500m are generally confined near to and 2,000m are largely either close to or north of the sounding location, indicating

that local surface fluxes surface fluxes from these regions have a significant influence on the atmospheric  $CO_2$  at 500m above the surface the two height levels. In comparison, the footprint of 4,500m is located more than 2,000km northwestward, mostly

370 covering Alaska; the particles move that far horizontally in the time it takes them to advect and mix 4,500m in the vertical. These findings emphasize the significant impact of vertical mixing on the spatial distribution of footprint at different altitudes, highlighting the unique patterns of horizontal and vertical transport in each case.

In additional MPAS-CO<sub>2</sub> adjoint model runs, we quantitatively compare the footprints of the entire OCO-2 track at each of the 14 height levels with the CT-L footprints. This comparison is conducted by performing a single MPAS-CO<sub>2</sub> adjoint model run for each height level to calculate the footprint at the end of the 10-day backward-in-time integrationfor each height level. We then compare these resulting footprints with their CT-L counterparts. Figure 8 shows the comparison at 4 height levels: 500m, 2,000m, 54,500m, and 10,000 m 000m above the surface. At each height level, the value in the figure represents the average of the footprints of all the cells that are part of the OCO-2 track. The figure reveals that the footprints calculated by the two systems have similar spatial patterns within the limited-area domain of CT-L. However, it is important to note that a substantial portion of the footprints extends beyond the CT-L domain. For instance, the footprints of 2,000m and 54,500m

- levels have significant coverage over Russian Siberia, while the footprint of the 10,000m level extends from the eastern Pacific Ocean to northeastern and western China, both of which are outside the CT-L model domain.
- In order to compare the footprints from the two systems quantitatively, we aggregated the footprints onto a 2° × 3° (lat×lon) grid within the area covered by the CT-L model domain for each of the 14 height levels. Figure 9 shows the comparison for each of the 14. In the figure, the CT-L calculated footprints are on the X-axis, and MPAS-CO<sub>2</sub> adjoint model calculated footprints are on the Y-axis. The solid line in each subfigure of Fig. 9 is the 1:1 line and the dashed line is a linear fit without intercept. The correlation coefficient R<sup>2</sup> is labeled in each subfigure. The figure demonstrates that the agreement between the two systems is better for footprints at lower heights than at higher heights. Specifically, at lower heights ranging from 500m to
- 2, particularly between 250m and 1,500m, with  $R^2$  all greater than 0.7. Footprints from the two systems agree to a much lesser degree at between 3,500m and 14,000m, where  $R^2$  is less than 0.5 in all cases. The linear fit lines (dashed lines) show that the MPAS-CO<sub>2</sub> adjoint model calculated footprints tend to have a somewhat higher magnitude than are of greater magnitude in general than their CT-L . However, at higher heights from 4,500m to 14counterparts at heights ranging from 50m to 1,000m;
- 395 Between 1, the footprints calculated by 500m and 2,500m, the two sets of footprints are of similar magnitude on average; At 3,500m and above, the CT-L tend to be of much higher magnitude compared to the MPAS-adjoint model. footprints are of larger magnitude in general.

These differences in magnitude between the two systems could be attributed to various factors, including differences in 400 model configurations, spatial resolution, and treatment of vertical mixing processes. Previous studies have shown that Lagrangian models, such as CT-L, can sometimes have different vertical mixing behavior compared to Eulerian models, especially at high altitudes (Karion et al., 2019).

## 5.2 Influence of vertical distribution of OCO-2 soundings on footprints

- In a final experiment, we use the MPAS- $CO_2$  adjoint model to examine the impact of different vertical distributions on footprint calculation. Two adjoint model simulations are were conducted for the OCO-2 orbit that crosses South America and North America between 17:36 UTC and 18:13 UTC on August 23, 2016 (the red color track in Fig. 1). Both simulations have the same adjoint forcing of 1 ppm  $X_{CO_2}$  added to each MPAS- $CO_2$  model cell along the orbital track at 18:00 UTC on August 23, 2016, and running backward in time for 30 days. The key-difference between the two simulations lies in the vertical distri-
- 410 butions of the adjoint forcing. For the first simulation, we adopt profile 1, which is obtained by combining the  $X_{CO_2}$  averaging kernel and pressure weight function (O'Dell et al., 2018). In contrast, profile 2 prioritizes  $X_{CO_2}$  information in the lower part of the troposphere (Figure Fig. 10). The 20 pressure levels in the figure are interpolated to the MPAS-CO<sub>2</sub> model's 55 vertical levels for the adjoint forcing placement. This experiment aims to highlight how these differences in vertical distribution impact the footprint calculation, leading to variations in flux estimation using variational assimilation. The results of this experiment
- 415 will provide valuable insights to the importance of selecting appropriate vertical distribution when using the adjoint model for  $CO_2$  flux estimation.

The top two panels of Fig. 11 show the footprints resulting from MPAS-CO<sub>2</sub> adjoint model simulations using the two distinct vertical distribution profiles for the adjoint forcing (Fig. 10). Although the two footprints may initially appear very similar, substantial differences become evident as shown in the bottom panel in Fig. 11. Specifically, the footprint calculated using Profile 1 exhibits lower magnitudes compared to that obtained using Profile 2 in most extratropical regions in both the North-Northern Hemisphere and Southern Hemisphere. Conversely, in most of the tropicaver some of the tropical regions, particularly the tropical Pacific Ocean, the footprint calculated using Profile 1 shows slightly higher magnitudes than for Profile 2. Profile 2, which allocates more adjoint forcing to the lower atmosphere and less to the upper atmosphere, appears to be more sensitive to the stronger Since the two adjoint model simulations have the same meteorology, these differences in the resulting footprints might be explained by how the convective transport of CO<sub>2</sub> impacts the two distinctive vertical distribution profiles of the adjoint forcing. The prevalence of deep convection over the tropical Pacific Ocean can more effectively transport surface CO<sub>2</sub> flux in the tropies than in the extratropies. These convective transport differences can account for the observed variations in the footprints between the two profiles to the upper atmosphere than over the extratropies, where surface CO<sub>2</sub> flux is more

430 likely to be confined in the lower atmosphere. Thus Profile 1's higher amount of adjoint forcing in the upper atmosphere results in its higher magnitude footprint over the tropical Pacific Ocean, but not over the extratropics, where its lower amount of adjoint forcing in the lower atmosphere leads to its lower magnitude footprint. These findings underscore the critical importance of selecting an appropriate vertical distribution for the model-data difference when using an adjoint model during variational assimilation.

## 435 6 Conclusions

The MPAS- $CO_2$  system consists of forward, TL, and adjoint models that are built upon the variable-resolution capability of the compressible non-hydrostatic MPAS-A model (Skamarock et al., 2012). It promises to be a useful tool for carbon flux inverse modeling at the global and regional scales. The forward model of MPAS- $CO_2$  is documented by Zheng et al. (2021). In this paper, we focus on the development of its tangent linear and adjoint models. Through rigorous testing, we have confirmed the correctness and accuracy of the newly developed MPAS- $CO_2$  TL and adjoint models. A key challenge in developing the adjoint model was efficiently accessing meteorological variables during the model's backward-in-time integration. We have

successfully implemented a strategy that combines recalculation and storage of meteorological variables. This approach significantly reduces the memory requirement, making the adjoint model feasible for long simulations, which are often necessary for  $CO_2$  inverse modeling.

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The results of the sensitivity analysis using the newly developed MPAS- $CO_2$  adjoint model provide valuable insights for designing  $CO_2$  data assimilation systems. The increasing homogeneity of the sensitivity to the initial atmosphere  $CO_2$  mixing ratio with longer integration length highlights the importance of selecting an appropriate assimilation window length. The comparison of the  $CO_2$  observation footprints between the MPAS- $CO_2$  adjoint model and the NOAA CT-L system demonstrates good agreement, validating the accuracy of the adjoint model's footprint calculations. The comparison of OCO-2  $X_{CO_2}$  foot-

- 450 good agreement, validating the accuracy of the adjoint model's footprint calculations. The comparison of OCO-2  $X_{CO_2}$  footprints reveals differences in sensitivity between the two systems at different altitudes. MPAS-CO<sub>2</sub> adjoint model-calculated footprints tend to have higher magnitudes at low altitudes and lower magnitudes at high altitudes compared to CT-L. These differences likely arise from variations in vertical transport in footprints could be caused by the differences in configuration, spatial resolution, and vertical mixing processes between the two model systems. Lastly, the sensitivity analysis using two
- 455 different vertical distribution profiles for adjoint forcing highlights the importance of correctly mapping model-data difference in  $X_{CO_2}$  to the transport model's vertical levels.

In addition to being a powerful tool for sensitivity analysis, the adjoint model plays a critical role in CO<sub>2</sub> variational data assimilation (Bosman and Krol, 2023; Tian and Zou, 2021; Zheng et al., 2018). Our future research efforts will focus on integrating the forward and adjoint models of MPAS-CO<sub>2</sub> into such a system. This integration has the potential to bridge a significant gap by establishing an online Eulerian transport model-based global variational assimilation system for CO<sub>2</sub> that targets high resolution in critical regions while at the same time avoiding the pitfalls associated with the lateral boundaries needed in regional-domain inversions.

## Code and data availability

465 The MPAS-CO<sub>2</sub> TL-forward, TL, and adjoint models v7.3 developed described in this paper can be downloaded from the CERN-based Zenodo archive at https://doi.org/10.5281/zenodo.8226620. This includes the model source code, instructions for compilation, and an example script for running models. Instructions for how to compile and run the models are provided in

the package. The computation and plotting scripts used in producing the figures in this manuscript can be downloaded from the CERN-based Zenodo archive at https://doi.org/10.5281/zenodo.10425739. CarbonTracker CO<sub>2</sub> flux and posterior mixing

470 ratio data can be obtained from the NOAA website: https://www.esrl.noaa.gov/gmd/ccgg/carbontracker/download.php. CT-L footprints can be obtained from the NOAA website: https://gml.noaa.gov/ccgg/carbontracker-lagrange/

## **Author contributions**

TZ designed and developed the MPAS-CO<sub>2</sub> TL and adjoint models. XT generated the 120-480km VR mesh used in model simulations. TZ, SF, JS, and XT designed and carried out the model accuracy verification experiments. TZ, SF, DB, and MB designed the adjoint sensitivity analysis experiments. All authors contributed to writing the paper.

**Competing interests** 

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The authors declare that they have no conflict of interest.

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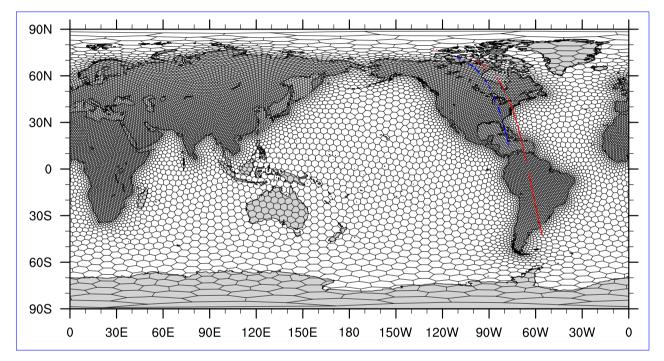
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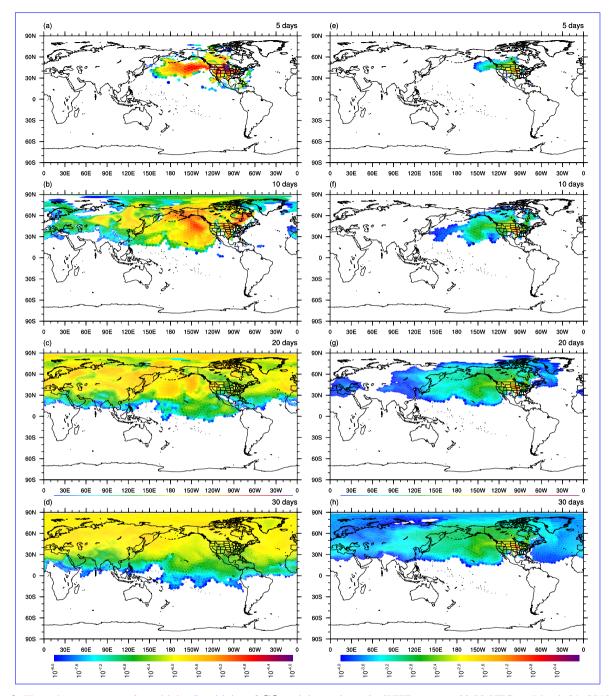
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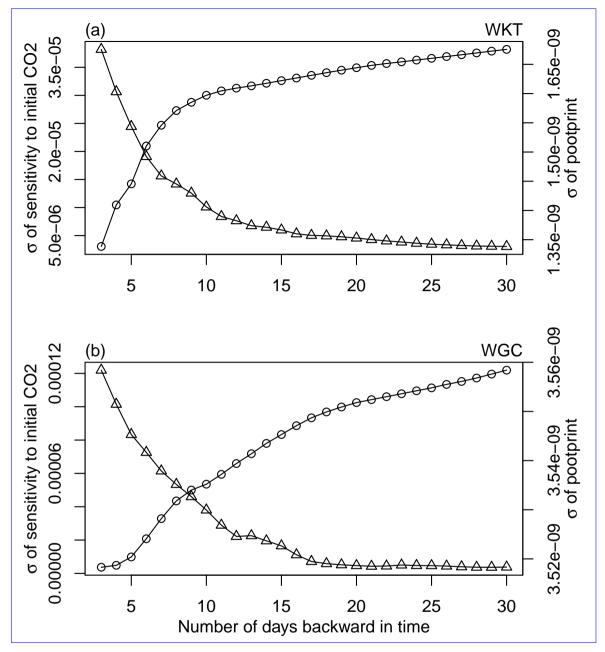
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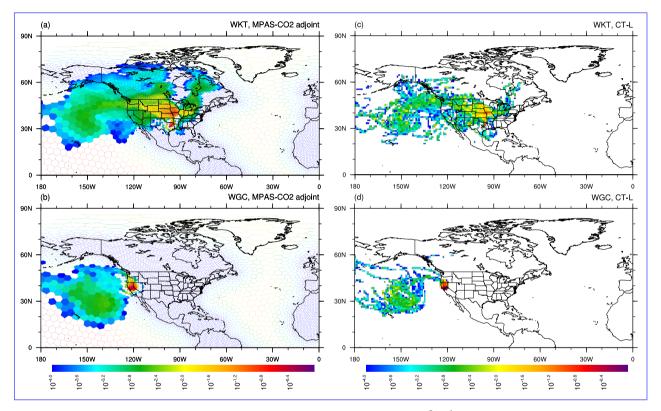
**Figure 1.** An A MPAS-CO<sub>2</sub> global variable resolution mesh ranging from  $\sim$ 120km over most of land regions to  $\sim$ 480km over oceans. Also shown in the figures are the ground tracks of two OCO-2 orbits, which are used for the adjoint sensitivity studies described in Section 5. The blue-colored ground track crosses North America from the Caribbean Sea northward between 18:31 UTC and 18:48 UTC on June 30, 2016. The red-colored ground track crosses from South America to North America between 17:36 UTC and 18:13 UTC on August 23, 2016.



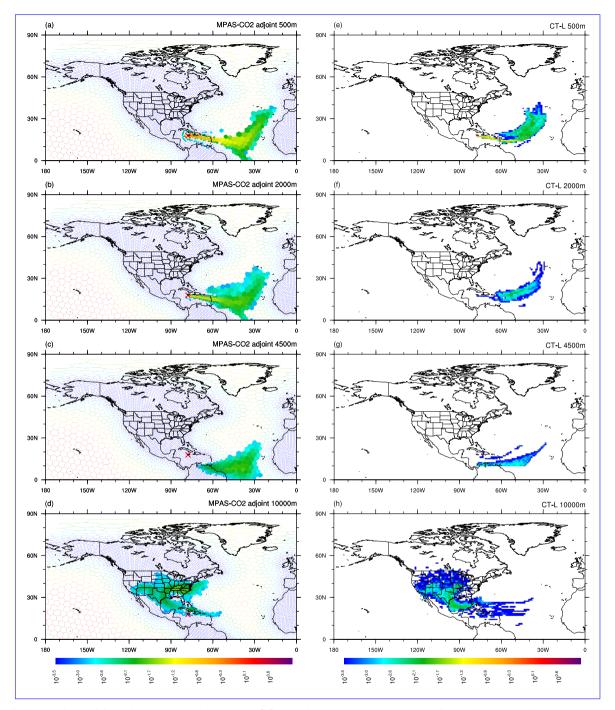
**Figure 2.** The column average of sensitivity Sensitivity of CO<sub>2</sub> mixing ratio at the WKT tower at 00:00 UTC on March 31, 2018 to the initial CO<sub>2</sub> mixing ratio (left column, units: ppm/ppm) and the surface flux scaling factor (right column, units:ppm/( $\mu$ mol m<sup>-2</sup> s<sup>-1</sup>)). The four rows from top to bottom show the sensitivities at 5, 10, 20, and 30 days backward in time (a) before the observation. The sensitivities to the initial CO<sub>2</sub> mixing ratio (deft column) are plotted as the column average. The WKT tower (31.3149°N, 97.3269°W) measurements used here are taken 457m at 457 meters above the ground level and labeled by the red color cross in the figures of the left column. Figures (e) (h) are the sensitivity of at the tower at the same time to the surface flux scaling factor (footprint, units:ppm/ $\mu$ mol m<sup>-2</sup> s<sup>-1</sup>) computed 5, 10, 20, and 30 days backward-in-time, respectively.



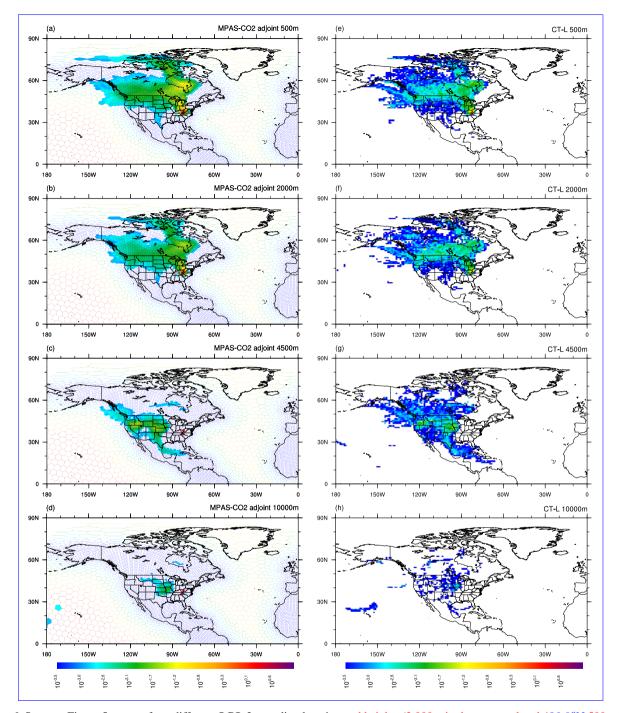
**Figure 3.** The variation <u>over time</u> of the standard deviation ( $\sigma$ ) of two quantities: the sensitivity to the initial CO<sub>2</sub> mixing ratio and the sensitivity to the flux scaling factor (footprint)<del>over time</del>. The standard deviations were calculated from MPAS-CO<sub>2</sub> adjoint model simulations starting on 2018 March 31 at 00:00 UTC, running 30 days backward in time, and ending on 2018 March 1 at 00:00 UTC. The top panel (a) is for the WKT tower (457 magl) while the bottom panel (b) is for the WGC tower (483 magl). In each figure, the triangles represent the standard deviation of sensitivity to the CO<sub>2</sub> mixing ratio field (units: ppm/ppm), and the circles represent the standard deviation of footprint (units:ppm/( $\mu$ mol m<sup>-2</sup> s<sup>-1</sup>)).



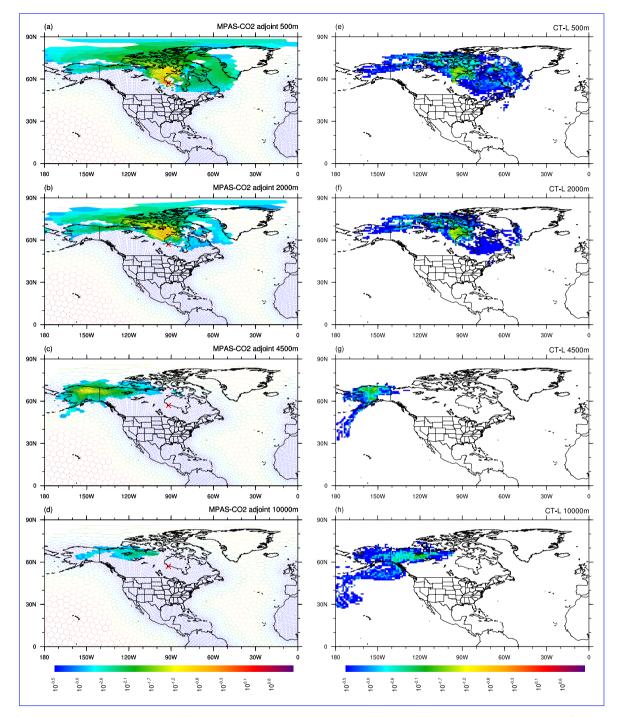
**Figure 4.** The 10-day backward in time  $CO_2$  measurement footprint (units:ppm/( $\mu$ mol m<sup>-2</sup> s<sup>-1</sup>)) given by two tall towers: WKT and WGC. The figures on the top panel are the footprint of the WKT tower calculated using the MPAS- $CO_2$  adjoint model (a) and CT-L (c). The figures on the bottom panel are the footprint of the WGC tower calculated by the MPAS- $CO_2$  adjoint model (b) and CT-L (d). The location of the towers is marked by the black crosses in the figure on the right panel.



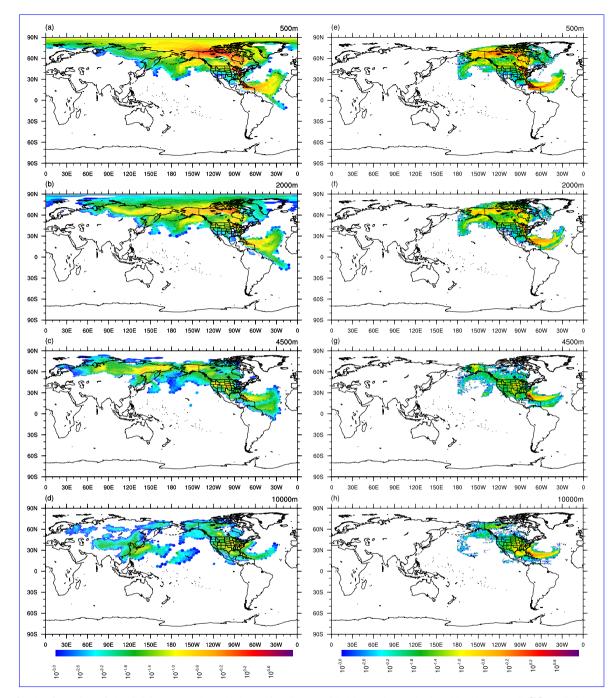
**Figure 5.** Comparison of footprints calculated by MPAS-CO<sub>2</sub> adjoint model and CT-L at a of an OCO-2 sounding location (17.82°N, 77.88°W) (red crosses, left panelspanel) along the OCO-2 ground track shown in Fig. 1 (blue color). The footprints are calculated at two four different heights: 500m(top panel), 2,000m, 4,500m, and 10,000m (bottom panel), and 10 days backward in time.



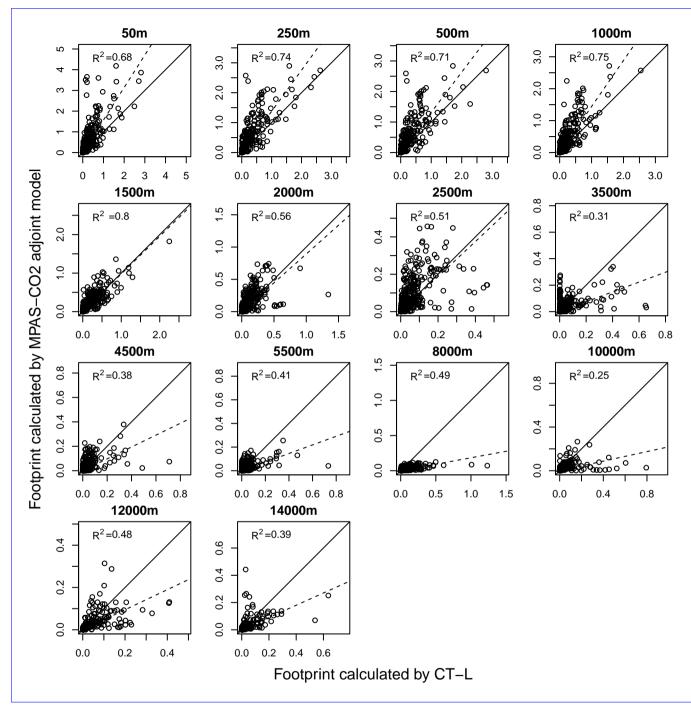
**Figure 6.** Same as Figure 5, except for a different OCO-2 sounding location and heights (2,000m in the top panel and  $436.8^{\circ}$ N, 500m in the bottom panel 82.9°W).



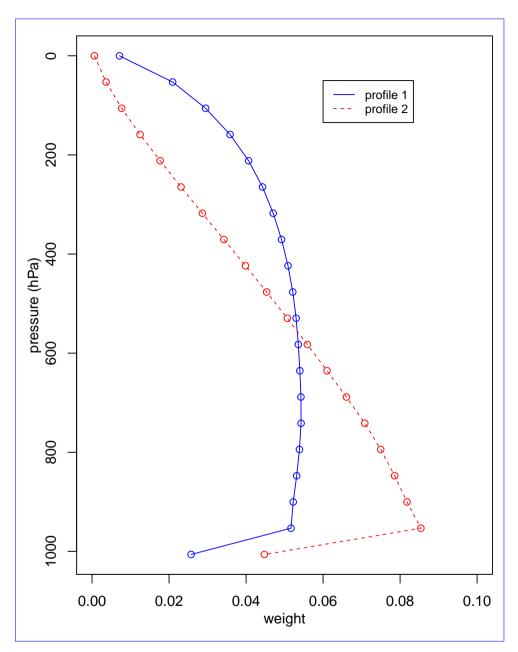
**Figure 7.** Same as Figure 5, except for a different OCO-2 sounding location and heights (500m in the top panel and  $456.96^{\circ}$ N, 500m in the bottom panel 91.89°W).



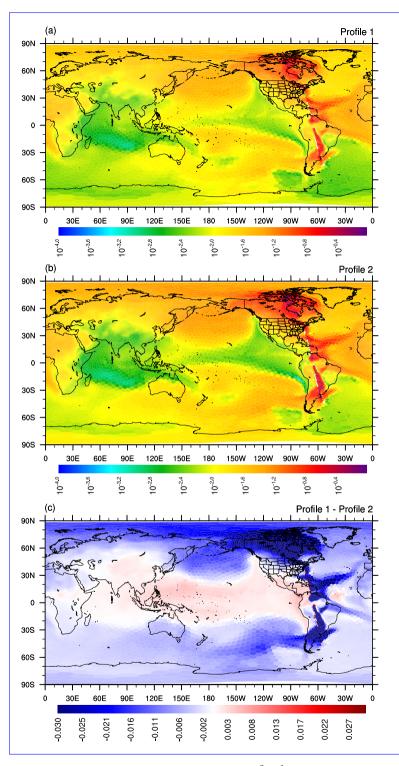
**Figure 8.** The footprint of the OCO-2 ground track shown in Fig. 1 (with blue color) calculated by the MPAS-CO<sub>2</sub> adjoint model (left panel) and by CT-L (right panel). The footprints are calculated by placing the adjoint forcing (for the MPAS-CO2 adjoint model) or releasing particles (for CT-L) at four different height levels above the ground: 500m, 2000m, 5500m4500m, and 10000m. The footprints are computed for 10 days backward in time.



**Figure 9.** Comparison of the OCO-2 groundtrack footprints from the MPAS-CO<sub>2</sub> adjoint model and CT-L after 10 days integration backwardin-time. For each of the 14 height levels, the values of the footprints (units:ppm/( $\mu$ mol m<sup>-2</sup> s<sup>-1</sup>)) are extracted as the average value of 2°x3° boxes within the range of the CT-L spatial domain ( $\frac{10-80^{\circ}10^{\circ}-80^{\circ}N}{180-10^{\circ}0^{\circ}-180^{\circ}W}$ ). The solid line in each subfigure is the 1:1 line and the dashed line is a linear fit with zero intercept. The correlation coefficient  $R^2$  of the linear fit is also labeled in each subfigure.



**Figure 10.** Two different profiles for vertically distributing a unit (ppm) of  $X_{CO_2}$ . Profile 1 is determined by OCO-2  $X_{CO_2}$  averaging kernel and pressure weight functions. Profile 2 is based on a redistribution of Profile 1 that gives more weight towards  $CO_2$  in the lower troposphere than in the upper part of the atmospheric column. The circles of profiles are on the twenty pressure levels of OCO-2  $X_{CO_2}$  pressure weight function. Both profiles integrate to unity.



**Figure 11.** MPAS-CO<sub>2</sub> adjoint model-calculated footprints (units:ppm/( $\mu$ mol m<sup>-2</sup> s<sup>-1</sup>)) obtained after 30 days of backward-in-time integration starting on August 23, 2016 at 18:00 UTC (the time of the OCO-2 measurement). The top figure is obtained when using Profile 1 (Fig. 10) to vertically distribute 1 ppm of adjoint forcing. The middle figure is the footprint using Profile 2. The bottom figure is the difference in footprint between the two profiles.

**Table 1.** Results of the correctness check for the newly-developed MPAS- $CO_2$  tangent linear model. The results are from 1-month integration (from 2018-10-01 00:00 UTC to 2018-11-01 00:00 UTC) of the forward and tangent linear models using the 120-480 km global variable-resolution mesh (Fig. 1). The terms in the table refer to Eq. (9).

α	$\  \mathcal{M}(\mathbf{x}_0, (1+\alpha)\mathbf{k}) - \mathcal{M}(\mathbf{x}_0, \mathbf{k}) \ $	$\parallel \mathbf{M}(0, \alpha \mathbf{k}) \parallel$	$\  \mathcal{M}(\mathbf{x}_{0},(1+\alpha)\mathbf{k}) - \mathcal{M}(\mathbf{x}_{0},\mathbf{k}) \  / \  \mathbf{M}(0,\alpha\mathbf{k}) \ $
$1.0 \times 10^3$	$2.07316571683768 \times 10^{1}$	$2.07316571683768 \times 10^{1}$	1.01.000000000000000000000000000000000
$1.0  imes 10^2$	$2.07316571683768 \times 10^{-1}$	$2.07316571683768 \times 10^{-1}$	<del>1.0</del> 1.000000000000000000000000000000000
$1.0  imes 10^1$	$2.07316571683768 \times 10^{-3}$	$2.07316571683768 \times 10^{-3}$	<del>1.0</del> 1.000000000000000000000000000000000
1.0	$2.07316571683769 \times 10^{-5}$	$2.07316571683768 \times 10^{-5}$	<del>1.0</del> 1.000000000000000000000000000000000
$1.0  imes 10^{-1}$	$2.07316571683765 \times 10^{-7}$	$2.07316571683768 \times 10^{-7}$	0.999999999999998
$1.0  imes 10^{-2}$	$2.07316571683799 \times 10^{-9}$	$2.07316571683768 \times 10^{-9}$	1.0000000000015
$1.0  imes 10^{-3}$	$2.07316571683735 \times 10^{-11}$	$2.07316571683768 \times 10^{-11}$	0.99999999999984
$1.0  imes 10^{-4}$	$2.07316571692815 \times 10^{-13}$	$2.07316571683768 \times 10^{-13}$	1.0000000004364

**Table 2.** Results of the correctness check for the newly-developed adjoint model of MPAS-CO<sub>2</sub>. All simulations are of the 120-480km variable-resolution mesh (Fig. 1). The LHS and RHS in the table refer to Eq. (11).

Integration length	LHS	RHS	(LHS-RHS)/LHS
	$\Delta \mathbf{k} = 10^{-10}$	<sup>1</sup> 1 and $\Delta \mathbf{x} = \mathbf{M}(0, \Delta \mathbf{k})$	
7-day	$1.436630106778291 \times 10^{-7}$	$1.436630106778298 \times 10^{-7}$	$-5.158974640379662 \times 10^{-15}$
31-day	$2.073165716837682 \times 10^{-7}$	$2.073165716837683 \times 10^{-7}$	$-2.553561385538706\times 10^{-16}$
	$\Delta \mathbf{k} = 10^{-1}$	1 and $\Delta \mathbf{x} = \mathcal{M}_{14d}(\mathbf{x_0}, 1)$	
7-day	$2.273936055720336 \times 10^{-5}$	$2.273936055720344 \times 10^{-5}$	$-3.421966688503031 \times 10^{-15}$
31-day	$7.640482494092126\times 10^{-5}$	$7.640482494092106 \times 10^{-5}$	$2.660668452525361 \times 10^{-15}$

**Table 3.** The computational costs for a 30-day simulation of MPAS-CO<sub>2</sub> at  $\sim$ 120km quasi-uniform resolution and at a variable resolution ranging from  $\sim$ 120 km to  $\sim$ 480 km. Computational costs are shown for the forward, tangent linear, and adjoint models. All simulations are conducted using 128 AMD EPYC 7H12 2.595 GHz processors running in parallel.

Model	Resolution (km)	Cost (min)	Time step (second)
Forward	120	45	720
	120-480	20	720
Tangent linear	120	48	720
-	120-480	22	720
Adjoint	120	48	720
-	120-480	22	720