

A flexible ~~z-coordinate~~ z-layers approach for the accurate representation of free surface flows in a coastal ocean model (SHYFEM v. 7_5_71)

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Abstract. We propose a ~~z-coordinate algorithm for ocean models~~ discrete multilayer shallow water model based on z-layers which, thanks to the insertion and removal of surface layers, can deal with an arbitrarily large tidal oscillation independently of the vertical resolution. The algorithm is based on a classical two steps procedure used in numerical simulations with moving boundaries (grid movement followed by a grid topology change, that is the insertion/removal of surface layers) which ~~leads to a~~ stable and accurate numerical discretization ~~avoids the appearance of surface layers with very small or even negative thickness.~~ With ad-hoc treatment of advection terms at non-conformal edges that may appear due to insertion/removal operations, mass conservation and ~~tracer constancy are preserved~~ the compatibility of the tracer equation with the continuity equation are preserved at a discrete level. This algorithm, called ~~z-surface-adaptive~~ z-surface-adaptive, can be ~~reverted~~ reduced, as a particular case when all layers are moving, to ~~other z-surface-following coordinates, such as z-star or quasi-z.~~ With simple analysis the z-star coordinate. With idealized and realistic numerical experiments, we compare the ~~surface-adaptive-z coordinate against z-star~~ z-surface-adaptive against z-star and we show that it can be used to simulate effectively coastal flows ~~with wetting and drying.~~

1 Introduction

The accuracy of ocean models in reproducing many dynamical processes is highly related to their vertical coordinate system. In literature, many choices exist covering the spectrum of coordinate systems. There are four main types of vertical coordinates which correspond to different vertical subdivisions of the fluid domain: 1) isopycnal ~~coordinates~~ layers with the interfaces that ~~follow the materials~~ are material surfaces (Lagrangian framework); 2) ~~z-coordinates~~ z-layers with fixed interfaces parallel to ~~geo-potentials~~ geopotentials (Eulerian framework); 3) terrain/surface-following ~~sigma or S-coordinates~~ σ or s-layers with interfaces adapted to the ocean surface and bottom boundaries; 4) adaptive coordinate with interfaces that dynamically adapt to better capture different flow features (Lagrangian tendencies, stratification and shear). The last two ~~coordinates~~ types move "arbitrarily" with respect to the flow, either to adapt to the free surface or any other features, and belong to the Arbitrary Lagrangian Eulerian framework (ALE).

~~Z-coordinates z -layers~~ were used in early ocean models. ~~Such discretization based on fixed interfaces has issues with the complex and moving boundaries represented by the free surface and by the ocean bottom. Despite this disadvantage,~~
25 ~~z -coordinate are still and are nowadays~~ implemented and used in some ocean models (HAMSOM, Backhaus, 1985), (TRIM-3D, Cheng et al., 1993), (~~SHYFEM, Umgiesser, 2022~~) and they (~~UNTRIM-3D, Casulli and Walters, 2000~~), (~~SHYFEM, Umgiesser, 2022~~). They are attractive when simulating ~~stratified flows as in Hordoir et al. (2015)~~ strongly stratified flows (Hordoir et al., 2015) and low frequency motions (Leclair and Madec, 2011). This occurs because the ~~z -interfaces isopycnals~~ are well aligned to ~~isopycnals and the z -interfaces or they slowly depart from them. At the same time, the truncation error of the internal pressure~~
30 gradient term ~~does not suffer from pressure gradient error~~ remains very weak.

~~A vertical discretization based on fixed interfaces is expected to have issues with the complex and moving boundaries represented by the free surface and by the ocean bottom. In this manuscript, we focus on z -layers performances relative to the treatment of the free surface boundary.~~ To simplify the boundary condition at the free surface, ~~z -coordinates z -layers~~ were typically coded allowing the surface layer to vary in thickness (Griffies et al., 2001). However, in such models, the surface
35 layer cannot vanish, which implies that the free surface variation must be smaller than the surface layer thickness. For coastal applications, this is a serious drawback, especially for the vertical resolution in shallow areas with high tidal elevations. In order to overcome this problem, other ~~z -type z -type~~ coordinates have been introduced over the years. ~~These vertical coordinates use the ALE transformation: the are based on z -layers that move~~ to accommodate the tidal oscillation, but the bottom is not a coordinate surface (they are surface-following but not terrain-following). These coordinates are clearly of ALE-type
40 but in the ocean modelling literature they are classified as ~~z - z~~ because the deviation from the ~~geo-potentials geopotentials~~ is very small. They combine small diapycnal mixing and small pressure gradient errors. ~~The z -star~~, specially for internal tides computations, and small truncation error on the pressure gradient term. The ~~z -star~~ of Adcroft and Campin (2004), the ~~quasi- z quasi- z~~ of Mellor et al. (2002) and the ~~hybrid z/s hybrid z/σ~~ of Burchard and Petersen (1997) all belong to such ~~z -surface-following z -surface-following~~ system, see Figure ???. An alternative to deal with the moving surface is to keep the
45 vertical grid perfectly aligned to ~~geo-potentials geopotentials~~, thus working in a truly Eulerian framework, but allowing the surface layer(s) to be removed or inserted. We refer to this system as ~~z -surface-adaptive z -surface-adaptive~~. Insertion/removal of the top layer has been discussed in Casulli and Cheng (1992) and it is used for example in Burchard and Baumert (1998). However "both the accuracy and stability are suspect; it is most likely difficult to make the transition of a vanishing layer smooth enough to not generate numerical problems; conservation issues are a major concern and the likelihood of vanishing
50 layers become more frequent with increasing vertical resolution" (Adcroft and Campin, 2004).

In this manuscript, ~~we review z -coordinate performances relative to the treatment of the free surface boundary. We propose a solution to the stability and conservation issues for the insertion/removal~~ ~~we propose an algorithm for the z -surface adaptive coordinate which goes beyond such limitations.~~ We employ a classical grid adaptation strategy when the adaptation is driven by a moving boundary (Guardone et al., 2011). It combines a first ALE grid movement step (surface interface displacement stretched by the free surface displacement) and a second topology modification step (layer insertion, layer removal). All these operations are easily performed on the one-dimensional vertical grid. ~~If the water depth is positive, the thickness of the surface layers remains positive, avoiding stability issues related to the appearance of small or even negative layers.~~ We show that

60 ~~this solution generalizes z-coordinates~~ the mass is conserved. Also the discrete preservation of a constant tracer can be easily accomplished, which guarantee a complete consistency at a discrete level of the tracer equation with the the continuity equation as shown since the work of Lin and Rood (1996); Gross et al. (2002).

~~This solution generalizes z-layers~~ in the sense that the same algorithm can be easily ~~reverted to z-surface-following coordinates-reduced to z-star~~ and can be added to a flexible vertical coordinate system. In fact, the grid adaptation has one free parameter that controls the number of moving layers. Tuning such parameter, so that all the layers along the water column are moving, we show the link of the proposed approach with the ~~z-surface-following coordinates-~~

65 ~~Finally, we look at a second potential drawback of using fixed interfaces with a free surface. The large vertical velocity triggered by the free surface oscillation can cause strong numerical mixing with respect to the surface-following coordinates (Klingbeil et al. -We quantify such additional spurious mixing of z-coordinates theoretically and numerically and we highlight the dependencies from the external forcing (tidal characteristics, stratification profile) and the numerics (vertical advection scheme, vertical grid size)-z-star.~~

70 The algorithm is implemented in the SHYFEM finite-element ocean model of the CNR-ISMAR (Umgiesser et al. (2004), <https://github.com/SHYFEM-model/shyferm>) which ~~implements the multilayer shallow water equations with z and sigma layers.~~ SHYFEM uses a popular choice for many coastal ocean models influenced by the work of Backhaus (1983), that is a semi-implicit finite element discretization on unstructured B-type grids.

The manuscript is organized as follows: in Section 2 we introduce the vertical discretization ~~, the layerwise Shallow Water equations, and we discuss the spurious mixing effect caused by a barotropic tide~~ ~~and the multilayer shallow water model. Three different vertical discretizations are considered: the standard multilayer shallow water model based on sigma-layers, then the z-star and the standard z-layers. In Section 3 we provide the semi-implicit finite element discretization of the multilayer equations.~~ In Section 4 we describe the ~~z-surface-adaptive z-surface-adaptive~~ algorithm, in Section 3-5 we detail the issue of a spatially variable number of surface layers caused by the insertion/removal operations. In Section 6 we provide numerical tests and in
80 Section 7 we conclude with a discussion.

2 ~~Layerwise Shallow Water~~ Multilayer shallow water model ~~with z-coordinate~~

~~One dimensional sketch of different vertical z-grids existing in the literature. From left to right: standard z with fewer layers due to the limitation for the surface layer thickness, z-star, quasi-z, hybrid z/sigma~~

~~We consider the layerwise~~ ~~We start considering the multilayer~~ (or layer integrated) shallow water model for stratified
85 flows ~~discussed in Burchard and Petersen (1997) and studied in Audusse et al. (2011b), Audusse et al. (2011a). We use the one-dimensional case to present the main concepts. The layerwise~~ ~~The space variable is $(\mathbf{x}, z) \in \mathbb{R}^3$ with $\mathbf{x} = (x, y) \in \mathbb{R}^2$ that denotes the horizontal space variable. We consider the fluid domain Ω :~~

$$\Omega = \left\{ (\mathbf{x}, z) : \mathbf{x} \in \Omega_{\mathbf{x}}, -z_b(\mathbf{x}) \leq z \leq \zeta(\mathbf{x}, t) \right\}$$

where $\Omega_{\mathbf{x}}$ is the projection of Ω onto the horizontal plane, $\zeta(\mathbf{x}, t)$ is a function that represents the free-surface elevation and $z_b(\mathbf{x})$ is the bathymetry that does not depend on time. The water depth is $H(\mathbf{x}, t) = \zeta(\mathbf{x}, t) + z_b(\mathbf{x})$. As depicted in Figure 1, right panel, the multilayer shallow water model is based on a discretization of the water-column domain Ω with a vertical grid composed of N layers denoted by greek letters and Ω_{α} with $\alpha = 1, \dots, N$, ordered from the free surface $\zeta(\mathbf{x}, t)$ ($\alpha = 1$) to the bottom $b(\mathbf{x})$ ($\alpha = N$). The layers are non-overlapping with $\Omega = \bigcup_{\alpha=1}^N \Omega_{\alpha}$. Each layer α is delimited by the Ω_{α} is delimited laterally by the vertical domain boundary and in the vertical by the time dependent interfaces $\Gamma_{\alpha \pm 1/2}(t)$ defined by the set of points of coordinates (\mathbf{x}, z) such that $z = z_{\alpha \pm 1/2}(\mathbf{x}, t)$. The free-surface Γ^{ζ} and the bottom interfaces Γ^b are described respectively by the free-surface elevation $z_{1/2} = \zeta(\mathbf{x}, t)$ and by the bathymetry function $z_{N+1/2} = -z_b(\mathbf{x})$. In order to provide the rules for such slicing of the domain, we define a reference domain which is constant in time, with space variables $(\mathbf{x}, s) \in \mathbb{R}^3$ such that:

$$\Omega^0 = \left\{ (\mathbf{x}, s) : \mathbf{x} \in \Omega_{\mathbf{x}}, -1 \leq s \leq 0 \right\}$$

and discretized by means of a vertical grid similarly composed of N layers, each denoted Ω_{α}^0 . The reference layers are delimited vertically by the fixed-in-time interfaces $z_{\alpha \pm 1/2}^0$. The surface and bottom $\Gamma_{\alpha \pm 1/2}^0$, which are placed at the vertical coordinate given by the function $s_{\alpha \pm 1/2}$. Such constants can be ordered:

$$s_{1/2} = 0 < s_{2-1/2} < \dots < s_{N+1/2} = -1$$

Then the interface position can be obtained by mapping the reference interface $\Gamma_{\alpha-1/2}^0$ to the actual or physical interface $\Gamma_{\alpha-1/2}(t)$. In general we assume that exists a function, for $\alpha = 1, \dots, N$:

$$A : \Gamma_{\alpha-1/2}^0 \rightarrow \Gamma_{\alpha-1/2}(t), \quad z_{\alpha-1/2} = A(\mathbf{x}, s_{\alpha-1/2}, t) \quad \mathbf{x} \in \Omega_{\mathbf{x}} \quad (1)$$

To prescribe this function we use the generalized vertical coordinate transformation, see Mellor et al. (2002):

$$z_{\alpha-1/2} = \zeta(\mathbf{x}, t) + s_{\alpha-1/2} (\zeta(\mathbf{x}, t) + z_b(\mathbf{x})) \quad (2)$$

which assures a surface and terrain-following grid that is limited by the interfaces $z_{1/2} = \zeta$ and $z_{N+1/2} = -b$. Standard z-coordinate models with fixed interfaces have been enhanced over time to deal with the oscillation of the free surface. Typically a vertical moving grid is introduced, defined by a surface-following transformation from a reference fixed space with coordinate $s \in [0, -z_b(x)]$ to the physical space with vertical coordinate $z \in [\zeta, -b(x)]$:

$$z = z(\mathbf{x}, s, t) = \zeta(\mathbf{x}, t) + f(\mathbf{x}, s, t)$$

$\Gamma_{1/2}(t) = \Gamma^{\zeta}(t)$ and $\Gamma_{N+1/2} = \Gamma^b$. The reference and the physical domains with their vertical subdivisions are sketched in Figure 1. Using this transformation, the layer thickness can be deduced from the water depth, for $\alpha = 1, \dots, N$:

$$h_{\alpha}(\mathbf{x}, t) \cong z_{\alpha-1/2}(\mathbf{x}, t) - z_{\alpha+1/2}(\mathbf{x}, t) \quad (3)$$

$$\cong (s_{\alpha-1/2} - s_{\alpha+1/2}) H(\mathbf{x}, t) = l_{\alpha} H(\mathbf{x}, t) \quad (4)$$

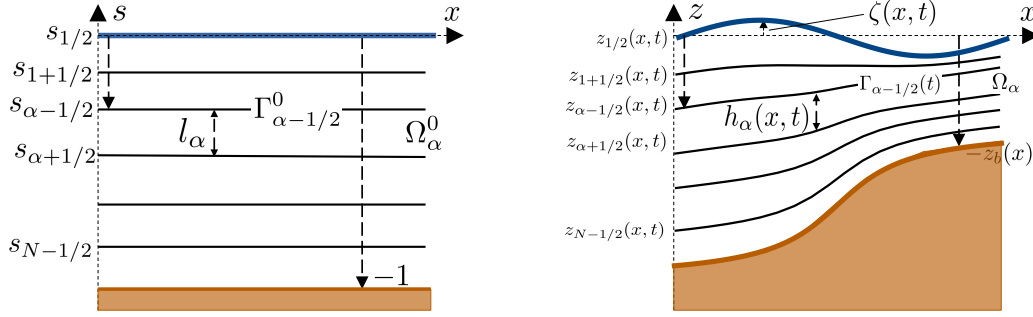


Figure 1. One-dimensional sketch of the reference (left) and physical (right) domains for the multilayer shallow water model.

with $f(x, s, t) = S(s)(z_b(x) + \zeta(x, t))$. Among the coordinates that have been proposed to enhance geo-potentials we mention: where the coefficients $l_{\alpha} = s_{\alpha-1/2} - s_{\alpha+1/2}$ are prescribed after the creation of the reference grid. They are positive and they sum to one $\sum_{\alpha=1}^N l_{\alpha} = 1$. The multilayer model is based on a piecewise constant approximation, on the vertical grid, of the horizontal fluid velocity and of a generic tracer. For $\alpha = 1, \dots, N$:

$$\underline{u_{\alpha}(\mathbf{x}, t)} \cong \frac{1}{h_{\alpha}} \int_{z_{\alpha+1/2}}^{z_{\alpha-1/2}} \underline{u(\mathbf{x}, z, t)} dz \quad (5)$$

$$\underline{T_{\alpha}(\mathbf{x}, t)} \cong \frac{1}{h_{\alpha}} \int_{z_{\alpha+1/2}}^{z_{\alpha-1/2}} \underline{T(\mathbf{x}, z, t)} dz \quad (6)$$

The tracer for us will be the salinity. We assume that the fluid density depends on salinity through an equation of state of type $\rho = \rho(T)$. The density vertical discretization derives from the tracer one, for $\alpha = 1, \dots, N$:

$$\underline{\rho_{\alpha}(\mathbf{x}, t)} \cong \underline{\rho(T_{\alpha}(\mathbf{x}, t))} \quad (7)$$

We introduce the following notation for a generic function $f(z)$:

- To express a function which is discontinuous at the interface, we use the same notation of Fernández-Nieto et al. (2014)
- ⋮

$$130 \quad \underline{f_{\alpha-1/2}^{+}} \cong \underline{(f|_{\Omega_{\alpha}})_{\Gamma_{\alpha-1/2}}}, \quad \underline{f_{\alpha-1/2}^{-}} = \underline{(f|_{\Omega_{\alpha-1}})_{\Gamma_{\alpha-1/2}}}$$

- if the function is continuous

$$\underline{f_{\alpha-1/2}} \cong \underline{f_{\alpha-1/2}^{+}} = \underline{f_{\alpha-1/2}^{-}} = \underline{f|_{\Gamma_{\alpha-1/2}}}$$

– the difference of the function between the upper and lower interface is

$$\left[f \right]_{\alpha+1/2}^{\alpha-1/2} \equiv \underline{f_{\alpha-1/2} - f_{\alpha+1/2}}$$

135 Mass conservation reads:

$$\frac{\partial \zeta}{\partial t} + \nabla \cdot \left(\sum_{\beta=1}^N h_{\beta} \mathbf{u}_{\beta} \right) = 0 \quad (8)$$

In this work we consider the multilayer shallow water model for stratified fluid with the Boussinesq assumption. Momentum and tracer equations in the multilayer approach can be written for $\alpha = 1, \dots, N$:

$$\frac{\partial h_{\alpha} \mathbf{u}_{\alpha}}{\partial t} + \nabla \cdot (h_{\alpha} \mathbf{u}_{\alpha} \otimes \mathbf{u}_{\alpha}) = \left[\mathbf{u}G \right]_{\alpha+1/2}^{\alpha-1/2} - gh_{\alpha} \nabla \zeta + \left[\mathbf{K} \right]_{\alpha+1/2}^{\alpha-1/2} + \mathbf{B}_{\alpha} \quad (9)$$

$$140 \quad \frac{\partial h_{\alpha} T_{\alpha}}{\partial t} + \nabla \cdot (h_{\alpha} T_{\alpha} \mathbf{u}_{\alpha}) = \left[TG \right]_{\alpha+1/2}^{\alpha-1/2} + \left[K_T \right]_{\alpha+1/2}^{\alpha-1/2} \quad (10)$$

where $G_{\alpha\pm 1/2}$ is the z-star coordinate (Aderoft and Campin, 2004) $z_b = b(x) \rightarrow s = z^*$ with stretching function $S = \frac{z^*}{b(x)}$; the quasi-z coordinate (Mellor et al., 2002) $z_b = \max b(x) \rightarrow s = z^{qz}$ with stretching function $S = \frac{z^{qz}}{\max b(x)}$; the hybrid z/sigma (Burchard and
 $z_b = b(x)$ since the transformation is linear in S , a blend between the z-star and the sigma coordinate $\sigma \in [0, -1]$ through a parameter θ is possible. The stretching function is $S = \frac{z^*}{b(x)}\theta + \sigma(1-\theta)$ mass-transfer function responsible for the vertical mass
145 exchange between the layers, $\mathbf{K}_{\alpha\pm 1/2}$ are the vertical viscous fluxes that model the shear stress between the layers, \mathbf{B}_{α} models the pressure force related to the buoyancy gradient. The system (8)(9) and (10) is implemented in the SHYFEM model, as well as in many other ocean models (Burchard and Petersen, 1997; Klingbeil et al., 2018). If N is the number of vertical layers, the equations are solved for $2N + 1$ unknown variables, which are: the free surface elevation, the layer discharges $h_{\alpha} \mathbf{u}_{\alpha}$ and the layer-integrated tracer $h_{\alpha} T_{\alpha}$. Standard z-coordinate is a particular case where coordinate lines do not depend on time and
150 space. Of course, this is implemented by allowing the top layer to vary in thickness without vanishing (Griffies et al., 2001), see Figure ?? for an illustrative example of these different z-grids. To account for the domain movement, the layerwise equations are written in a moving frame and, hereinafter, all partial derivatives $\partial_{\bar{a}}$ are not the standard Eulerian ones but they have to be intended in the moving frame (the so-called ALE derivatives (Hirt et al., 1974)): horizontal derivatives are taken along constant s -line $\partial_x = \partial_x|_s$ while temporal derivatives are measured from an observer moving with the grid $\partial_t = \partial_t|_s$. Please note the
155 difference between the ALE time derivative and the Lagrangian time derivative of the position:-

$$\underline{\sigma_{\alpha+1/2} = \frac{\partial z_{\alpha+1/2}}{\partial t} \quad w_{\alpha+1/2} = \frac{dz_{\alpha+1/2}}{dt}}$$

The layer thickness is deduced from the water depth through equation (4). In the following we give the details of the SHYFEM implementation of each term of the right-hand side.

From the derivation of Fernández-Nieto et al. (2014), the definition of the mass-transfer function is:

$$\begin{aligned}
 160 \quad G_{\alpha-1/2} &\equiv (\nabla z_{\alpha-1/2} \cdot \mathbf{u}_\alpha) + \sigma_{\alpha-1/2} - w_{\alpha-1/2}^+ \\
 &\equiv (\nabla z_{\alpha-1/2} \cdot \mathbf{u}_{\alpha-1}) + \sigma_{\alpha-1/2} - w_{\alpha-1/2}^-
 \end{aligned} \tag{11}$$

with σ the velocity of the grid interface and w :

$$\sigma_{\alpha-1/2} = \frac{\partial z_{\alpha-1/2}}{\partial t} \tag{12}$$

and $w_{\alpha-1/2}^\pm$ the vertical fluid velocity at $z_{\alpha+1/2}$. For each layer we define the layer thickness:

$$165 \quad h_\alpha = z_{\alpha-1/2} - z_{\alpha+1/2}$$

the interface. The vertical velocity is computed from the following relationships:

$$w_{\alpha-1/2}^+ = -w_{\alpha+1/2}^- - h_\alpha \nabla \cdot \mathbf{u}_\alpha \quad \text{and} \quad w_{\alpha-1/2}^- = w_{\alpha-1/2}^+ + \nabla z_{\alpha-1/2} \cdot (\mathbf{u}_\alpha - \mathbf{u}_{\alpha-1}) \tag{13}$$

The layerwise model is based on a piecewise constant approximation of the horizontal velocity on the vertical grid. The layer average is:

$$170 \quad u_\alpha = \frac{1}{h_\alpha} \int_{z_{\alpha+1/2}}^{z_{\alpha-1/2}} u dz$$

which are evaluated starting from the bottom $\alpha = N, \dots, 1$, where the no slip condition is imposed $w_{N+1/2}^- = \mathbf{u}_N \cdot \nabla z_b$. In practice and as it is standard in ocean models, the mass-transfer function is computed directly from the layer-integrated mass equation

$$G_{\alpha-1/2} = G_{\alpha+1/2} + \frac{\partial h_\alpha}{\partial t} + \nabla \cdot (h_\alpha \mathbf{u}_\alpha) \tag{14}$$

175 Then the layerwise shallow water model reads:

$$\frac{\partial \zeta}{\partial t} + \frac{\partial}{\partial x} \left(\sum_{\alpha=N}^1 h u_\alpha \right) = 0$$

Summing from N to α as:

$$G_{\alpha-1/2} = G_{N+1/2} + \sum_{\beta=N}^{\alpha} \frac{\partial h_\beta}{\partial t} + \sum_{\beta=N}^{\alpha} \nabla \cdot (h_\beta \mathbf{u}_\beta) \tag{15}$$

$$180 \quad \frac{\partial h u_\alpha}{\partial t} + \frac{\partial h u_\alpha u_\alpha}{\partial x} = \left[u G \right]_{\alpha+1/2}^{\alpha-1/2} - g h_\alpha \frac{\partial \zeta}{\partial x} + I P G_\alpha + \left[\nu_v \frac{\partial u}{\partial z} \right]_{\alpha+1/2}^{\alpha-1/2}$$

which implies $G_{1/2} = 0$ or no mass loss at the free-surface. The vertical velocity at the interfaces $w_{\alpha-1/2}^{\pm}$ no more appears in the system but it can be computed from the incompressibility condition (13) in a post-processing step. With a horizontal velocity and tracer discontinuous at the interfaces, the vertical momentum flux in (9) is computed with a numerical flux. An upwind flux is used in this study, for $\Gamma_{\alpha-1/2}$ it reads:

$$185 \quad G_{\alpha-1/2} \mathbf{u}_{\alpha-1/2} = G_{\alpha-1/2}^+ \mathbf{u}_{\alpha} + G_{\alpha-1/2}^- \mathbf{u}_{\alpha-1}$$

As is customary, the mass equation is integrated over the whole water column. IPG_{α} is the internal pressure gradient force written in the density Jacobian form of Song (1998) and based on a piecewise constant approximation of the density ρ_{α} as in $\nu_{\bar{v}}$ with $G_{\alpha-1/2}^+ = \max(0, G_{\alpha-1/2})$ and $G_{\alpha-1/2}^- = \min(0, G_{\alpha-1/2})$. For the tracer a TVD flux is employed (LeVeque, 2002).

The terms $K_{\alpha-1/2}$ and $K_{T,\alpha-1/2}$ are the vertical viscous and diffusive fluxes computed at the interface $\Gamma_{\alpha-1/2}$:

$$190 \quad \begin{aligned} K_{\alpha-1/2} &= \nu_{\alpha-1/2} D_z \mathbf{u}_{\alpha-1/2} \\ K_{T,\alpha-1/2} &= \nu_{T,\alpha-1/2} D_z T_{\alpha-1/2} \end{aligned}$$

where $\nu_{\alpha-1/2}$ is the vertical viscosity and $\nu_{T,\alpha-1/2}$ the vertical diffusivity. $D_z(\cdot)$ is an approximation of the vertical derivative in the diffusion term is evaluated at the interface and resolved with finite differences. The definition of the mass-transfer function $G_{\alpha \pm 1/2}$ responsible for the exchange between the layers is:

$$195 \quad G_{\alpha-1/2} = \left(\frac{\partial z}{\partial x} \Big|_{\alpha-1/2} u_{\alpha-1/2} \right) + \sigma_{\alpha-1/2} - w_{\alpha-1/2}$$

vertical viscosity and diffusivity can be laminar or computed with a turbulent model. The bottom momentum flux is specified with a quadratic formulation. Then, the viscous fluxes read:

$$K_{\alpha-1/2} = \begin{cases} \tau_w = 0, & \alpha = 1 \\ \nu_{\alpha-1/2} \frac{\mathbf{u}_{\alpha-1} - \mathbf{u}_{\alpha}}{(h_{\alpha-1} + h_{\alpha})/2}, & \alpha = 2, \dots, N \\ \tau_b = -C_F |\mathbf{u}_N| \mathbf{u}_N, & \alpha = N + 1 \end{cases}$$

which is typically computed by summing the layerwise mass equation:-

$$200 \quad G_{\alpha-1/2} = G_{\alpha+1/2} + \frac{\partial h_{\alpha}}{\partial t} + \frac{\partial h u_{\alpha}}{\partial x}$$

with C_F the bottom friction coefficient. Similarly the diffusive fluxes read:

$$K_{T,\alpha-1/2} = \begin{cases} 0, & \alpha = 1 \\ \nu_{T,\alpha-1/2} \frac{T_{\alpha-1} - T_{\alpha}}{(h_{\alpha-1} + h_{\alpha})/2}, & \alpha = 2, \dots, N \\ 0, & \alpha = N + 1 \end{cases}$$

from the bottom layer N to layer α with $G_{N+1/2}$ that accounts for the bottom boundary condition and $G_{1/2} = 0$ that ensures vertical mass conservation. At the end we solve for $N + 1$ unknowns, namely the free surface level ζ and N momenta ht_{α} $\alpha = 1, N$, with no tracer fluxes through the free-surface and the bottom.

We assume that the fluid density depends on a given set of tracers through an equation of state of type $\rho(T, S)$ where $T(x, t)$ is the temperature and $S(x, t)$ is the salinity. Each tracer is governed by an advection-diffusion equation:-

$$\frac{\partial ht_{\alpha}}{\partial t} + \frac{\partial ht_{\alpha} u_{\alpha}}{\partial x} = \left[tG \right]_{\alpha+1/2}^{\alpha-1/2} + \left[\nu_{tv} \frac{\partial t_{\alpha}}{\partial z} \right]_{\alpha+1/2}^{\alpha-1/2}$$

Finally, the term B_{α} represents the internal pressure gradient force. The layer-integrated pressure gradient term $\int_{z_{\alpha+1/2}}^{z_{\alpha-1/2}} \nabla p(z) dz$, instead of applying the Leibniz rule (Audusse et al., 2011a), it as been split into the external pressure gradient, related to the free-surface slope, and the internal pressure gradient, related to the buoyancy gradient. The internal pressure gradient term is written in the density Jacobian form of Song (1998):

$$B_{\alpha} = h_{\alpha} b_1 \nabla \zeta + h_{\alpha} \sum_{\beta=1}^{\alpha} J(b_{\beta-1/2}, z_{\beta-1/2}) h_{\beta-1/2}$$

where $h_{\beta-1/2}$ is the distance between the layer centers, that is $h_{\beta-1/2} = (h_{\beta-1} + h_{\beta})/2$ for $\beta = 2, \dots, N$ and $h_{\beta-1/2} = h_1/2$ for $\beta = 1$. The summation over the layers corresponds to a vertical integration of the density Jacobian based on the piecewise constant profile of the density with the quadrature points placed at the interfaces. The density Jacobian at the interface is:

$$J(b_{\beta-1/2}, z_{\beta-1/2}) = \nabla b_{\beta-1/2} - D_z(b_{\beta-1/2}) \nabla z_{\beta-1/2}$$

where ν_{tv} is the vertical tracer diffusivity. This advection diffusion equation If $b_{\beta} = g \frac{\rho_0 - \rho_{\beta}}{\rho_0}$ is the layer buoyancy, the buoyancy at the interface is computed with an average $b_{\beta-1/2} = \frac{1}{2} (\nabla b_{\beta-1} + \nabla b_{\beta})$ for $\beta = 2, \dots, N$ and $b_{\beta-1/2} = \frac{1}{2} \nabla b_1$ for $\beta = 1$. The approximation of the vertical derivative evaluated at the interface is resolved with finite differences. It is taken zero for the first interface $D_z(b_{\beta-1/2}) = 0$ for $\beta = 1$ and $D_z(b_{\beta-1/2}) = (b_{\beta-1} - b_{\beta})/h_{\beta-1/2}$ for $\beta = 2, \dots, N$. These choices allows to recover a standard formula that can be found in Shchepetkin and McWilliams (2003) or in Klingbeil et al. (2018).

The tracer equation (10) admits a trivial solution which we want to inherit also at the discrete level, the so-called tracer constancy condition. In fact, for constant tracer $t_{\alpha} = const$: for a constant tracer, equation (10) reduces to the layerwise mass equation (14). This is also called the Geometric Conservation Laws (GCL) condition in ALE compressible flow simulations. The importance of preserving this property at a discrete level has been discussed extensively in Gross et al. (2002).

For a standard z -layer model, The system (8)(9) and (10) is similar to the one presented in Audusse et al. (2011a). They differ for the more stringent Boussinesq assumption used here and for the expression of the pressure gradient term, written with a pressure Jacobian form in the reference.

2.1 z -star

The multilayer model presented so far is based on vertical subdivision of the fluid domain through the surface/terrain-following transformation (2) which leads to the coefficients l_{α} given in (4). Other vertical subdivisions can be used leading to different

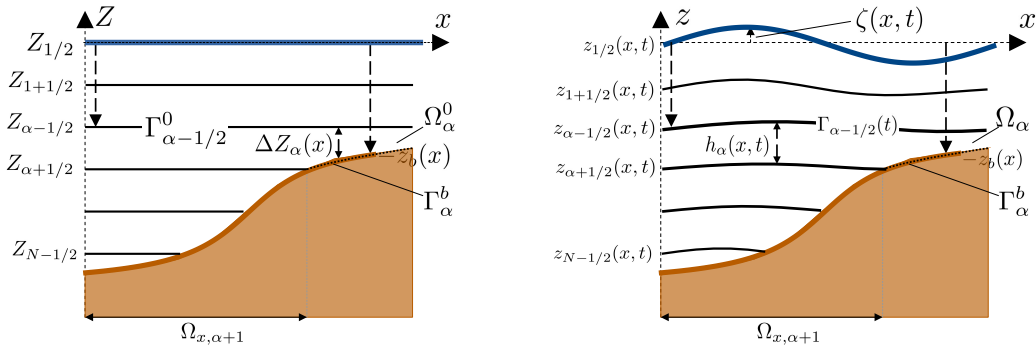


Figure 2. Figure. One-dimensional sketch of the reference (left) and physical (right) domains for the multilayer shallow water model with z -star layers.

coefficients that however, must verify both the positivity constraint and they have to sum to one. In the following we specify a slicing of the domain with both these properties based on a vertical coordinate transformation called z -star (Adcroft and Campin, 2004)

235 The reference domain, with vertical coordinate Z , is:

$$\Omega^0 = \left\{ (\mathbf{x}, Z) : \mathbf{x} \in \Omega_{\mathbf{x}}, -z_b(\mathbf{x}) \leq Z \leq 0 \right\}$$

This domain is discretized by means of a vertical grid composed of N layers, with interfaces $\Gamma_{\alpha-1/2}^0$, which are aligned to the geopotential. These interfaces can be described by constant functions:

$$Z_{1/2} = 0 < Z_{2-1/2} < \dots < Z_{N+1/2} = -\max z_b(\mathbf{x})$$

240 As shown in Figure 2, there is a substantial difference with the vertical subdivision of the terrain-following grid. The grid interfaces could intersect the bathymetry and should be defined only in the fluid domain. We define the projection of the interface $\Gamma_{\alpha-1/2}^0$ onto the horizontal plane as:

$$\Omega_{\mathbf{x},\alpha} = \left\{ \mathbf{x} : \mathbf{x} \in \Omega_{\mathbf{x}} \text{ and } -z_b(\mathbf{x}) \leq Z_{\alpha-1/2} \right\} \quad (16)$$

If a layer is bounded laterally by the bathymetry interface we can denote this lateral land boundary of the layer as :

$$245 \Gamma_{\alpha}^b \equiv \left\{ (\mathbf{x}, Z) : Z = -z_b(\mathbf{x}) \text{ and } Z_{\alpha+1/2} \leq Z \leq Z_{\alpha-1/2}, \mathbf{x} \in \Omega_{\mathbf{x},\alpha} \setminus \Omega_{\mathbf{x},\alpha+1} \right\}$$

Each layer Ω_{α}^0 results delimited on the upper and bottom side by $\Gamma_{\alpha-1/2}^0$ and laterally by the vertical domain boundary as well as it could be delimited by Γ_{α}^b (see Figure 2, right panel). To map the reference interface $\Gamma_{\alpha-1/2}^0$ to the interfaces do not depend on location or time, except for the free surface interface. In , or equivalently in using a layerwise integration of the incompressibility $[w]_{\alpha+1/2}^{\alpha-1/2} = -h_{\alpha} \frac{\partial u_{\alpha}}{\partial x}$, if the depth of layers does not change in time, physical interface $\Gamma_{\alpha-1/2}$, again, we

250 can use a generalized coordinate transformation, for $\alpha = 1, \dots, N$:

$$z_{\alpha-1/2} = \zeta(\mathbf{x}, t) + S_{\alpha-1/2}(\mathbf{x}) (\zeta(\mathbf{x}, t) + z_b(\mathbf{x})), \quad \mathbf{x} \in \Omega_{\mathbf{x},\alpha} \quad (17)$$

with $S_{\alpha-1/2}$ a stretching function defined as:

$$S_{\alpha-1/2}(\mathbf{x}) = \frac{Z_{\alpha-1/2}}{z_b(\mathbf{x})}$$

As in the previous Section, the layer thickness can be deduced from the total water depth. After some calculations we get:

$$\begin{aligned} 255 \quad h_{\alpha}(\mathbf{x}, t) &\approx z_{\alpha-1/2}(\mathbf{x}, t) - \max(z_{\alpha+1/2}(\mathbf{x}, t), -z_b(\mathbf{x})) \\ &\approx (Z_{\alpha-1/2} - \max(Z_{\alpha+1/2}, -z_b(\mathbf{x}))) H(\mathbf{x}, t) = l_{\alpha}(\mathbf{x}) H(\mathbf{x}, t), \quad \mathbf{x} \in \Omega_{\mathbf{x}, \alpha} \end{aligned} \quad (18)$$

If we define $\Delta Z_{\alpha}(\mathbf{x}) = Z_{\alpha-1/2} - \max(Z_{\alpha+1/2}, -z_b(\mathbf{x}))$ we can rewrite the coefficients, for $\alpha = 1, N$:

$$l_{\alpha}(\mathbf{x}) = \frac{\Delta Z_{\alpha}(\mathbf{x})}{z_b(\mathbf{x})}, \quad \mathbf{x} \in \Omega_{\mathbf{x}, \alpha}$$

which is prescribed once the reference grid is created. The coefficient satisfy both the positivity constraint and locally they sum to one.

260

An important property of the z -star transformation is the that the horizontal domain $\Omega_{\mathbf{x}, \alpha}$ where the layer thickness h_{α} is defined, does not depend on time, as one can verify after computing the transformation (17) for $Z_{\alpha-1/2} = -z_b(\mathbf{x})$. This is particularly helpful because the number of layers does not depend on time, and the coefficients too. Other z -layers formulations based on similar mappings, such as the quasi- z layers (Mellor et al., 2002) or the hybrid z/σ layers (Burchard and Petersen, 1999) do not share this property. For these coordinates a special treatment of the bottom is necessary: either an *ad hoc* modification of the bottom geometry or more interestingly these coordinates could be coupled with the porosity approach recently proposed by Debreu et al. (2020) where all the layers present in the computation. For z -star the bottom momentum and tracer fluxes must be properly modified, replacing the maximum number of layers N , with the local number of layers $N_b(\mathbf{x}) = \{\alpha : Z_{\alpha+1/2} \leq -z_b(\mathbf{x}) \leq Z_{\alpha-1/2}\}$.

265

270 2.2 z -layers

The z -layers are a particular case where the interfaces do not depend on time and space:

$$z_{\alpha-1/2} = Z_{\alpha-1/2}$$

This method is implemented in the ocean models by allowing the top layer to vary in thickness without vanishing (Griffies et al., 2001). For the above transformation with fixed interfaces, the mass-transfer function coincides with the vertical velocity:

$$275 \quad \frac{\partial z}{\partial x} \Big|_{\alpha-1/2} = 0, \quad \sigma_{\alpha-1/2} = 0 \quad \rightarrow \quad G_{\alpha-1/2} = -w_{\alpha-1/2}, \quad \alpha = 2, N+1$$

function (eq. (14)) coincides with the vertical velocity:

$$G_{\alpha-1/2} = -w_{\alpha-1/2}^- = -w_{\alpha-1/2}^+, \quad \alpha = 2, N+1$$

A classical Eulerian model in the vertical is obtained. Replacing the mass transfer function with the vertical velocity in the multilayer model, we obtain the Eulerian model of Rambaud (2011).

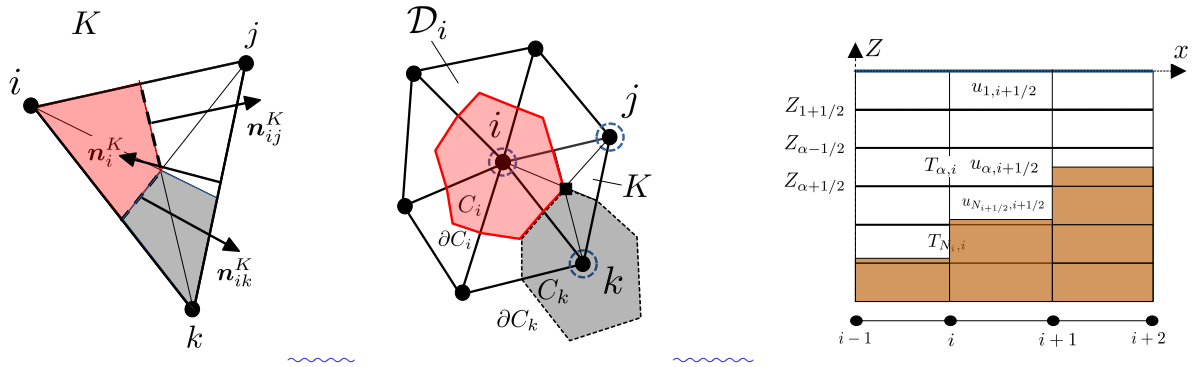


Figure 3. Grid and notation. Left: triangle K with nodes and scaled normals. Middle: set \mathcal{D}_i with dual cell area C_i and dual cell boundary ∂C_i . The degrees of freedom are also shown: discharge \blacksquare , tracer and free-surface \circ . Right: stepped bathymetry with masked boxes in brown, after the horizontal discretization.

280 2.3 Numerical mixing induced by the free surface

3 Semi-implicit staggered finite element discretization

To complete and we have to give the expressions for the prognostic variables at the top/bottom interfaces. Consistently with the Finite Volume vertical discretization, the tracer and the horizontal velocity at the interface are computed with a numerical flux. The majority of ocean models, including SHYFEM, use a Total Variation Diminishing (TVD) flux. For the tracer,

285 The discretization for both the z -star and the TVD flux reads (LeVeque, 2002):

$$G_{\alpha-1/2} t_{\alpha-1/2} = G_{\alpha-1/2}^+ t_{\alpha} + G_{\alpha-1/2}^- t_{\alpha-1} + \frac{|G_{\alpha-1/2}|}{2} \left(1 - \left| \frac{G_{\alpha-1/2} \Delta t}{\Delta z_{\alpha-1/2}} \right| \right) (t_{\alpha} - t_{\alpha-1}) \phi$$

z -layers shallow water model can proceed in an equivalent fashion. We consider a discretization of the horizontal domain $\Omega_x \in \mathbb{R}^2$ composed by non-overlapping triangular elements. We denote the horizontal grid by \mathcal{T} with $K \in \mathcal{T}$ the generic triangle, $|K|$ its area. The local reference element length is h_K and it is computed as the minimum length of the triangle sides.

290 With $i \in \mathcal{T}$ we denote the nodes of the grid. When no confusion is generated, we will locally number as $(j = 1, 2, 3$ or $j \in K)$ the nodes of the generic triangle. Given a node i in an element K , \mathbf{n}_i^K denotes the inward vector normal to the edge of K opposite to i , scaled by the length of the edge, see Figure 3, left panel. For every node of the triangulation, \mathcal{D}_i denotes the subset of triangles containing i . The dual cell C_i is obtained by joining the barycenters of the triangles in \mathcal{D}_i with the midpoints of the edges meeting in i as illustrated in Figure 3, middle panel. Its area is

295
$$|C_i| = \sum_{K \in \mathcal{D}_i} \frac{|K|}{3}$$

delimited by the boundary ∂C_i . The edge of ∂C_i separating $C_i \cap K$ and $C_j \cap K$ has an exterior normal called \mathbf{n}_{ij}^K , as illustrated in Figure 3, left panel. As before it is scaled by the edge length. Moreover, due to the definition of the dual cell, we have:

$$\sum_{j \in K, j \neq i} \mathbf{n}_{ij}^K = -\frac{\mathbf{n}_i^K}{2} \quad (19)$$

After the horizontal discretization, the domain results subdivided into prismatic boxes $K \times [z_{\alpha+1/2}, z_{\alpha-1/2}]$. At the bottom, z -layers models apply a mask to non-existing land boxes that make the bathymetry stepped, as sketched in Figure 3, right panel. The bottom layer for each element will be denoted as N_K . For a staggered discretization it is helpful also to define a nodal bottom layer $N_i = \max_{K \in \mathcal{D}_i} N_K$. The projections of the interfaces onto the horizontal plane are still denoted as $\Omega_{\mathbf{x}, \alpha}$ and defined with (16), this time evaluated with the stepwise approximation of the bathymetry. Then a layer dual cell $C_{\alpha, i}$ can be defined by considering $\mathcal{D}_{\alpha, i}$ the subset of elements sharing node i and in $\Omega_{\mathbf{x}, \alpha}$. Its area is

$$|C_{\alpha, i}| = \sum_{K \in \mathcal{D}_{\alpha, i}} \frac{|K|}{3}$$

with $G^+ = \max(0, G)$, $G^- = \min(0, G)$, $\Delta z_{\alpha-1/2} = \frac{h_{\alpha} + h_{\alpha-1}}{2}$ and Δt the time step. Here we consider the Superbee flux limiter ϕ which is close to one in smooth regions (second-order accurate Lax-Wendroff flux) while it is close to zero in presence of large vertical gradients (first-order accurate upwind flux).

With a local truncation error analysis, we can further analyze the error typically associated with the vertical z -coordinate discretization when large vertical velocities induced by the tidal flow are present. Under the hypothesis of a passive tracer advected by a linearized barotropic tidal flow, we have computed the following upper bound for the vertical numerical diffusion induced by the oscillation of the water level:

$$D_{\alpha}^{num} \leq \frac{1 - \phi_{\alpha}}{2} A \Omega \left. \frac{\partial^2 t}{\partial z^2} \right|_{\alpha} h + \frac{1}{6} \frac{A \Omega}{H_0} \left. \frac{\partial^2 t}{\partial z^2} \right|_{\alpha} h^2 + O(h^3)$$

On a B-staggered grid the free-surface elevation, the discharges and the tracers are described with basis functions of different order and support. The discharge field and the tracer field belong to a finite dimensional space with basis composed by the piecewise constant functions. For the discharges, the space has basis $\{\psi_K\}_{K \in \mathcal{T}}$ composed by the characteristic functions on the triangle, while for the tracers we choose $\{\phi_i\}_{i \in \mathcal{T}}$ composed by the characteristic functions on the dual cell. The discharge fields $\mathbf{q}_{\alpha} = h_{\alpha} \mathbf{u}_{\alpha}$ and the tracers T_{α} are approximated through (we use an abuse of notation employing the same symbol of the continuous variable):

$$\mathbf{q}_{\alpha}(\mathbf{x}, t) \equiv \sum_{K \in \mathcal{T}} \psi_K(\mathbf{x}) \mathbf{q}_{\alpha, K}(t) \quad (20)$$

$$T_{\alpha}(\mathbf{x}, t) \equiv \sum_{i \in \mathcal{T}} \phi_i(\mathbf{x}) T_{\alpha, i}(t) \quad (21)$$

with $\mathbf{q}_{\alpha, K}(t)$, defined for $\alpha = 1, \dots, N_K$, being the elemental discharge values and with $T_{\alpha, i}(t)$, defined for $\alpha = 1, \dots, N_i$, the nodal tracer values. The free-surface belongs to a space of finite dimension with basis $\{\varphi_i\}_{i \in \mathcal{T}}$ which denotes the standard

continuous piecewise linear Lagrange basis. The discrete free-surface is given by:

$$325 \quad \zeta(\mathbf{x}, t) = \sum_{i \in \mathcal{T}} \varphi_i(\mathbf{x}) \zeta_i(t) \quad (22)$$

where h the uniform vertical grid-spacing, A the tidal amplitude, $\Omega = 2\pi/T$, T the tidal period and H_0 is the bottom depth. Unsurprisingly, $\zeta_i(t)$ are the nodal free-surface values. Note that the leading order term is a discrete discharges and discrete tracers are discontinuous respectively across the boundaries of the triangles and of the dual cells whereas the discrete free-surface is globally continuous. On a B-grid the layers thickness is naturally computed at the grid nodes $h_{\alpha,i}$, where the free-surface is available. The element values $h_{\alpha,K}$ are a conservative average of the nodal values. The element velocities are obtained from $\mathbf{u}_{\alpha,K} = \frac{q_{\alpha,K}}{h_{\alpha,K}}$

We obtain the weak formulation multiplying mass and momentum equations (8) and (9) by the test functions that belongs to the same space of the solution and integrating it on the horizontal domain. The finite element discretization reduces to compute the integrals accounting for the different terms. For the mass flux term, which is integrated by parts we need to compute with a proper quadrature rule the following integral (only x -component shown):

$$335 \quad a_{iK}^x = \int_K \frac{\partial \varphi_i}{\partial x} dx$$

The boundary term has been neglected since it cancels out except at the lateral domain boundary. Similarly, for the terms that will be treated explicitly in the momentum equation namely the horizontal/vertical advection and the internal pressure gradient, we have:

$$340 \quad f_{\alpha,K}^x \equiv - \int_{\partial K} \widehat{\mathbf{q}}_{\alpha} u_{\alpha} \cdot \mathbf{n} ds + \int_K \left(B_{\alpha}^x + [uG]_{\alpha+1/2}^{\alpha-1/2} \right) dx$$

The horizontal advection term is resolved with a first-order upwind diffusion with a coefficient that depends on the tidal amplitude and is tuned by the limiter. For a smooth profile this term is zero ($\phi \approx 1$) or even of anti-diffusive nature ($\phi > 1$), while for a non-smooth profile ($\phi \approx 0$) this term dominates. Interestingly there is also a second-order term that comes from the linear advection velocity, with a coefficient that depends on the upwind flux $\widehat{\mathbf{q}}_{\alpha} u_{\alpha}$ (Umgiesser et al., 2004). In order to write the scheme in matrix form, exploiting the compactness of the staggered discretization, we introduce "vertical" vectors/matrix, that pile-up all the layers for a single element K , and we denote them with bold capital letters. For example, the layer discharges and the layers thickness are regrouped in the following vectors:

$$345 \quad \mathbf{U}_K = \begin{pmatrix} q_{1,K}^x \\ \vdots \\ q_{\alpha,K}^x \\ \vdots \\ q_{N_K,K}^x \end{pmatrix}, \quad \mathbf{V}_K = \begin{pmatrix} q_{1,K}^y \\ \vdots \\ q_{\alpha,K}^y \\ \vdots \\ q_{N_K,K}^y \end{pmatrix}, \quad \mathbf{H}_K = \begin{pmatrix} h_{1,K} \\ \vdots \\ h_{\alpha,K} \\ \vdots \\ h_{N_K,K} \end{pmatrix}$$

and analogously the explicit terms:

$$350 \quad \mathbf{F}_K^x = \begin{pmatrix} f_{1,K}^x \\ \dots \\ f_{\alpha,K}^x \\ \dots \\ f_{N_K,K}^x \end{pmatrix}, \quad \mathbf{F}_K^y = \begin{pmatrix} f_{1,K}^y \\ \dots \\ f_{\alpha,K}^y \\ \dots \\ f_{N_K,K}^y \end{pmatrix}$$

The vertical viscous term is recast in matrix form via a tridiagonal matrix $\mathbf{A}_K^d \in \mathbb{R}^{N_K \times N_K}$. The bottom momentum flux has to be integrated into this matrix. Note that all these vectors/matrix are restricted to non-masked boxes.

We build a semi-implicit time discretization, as it is standard for ocean models, by treating semi-implicitly the mass flux and the free surface gradient in the momentum equation. The vertical viscous term can also cause a restrictive time-step and is handled here implicitly without major computation issues but allowing to relax the CFL condition. We define the variation of a quantity in a time step as $\Delta u = u^{n+1} - u^n$, then:

$$u^{n+\theta} = \theta u^{n+1} + (1-\theta)u^n = \theta \Delta u + u^n$$

We consider different implicitness parameters for the mass fluxes (θ_z) and for the external pressure gradient (θ_m). After applying the previous definition into the semi-discrete equations, the semi-implicit momentum equations on an unstructured B-grid read:

$$\Delta \mathbf{U}_K \equiv \Delta \mathbf{U}_K^* - \Delta t g \mathbf{A}_K^{-1} \mathbf{H}_K^n \sum_{j \in K} a_{jK}^x \theta_m \Delta \zeta_j \quad (23)$$

$$\Delta \mathbf{V}_K \equiv \Delta \mathbf{V}_K^* - \Delta t g \mathbf{A}_K^{-1} \mathbf{H}_K^n \sum_{j \in K} a_{jK}^y \theta_m \Delta \zeta_j \quad (24)$$

with $\mathbf{A}_K = (\mathbf{I}|K| - \Delta t \mathbf{A}_K^d)$ a tridiagonal, positive definite and diagonally dominant matrix. The non-linear parameter of the tidal wave A/H_0 . This can also be large for shallow depths. The numerical diffusion should be always compared to the physical diffusion $D_\alpha^{phy} = \nu_{\tau 0} \partial_{zz} t$. dependence of the external pressure gradient term from \mathbf{H}_K has been resolved by using the old value. Also the viscous matrix has been computed with frozen values at t^n . In \mathbf{F}_K^n all the quantities are computed at t^n , included the mass-transfer function. These choices avoid to solve a non-linear system at each time step. The magnitude of each contribution depends on the tracer vertical profile as well as on the tidal parameter and the bottom depth. In variation $\Delta(\cdot)^* = (\cdot)^* - (\cdot)^n$ is the Appendix, we give the details of the formula and we compute it for some idealized situations. We also confirm numerically the results. Both the theoretical and numerical results suggest that solution of the following Euler step with an explicit external pressure gradient:

$$\Delta \mathbf{U}_K^* \equiv \Delta t \mathbf{A}_K^{-1} \left(\mathbf{F}_K^{x,n} + \mathbf{A}_K^d \mathbf{U}_K^n - g \mathbf{H}_K^n \sum_{j \in K} a_{jK}^x \zeta_j^n \right) \quad (25)$$

$$\Delta \mathbf{V}_K^* \equiv \Delta t \mathbf{A}_K^{-1} \left(\mathbf{F}_K^{y,n} + \mathbf{A}_K^d \mathbf{V}_K^n - g \mathbf{H}_K^n \sum_{j \in K} a_{jK}^y \zeta_j^n \right) \quad (26)$$

If the expressions for ΔU_K and ΔV_K , for micro-tidal applications and typical vertical resolution of coastal models, the additional numerical error of z-coordinate is negligible while for higher tidal amplitude/coarser resolution the use of z-coordinate should be discouraged. (23) and (24), are introduced into the discrete mass equation, we obtain a linear system with only the free-surface coefficients as unknowns:

$$\sum_{K \in \mathcal{D}_i} \sum_{j \in K} \left(m_{ij}^K + g \theta_z \theta_m \Delta t^2 \left(a_{iK}^x \mathbf{1}^T \mathbf{A}_K^{-1} \mathbf{H}_K^n a_{jK}^x + a_{iK}^y \mathbf{1}^T \mathbf{A}_K^{-1} \mathbf{H}_K^n a_{jK}^y \right) \right) \Delta \zeta_j = \Delta t \sum_{K \in \mathcal{D}_i} \left(a_{iK}^x \mathbf{1}^T (\theta_z \Delta \mathbf{U}_K^* + \mathbf{U}_K^n) + a_{iK}^y \mathbf{1}^T (\theta_z \Delta \mathbf{V}_K^* + \mathbf{V}_K^n) \right) \quad (27)$$

where $m_{ij}^K = \int_K \varphi_i \varphi_j d\mathbf{x}$ is the Galerkin mass matrix based on the piecewise linear Lagrange basis functions. The Galerkin mass matrix, in SHYFEM, is lumped. The vector $\mathbf{1} \in \mathbb{R}^{N_K}$ has all components being one.

4 z-surface-adaptive coordinate

The hydrodynamic time step flow chart is thus the following: we first perform the Euler step (25) and (26). Then we resolve the mass equation (27) and we complete momentum update with the semi-implicit step (23) and (24). Finally we compute the layers thickness at the grid nodes. For a z-star we use the expression (18) at the grid nodes. For the z-layers, the layers thickness does not change except for the first layer.

In this section, we detail the algorithm for the novel z-surface-adaptive coordinates. It is based on two steps: a first vertical grid movement step (interface displacement) and a second topology modification step (layer insertion, layer removal). The solution is interpolated across the grids: 1) for the grid movement, we have already written the layerwise equations in a moving frame, thus we compute the solution directly onto the new deformed grid; 2) for the grid topology change, we use conservative remaps. Both operations are described in the following paragraphs.

3.1 Mass-transfer function

We consider numerical schemes for the layerwise Shallow Water equations that work with a After the hydrodynamic update of the previous paragraph, the discrete mass-transfer function is computed. We employ the same continuous piecewise linear approximation used for the free-surface. The nodal values are computed from a finite-element mass-lumped discretization of the computational domain $[0, L]$ composed by a sequence of non-overlapping intervals or elements E , each with length Δx_E . The nodes of the horizontal grid are placed at $x_i = \sum_{E=1}^{i-1} \Delta x_E$, $i = 1, M + 1$. The element sharing node i and $i + 1$ is also denoted as $E = i + 1/2$. For example, the median dual cell is obtained by joining the barycenters of the elements joining in i , $C_i = \frac{1}{2} (\Delta x_{i-1/2} + \Delta x_{i+1/2})$. On such horizontal grid, we denote the space discrete variables as $u_{\text{h}}(x) \approx u(x)$ and we identify approximation of variables at nodes as $u_i = u_{\text{h}}(x_i)$ and at elements as $u_{i+1/2} = u_{\text{h}}(x_{i+1/2})$. In a Finite Volume context the pointwise notation stands for the averaged values. We suppose that the numerical scheme computes the variables at the discrete time instants $t^n = t^0 + n \Delta t$ with time step Δt . We note by $u_{\text{h}}^n(x) = u_{\text{h}}(x, t^n)$ the fully discrete variable, that is

the value of u_h at time t^n . layerwise mass equation (14). As for the depth-integrated mass equation, the discharge is evaluated semi-implicitly. Starting from the bottom with $G_{N_i+1/2,i}^{n+1} = 0$, for $\alpha = N_i, \dots, 1$:

$$405 \quad |C_{\alpha,i}| G_{\alpha-1/2,i}^{n+1} = |C_{\alpha+1,i}| G_{\alpha+1/2,i}^{n+1} + |C_{\alpha,i}| \frac{\Delta h_{\alpha,i}}{\Delta t} - \sum_{K \in \mathcal{D}_{\alpha,i}} \left(a_{iK}^x q_{\alpha,K}^{x,n+\theta_z} + a_{iK}^y q_{\alpha,K}^{y,n+\theta_z} \right) \quad (28)$$

Note that the semi-implicit discretization ensures vertical mass-conservation. Summing up (28) for all the layers and using equation (27) with a lumped Galerkin mass-matrix to cancel the right-hand side, we get the impermeability condition at the free-surface $G_{1/2,i}^{n+1} = 0$. With standard z -layers, the contribution related to the grid velocity is zero $\Delta h_{\alpha,i} = \Delta t [\sigma_i]_{\alpha+1/2}^{\alpha-1/2} = 0$, except for the first layer.

410 On the vertical, layers are contained in-

3.2 Tracers

The semi-implicit update is completed with the time-stepping of the tracer. Vertical diffusion is treated implicitly and the remaining advection terms are explicit. The spatial discretization of the the explicit terms implies the computation of the following integrals which account for the horizontal and vertical advection terms:

$$415 \quad \underline{f_{\alpha,i}} \cong - \int_{\partial C_{\alpha,i}} \widehat{T_{\alpha} \mathbf{q}_{\alpha}} \cdot \mathbf{n} ds + \int_{C_{\alpha,i}} [TG]_{\alpha+1/2}^{\alpha-1/2} dx$$

where $\widehat{T_{\alpha} \mathbf{q}_{\alpha}}$ is an appropriate numerical tracer flux across the dual cell boundary. At the lateral boundary $\partial \Omega_{x,\alpha}$, the tracer flux is zero for land boundaries while it is determined by the set $\alpha = \{1, 2, \dots, N\}$. For a z -grid the number of layers varies with x and it is defined locally, e.g. at nodes $\alpha_i = \{1, 2, \dots, N_i\}$ and at elements $\alpha_E = \{1, 2, \dots, N_E\}$. We denote each layer interface at rest as $z_{\alpha \pm 1/2}^0$ and each layer thickness at rest as Δz_{α}^0 . After both the horizontal and the boundary conditions at the domain

420 boundary. In the discussion that follows we consider only nodes that do not lie on the domain boundary. On a triangular grid the two terms read:

$$\int_{\partial C_{\alpha,i}} \widehat{T_{\alpha} \mathbf{q}_{\alpha}} \cdot \mathbf{n} ds \cong \sum_{K \in \mathcal{D}_{\alpha,i}} \sum_{j \in K, j \neq i} \widehat{T_{\alpha} \mathbf{q}_{\alpha}} \cdot \mathbf{n}_{ij}^K = \sum_{K \in \mathcal{D}_{\alpha,i}} \sum_{j \in K, j \neq i} \widehat{H}_{\alpha}(T_{\alpha,i}, T_{\alpha,j}) \quad (29)$$

$$\int_{C_{\alpha,i}} [TG]_{\alpha+1/2}^{\alpha-1/2} dx \cong |C_{\alpha,i}| T_{\alpha-1/2,i} G_{\alpha-1/2,i} - |C_{\alpha+1,i}| T_{\alpha+1/2,i} G_{\alpha+1/2,i} \quad (30)$$

with $\widehat{H}_{\alpha}(T_{\alpha,i}, T_{\alpha,j})$ being the numerical flux in the horizontal direction and $T_{\alpha+1/2,i} G_{\alpha+1/2,i}$ the numerical flux in the vertical direction. The SHYFEM model implements second-order consistent TVD fluxes in both directions.

Using the notation with bold capital letters denoting "vertical z -coordinate discretizations," vectors, the domain is subdivided into quadrilateral boxes $E \times [z_{\alpha+1/2}, z_{\alpha-1/2}]$. At the bottom, z -coordinate models apply a mask to non-existing boxes that

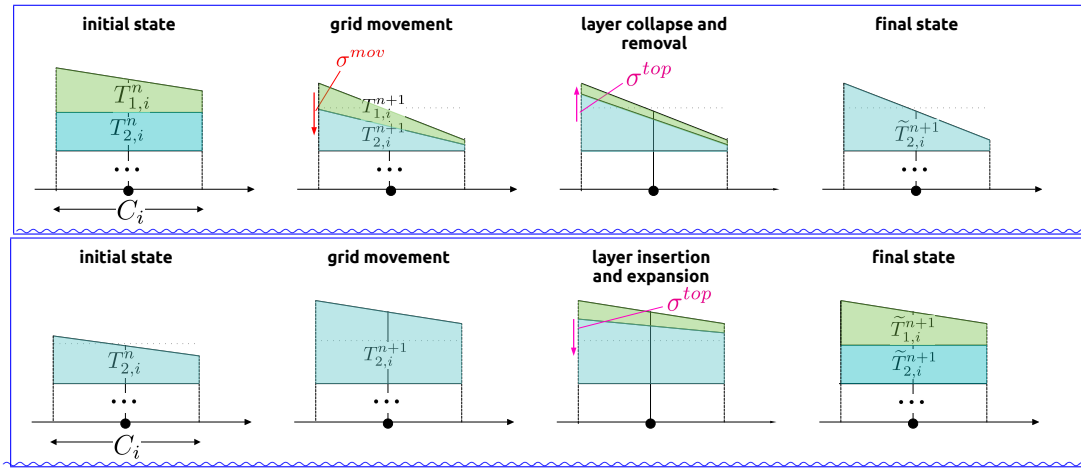


Figure 4. Grid and tracer evolution during one time step. The process is interpreted as four stages which bring from the pair (T^n, ζ_i^n) to $(\tilde{T}^{n+1}, \zeta^{n+1})$. The vector $T = \{T_1, T_2\}$ collects the layer values of the tracer. Dashed line means removed interface. Left: case of top layer insertion. Right: case of top layer removal.

~~make the grid stepped.~~ tracer values and the explicit term at the nodes are regrouped in the following:

$$T_i = \begin{pmatrix} T_{1,i} \\ \dots \\ T_{\alpha,i} \\ \dots \\ T_{N_i,i} \end{pmatrix}, \quad F_i = \begin{pmatrix} f_{1,i} \\ \dots \\ f_{\alpha,i} \\ \dots \\ f_{N_i,i} \end{pmatrix}$$

430 Vertical diffusion can also be assembled in matrix form through the discrete matrix $A_i^d \in \mathbb{R}^{N_i \times N_i}$. Then, the discretization of the layerwise tracer equation (10) read:

$$A_i T_i^{n+1} \cong \text{Diag}\{|C_{\alpha,i}|h_{\alpha,i}^n\} T_i^n + \Delta t F_i^n \quad (31)$$

with $A_i = \left(\text{Diag}\{|C_{\alpha,i}|h_{\alpha,i}^{n+1}\} - \Delta t A_i^d \right)$ the vertical tracer matrix. Although the advection terms are explicit, it should be noted that the horizontal numerical flux are computed with the discharges evaluated at $g_{\alpha}^{n+\theta_z}$ while the vertical numerical flux uses the last available mass-transfer function $C_{\alpha \pm 1/2}^{n+1}$ from (28). This choice is important in order to maintain a consistency of the discrete tracer equation with the layerwise mass equation. In fact inserting a constant tracer in equation (31), yields exactly the discrete layerwise mass equation (28). The proof is left in the Appendix.

To conclude, we summarize the whole time step flow chart: after the hydrodynamic update described in Section 3, we compute the mass-transfer function (28) and, lastly, we update the tracers with (31).

440 4 z -surface-adaptive layers

In this section, we enhance the z -layers shallow water model by introducing a new algorithm that allows for the dynamic insertion and removal of surface boxes or, with an abuse of language, of surface layers. To differentiate it from the standard

445 z -layers, we will refer to this enhanced version as z -surface-adaptive layers. The key idea is to interpret the area swept by the layer interface in the time step $\Delta t \in [t^n, t^{n+1})$ as the sum of two contributions: one due to the mesh movement driven by the free surface oscillation (grid movement) and one due to the collapse/expansion of the layer (topology change). These topology changes in fact can be seen as a continuous deformation of the layer interfaces performed within the time step. With this in mind, the final position of the interfaces at the grid nodes $\tilde{z}_{\alpha-1/2,i}^{n+1} = \tilde{z}_{\alpha-1/2}(\mathbf{x}_i, t^{n+1})$ is:

$$\tilde{z}_{\alpha-1/2,i}^{n+1} = z_{\alpha-1/2,i}^{n+1} + \Delta \tilde{z}_{\alpha-1/2,i}$$

450 where $z_{\alpha-1/2,i}^{n+1} = z_{\alpha-1/2}(\mathbf{x}_i, t^{n+1})$ is the interface position after the grid movement and $\Delta \tilde{z}_{\alpha-1/2,i}$ is the contribution of the interface collapse/expansion, basically a correction term. Similarly, the grid velocity in the time step can be decomposed as:

$$\sigma_{\alpha-1/2,i} = \frac{\tilde{z}_{\alpha-1/2,i}^{n+1} - z_{\alpha-1/2,i}^n}{\Delta t} = \sigma_{\alpha-1/2,i}^{mov} + \sigma_{\alpha-1/2,i}^{top}$$

with:

$$\sigma_{\alpha-1/2,i}^{mov} = \frac{z_{\alpha-1/2,i}^{n+1} - z_{\alpha-1/2,i}^n}{\Delta t}, \quad \sigma_{\alpha-1/2,i}^{top} = \frac{\Delta \tilde{z}_{\alpha-1/2,i}}{\Delta t}$$

455 In the solution of the multilayer shallow water equations we employ a splitting procedure, where the two aforementioned contributions are treated in two steps. In a first step (grid movement) we solve the multilayer model on a vertical grid where the surface layers adjust locally in order to maintain a positive thickness. In the subsequent step, we locally remove surface fluid boxes with minimal thickness or split fluid boxes that are excessively thick. The evolution of the vertical grid and of the tracer in one time step is shown in Figure 4. The top row shows the case of a layer removal and the bottom row the case of a layer insertion. As a remark, we stress that the above interpretation of the interface displacement, reveals many beneficial aspects with respect to a direct insertion and removal of a layer. Without the grid movement step, it would be more complicated to time step the tracers on a grid with positive layer thickness, with all the related stability issues. In fact in the tracer update (24) the layer thickness at t^{n+1} is needed. One may think to compute the tracer after the insertion/removal operations have been performed (thus having positive layer thickness both at t^n and t^{n+1}), but then the configuration on which the discrete tracer equation is solved is ambiguous and it seems hard to ensure the consistency with the continuity or to verify the tracer constancy property.

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In the following we provide the technical details to realize such adaptation to the free-surface with the z -layers. First we notice that, since the beginning of the simulation, the index of the surface layer may change spatially at the element boundaries. Given the initial free-surface elevation $\zeta^0(\mathbf{x})$, we define a set of active indices and the surface layer index, by element, as:

$$\alpha_{active,K} = \left\{ \alpha \in \alpha_K : Z_{\alpha+1/2} + \epsilon_{top} < \min_{\mathbf{x} \in K} \zeta^0(\mathbf{x}) \right\}, \quad \alpha_{top,K} = \min \alpha_{active,K} \quad (32)$$

470 with $\alpha_K = \{1, \dots, N_{b,K}\}$. Due to the staggering of the grid, it is convenient to define also at each node:

$$\alpha_{active,i} = \left\{ \alpha \in \alpha_i : Z_{\alpha+1/2} + \epsilon_{top} < \zeta_i^0 \right\}, \quad \alpha_{top,i} = \min \alpha_{active,i} \quad (33)$$

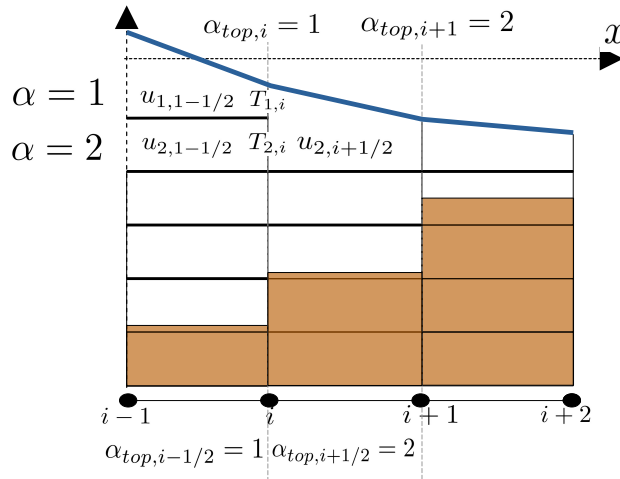


Figure 5. Grid and solution evolution during one time step. The process is interpreted as four stages which bring from [This one-dimensional example](#) shows the pair (U_h^n, ζ_h^n) to $(\tilde{U}_h^{n+1}, \zeta_h^{n+1})$. The vector $U = \{u_1, u_2\}$ collects grid for the layer values of a generic layerwise-scalar variable. Dashed-line means removed interface z -surface-adaptive layers. Left: case of top Elemental surface layer insertion. Right: case of top indices are shown on the bottom, nodal surface layer removal indices are shown on the top.

with $\alpha_i = \{1, \dots, N_{b,i}\}$. The parameter ϵ_{top} is a small positive constant that fixes the minimum allowable depth for a top layer to exist. Below this threshold the layer is removed. We have fixed it as $\epsilon_{top} = 0.2\Delta Z_\alpha$. It turns out that this parameter is quite important since it avoids the presence of very small layers, for which the vertical diffusion matrix becomes ill-conditioned. In
 475 [Figure 5](#) we illustrate the spatial variation of the top layer index for a one-dimensional example.

4.1 Vertical grid movement

We restrict either to explicit or to evolve the discrete multilayer shallow water equations with the semi-implicit time marching schemes that update the free surface from the discrete version of [. Once \$\zeta_h^{n+1}\$ is available \(without loss of generality, we assume that the free surface is updated at nodes \$\zeta_i^{n+1}\$ \), we move finite element method detailed in Section 3. The vertical
 480 vectors/matrices are restricted to the layers with active index. Moreover, to account for the movement of the surface layers with the following steps, the layer thickness is updated as follows:](#)

- Identification of the layers spanned by the free surface, through we identify the indices associated to the layers that, locally, undergo a deformation. They are defined as the layers of the reference grid whose top-interface finds above the free-surface or by the set of indexes: indices:

$$485 \quad \alpha_{mov,i} = \left\{ \alpha \in \alpha_i : \underline{z}^0 Z_{\alpha-1/2} + \epsilon_{mov} > \underline{\zeta}_i^{n+1} \right\} \quad (34)$$

ϵ_{mov} is a small and positive constant that fixes the minimum allowable depth for a layer. we have added. Below this threshold, the vertical grid movement is deployed. ϵ_{mov} can be used to control the number of moving layers. The

490 number of layers contained in the set is $N_{mov,i}$ and the upper-most and bottom-most layers are denoted respectively by $\alpha_{movTop,i} = \min \alpha_{mov,i}$ and $\alpha_{movBot,i} = \max \alpha_{mov,i}$. The depth of the moving layers is:

$$\underline{b_{mov,i} z_{mov,i}} = \max \left(\underline{z_{\alpha_{movBot,i}+1/2} Z_{N_{mov,i}+1/2}}, \underline{-b_i - z_{b,i}} \right)$$

495 – **Computation of the new depth** we compute the new layers thickness after a local grid deformation that absorbs the free surface movement. **We To move the interfaces of the layers contained in the set, we** use the generalized coordinates which, at a discrete level, takes transformation (1) which take the form:

$$z_{\alpha+1/2,i}^{n+1} = \zeta_i^{n+1} i + S_{\alpha+1/2,i} \left(\zeta_i^{n+1} i + \underline{b_{mov,i} z_{mov,i}} \right) \quad (35)$$

this time with S -function $S_{\alpha+1/2}$ such that $S_{\alpha+1/2} = 0 \rightarrow z_{\alpha+1/2} = \zeta_i$ and $S_{\alpha+1/2} = -1 \rightarrow z_{\alpha+1/2} = b_{mov,i}$. With $S_{\alpha+1/2,i} = -\sum_{\beta=\alpha_{top,i}}^{\alpha} l_{\beta,i}$. Then, the nodal layer thickness reads:

$$h_{\alpha,i}^{n+1} = l_{\alpha,i} \left(\zeta_i^{n+1} i + \underline{b_{mov,i} z_{mov,i}} \right), \quad \alpha \in \underline{\alpha_{top,i}, \dots, N_{mov,i}} \quad (36)$$

500 For the proportionality coefficients, we have used a z -star definition $l_{\alpha,i} = \frac{\Delta z_{\alpha}^0}{b_{mov,i}}$ tried different definitions allowing a smooth movement on the interfaces between the time steps, without experiencing any major impact on the results. For simplicity we have thus implemented a z -star definition $l_{\alpha,i} = \frac{\Delta Z_{\alpha}}{z_{mov,i}}$, see Section (2).

505 After the prognostic variables update on the moving grid, i.e. momentum $hu_{\alpha,h}^n \rightarrow hu_{\alpha,h}^{n+1}$ and tracers $t_{\alpha,h}^n \rightarrow t_{\alpha,h}^{n+1}$, this step is completed. Within this update step, This is shown in Figure 4, first and second columns. The new layer thickness is used in the update of the tracers, equation (31). We stress the fact that the vertical configuration is taken constant and equal to α_i^n, α_E^n . The whole step is shown in Figure 4, top-right panel, i.e. the number of layers at each element remain constant during the timestepping of the the discharges and of the tracers.

4.2 Removal/Insertion of top layers

Then we perform the insertion/removal of layers operation based on:

510 – An evaluation of the top layer indexes which become time-dependent. We call them the active ones $\alpha_{active} \subset \alpha$ and they have to be defined at nodes:-

$$\underline{\alpha_{active,i}^{n+1} = \left\{ \alpha : z_{\alpha+1/2}^0 + \epsilon_{top} < \zeta_i^{n+1} \right\}}, \quad \underline{\alpha_{top,i} = \min \alpha_{active,i}}$$

and at elements:-

$$\underline{\alpha_{active,E}^{n+1} = \left\{ \alpha : z_{\alpha+1/2}^0 + \epsilon_{top} < \min_{x \in E} \zeta_h^{n+1}(x) \right\}}, \quad \underline{\alpha_{top,E} = \min \alpha_{active,E}}$$

515 ϵ_{top} is a small and positive constant that fixes the minimum allowable depth for a top layer to exist. Below this threshold, the update of the active layers and of the top layer is too thin and it is removed. It turns out that this parameter is quite important since it avoids the presence of very thin layers, for which the vertical diffusion matrix becomes ill-conditioned. We have fixed it as $\epsilon_{top} = 0.2 \Delta z_{\alpha}^0$. index by re-evaluating (32) and (33) with the new free-surface elevation ζ^{n+1} . We get the new top layer indices $\alpha_{top,K}^{n+1}$ and $\alpha_{top,i}^{n+1}$.

520 – Once we have identified the index that should be inserted/removed in the active set, we proceed with the collapse/expansion of the surface boxes. A conservative remap step is necessary to pass the solution obtained in the grid movement step on a grid with layers α_{active}^n unknowns from the old vertical grid to the new grid with layers α_{active}^{n+1} one.

We use \tilde{u}_{α}^{n+1} the tilde \tilde{T}_{α}^{n+1} to distinguish a generic layerwise layer variable (the tracer in this case) remapped onto the new grid from the solution time stepped on the old grid u_{α}^{n+1} . This insertion/removal operation can be interpreted, at a continuous level, as an expansion/collapse of the layer in a pseudo time (see the bottom-left panel in Figure 4). After the expansion/collapse, the interface location moves to $z_{\alpha+1/2}^{n+1} \rightarrow \tilde{z}_{\alpha+1/2}^{n+1}$. Then, the T_{α}^{n+1} . The remapped value is the solution of the following advection equation in a pseudo time:-

$$\frac{\partial J \tilde{u}_{\alpha}}{\partial \tau} - J \frac{\partial \tilde{u}_{\alpha}}{\partial z} = 0$$

integrated on the layer thickness:

$$530 \quad \frac{\partial \tilde{h}_{\alpha} \tilde{T}_{\alpha}}{\partial t} = \left[\sigma^{top} \tilde{T} \right]_{\alpha+1/2}^{\alpha-1/2} \quad (37)$$

with J the Jacobian of the grid expansion/collapse and $\sigma = \frac{\partial z}{\partial \tau}$ the velocity of the grid. After integration over a layer:-

$$\frac{\partial}{\partial \tau} \int_{\tilde{h}_{\alpha}(\tau)} \tilde{u}_{\alpha} dz = \left[\sigma \tilde{u}_{\alpha} \right]_{\alpha+1/2}^{\alpha-1/2}, \quad \sigma_{\alpha+1/2} = \frac{\partial z_{\alpha+1/2}}{\partial \tau}$$

with an upwind flux:

$$\sigma_{\alpha-1/2}^{top} T_{\alpha-1/2}^{n+1} = \left(\sigma_{\alpha-1/2}^{top} \right)^+ T_{\alpha}^{n+1} + \left(\sigma_{\alpha-1/2}^{top} \right)^- T_{\alpha-1}^{n+1} \quad (38)$$

535 In We consider the discrete case. After integration on the dual cell and with a simple forward Euler time stepping (with initial condition $\tilde{u}_{\alpha}^n = u_{\alpha}^{n+1}$) and upwind flux, we get: T_{α}^{n+1} we have:

$$\tilde{h}_{\alpha,i}^{n+1} \tilde{T}_{\alpha,i}^{n+1} = \tilde{h} u_{\alpha,i}^{n+1} + \Delta \tau t \left(\sigma_{\alpha-1/2,i}^{top} T_{\alpha-1/2,i}^{n+1} \frac{\alpha-1/2}{\alpha+1/2, \alpha-1/2, i} - \sigma_{\alpha+1/2} = \frac{\tilde{z}_{\alpha+1/2}^{n+1} - z_{\alpha+1/2}^{n+1, top}}{\Delta \tau} T_{\alpha+1/2,i}^{n+1} \right) \quad (39)$$

We can apply such a remapping to the variables discretized on the horizontal grid u_h and for element removal/insertion operations with the new nodal layer thickness:

$$540 \quad \tilde{h}_{\alpha,i}^{n+1} = \tilde{z}_{\alpha-1/2,i}^{n+1} - \tilde{z}_{\alpha+1/2,i}^{n+1}$$

In the case of an element removal ($\alpha_{top,E}^{n+1} > \alpha_{top,E}^n \alpha_{top,i}^{n+1} > \alpha_{top,i}^n$), we identify the layer that should disappear and we proceed with a collapse of the lower interface to the upper one. For the existing and removed layer $\alpha = \alpha_{top,i}^n \dots \alpha_{top,i}^{n+1}$, equation the discrete remap (39) with (38) reduces trivially to transfer the depth-integrated variable tracer that belongs to the removed layers to the upper active layer. In the case of an element insertion ($\alpha_{top,E}^{n+1} < \alpha_{top,E}^n \alpha_{top,i}^{n+1} < \alpha_{top,i}^n$), we identify the layer that should appear and we expand the interface. Then equation the remap for $\alpha = \alpha_{top,i}^{n+1} \dots \alpha_{top,i}^n$ reduces to distribute the depth-integrated variable across the existing and inserted layers. The same arguments can be applied to nodal variables, replacing $\alpha_{top,E}$ with $\alpha_{top,i}$, with a weighted average. This is shown in Figure 4, third and fourth columns. All the unknowns must be remapped. For the discharges, that are defined on the elements, (37) should be integrated on the element. This completes the time step.

550 4.3 Connection to z-surface-following coordinates z-star

The vertical coordinate described so far is controlled by the We have a small parameter ϵ_{mov} that prescribes the number of moving surface layers to fix. It is convenient to express this constant as a percentage of the z-layer depth at rest $\epsilon_{mov} = r_{mov} \Delta z_{\alpha}^0$. Due to the presence of the free surface (unknown at the beginning of the simulation) in , it is not easy, even for equispaced z-grid, to find a simple formula that links r_{mov} to the number of moving layers N_{mov} . However, we can compute an estimate of the maximum free surface height during the simulation, $\max \zeta$, and use the relation $r_{\alpha} = \frac{\max \zeta - z_{\alpha}^0 - 1/2}{\Delta z_{\alpha}^0}$ to state that:

- $0 < r_{mov} \ll 1$ means that only the layers spanned by the free surface movement will undergo deformation. As we increase r_{mov} , the deformation becomes less local and more layers are progressively deformed.
- if we set $r_{mov} = r_{N_{mov}}$, we will move, at minimum, N_{mov} layers.
- if we increase the parameter beyond $r_{mov} > r_N$, then all layers are moving.

560 In Figure ?? we have plotted different grids obtained in the vertical movement step with a varying grid parameter r_{mov} and different corresponding moving surface layers N_{mov} .

From top to bottom: different grids obtained in the vertical movement step with different r_{mov} . In red is the highlighted the depth of the moving layers b_{mov} .

The z-surface-adaptive coordinate and the z-surface-following coordinate are then obtained with the following choices:
 565 z-surface-adaptive: $r_{mov} \leq r_{top} \ll 1$ reference layer thickness $\epsilon_{mov} = r_{mov} \Delta Z_{\alpha}$. In order to obtain the z-surface-adaptive grid we have chosen $r_{mov} \leq r_{top}$, in practice we have set $r_{mov} = 0.15$. The grid deformation is localized to the free surface. As long as elements the surface fluid boxes are deformed, they are recognized as too small and immediately removed in the grid topology step. This implies working, at the next time step, with a true z-grid. We stress the importance of the grid movement step. Without such a step, it would be impossible to timestep the variables on layers with positive depth, with all the related stability issues, included for the tracer equation where you need layer thickness at t^n and t^{n+1} . One may think to compute the tracer after the insertion/removal operations have been performed (thus having positive layer thickness both at t^n and t^{n+1}), but in this way the configuration on which the discrete tracer equation is solved is ambiguous (it is the old one, the new one?) and it seems hard to verify tracer constancy property. z-layers having all the interfaces aligned to the geopotentials.

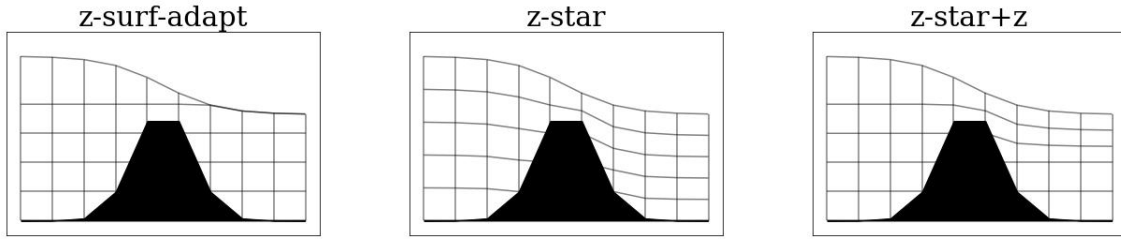


Figure 6. The different vertical z-grids outlined in Section 4.3.

Interestingly we can obtain other grids by increasing r_{mov} . We define:

$$575 \quad R_\alpha = \frac{\zeta_{max} - Z_{\alpha-1/2}}{\Delta Z_\alpha} \quad (40)$$

with $\zeta_{max} = \max_{x,t} \zeta(x,t)$ an estimate of the maximum free surface height during the simulation. We get:

- z-star: $r_{mov} > r_N$ z-star if $r_{mov} \geq R_N$ and no insertion/removal. The whole water column is subjected to the grid movement while the number of layers does not change. These are z-star z-star coordinates, or any z-surface-following z-surface-following coordinates depending on which coefficients $l_{\alpha,i}$ are plugged in equation (36).
- 580 - z-star z-star+z: $r_\gamma = \frac{\max \zeta - z_{\gamma-1/2}^0}{\Delta z_\gamma^0}$ and z if $r_{mov} = R_M$ and no insertion/removal. The upper part of the water column, at minimum γM layers, is subjected to the grid movement while the lower part is fixed. This corresponds to a partially z-star and partially z-system.

Figure 6 shows a sketch of the different possibilities. Tuning properly r_{mov} we will compare the newly developed z-surface adaptive layers against z-star.

585 5 Advection with spatially variable number of layers

We have used an approach where the grid topology does not change during the time step of the conserved variables, i.e. the scheme-numerical scheme of Section 3 works on the deforming grid of Section 4.1, with a *temporally* constant number of layers between t^n and t^{n+1} . However, in the previous time step, a layer insertion/removal may occur (to remove very thin surface layers, or to split a thicker layer) on a certain element and not on its neighbors. This results in a grid-vertical discretization
 590 with a *spatially* variable number of layers. Hanging interfaces appear for the top layers, see the top-left panel of Figure. Some modifications have to be implemented to deal properly with such hanging interfaces, see Figure 7, which slightly complicate the treatment of advection terms, see on this topic Bonaventura et al. (2018).

Consider the one dimensional example in Figure 7, where two contiguous elements with different top-layer index $\alpha_{top,i+1/2} > \alpha_{top,i-1/2}$ exist. In correspondence with node i a change of the element top layer index takes place. Borrowing the vocabulary

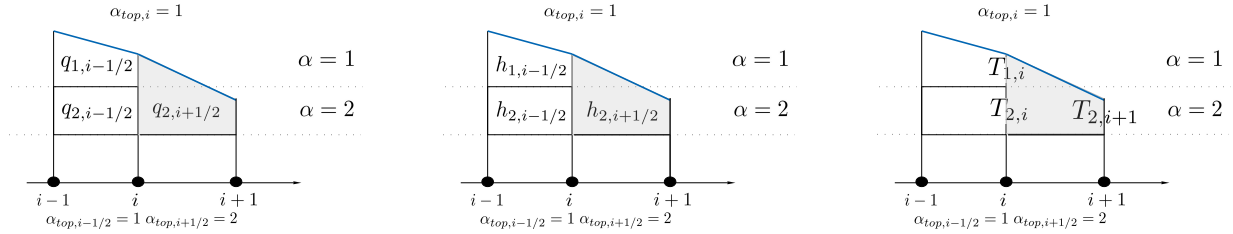


Figure 7. Treatment of non-conformal box for the one-dimensional case. Top left: non-conformal box. Top right: splitting with fictitious layers. Bottom left: mass-transfer function $G_{T+1/2,i}$ at hanging node is represented by a red arrow in grey. Bottom right: horizontal advection terms $f_{2,i}, f_{2,i+1}$ and $f_{1,i}, f_{1,i+1}$ computed for each fictitious layer thickness and tracers are represented by red arrows shown.

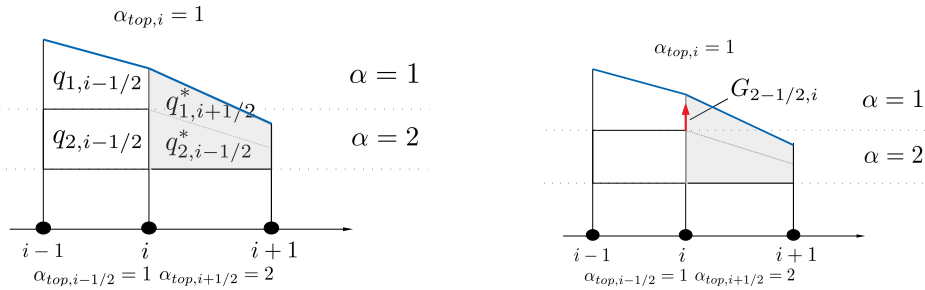


Figure 8. Treatment of non-conformal box for the one-dimensional case. Left: splitting with fictitious layers. Right: the mass-transfer function $G_{1+1/2,i}$ at hanging point is represented by a red arrow.

595 from the literature on non conformal meshes, we have a non-conformal-vertical edge with two hanging-layers which slightly
sophisticate the treatment of advection terms a hanging point. We call hanging layer, a layer for which at least one interface
ends with a hanging point. The boxes that have vertical edges across which the element top-layer index varies, deserve a special
treatment. In our case, with only insertion/removal of surface layers, we can easily flag boxes that deserve a special treatment
such boxes by checking, for each element, that the nodal top layer index is different from the elemental one. The elements of
600 the grid with a non-conformal surface box are indicated by an asterisk:

$$\text{if } \alpha_{\min,E} < \alpha_{\text{top},E} \text{ then } EK = E^*K^*$$

with $\alpha_{\min,E} = \min_{j \in E} \alpha_{\text{top},j}$ with $\alpha_{\min,K} = \min_{j \in K} \alpha_{\text{top},j}$. Then the boxes called hereinafter for simplicity "non-conformal"
can be identified by the pair of index $(\alpha_{\text{top},E}, E^*)$. Since horizontal and vertical advection terms/indices $(\alpha_{\text{top},K}, K^*)$. Since
both mass and tracer fluxes need communication with the neighbors' boxes, they have to be treated differently.

605 Moreover, for the tracer discrete update, we have to take care of preserving the constancy property. **The key ingredient**
to verify tracer constancy for a hydrostatic numerical model is that the tracer discrete update, in case of a constant solution,
collapses to the discrete layerwise mass conservation. The last is always verified because it is used to compute the mass-transfer
function. Assuming that the time derivative and the vertical advection terms in and are treated equally, it is enough to
verify that the horizontal advection term reduces to the mass flux term, also for non-conformal boxes. However, the practical
610 implementation depends on the specific numerical scheme. In the next paragraph, we show the case of a B-type staggered finite
element discretization as the one used in the SHYFEM model.

5.1 Case of staggered Finite Element on a B-grid

We consider a discretization where the water levels and the momenta (transports) are described using form functions of different
order and support. Momentum is approximated through:-

$$615 \quad hu_{\alpha,h}(x,t) = \sum_{E=1,M} \psi_E(x) hu_{\alpha,E}(t)$$

with $\psi_E(x) \in E$ the constant piecewise functions and $hu_{\alpha,E}(t)$ the elemental momentum. The elemental currents are obtained
from $u_{\alpha,E} = \frac{hu_{\alpha,E}}{h_{\alpha,E}}$. For the free surface, given an approximation of nodal values $\zeta_i(t) = \zeta(x_i, t)$, we introduce a continuous
numerical approximation:-

$$\zeta_h(x,t) = \sum_{i=1,M+1} \varphi_i(x) \zeta_i(t)$$

620 $\{\varphi_i\}_{i=1,M+1}$ is the standard P^1 continuous piecewise linear Lagrange kernel. Tracers are approximated with the same formula
: $t_{\alpha,h}(x,t) = \sum_{i=1,M+1} \varphi_i(x) t_{\alpha,i}(t)$. A sketch of the vertical grid is reported in Figure .-

Sketch of the staggered grid with elemental velocities and nodal tracers values.

We obtain the weak formulation multiplying the governing equation by a test function that belongs to the same space of
the solution and integrating it in the computational domain. Then, the finite element discretization of the mass flux term in the
625 layerwise mass equation is computed, for each element, after integration by part:-

$$\int_{\Delta x_{i+1/2}} \frac{\partial \varphi_i}{\partial x} hu_{\alpha,h} dx = a_{i,i+1/2} hu_{\alpha,i+1/2}$$

with the coefficient:-

$$a_{i,i+1/2} = \int_{\Delta x_{i+1/2}} \frac{\partial \varphi_i}{\partial x} dx$$

For the computation of horizontal advection we consider the tracer equation. The elemental contribution to the advection term

630 reads, after integration by parts:-

$$\int_{\Delta x_{i+1/2}} \frac{\partial \varphi_i}{\partial x} h u_{\alpha,h} t_{\alpha,h} dx = \sum_{j=i,i+1} k_{\alpha,ij} t_{\alpha j} = f_{\alpha i}^{i+1/2}$$

with the coefficient:-

$$k_{\alpha,ij} = \int_{\Delta x_{i+1/2}} \frac{\partial \varphi_i}{\partial x} \varphi_j dx h u_{\alpha,i+1/2}$$

We consider any P^1 stabilized method written in the form (neglecting the subscript α in the matrix entries):-

635
$$f_{\alpha i}^{i+1/2} = \sum_{j=i,i+1} (k_{ij} + d_{ij}) t_{\alpha j}$$

with d_{ij} a consistent discrete stabilization operator which has to be symmetric with zero row sum $\sum_{j=i,i+1} d_{ij} = -d_{ii}$ (Kuzmin and Turek, 2002). For instance, d_{ij} can be the discrete Laplacian, the streamline diffusion operator or, as in SHYFEM model, a first-order upwind dissipation plus a second-order TVD correction tuned by a flux limiter, see always Kuzmin and Turek (2002)

640 In case of a non-conformal box we proceed as follows. First, we split the box vertically in $\alpha_{top,E} - \alpha_{min,E} + 1$ fictitious layers through planar interfaces passing through the hanging points of non-conformal edges and some fraction of the conformal edge length, see Figure 8, top right panel. From this geometrical configuration we compute the element layers thickness $h_{\alpha,K}^*$ for the fictitious layers. Then we distribute the momentum discharge of the top layer among the fictitious layers:- for $\alpha = \alpha_{min,K}, \dots, \alpha_{top,K}$:

645
$$h u_{\alpha,E}^* q_{\alpha,K}^* = h u_{\alpha_{top,E}} l_{\alpha,E}^* \alpha = \alpha_{top,E}, \dots, \alpha_{min,E} q_{\alpha_{top,K},K}^* \quad (41)$$

with $l_{\alpha,E}^* = \frac{h_{\alpha,E}^*}{h_{\alpha_{top,E}}}$ and $h_{\alpha,E}^*$ the fictitious layer thickness. Finally, these with $l_{\alpha,K}^* = \frac{h_{\alpha,K}^*}{h_{\alpha_{top,K}}}$. These values are used to complete both vertical and horizontal advection mass and tracer fluxes for the missing layers of non-conformal boxes (see Figure ??, bottom panels). Without loss of generality, we consider the case of node i sharing a non conformal right box $(i+1/2, \alpha_{top,i+1/2})$, as box $(\alpha_{top,K}, K)$ with node $i \in K$, as illustrated in one dimension in Figure 7. After the splitting (41),

650 the mass-flux term reads: (only the x -component shown) reads, for $\alpha = \alpha_{top,i}, \dots, \alpha_{top,K}$:

$$\int_{\Delta x_{i+1/2,K}} \frac{\partial \varphi_i}{\partial x} h u_{\alpha,h}^* dx q_{\alpha}^* dx = a_{iK} c_{\alpha,i}^* a_{i,i+1/2} h u_{\alpha_{top,i+1/2,i+1/2}} \alpha_{top,i+1/2} q_{\alpha_{top,K},K}^* \quad (42)$$

withwith:

$$c_{\alpha,i}^* = \begin{cases} \sum_{\beta=\alpha_{top,i}}^{\alpha_{min,K}} l_{\beta,K}^* & \text{if } \alpha = \alpha_{top,i} \text{ and } \alpha_{min,K} < \alpha_{top,i} \\ l_{\alpha,K}^* & \text{otherwise (hanging layer)} \end{cases} \quad (43)$$

where the two cases account for the contribution of element $i+1/2$ to both nodes with and K to nodes with or without hanging layers, respectively node i and $i+1$ in Figure 8. Such contribution from the non-conformal box is added to the mass-flux term in the layerwise mass equation. It allows to compute the mass-transfer function at the hanging points $G_{\alpha-1/2,i}^{n+1}$ for $\alpha = \alpha_{top,i}, \dots, \alpha_{top,K}$ as shown in Figure 8, right panel. One can check that this treatment is mass-conserving. Summing the mass-transfer function for all the layers, even in presence of non-conformal boxes, still yields to the discrete mass equation (27).

The horizontal advection scheme (29) on the non-conformal box can be applied straightforwardly to the fictitious layers with modified coefficients $k_{\alpha,i,j} = l_{\alpha,i+1/2}^* k_{\alpha_{top,i+1/2},ij}$. Then, the advection term numerical flux in non-conformal boxes reads (neglecting for simplicity the stabilization operator):

$$f_{\alpha,i}^{*i+1/2} = \begin{cases} \sum_{\beta=\alpha_{top,i}}^{\alpha_{min,i+1/2}} \sum_{j=i,i+1} l_{\beta,i+1/2}^* k_{\alpha_{top,i+1/2},ij} t_{\beta^*,j} & \text{if } \alpha = \alpha_{top,i} \text{ and } \alpha_{min,i+1/2} < \alpha_{top,i} \\ \sum_{j=i,i+1} l_{\alpha,i+1/2}^* k_{\alpha_{top,i+1/2},ij} t_{\alpha^*,j} & \text{otherwise (hanging layer)} \end{cases}$$

for $\alpha = \alpha_{top,i}, \dots, \alpha_{top,K}$:

$$\hat{H}_{\alpha} \equiv \begin{cases} \sum_{\beta=\alpha_{top,i}}^{\alpha_{min,K}} l_{\beta,K}^* \hat{H}_{\alpha_{top,K}}(T_{\beta^*,i}, T_{\beta^*,j}) & \text{if } \alpha = \alpha_{top,i} \text{ and } \alpha_{min,K} < \alpha_{top,i} \\ l_{\alpha,K}^* \hat{H}_{\alpha_{top,K}}(T_{\alpha^*,i}, T_{\alpha^*,j}) & \text{otherwise (hanging layer)} \end{cases} \quad (44)$$

Again we have separated the cases of a node with α without hanging layers. Note that the subscript $(\alpha^*, j) = (\max(\alpha, \alpha_{top,j}), j)$ $\alpha^* = \max(\alpha, \alpha_{top,i})$ avoids selecting tracer values in removed layers. The splitting of non-conformal boxes and the consequent treatment of advection terms for such boxes allows simple verification of the tracer constancy also in presence of a spatially variable number of layers. We have already mentioned that it is enough to verify that the horizontal advection term. In the Appendix we show that, when a constant tracer is imposed, the horizontal tracer flux reduces to the mass-flux term, also for non-conformal boxes. We can verify this property by element. For a constant tracer ($t_{\alpha} = 1$), we write the advection term for a mass flux even in the case of a non-conformal box as:

$$f_{\alpha,i}^{*i+1/2} = \begin{cases} \sum_{\beta=\alpha_{top,i}}^{\alpha_{min,i+1/2}} l_{\beta,i+1/2}^* \sum_{j=i,i+1} k_{\alpha_{top,i+1/2},ij} & \text{if } \alpha = \alpha_{top,i} \text{ and } \alpha_{min,i+1/2} < \alpha_{top,i} \\ l_{\alpha,i+1/2}^* \sum_{j=i,i+1} k_{\alpha_{top,i+1/2},ij} & \text{otherwise} \end{cases}$$

Through the definitions and , it can be simplified to : α .

6 Numerical tests

The tests have been run with implicitness parameters $\theta_z = \theta_m = 0.5$. We will check discrete mass-conservation at t^{n+1} by computing the following relative volume error for the dual cell area, which results from the sum of (28) from N_i to $\alpha_{top,i}$:

$$f_{\alpha,i}^{*i+1/2} e_i^{n+1} = c_{\alpha,i}^* \Delta t \left| \sum_{j=i,i+1} k_{\alpha_{top,i+1/2},j} \frac{\alpha_{top,i}}{\alpha=N_i} |C_{\alpha,i}| G_{\alpha-1/2,i}^{n+1} \right|, \quad e_i^{n+1} = c_{\alpha,i}^* a_{i,i+1/2} h u_{\alpha_{top,i+1/2},i+1/2} \max_{i \in \mathcal{T}} \left(\frac{e_i^{n+1}}{\sum_{\alpha=N_i}^{\alpha_{top,i}} |C_{\alpha,i}| \Delta h_{\alpha}} \right)$$

680 which is the discrete mass-flux for non-conformal box. This completes To quantify the tracer constancy verification error, we use the L^1 -norm:

$$e_{\alpha,i}^{n+1} = |T_{\alpha,i}^{n+1} - T_0|, \quad e^{n+1} = \frac{\sum_{\alpha,i} |C_{\alpha,i}| h_{\alpha,i}^{n+1} |T_{\alpha,i}^{n+1} - T_0|}{\sum_{\alpha,i} |C_{\alpha,i}| h_{\alpha,i}^{n+1} T_0}$$

with T_0 the initial tracer value.

7 Numerical tests

685 All the tests have been run with the ocean model SHYFEM which is based on the Finite Element procedure of Section ?? applied to unstructured triangular grids. The extension of the z -surface-adaptive algorithm to unstructured grids is straightforward. In particular, nodal definitions apply identically and elemental definitions apply to triangular elements K . SHYFEM uses a semi-implicit method to march variables in time. In the next paragraphs, we check the accuracy and conservation properties of the z with insertion/removal and then we compare it against z -star for a realistic environment.

6.1 Impulsive Wave

690 As the first test, we check the accuracy of the z -surface-adaptive coordinate z -surface-adaptive layers with an increasing vertical resolution. We use a closed basin $[-5,5] \times [-5,5] \times [-5\text{ m}, 5\text{ m}] \times [-5\text{ m}, 5\text{ m}]$ with constant depth $b = 1\text{ m}$. The basin is initially at rest and the free surface is perturbed by the following Gaussian hump:

$$\zeta(\underline{x}, \underline{y}, t = 0) = A \exp(-r^2/\tau)$$

695 with $A = 1/2$, $\tau = 1/2$, $A = 0.5\text{ m}$, $\tau = 0.5\text{ m}^2$ and $r = \sqrt{x^2 + y^2}$. A constant passive tracer is prescribed on the background and such a constant state should be preserved along the simulation. The mesh has a uniform horizontal element size of $h_K = 0.25\text{ m}$. We compare different vertical resolutions with variable layer thicknesses layers thickness. The coarsest grid has three layers: a first top layer with thickness of $\Delta z_1 = 0.2\text{ m}$, the second and the third layers have thicknesses of $\Delta z_{2,3} = 0.4\text{ m}$. The other vertical grids are obtained by halving each of these layers. The finest grid has 24 layers with minimum layer thickness at the surface of $\Delta z = 0.025\text{ m}$.

700 Without bottom/surface forcing, if the initial ~~currents are constant along z~~velocities are constant over the layers, they must remain barotropic and equal to the depth-integrated ~~currents of the Shallow Water~~velocities of the shallow water equations (1-layer case). Of course, this is not a property of the ~~discrete z-coordinate scheme~~z-layers (but the scheme should converge to a barotropic solution refining the resolution). It is however desirable that the results of 2d and 3d models are similar for the typical resolution of an ocean simulation (Kleptsova et al., 2010). The 1-layer discrete solution is considered here as a reference solution against which we compare our implementation of the ~~z-layers~~z-layers. The coarse grid with 3-layer is also used for comparison since the free surface is ~~always~~ contained in the first layer and no insertion/removal is necessary. For the 24-layer grid, up to six layers are progressively removed (and then re-inserted). In Figure ??, all resolutions show a good agreement for both the water level and the barotropic ~~current~~velocity. We can check some conservation properties of the scheme. As usual for such an adaptation strategy, mass is conserved up to machine precision (SHYFEM is coded in single-precision). This is what we check in Figure ??, left panel, ~~where no~~. With the exception of a small additional noise associated to the insertion/removal operations, no significant source of mass error is present with respect to the 3-layer case. ~~A direct consequence of mass conservation is tracer constancy~~preservation. Tracer constancy, as expected, is also preserved up to machine precision, ~~Figure see Figure ??~~, right panel.

6.2 1-d tidal flow in a sloping channel

715 Coastal applications include extensive intertidal flats. As with many ocean models, SHYFEM handles wetting and drying processes in a simplified manner, applying ad-hoc treatments in dry cells. An extrapolation algorithm for the free surface is used to track the shoreline and identify dry and wet regions. Then, the two regions are treated separately, see Umgiesser (2022) for the details. The test that we propose, presented in Oey (2005), is a benchmark for wetting/drying algorithms used in ocean models. The domain consists of a 1d sloping channel that ranges from ~~$x = 0 \text{ km}$~~ $x = 0$ at the landward end to ~~$x = 25 \text{ km}$~~ $x = L$ at the seaward boundary. ~~The slope of the bathymetry is $b(x) = 10x/(25 \text{ km})$~~ , with $L = 25 \text{ km}$. The bathymetry is represented by the following function $z_b(x) = -H_0/Lx$ and $H_0 = 10 \text{ m}$. The horizontal ~~mesh size is~~element size is uniform and equal to $h_K = 250 \text{ m}$. A periodic water level is imposed at the seaward boundary ~~$\zeta = 10(1 - \sin(10\pi t))$~~ as $\zeta(t) = A(1 - \sin(\frac{2\pi t}{T}))$ with amplitude $A = 10 \text{ m}$, period $T = 1 \text{ day}$ and the time t ranging from 0 to 0.5 day. At the beginning of the simulation, the channel is dry. Typically this test is run with 1-layer models (Warner et al., 2013). Here we use the 1-layer solution (1L) as a reference and we test the 5-layer with surface-adaptation and the 5-layer with ~~z-star~~z-star. In the 5L ~~z-surface-adaptive~~z-surface-adaptive simulation, only one layer is present at the beginning of the simulation and then, as long as the free surface is tilted by the boundary signal, more levels are inserted and then removed during the drying phase. Flooding is thus performed with a 1-layer ~~Shallow Water~~shallow water model with the classical wetting/drying algorithms that may be deployed in dry or nearly dry areas (e.g. positivity limitation, ~~momentum discharge~~ regularization, etc...). With ~~z-star~~z-star instead, such wetting and drying algorithms are applied to all layers.

730 In Figure ?? we check the along-channel solution profiles. Despite the different manner of handling wetting/drying for the 5L ~~z-surface-adaptive~~z-surface-adaptive and 5L ~~z-star~~z-star simulations, a quite good agreement is observed for the free surface, while larger differences are found for the barotropic ~~current~~velocity where both the 5-layers simulations appear

noisier at the wet/dry interface. In Figure ??, left panel, we check volume conservation for this case which involves an uneven bathymetry and wetting/drying. Although in correspondence of wet/dry nodes the relative volume error is much larger, we can verify that the z -surface adaptive has the same level of relative error of z -star, which we accept to be within the round off errors. The same argument applies to the error for the tracer constancy.

6.3 Venice Lagoon-Po delta idealized test

Here we test the different z -coordinates- z -layers in a realistic lagoon-coastal environment forced by the tidal oscillation. The Venice Lagoon is characterized by a complex system of shallow areas subjected to wet-dry processes (the average basin depth is of the order of 1 m) and deeper channels (maximum depth around 15 m). We simulate a summer period when the strong diurnal heating sums up river runoff and make the lagoon less dense than the sea water entering from the inlets. The flow is mainly driven by the tidal currents that transport water masses with different densities along the lagoon channels. The deeper channels can experience surface stratification during summer. In this test, the lagoon is forced with analytical functions representative of a calm summer period characterized by strong solar radiation: the Po delta. We study both the river plume and the penetration of the salt water into the river branches. The numerical reproduction of such phenomena for numerical models is a very delicate issue. Specifically, spurious numerical mixing related to the horizontal and vertical numerical fluxes, the vertical grid and the time-stepping can destroy stratification and frontal characteristics, potentially modifying the plume dynamics (Fofonova et al., 2021). In this discussion we solely focus on the impact of the vertical discretization: the resolution at the surface and the comparison between the z -surface adaptive with fixed interfaces and z -star with moving interfaces.

The vertical eddy viscosity μ_{τ} and the vertical tracer eddy diffusivity $\mu_{\tau\tau}$ are computed with the turbulence module GOTM (Buchard et al. 2015). At the inlets, the lagoon. The bottom friction is fixed to $C_F = 0.002$. Because of their fundamental role in the plume dynamics, two more terms have been added to the multilayer shallow water model of Section 2: the Coriolis force which is timestepped with an implicitness parameter of 0.5 and an horizontal diffusion term for the salinity equation, treated explicitly. The horizontal viscosity is taken as the Smagorinsky eddy viscosity. The sea boundary is forced with a semi-diurnal tidal signal with amplitude 0.4 m and period 12 hours, sea water at $T = 25^\circ\text{C}$ and $S = 35$ PSU. The salinity at the sea boundary is constant and fixed to 38 PSU. A weak freshwater flow with a discharge of 500 m^3 , which is characteristic of the summer season, is enforced at the Pontelagoscuro river boundary. The lagoon is initialized with constant temperature $T = 25^\circ\text{C}$ and salinity $S = 30$ PSU a salinity equal to the boundary value of 38 PSU. The simulation lasts ten days one month, after which the salinity shows a periodic behaviour modulated by the tidal cycle.

A coarse horizontal grid made out of 7842 triangular elements and 4359 nodes is used. This grid however is capable of representing the main channels and islands where smaller elements are placed (Figure ??). The computational domain encompasses the entire river network of the delta, stretching from Pontelagoscuro to the sea, including all delta lagoons, as well as a portion of the adjacent shelf sea (Bellafore et al., 2021). Horizontal resolution ranges from $h_K = 2\text{ km}$ at the sea boundary, to around $h_K = 100\text{ m}$ in the inner shelf close to the lagoons and river branches, and to around $h_K = 50\text{ m}$ in the inner delta system. The horizontal grid, composed of 38884 nodes and 69364 elements, is in Figure ?. We consider two vertical resolutions summarized in Table ??, one with $N = 24$ layers and one with $N = 27$ layers. The deeper part (from the bottom to

~~-2m from the reference level ($Z = -1\text{ m}$) is equal for the two z -grids and it is composed of 16-23 levels with variable thicknesses, going from $\Delta z = 0.5\text{ m}$ near the surface up to $\Delta z = 4\text{ m}$ at 40 m . $\Delta Z_N = 4\text{ m}$ for the last layer. The resolution of the upper part of the water column differs: the coarse grid has the first layer of $\Delta z_1 = 1\text{ m}$ followed by two layers with a thickness of $\Delta z = 0.5\text{ m}$ one layer with $\Delta Z_1 = 1\text{ m}$. This choice avoids the drying of the first layer. In the fine grid, in the upper part, the fine grid has 8 layers with a constant thickness of $\Delta z = 0.25\text{ m}$ has 4 layers with constant thickness, $\Delta Z_1 = \Delta Z_2 = \Delta Z_3 = \Delta Z_4 = 0.25\text{ m}$. Three simulations have been performed: a coarse one with standard z -coordinate (19L- z -layers (24L- z), a fine one with z -surface-adaptive coordinate (24L- z -surf-adapt z -surface-adaptive layers (27L- z -surf-adapt) and a fine one with z -star (24L- z -star)- z -star (27L- z -star).~~

Given the fine vertical resolution and the tidal amplitude of 0.4 m , the 24L- z -surf-adapt 27L- z -surf-adapt simulation should undergo extensive element insertion/removal of the surface fluid boxes. In the right picture of Figure ??-?? we have reported the time evolution of the number of elements-boxes inserted and removed during two tidal periods. More than 150 surface elements Almost 4000 surface boxes happened to be inserted or removed in a single time step. As it is customary we have reported mass conservation and tracer constancy error in Figure ??. These figures are referred to a shorter simulation that lasted 4 days with a constant salinity obtained by imposing the river salinity equal to the interior one. In Figure ??, we show the free surface and the barotropic velocity recorded at two stations, at "Punta della Salute" in Venice, quite close to the northern inlet and at "Canale dei Petroli" placed in the deep tanker ship channel, (named respectively G2 and G8 in Figure ??). The signals of the three simulations are almost overlapping with small differences in the velocities.

Always To diagnose the river plume we look to the minimum surface salinity during the simulation. From Figure ??, it is clear that both the fine grids simulations allow a stronger gravitational circulation with a more extended freshwater plume. Also, the opposite bottom circulation penetrates more upstream, with stronger salinity recorded at the stations G2 and G8 we show the velocity and tracer profiles. At the station G2, G5, as shown in Figure ??, the tracer profile is mostly well-mixed. At station G8, in Figure ??, we observe that the ebb phase is followed by a stratification of the water column which is then erased after the flood phase. First, we note that the vertical resolution seems to strongly affect the tracer evolution. Although the coarse and fine simulations show similar periodic profiles, ?? To inspect the extension of the saltwater intrusion we have extracted a section of the salinity field in the Pila branch when saltwater reaches the maximum extent, during a flood tide. This is shown in Figure ??. The higher resolution at the surface allows to capture also some small scale internal structure which are present under the surface. Differently from the previous test, the 19L- z simulation shows significantly lower temperatures. For the temperature, we believe this is due to the different mechanisms of heating and cooling. Heating is mainly associated with the incoming short-wave solar radiation which acts as a body force for the upper water column. On the contrary heat loss through latent and sensitive heat flux occurs via a boundary condition (in a layerwise model, a source term for the first layer only). Thus the first layer thickness strongly impacts the temperature evolution, in particular in our case a thinner layer causes a more rapid cooling during the night, which leads the lagoon to a colder state. Second, comparing the two fine simulations (24L- z -surf-adapt and 24L- z -star), we found that they are in close agreement which seems to confirm the analysis of Section 2 (see also the Appendix): for micro-tidal applications and fine vertical resolutions, the mixing related to the free surface oscillation is small. differences between the z -surface adaptive and z -star grids are clearly visible. The z -surface

adaptive simulation exhibits a stronger plume and a more extended salt wedge as well as a more sharper surface structure.

A possible explanation could be related to the fact that, due to the strong internal motion, the vertical velocity is not in phase with the time

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All the tests have been accomplished with a serial run. We report the CPU time of the ~~three~~ serial simulations which have been run on a modern workstation with a AMD EPYC 7643 Processor : ~~7099 s (19L-z), 12227-2073005 s (24L z-star), 13261-z-star), 1998969 s (24L z-surf-adaptz-surf-adapt)~~ showing an overhead of around ~~83.6%~~ for the insertion/removal operations. Although we have not covered parallel implementation aspects, we mention that the algorithm (grid movement,
810 insertion/removal) mainly operates on the vertical grid, and the parallel execution of these tasks should not encounter any issues. The stencil of the numerical scheme is not enlarged with respect to the standard method. However some variables have been introduced only for the insertion/removal operations. This is the case of the nodal top layer index which must be exchanged between the domains.

7 Conclusions

815 In this work, we have ~~reviewed~~ studied the performances of ~~geo-potential-coordinates-multilayer shallow water models based on z-layers~~ for the simulation of free surface coastal flows. We have investigated a well-known issue of ~~geo-potential-coordinates z-layers~~ when incorporating the free surface: the limitation on the resolution of the surface layer thickness. We have proposed a flexible algorithm based on a vertical adaptation to the tidal oscillation called ~~z-surface-adaptive~~ z-surface-adaptive. With a dynamic insertion and removal of surface layers, the grid (at least the internal interfaces) is ~~always aligned to geo-potential aligned~~
820 to geopotential, canceling the pressure gradient error. Thanks to a two-step procedure (vertical grid movement of surface layers followed by the insertion/removal operations), ~~this algorithm preserves the stability and conservation property of the numerical scheme~~ we have been able to evolve the multilayer model on a grid with a temporally constant number of layers in the time step which allowed a simple implementation. Moreover this leads to a consistency, at a discrete level, of the tracer equation with the continuity equation as well as to a simple verification of mass-conservation. As a particular case, the algorithm can be
825 ~~reverted to z-surface-following coordinates, such as the popular z-star~~ reduced to the popular z-star.

Without the limitation on the surface resolution, we have been able to compare the ~~z-coordinate~~ z-layers with insertion/removal (surface-adaptive) against ~~z-star~~ z-star for typical coastal applications of semi-enclosed shallow seas with a tidal signal imposed at the openings and wetting/drying at intertidal flats. The comparison has been carried out with ~~numerical experiments idealized and realistic numerical experiments.~~ We shows that z-surface-adaptive layers can be used to simulate wetting and
830 drying and without a significant loss of accuracy with respect to z-star. We found that z-layers and simple analysis. In particular, using a local truncation error analysis we have investigated the additional numerical mixing associated with z-coordinates with the free surface. The analysis shows that , for high tidal ranges, the z-coordinate may suffer from spurious mixing or even from over-compressive effects, depending on the resolution and the flux limiter. However, as to be expected intuitively z-star exhibit differences when simulating large, low frequency internal motions combined with a barotropic tide, such as the gravitational
835 circulation in the Po Delta. These differences deserve further attention. We speculate that for such cases, keeping z-layers may

be convenient to reduce truncation errors in the computation of both the internal pressure gradient term and of the vertical advections terms.

840 We conclude mentioning that the overhead related to insertion/removal operation should be further assessed in realistic applications. With the actual implementation of the z -surface adaptive layers, we have found that, for micro-tidal ranges and typical vertical resolutions of coastal models, these errors are small. In such conditions, with a simulation of the Venice Lagoon circulation, we shows that surface-adaptive z coordinates can be used without a significant loss of accuracy.

experienced some stability issue in the computation of the tracers. This occurred for non-conformal boxes undergoing wetting/drying and it is under current investigation. We are trying a simpler treatment of the non-conformal surface boxes as in Bonaventura et al. (2018).

845 *Code and data availability.* The SHYFEM hydrodynamic model is open source (GNU General Public License as published by the Free Software Foundation) and freely available through GitHub at <https://github.com/SHYFEM-model>. The current developments have been implemented in a branch of the SHYFEM code that can be accessed from Zenodo (Arpaia, 2023, <https://doi.org/10.5281/zenodo.8147444>). Configuration files and data used to run each test case are also available at the same Zenodo repository.

Appendix A: Numerical mixing induced by a tidal flow Tracer constancy

850 ~~We derive a closed-form expression for the numerical mixing of z -coordinate layerwise models when large vertical velocities associated with tidal flows are present (Klingbeil et al., 2018). To simplify the analysis we assume the case of a passive tracer advected by a barotropic linearized flow with water depth $H(x,t)$ and barotropic velocity $u(x,t)$. We note that, for surface-following coordinates, the mass-transfer function is zero (because of $h_\alpha = l_\alpha H$). The layers are thus aligned along the materials and the tracer is just advected along a layer without any discretization error arising from the vertical approximation.~~

855 ~~For this reason, hereinafter in the section, we take the z -star coordinate as the reference solution. On the contrary for z -coordinate models, the mass-transfer is the vertical velocity, a linear function of depth:-~~

$$G_{\alpha-1/2} = -w_{\alpha-1/2} = \frac{\partial u}{\partial x} \sum_{\beta=N}^{\alpha} h_\beta$$

~~Then, the vertical advection fluxes will trigger some numerical noise (diffusion or dispersion). For a linearized barotropic flow, we can use the mass equation $\partial_t \zeta + H_0 \partial_x u = 0$ to replace:-~~

860
$$\left| \frac{\partial u}{\partial x} \right| = \frac{1}{H_0} \left| \frac{\partial \zeta}{\partial t} \right| \leq \frac{A\Omega}{H_0}$$

We start with the case without non-conformal boxes. We impose a constant tracer vector $T_i = \mathbf{1}$ in the discrete tracer equation (31). Each row reduces to:

$$\underline{|C_{\alpha,i}| h_{\alpha,i}^{n+1}} \cong \underline{|C_{\alpha,i}| h_{\alpha,i}^n + \Delta t f_{\alpha,i}^n}$$

with A the tidal amplitude, $\Omega = 2\pi/T$, T the tidal period and H_0 the bottom depth.

865 The exact solution satisfies the layer-averaged continuous conservation law:-

$$\frac{\partial t_\alpha^{ex}}{\partial t} \Big|_s + \frac{\partial ut_\alpha^{ex}}{\partial x} + \frac{\partial wt_\alpha^{ex}}{\partial z} = 0$$

with

$$f_{\alpha,i}^n = - \sum_{K \in \mathcal{D}_{\alpha i}} \sum_{j \in K, j \neq i} \hat{H}_\alpha(1,1) + \left(|C_{\alpha,i}| G_{\alpha-1/2,i}^{n+1} - |C_{\alpha+1,i}| G_{\alpha+1/2,i}^{n+1} \right)$$

870 where $t_\alpha^{ex} = \overline{t^{ex}}$ and the average operator is $\overline{(\cdot)} = h_\alpha^{-1} \int_{z_{\alpha+1/2}}^{z_{\alpha-1/2}} (\cdot) dz$. The local truncation error (LTE) measures the error introduced by the numerical method, in our case the vertical discretization only. We define it after applying the true solution to the layerwise conservation for the tracer restricted to the grid points z_α (the diffusion term is not considered):-

$$\frac{\partial t_\alpha^{ex}}{\partial t} \Big|_s + \frac{\partial ut_\alpha^{ex}}{\partial x} + \frac{1}{h_\alpha} [wt^{ex}]_{\alpha+1/2}^{\alpha-1/2} + LTE_\alpha = 0$$

Using, first, the numerical flux consistency $\hat{H}_\alpha(1,1) = \mathbf{q}_\alpha^{n+\theta_z} \cdot \mathbf{n}_{ij}^K$ and then the relationship between the element normals and the dual cell ones (19):

$$\begin{aligned} 875 \sum_{K \in \mathcal{D}_{\alpha i}} \sum_{j \in K, j \neq i} \hat{H}_\alpha(1,1) &\equiv \sum_{K \in \mathcal{D}_{\alpha i}} \sum_{j \in K, j \neq i} \mathbf{q}_\alpha^{n+\theta_z} \cdot \mathbf{n}_{ij}^K = - \sum_{K \in \mathcal{D}_{\alpha i}} \mathbf{q}_\alpha^{n+\theta_z} \cdot \frac{\mathbf{n}_i^K}{2} \\ &\equiv - \sum_{K \in \mathcal{D}_{\alpha i}} \left(a_{iK}^x q_{\alpha,K}^{x,n+\theta_z} + a_{iK}^y q_{\alpha,K}^{y,n+\theta_z} \right) \end{aligned}$$

Since In the last step we have used the layer-integrated form of the conservation law, we have divided it by the layer depth, which is constant for internal z-layers. After canceling common terms:-

$$LTE_\alpha = \frac{\partial wt_\alpha^{ex}}{\partial z} - \frac{1}{h_\alpha} [wt^{ex}]_{\alpha+1/2}^{\alpha-1/2}$$

880 fact the for piecewise linear basis functions we have $\frac{\mathbf{n}_i^K}{2} = |K| \nabla \varphi_i|_K$. For each element in the subset $\mathcal{D}_{\alpha i}$, the horizontal tracer flux has been reduced to the mass flux. We can write the discrete tracer update:

$$|C_{\alpha,i}| \frac{\Delta h_{\alpha,i}}{\Delta t} \equiv \sum_{K \in \mathcal{D}_{\alpha i}} \left(a_{iK}^x q_{\alpha,K}^{x,n+\theta_z} + a_{iK}^y q_{\alpha,K}^{y,n+\theta_z} \right) + |C_{\alpha,i}| G_{\alpha-1/2,i}^{n+1} - |C_{\alpha+1,i}| G_{\alpha+1/2,i}^{n+1}$$

where the numerical fluxes at the interfaces are computed with the TVD scheme. In our time-continuous analysis $\Delta t \rightarrow 0$, corresponds to combine an upwind flux formula with a second-order centered flux which corresponds to the discrete layerwise

885 mass equation (28).

In case of a non-conformal box, we have to show that the modified horizontal tracer fluxes still reduces to the mass-fluxes. According to (44), the horizontal tracer fluxes in non-conformal boxes should be computed with:

$$w_{\alpha-1/2} t_{\alpha-1/2} = w_{\alpha-1/2}^+ t_{\alpha} + w_{\alpha-1/2}^- t_{\alpha-1} + \frac{|w_{\alpha-1/2}|}{2} (t_{\alpha} - t_{\alpha-1}) \phi_{\alpha-1/2}$$

We recall that $\phi_{\alpha-1/2} = \phi(r_{\alpha-1/2})$ is the Superbee limiter and r is a measure of the smoothness of the tracer profile. Typically the solution is expanded in a Taylor series about z_{α} :

$$t^{ex}(z) = t_{\alpha} + \frac{\partial t}{\partial z} \Big|_{\alpha} (z - z_{\alpha}) + \frac{1}{2} \frac{\partial^2 t}{\partial z^2} \Big|_{\alpha} (z - z_{\alpha})^2 + \frac{1}{6} \frac{\partial^3 t}{\partial z^3} \Big|_{\alpha} (z - z_{\alpha})^3 + O((z - z_{\alpha})^4)$$

We consider a z-grid with uniform vertical grid spacing h . Note that, for a z-grid, the first layer cannot have the same thickness as other layers but this makes the analysis more complex, so we restrict to equispaced internal layers. We replace the expanded expression of the true solution into the definition, see e.g. Nishikawa (2020). After some algebra, we get (only leading order diffusive terms shown):

$$LTE_{\alpha} = \frac{1}{2} ((|w_{\alpha}| - (|w|\phi)_{\alpha}) \frac{\partial^2 t}{\partial z^2} \Big|_{\alpha} h + \frac{1}{6} |[w]| \frac{\partial^2 t}{\partial z^2} \Big|_{\alpha} h + O(h^3))$$

where w_{α} is the vertical velocity at the layer mid-point and $[w]_{\alpha+1/2}^{\alpha-1/2}$ is the difference over the layer. We collect the diffusive terms and replace the expression for the vertical velocity

$$\hat{H}_{\alpha} \approx \begin{cases} \sum_{\beta=\alpha_{top,i}}^{\alpha_{min,K}} l_{\beta,K}^* \hat{H}_{\alpha_{top,K}}(T_{\beta^*,i}, T_{\beta^*,j}) & \text{if } \alpha = \alpha_{top,i} \text{ and } \alpha_{min,K} < \alpha_{top,i} \\ l_{\alpha,K}^* \hat{H}_{\alpha_{top,K}}(T_{\alpha^*,i}, T_{\alpha^*,j}) & \text{otherwise (hanging layer)} \end{cases}$$

which, in case of a constant tracer, can be rewritten for $\alpha \equiv \alpha_{top,i}, \dots, \alpha_{top,K}$:

$$D_{\alpha}^{num} = \frac{1}{2} \left(\left| \frac{\partial u}{\partial x} \right| ((b+z) - ((b+z)\phi)_{\alpha}) \frac{\partial^2 t}{\partial z^2} \Big|_{\alpha} h + \frac{1}{6} \left| \frac{\partial u}{\partial x} \right| \frac{\partial^2 t}{\partial z^2} \Big|_{\alpha} h^2 + O(h^3) \right)$$

Finally using the upper bound and $(b+\zeta)/H_0 \approx 1$ we get:

$$D_{\alpha}^{num} \leq \frac{1-\phi_{\alpha}}{2} A\Omega \frac{\partial^2 t}{\partial z^2} \Big|_{\alpha} h + \frac{1}{6} \frac{A\Omega}{H_0} \frac{\partial^2 t}{\partial z^2} \Big|_{\alpha} h^2 + O(h^3) \quad \square$$

$$\hat{H}_{\alpha} = c_{\alpha,i}^* \hat{H}_{\alpha_{top,K}}(1,1)$$

and thus:

$$\sum_{j \in K, j \neq i} c_{\alpha,i}^* \hat{H}_{\alpha_{top,K}}(1,1) = c_{\alpha,i}^* \left(a_{iK}^x q_{\alpha_{top,K},K}^{x,n+\theta_z} + a_{iK}^y q_{\alpha_{top,K},K}^{y,n+\theta_z} \right)$$

We perform here a simple experiment in a coastal environment (depth $H_0 = 50$ m and $\Omega = \frac{2\pi}{12.41 \text{ hours}}$) with two smooth tracer profiles, an exponential one $t(z) = t_0 \exp\{-z/\Lambda\}$ with small vertical derivatives ($\Lambda = 100$) and a hyperbolic tangent $t(z) = t_0 + \alpha \tanh\{(z + z_0)/\Lambda\}$ which exhibits larger vertical derivatives at the surface ($\Lambda = 2$). We consider a constant tracer diffusivity $\nu_{tr} = 5 \text{ cm}^2 \text{ s}^{-1}$. In Figure ?? we compare the L2-norm of the two contributions, $\|D_\alpha^{phy}\|$ and $\|D_\alpha^{num}\|$, the latter divided in a diffusive and anti-diffusive contribution. Different tidal amplitudes and vertical resolutions are investigated. To confirm the theoretical results we compute also the solution numerically with SHYFEM using the same vertical data and numerics of the analytical case. The numerical experiment has been carried out in a one-dimensional basin 21 km long with a mesh size of 50 m and a time step of 120 s. The numerical tracer profile is evaluated after 5 tidal periods. In Figure ?? the z-coordinate numerical profiles are compared against the reference z-star numerical profiles. This gives exactly the contribution from non-conformal boxes to the mass-transfer (42).

For the exponential profile, in the top panel of Figure ??, both the theoretical and the experimental numerical mixing are very small compared to the physical mixing. Only at large resolution and for large tidal amplitude does the numerical diffusion reaches the same order as the physical one and the profile starts to be slightly smeared out at the surface. Since the limiter is, at all depths, close to one such a diffusive effect could be attributed, from our analysis, to the second-order term. The situation changes for the hyperbolic tangent profile in the bottom panel of Figure ?. The limiter is active at the surface and introduces first-order diffusion which, at low resolution, overtakes the physical diffusion making the profile very smeared out. At finer resolutions the numerical mixing reduces and it becomes negligible for all tidal amplitude with $h \leq 2.5$ m. At such resolutions the profile follows well the reference solution, although, for large tidal amplitudes, the anti-diffusive term is large and a small overcompression of the profile can be observed at the surface. Finally, the tracer remap (39) preserves the constancy property. It is enough to verify that with a constant solution it reduces to:

$$\tilde{h}_{\alpha,i}^{n+1} = h_{\alpha,i}^{n+1} + \Delta t \left(\sigma_{\alpha-1/2,i}^{top} - \sigma_{\alpha+1/2,i}^{top} \right)$$

which, thanks to the definition provided in Section 4.2 of grid velocity $\sigma_{\alpha-1/2,i}^{top} = \frac{\tilde{z}_{\alpha-1/2,i}^{n+1} - \tilde{z}_{\alpha-1/2,i}^{n+1}}{\Delta t}$ and layer thickness $\tilde{h}_{\alpha,i}^{n+1} = \tilde{z}_{\alpha-1/2,i}^{n+1} - \tilde{z}_{\alpha+1/2,i}^{n+1}$ is an identity.

— Smooth stratification experiment. Top: numerical mixing (normalized by physical mixing) for different tidal amplitudes. Bottom: Numerical tracer profiles computed with SHYFEM for different tidal amplitude. From left to right: increasing vertical resolution, $h = 5$ m, $h = 2.5$ m, $h = 1$ m

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