New Routine NLTE15μmCool-E v1.0 for Calculating the non-LTE CO$_2$ 15 μm Cooling in GCMs of Earth's atmosphere

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Abstract. We present a new routine for calculating the non-local thermodynamic equilibrium (non-LTE) 15 μm CO$_2$ cooling/heating of mesosphere and lower thermosphere in General Circulation Models. It uses the optimized models of the non-LTE in CO$_2$ for day and ~~nigh~~ night conditions and delivered cooling/heating with an error not exceeding 1 K/~~Day~~ day even for strong temperature disturbances. The routine uses the Accelerated Lambda Iteration and Opacity Distribution Function techniques for the exact solution of the non-LTE problem and is about 1000 faster than the standard matrix/line-by-line solution. It has an interface for feed-backs from the model and is ready for implementation. It may use any quenching rate coefficient of the CO$_2(\nu_2)$+O(^{3}P) reaction, handles large variations of O(^{3}P) and allows the user to vary the number of vibrational levels and bands to find a balance between the calculation speed and accuracy. The suggested routine can handle the broad variation of CO$_2$ both below and above the current volume mixing ratio, up to 4000 ppmv. This allows using this routine for modeling the Earth's ancient atmospheres and the climate changes caused by increasing CO$_2$.

1 Introduction

~~The energy~~

The infra-red radiative cooling of atmosphere is an important component of its energy budget, which requires special techniques for its reliable estimation. For the local thermodynamic equilibrium (LTE), when the molecular emissions of the atmospheric unit volume are described by the Planck function for local temperature, this estimation confines on the solution of the radiative transfer equation in broad spectral regions occupied by molecular bands. In the middle and upper atmosphere, the breakdown of LTE (non-LTE) requires finding the sources of the non-equilibrium molecular emissions, which are obtained by the solution of the non-LTE problem. This makes the non-LTE cooling calculation significantly more time consuming. Today, the common opinion is that it is impossible to use exact methods for calculating the radiative cooling in GCMs, see, for instance, (López-Puertas et al., 2023) who promote this point of view. Various parameterizations were developed for fast calculating this cooling in GCMs, see (Fomichev et al., 1998; Fomichev, 2009), and (Feofilov and Kutepov, 2012) for review of works on parameterizing the non-LTE cooling of the Earth's middle atmosphere in the 15 μm CO$_2$, 9.6 μm O$_3$ and rotational H$_2$O bands. These algorithms, however, lack the accuracy needed for current GCMs.

Infrared emission in the 15 μm CO_2 band is the main cooling mechanism of middle and upper atmospheres of Earth, Venus and Mars (e.g. Goody and Yung, 1995; Sharma and Wintersteiner, 1990; Pollock et al., 1993; Bougher et al., 1994; Lopez-Puertas and Tay On Earth, the magnitude of MLT cooling affects both the mesospheric temperature and height: the stronger the cooling, the colder and higher is the mesopause (Bougher et al., 1994).

The goal of this work is to present a new routine for calculating the non-LTE 15 μm CO_2 cooling of the Earth's mesosphere and lower thermosphere (MLT), which utilizes exact radiative transfer and non-LTE problem solution techniques and is fast enough to be applied in GCMs. The new routine can handle the broad variation of CO_2 both below and above the current volume mixing ratio, up to 4000 ppmv. This allows using this routine for modeling the Earth's ancient atmospheres and the climate changes caused by increasing CO_2.

The routine we present is the optimized version of the research ALI-ARMS (for Accelerated Lambda Iteration for Atmospheric Radiation and Molecular Spectra) model and code (Kutepov et al., 1998; Feofilov and Kutepov, 2012). In this code the atmospheric cooling is the by-product of the non-LTE problem solution. For nearly 20 year the earlier version of this routine is being successfully applied (Hartogh et al., 2005; Medvedev et al., 2015) in the GCM of Martian atmosphere.

We demonstrate in this paper the performance of the routine for calculation of the 15 μm CO_2 cooling of the Earth's MLT. However, generally this is a universal code, which potentially may be applied to modeling the non-LTE cooling in any molecular band or bands of several molecules in any planetary atmosphere. We successfully tested it calculating the non-LTE cooling of the Earth's MLT in the 6.3 μm H_2O (Feofilov et al., 2009) and 9.6 and 4.7 μm O_3 (Manuilova et al., 1998) as well as the cooling of Titan atmosphere in the 6.7 and 3.3 μm CH_4 bands (Kutepov et al., 2013; Feofilov et al., 2016). This potentially allowed applying this algorithm for calculating the radiative cooling in GCMs of various atmospheres, among them the atmospheres of water reach exoplanets (e.g. Valencia et al., 2007; Acuña et al., 2021) and gas giants.

In the next section, we outline techniques applied currently in GCMs for calculating the non-LTE CO_2 15 μm cooling. In section 3 we briefly discuss method and techniques applied for calculating this cooling in our new routine. In section 4, we present the model of non-LTE in CO_2 used in the routine and the routine computational performance. section 5 discusses the accuracy of KF23 compared to the reference calculations. The Conclusion summarizes the results of our study. Appendix A contains technical details of the code and recommendations for its implementing and usage in GCMs.

2   The non-LTE radiative cooling of atmosphere and its calculations in General Circulation Models

The energy loss of the atmospheric unit volume due to the infra-red radiation is calculated as the radiative flux divergence taken with the opposite sign:

$$h = -\frac{1}{4\pi} \int d\omega \int d\nu \frac{dI_{\nu\omega}}{ds}, \tag{1}$$

where $I_{\mu\nu}$ is the intensity of radiation at the frequency ν along the ray ω,

With the local thermodynamic equilibrium (LTE), the discretization of integral radiative transfer equation (RTE) (Goody, 1964; Goody an (e.g. Goody, 1964; Goody and Yung, 1995) leads to a simple linear algebra operation for calculating the LTE 15 μm band cool-

ing:

$$h = W \times B,$$ (2)

where h is the vector of cooling in N_D grid points, B is the vector of Planck function for a local T, and W is $N_D \times N_D$ matrix, which accounts for radiative transfer in a number of 15 μm CO_2 bands contributing to the total cooling.

Extension of ~~GCMs~~ General Circulation Models (GCMs) on the mesosphere and thermosphere required accounting for the non-LTE for calculating the CO_2 15 μm cooling. The standard way of solving the non-LTE problem ~~(Curtis and Goody, 1956; Goody, 1964~~ (e.g. Curtis and Goody, 1956; Goody, 1964; Goody and Yung, 1995) requires inverting $(N_L \times N_D) \times (N_L \times N_D)$ matrix, where N_L is the number of CO_2 vibrational levels included in the model. The equation (2) in this case remains unchanged, however, the matrix W is rebuilt to account for differences between the Planck function and the non-LTE source functions in each band resulting from the non-LTE problem solution. This makes the calculation of the non-LTE cooling dramatically costlier (see for more details ~~Sect.~~ section 3).

Fomichev et al. (1998) and Fomichev (2009) (see references therein) discussed in detail various routines, which were suggested in previous studies for calculating the 15 μm cooling in GCMs with accounting for the non-LTE. The direct matrix solution of simplified non-LTE problem in CO_2 (often with an approximate radiative transfer treatment) or using pre-calculated W matrices for a limited number of atmospheric situations for further interpolation of its elements helped to reduce the computational time at the expense of calculation accuracy. The low computational efficiency kept the accurate accounting for the non-LTE in GCM difficult those days.

A new way of calculating the non-LTE 15 μm CO_2 cooling in GCMs was suggested by Kutepov (1978). Relying on results of Kutepov and Shved (1978) who showed that the fundamental 15 μm CO_2 band 01101 - 00001 (see below Figure 1) of main CO_2 isotope dominates the cooling above about 85 km, he derived the recursive expression for h coming from the analytical solution of the first-order differential equation for the non-LTE cooling h in the fundamental band. This expression directly accounted for the $CO_2(\nu_2)$+$O(^3P)$ quenching rate coefficient k and the $O(^3P)$ density. It was derived using the "second-order escape probability" approach (Frisch and Frisch, 1975; Frisch, 2022) for the approximate solution of the Wiener-Hopf type integral radiative transfer equation in the semi-infinite atmosphere. The algorithm of Kutepov (1978), see its refined version by Kutepov and Fomichev (1993), calculates h upward in the non-LTE layers using as a lower boundary condition the LTE h or the non-LTE h obtained using other technique. Fomichev et al. (1993) linked this algorithm to the matrix routine for calculating h in the LTE layers developed by Akmaev and Shved (1982). Later Fomichev et al. (1998) modified the routine of Fomichev et al. (1993) by adding the interpolation of the W matrices for the CO_2 within 150–720 ppmv using tables of pre-calculated elements and described in detail the structure of revised matrix W. These authors also extended the routine altitude range to layers above 110 km. Cooling in this region is calculated from the simple balance equation for the first excited vibrational level of main CO_2 isotope with accounting for absorption of the radiative flux from below, cooling-to-space and collisional quenching. For smooth temperature profiles, Fomichev et al. (1998) reported the maximal cooling calculation errors of less than 2 and up to 5 K/day, for 360 and 720 ppmv CO_2, respectively. ~~Below~~ In this paper we will call this routine F98.

Basic features of F98, namely (a) broad altitude range covered, (b) straightforward accounting for the non-LTE, (c) high computational efficiency attracted many users. For more than two decades F98 routine has been the most widely used algorithm for calculating the 15 μm CO_2 cooling in GCMs of mesosphere and thermosphere, see, for instance, (Eckermann, 2023) for its latest application. However, as we show below, the F98 errors are large for non-smooth temperature profiles reaching 20-25 K/day in the mesopause region. On the other hand, even very minor variation of the CO_2 cooling may have significant impact on the GCM results in ~~MLT. ?~~ the Mesosphere and Lower Thermosphere (MLT). Kutepov et al. (2013b) showed (Figure 18.2) that variation of the CO_2 cooling of $\sim$ 1-3 K/~~Day in the LIMA model~~ day in the Leibniz-Institute middle atmosphere model (LIMA) (Berger, 2008) in the mesopause region caused significant warming up to 5-6 K (about 105 km) and cooling up to -10 K (below 105 km) at latitudes between 90°S and 40°N for July 2005. This and other test lead to the conclusion (Berger, private communications), that the accuracy of cooling/heating rate calculations in GCMs "should not exceed 1 K/day for any temperature distribution".

Fortunately, this accuracy requirement overlapped in time with the dramatic progress in the non-LTE radiative transfer calculations. This allowed developing a new routine NLTE15μmCool-E ~~for~~ (hereafter KF23 for brevity within this manuscript) for calculating the non-LTE 15 μm CO_2 cooling in GCMs of the Earth's atmosphere, which exploits new exact algorithms for solving the non-LTE problem and, therefore, fits enhanced accuracy requirements. At the same time, it is fast enough to be used in GCMs.

~~In the next Section, we briefly discuss techniques applied in our new routine (hereafter KF2023 for brevity within this manuscript). In Sect. 4, we present the model of non-LTE in CO_2 used in the routine and the routine computational performance. Sect. 5 discusses the accuracy of KF2023 compared to the reference calculations. The Conclusion summarizes the results of our study. Appendix A contains technical details of the code and recommendations for its implementing and usage in GCMs.~~

3 ~~Method and technical approach. The ALI-ARMS code~~

~~New routine for calculating the non-LTE 15 μm CO_2 cooling we present~~ KF23 is the optimized version of our basic ALI-ARMS model and code (Kutepov et al., 1998; Feofilov and Kutepov, 2012), which utilizes two advanced techniques: (1) the ALI technique for the solution of the non-LTE problem, and (2) the ~~ODF~~ opacity distribution function (ODF) technique for optimizing the radiative transfer calculations. In this section, we outline these techniques and the current status and latest applications of ALI-ARMS code.

3 Method and techniques applied in a new routine for calculating the non-LTE cooling

3.1 Solution of the non-LTE problem. ~~The ALI technique~~

The non-LTE problem has two primary constituents ~~(Hubeny and Mihalas, 2015)~~: (1) the statistical equilibrium equations (SEE), which express the equality of the total population and de-population rates for each molecular level; (2) the radiative transfer equation (RTE) which relates the radiation field to the populations of levels, at *all altitudes* in the atmosphere

120 (Hubeny and Mihalas, 2015). Hence, the system of equations for the level populations is *nonlocal* (and nonlinear). The most obvious way of dealing with this situation is to iterate between the SEE and RTE. This process, traditionally called "lambda iteration" (LI), has been investigated in the astronomical context since 1920's (Unsoeld, 1968). It inverts N_D matrices $N_L \times N_L$ at each iteration step. This simple approach has been from time applied in the Earth's and planetary atmosphere radiative transfer, see, for instance, ~~(Appleby, 1990; Wintersteiner et al., 1992)~~(e.g. Appleby, 1990; Wintersteiner et al., 1992). If the optical

125 depths are large (as it is the case for the CO_2 15 μm band) the algorithm converges slowly. Kutepov et al. (1998) studied several LI schemes and showed that ~~in case of~~ for the CO_2 non-LTE problem, the number of iterations I_{LI} for these algorithms may reach ~ 200 for even moderate convergence criterion 1e-3. This results from the photons trapped in the cores of the most optically thick lines and of the strong SEE non-linearity related to quasi-resonant exchange of vibrational energy by the molecular collisions.

130 An alternative way of dealing with the non-LTE is a joint treatment of SEE and RTE, when RTE is discretized with respect to the optical depth or altitude grid to get a matrix representation of radiative terms in SEE. This approach, known in the atmospheric science as Curtis-matrix (CM) technique ~~(Goody, 1964; Goody and Yung, 1995; Lopez-Puertas and Taylor, 2001)~~ (e.g. Goody, 1964; Goody and Yung, 1995; Lopez-Puertas and Taylor, 2001)), leads to the matrix of dimension $(N_L \times N_D) \times (N_L \times N_D)$. In stellar atmosphere studies the generalized version of this technique is known as the Rybicki method (Mihalas,

135 1978). The time required for the solution of the non-LTE problem using the CM technique is controlled by the number of operations for matrix inversion. The advantage of classic matrix method lies in the simultaneous determination of all populations at all altitudes instead of the sequential evaluation of populations step by step at each altitude using the radiative field from the previous iteration. Therefore, "matrix iteration" converges usually better than lambda iterations. However, the convergence of both algorithms depends ~~, strongly on the way the~~ strongly on how the local non-linearity is treated, see next section. To

140 construct an adequate model, one must account for a large number of exited levels of various molecular species plus use a detailed model of atmospheric stratification. As a result both N_L and N_D can become very large. The dimensions of primary matrices are reduced by introducing various assumptions (for instance, the LTE assumption for rotational sub-levels as well as LTE in the groups of vibrational levels closely spaced in energy, etc, see also the discussion of GRANADA code in ~~Sect.~~ section 3.4). Nevertheless, usually the time to solve the non-LTE problem using CM method exceeds significantly the time

145 when LI algorithm is applied to the same problem (see ~~Sect.~~ section 5 for more details).

In the 1990s, stellar astrophysicists have developed a family of powerful techniques, which utilize lambda iteration with an approximate (or accelerated) lambda operator (see, Rybicki and Hummer (1991, 1992) and references therein). In these so-called ALI techniques (for Accelerated Lambda Iteration) the integral lambda operator, which links the radiation intensity at a given point with source function at all points, is approximated by a local (or nearly local) operator. With a local operator,

150 the largest matrices again, as in the LI case, have dimension $N_L \times N_L$. However, in this case, the convergence is rapid since most of the transfer in cores of the lines (described by the local part of lambda operators) cancels analytically and only the difference between exact and approximate radiative terms in the SEE is treated iterative. Kutepov et al. (1998) shoved that for the CO_2 non-LTE problem $I_{ALI} << I_{LI}$ (see ~~Sect.~~ section 5 for more details).

3.2 Treating the strong local non-linearity caused by intensive VV-exchange~~. Decoupling~~

155 Strong local non-linearity of the non-LTE radiative transfer problem in molecular bands caused by intensive near-resonant exchange of vibrational energy between molecules was studied by Kutepov et al. (1998). They showed that this non-linearity causes a dramatic deceleration of the convergence. Various schemes of additional "internal" iterations (without recalculating radiative excitation rates) aimed at adjusting populations of levels coupled by strong ~~VV exchange (without recalculating radiative excitation rates)~~ inter- and intramolecular vibrational-vibrational (VV) exchange, did not bring any help. To accelerate

160 the convergence, Kutepov et al. (1998) suggested "decoupling" which utilizes the Avrett (1966) approach of treating the "source function equality in the line multiples". The SEE terms, which describe the VV coupling, depend on the products $n_v n_{v'}$, where n_v is the population of vibrational level v of one molecular specie, whereas $n_{v'}$ is the population of level v' of the same or another molecular specie. In the iteration process, one needs to present these terms as $n_v n_{v'}^{\dagger}$, where $\dagger$ denotes the population of level with the *lower* degree of excitation, which is taken from the previous iteration. Kutepov et al. (1998) showed that

165 this stops "the propagation of errors" by iterations and guarantee the fastest convergence. This decoupling requires only slight modification of matrices to be inverted (without additional linearization of the non-LTE problem and, therefore, additional programming efforts) provides, however, the same acceleration of convergence as the application of the Newton–Raphson method for the solution of system of non-linear equations (Gusev and Kutepov, 2003).

3.3 The radiative transfer in the molecular ~~band. The ODF technique~~ bands

170 With line-by-line (LBL) calculations, a very large number of frequency points to be accounted for significantly decelerate calculations the 15 μm CO_2 radiative fluxes. In LTE the reduction of frequency points is usually achieved by utilizing the so-called CKD (for correlated k-distribution) method that is based on grouping the gaseous spectral transmittances in accordance with the absorption coefficient k. The accuracy of this approach is better than 1%, see, for instance, (Fu and Liou, 1992). However, the k-correlation is not applicable under the non-LTE conditions because the vibrational level populations involved

175 in the k-distributions are unknown and depend themselves on the solution of radiative transfer equation.

To overcome this problem, stellar astrophysicists developed the ~~opacity distribution function (ODF)~~ ODF technique. In this approach, they treat the non-LTE radiative transfer in "super-lines" associated with multiplets of very large line numbers ~~(Hubeny and Lanz, 1995; Hubeny and Mihalas, 2015)~~ (e.g. Hubeny and Lanz, 1995; Hubeny and Mihalas, 2015). They re-sample the normalized absorption and emission cross sections of "super-lines", consisting of hundreds or thousand of lines to yield a

180 monotonic function of frequency that can be represented by relatively small numbers of frequency points. Though the idea is like the k-correlation, these normalized absorption and emission profiles do not depend on the total populations of upper and lower "super-levels", but only on the relative population of closely spaced in energy sublevels within each "super-level", which are supposed to be in LTE.

Feofilov and Kutepov (2012) described the adaptation of the ODF technique to the solution of the CO_2 non-LTE prob-

185 lem. They treated each CO_2 band branch as "superline". Therefore, each CO_2 band was presented by only 3 "lines" for perpendicular- and 2 "lines" for parallel bands. This way of treating the radiative transfer in the molecular band is about 50-100

times faster than the classic LBL approach. ~~The~~ Whereas in LBL approach the radiation transfer equation is solved for each of N_F frequency grid points within each rotational-vibrational line, in the ODF techniques the same number of frequency grid points as applied only to each "superline". Thus, the acceleration factor is approximately equal to the number of ~~ro-vibrational~~ rotational-vibrational lines in the branch. As ~~they~~ Feofilov and Kutepov (2012) show, the ODF approach ~~does not lead to any significant errors in cooling~~ introduces very small errors in the 15 μm cooling. For current CO_2 density (400 ppm in the lower atmosphere), these errors do not exceed 0.3 K/~~heating rates.~~ Day in a broad range of temperature variations, see Figure 18 of (Feofilov and Kutepov, 2012). They increase roughly linearly with the CO_2 increase.

3.4 From matrix and LI to ALI technique. ~~The ALI-ARMS code~~

Since the 1960s the Curits Matrix algorithms, with the rare exceptions for LI mentioned above in section 3.1, have been dominating the solution of the non-LTE problems in the Earth's and planetary atmosphere including the studies of the the the 15 μm CO_2 cooling (see, for instance, the work by Zhu (1990), who developed very advanced for that time Curtis Matrix parameterizations of CO_2 cooling of MLT). Numerous non-LTE studies of the research group from the Institute of Astrophysics in Granada applied the GRANADA (for Generic RAdiative traNsfer AnD non-LTE population algorithm) code described by Funke et al. (2012). The core of it is a standard CM algorithm, which the authors in this and their earlier publications prefer to called MCM (for Modified Curtis Matrix). The paper discusses various ways of splitting large matrices into blocks, solving the non-LTE problem for selected sub-sets of levels and iterating to get the solution for all vibrational levels. In stellar astrophysics (Mihalas, 1978) this approach is known as the "generalized equivalent two-level approach for multi-level problems". For many years it has no use because of convergence problems. The GRANADA code also includes the LI, but not the ALI technique, although the transformation of LI into the ALI requires a minimum of programming efforts~~(Rybicki and Hummer, 1991; Kutepov et al., 1998)~~, but speeds up the convergence for optically thick problems ~~by at least an order of magnitude~~ at least 10 times (e.g. Rybicki and Hummer, 1991; Kutepov et al., 1998). Additionally, Funke et al. (2012) neither compared the computational performance of MCM and LI algorithms nor described the handling of a strong local non-linearity caused by VV-coupling.

3.5 The ALI-ARMS code

Kutepov et al. (1991, 1997) successfully applied the ALI technique to study the non-LTE emissions of molecular gases in planetary atmospheres (the 4.3 μm CO_2 band in the Martian atmosphere, and the 4.7 μm CO band in the Earth's atmosphere, respectively). Kutepov et al. (1998) and Gusev and Kutepov (2003) described in detail the adaptation of the ALI code developed by Rybicki and Hummer (1991) for stellar atmospheres to the solution of the non-LTE problem for molecular bands of planetary atmospheres~~,~~. They studied the performance of new the ALI-ARMS ~~(for Accelerated Lambda Iteration for Atmospheric Radiation and Molecular Spectra)~~ code, and demonstrated computational superiority of ALI-ARMS compared to various LI and CM/MCM techniques. The ALI-ARMS and its applications were described by Feofilov and Kutepov (2012). Later it was applied to study the rotational non-LTE in the CO_2 4.3 μm band in Martian Atmosphere, observed by ~~PFS-MEX~~ (the Planetary Fourier Spectrometer (PFS) in the Mars Express mission ((Kutepov et al., 2017) and references therein), to self-

220 consistent two-channel CO_2/temperature retrievals from the ~~SABER/TIMEDlimb radiances (Rezac et al., 2015)~~limb radiance measured by the SABER (for Sounding of the Atmosphere using the Broadband Emission Radiometer) instrument on board of the Thermosphere Ionosphere Mesosphere Energetics and Dynamics (TIMED) Mission(Rezac et al., 2015), and for explaining the SABER nighttime CO_2 4.3 μm limb emission enhancement caused by recently discovered new channel of energy transfer from $OH(\nu)$ to CO_2. Earlier, the ALI-ARMS code was used (Kutepov et al., 2006) to pinpoint an important missing process of

225 strong V-V coupling between the isotopes in the CO_2 non-LTE model of the SABER operational algorithm, and to modeling the H_2O 6.3 μm emission and the H_2O density retrievals in the MLT from the SABER 6.3 μm limb radiances (Feofilov et al., 2009). As we show below in sections 4 and 5, the ALI-ARMS code also provides an efficient way of calculating the 15 μm CO_2 cooling/heating in the GCMs.

4   New routine for the CO_2 cooling calculations

230 ### 4.1   The CO_2 non-LTE day- and night-time models

To optimize the cooling calculations we used as a reference one our working line-by-line non-LTE model in CO_2, which comprises 60 vibration level of 5 CO_2 isotopic species and two-levels N_2, O_2 and $O(^3P)$. In Figure 1, we show the lower levels of this model (up to 5000 cm^{-1}). The set of collisional rate coefficients for ~~VT~~ the vibrational-translational (VT) and VV exchanged we apply is described by Shved et al. (1998) and is similar to rates used by Lopez-Puertas and Taylor (2001).

235 However, it relies on different scaling rules based on the first-order perturbation theory. Compared to our extended line-by-line model (Feofilov and Kutepov, 2012), which includes total about 350 vibrational levels of 7 CO_2 isotopes and over 200000 ~~ro-vibrational~~ rotational-vibrational lines, the CO_2 cooling of the 60-level model differs by less than 0.05 K/day and 0.5 K/day for the CO_2 mixing ratios of 400 ppmv and 4000 ppmv, respectively, both for daytime and nighttime conditions and for any temperature profile.

240   In the next steps, we gradually reduced the number of levels and bands in the model to optimize the calculations, keeping the cooling rate errors smaller than 1 K/day compared to the reference model.
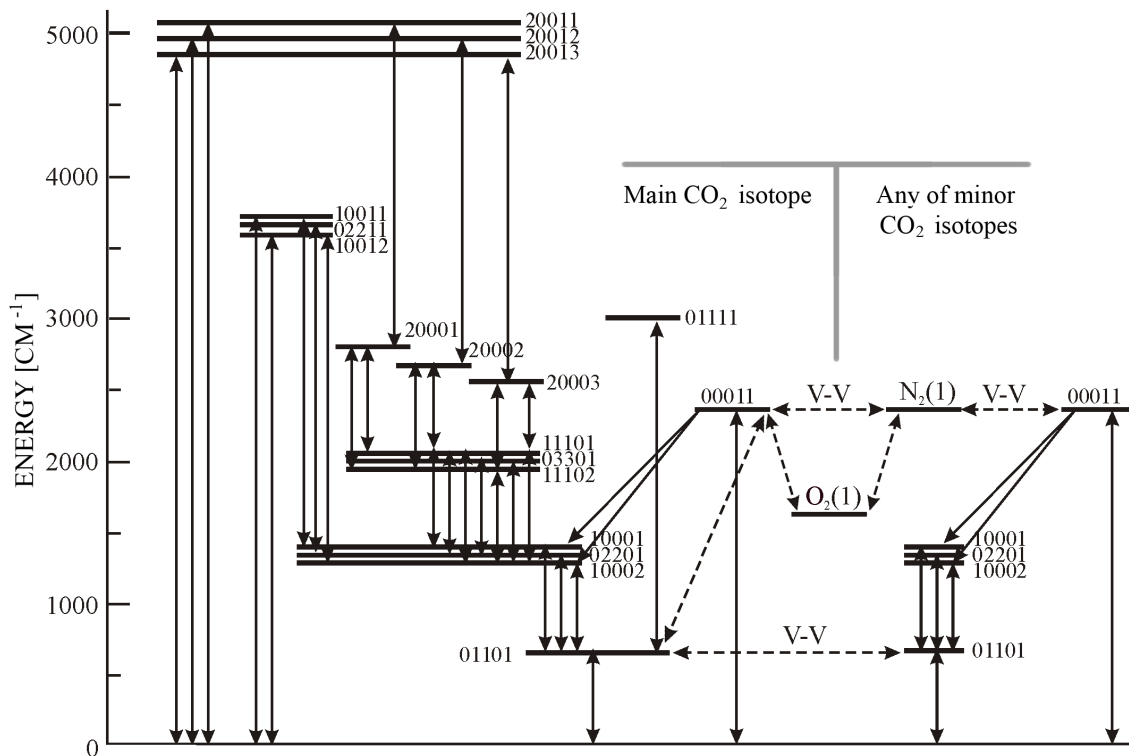
Figure 1. CO_2 vibrational levels diagram (Feofilov and Kutepov, 2012). ~~The levels are marked in accordance with~~ We use the HITRAN _(for High-resolution Trans_mission Molecular Absorption database) notation ~~, Solid~~ for vibrational levels. Main optical transitions are shown by solid lines with arrows~~show optical transitions~~, dashed lines with arrows refer to the inter-molecular V–V energy exchange processes~~,~~. V–T transitions are not shown for the sake of ~~readability~~simplicity. The main CO_2 isotope levels are shown up to the 5,000 cm^{-1} energy level~~, the~~. The minor isotopes levels are shown only up to 00011 level for simplicity.

Table 1. CO_2 vibrational levels included in the night- and daytime model			
Isotope, HITRAN level notification, energy in cm-1			
626 00001	0.0	636 00001	0.0
626 01101	667.379960	636 01101	648.478030
626 10002	1285.40834	636 02201	1297.26326
626 02201	1335.13161		
626 10001	1388.18432	628 00001	0.0
626 11102	1932.47013	628 01101	662.37335
626 03301	2003.24615		
626 11101	2076.85588	627 00001	0.0
D 626 00011	2349.14291	627 01101	664.72941
D 626 01111	3004.01227		
D 626 10012	3612.84080	44 0	0.0
D 626 02211	3659.27229	D 44 1	2329.9116
D 626 10011	3714.78193		
D 626 20013	4853.62341	66 0	0.0
D 626 20012	4977.83500	D 66 1	556.3519
D 626 20011	5099.66050		
		6 0	0.0
D marks levels added in daytime model			

In the Table 1, we show vibrational levels included in the optimized day- and nighttime models. The isotopes in the table are marked using the lower digit of the atomic weight: 626 corresponds to $^{16}O^{12}C^{16}O$, 636 corresponds to $^{16}O^{13}C^{16}O$ and so on. We account for 28 and 18 vibrational levels in the day- and nighttime models, respectively, which include the levels of four most abundant CO_2 isotopes and N_2 and O_2 levels (two and one for each at daytime and nighttime, respectively). We also include $O(^3P)$, but not $O(^1D)$ because its effect on the total CO_2 cooling/heating is negligible, both for nighttime and daytime conditions. The model uses the CO_2 spectroscopic information for all transitions available of the HITRAN-2016 (Gordon et al., 2017) for the levels listed in Table 1. In Table 2, we provide the numbers of bands, band branches, and lines used for daytime and nighttime calculations.

4.2 Computational performance ~~. Comparison~~ and comparison with other algorithms

In the astronomical context, the detailed analysis of the operation numbers and times needed for the solution of the non-LTE problem is a must because of the complexity of the problem (Hubeny and Mihalas, 2015). Even though the number of levels and lines involved in the non-LTE problem of planetary atmospheres is smaller, the speed is a crucial parameter for the GCMs, so we perform the same type of analysis in this section below.

We compared three algorithms of the non-LTE problem solution, namely LI, ALI, and matrix method (hereafter MM), see for details ~~Sect.~~ section 2. Although LI technique is much more computationally expensive compared to ALI algorithms (Kutepov et al., 1998; Gusev and Kutepov, 2003), one cannot say the same about MM approach applied to a problem with a reduced number of levels because of the low number of iterations it usually requires, and this required testing. We generated the matrices of the MM-algorithm from the matrix presentations of lambda operators, as discussed by Kutepov et al. (1998). We used the discontinuous finite element (DFE) algorithm as the most efficient way of solving the radiative transfer equation (Gusev and Kutepov, 2003; Hubeny and Mihalas, 2015), and we compared the LBL and ODF techniques (see ~~Sect.~~ section 2.3). Below in this section, we discuss the performances of all algorithms only with the non-linearity caused by near-resonance VV energy exchanges resolved as outlined in the ~~Sect. 2.2.~~ section 3.2. Without this, the number of iterations of all considered algorithms would be a few times higher.

For each of the three techniques, we checked the numbers of operations and times needed for each single iteration, then accounted for a number of iterations and compared total numbers of operations and times for the entire non-LTE problem solution.

We found that the time required for each iteration of the algorithms we studied is dominated by 3 components: ~~time for solving the radiative transfer equation (T_{Rad}) and forming the radiative rate terms in the SEE,~~ 1) time for auxiliary operations T_{Aux} (such as filling of large arrays like vectors or matrices to be inverted), ~~and~~ 2) time for solving the radiative transfer equation (T_{Rad}) and forming the radiative rate terms in the SEE, and 3) time for matrix inversions (T_{Inv}). The cooling itself is the by-product of the non-LTE problem solution and is estimated nearly instantaneously as in (Kutepov et al., 1998):

$$h = \sum_b \left[\left(n_{lo} B_{lo,up} \overline{J_{lo,up}} - A_{up,lo} n_{lo} \right) \times (E_{up} - (E_{lo}) \right]_b, \tag{3}$$

where $B_{lo,up}$ and $A_{up,lo}$, the band Einstein coefficients, and $\overline{J_{lo,up}}$, mean intensity in the band, which enter radiative rate coefficients of SEE matrices, whereas n_{lo}/E_{lo} and n_{up}/E_{up} are the populations/energies of lower and upper vibrational levels in the band, respectively. The sum in (3) goes along all CO_2 transitions in the model.

Table 2. Numbers of operation and computing times.

NIGHT: $N_L = 18$; $N_B = 18$, $N_{Br} = 54$, $N_{RT} = 3078$; $N_F = 32$; $N_A = 2$: $N_D = 125$; $CO_2 x1$

	N_{Aux}/T_{Aux}	N_{Rad}/T_{Rad}	N_{Inv}/T_{Inv}	N_I	T_{tot}	K
MM/LBL	5e4 / 9e-2	2.5e7 / 0.25	1.14e10/43	2	86	860
LI / ALI, LBL	5e4 / 8.5e-3	2.5e7 / 0.25	7.3e5/7.7.0e-3	60/5	16/1.3	160/ 13
ALI, ODF	5e4 / 8.5e-3	4.5e5 / 4.5e-3	7.3e5/7.7.0e-3	5	0.1	1

DAY: $N_L = 28$; $N_B = 46$, $N_{Br} = 119$, $N_{RT} = 6039$; $N_F = 32$; $N_A = 2$: $N_D = 125$; $CO_2 x1$

	N_{Aux}/T_{Aux}	N_{Rad}/T_{Rad}	N_{Inv}/T_{Inv}	N_I	T_{tot}	K
MM/LBL	1.1e5/2e-1	4.8e7/0.48	4.3e10/160	2	321	1284
LI / ALI, LBL	1.1e5/1.9e-2	4.8e7/0.48	2.7e6/2.2e-2	60/5	31/2.6	124/10
ALI, ODF	1.1e5/1.9e-2	9.5e5/9.5e-3	2.7e6/2.2e-2	5	0,25	1

T_{Aux}, T_{Rad}, etc. are in s.

In Table 2, we present the summary of our study. The table gives the main parameters of the non-LTE models for day and night conditions described in ~~Sect.~~ section 4.1, operation numbers and the times in seconds (measured with the help of timing routine withing the code), which are required for each calculation part. We performed this study at two different machines, with x86~~64-bit~~ _64 Intel and Intel Xeon Gold processors operating at 2.2 and 2.5 GHz, respectively. We compiled the ALI-ARMS code to be used in 64-bit architecture with the help of a standard ~~gcc~~ gnu compiler collection (gcc) compiler and we ran it on a single processor. We provide the results only for one 2.2 GHz Intel processor; the timing for the second processor is roughly 1.4 times shorter.

Compared to the reference code, we ran the routine using the convergence criterion 1.0e-2 instead of 1.0e-4. This allowed reducing the number of iterations by a factor of about 2 without sacrificing the accuracy.

Similar to the study by Hubeny and Mihalas (2015), we found that time T required for any procedure like the radiative transfer equation solution or matrix inversion may be presented as:

$$T = CN,$$ (4)

where N is the number of operations. ~~Whereas~~ Thus, whereas N is defined by mathematical nature of the problem, and the algorithm applied the coefficient C may depend on many factors like the quality of programming, language used, operational system, interpreter, computer architecture and performance, etc.

We found that the number of operations for the solution of the radiating transfer equation N_{Rad} in case of the non-overlapping lines may be approximated by the expression:

$$N_{Rad} \simeq N_D \times N_{RT} \times N_F \times N_A \tag{5}$$

and is the same for all algorithms compared. Here N_{RT} is the total numbers of lines (or band branches in the ODF case), and N_F and N_A are the numbers of points in the frequency and angle integrals used, respectively. The coefficient C in (4) which links radiative transfer operation numbers and corresponding times was found to be $\simeq 1.0\text{e-}8$ s.

We found that with the LI/ALI algorithms, the number of auxiliary operations N_{Aux} is well approximated by the expression:

$$N_{Aux}^{LI/ALI} \simeq N_L^2 \times N_D, \tag{6}$$

~~which~~ where N_L is the number of CO_2 vibrational levels. This expression gives the number of terms to be filled in the block-diagonal matrix comprising N_D blocks $N_L \times N_L$, where N_L is the number of vibrational levels. In case of the LI/ALI techniques these are the N_D matrices generated and inverted one after another at each iteration step. The coefficient C in (4) which links auxiliary operations and corresponding times is $C \simeq 1.7\text{e-}7$ s.

In case of MM technique the matrix to be generated at each iteration is much larger, namely it has the size $(N_L \times N_D) \times (N_L \times N_D)$ and consists of N_L fully filled diagonal blocks $N_D \times N_D$ which represent non-local radiative terms, whereas the same as for LI/ALI case collisional terms are now spread over non-diagonal parts of this large matrix. We found that when we present the number of operations to fill this matrix as:

$$N_{Aux}^{MM} \simeq N_D^2 \times N_L \tag{7}$$

then approximately the same coefficient $C \simeq 1.7\text{e-}7$ s links this number with the time needed for its filling.

The number of operation needed to matrix inversion ~~$\simeq N^3$~~ N_{Inv} is approximately N^3, where N is the matrix dimension. ~~Therefore,~~ Thus, we have the following expressions

$$N_{Inv}^{MM} \simeq (N_L \times N_D)^3 \tag{8}$$

for the MM algorithm, and

$$N_{Inv}^{LI/ALI} \simeq (N_L \times N_L)^3 \times N_D \tag{9}$$

for the LI/ALI techniques. In the latter case the number of operations is N_D^2 times lower, since only N_D matrices $N_L \times N_L$ are inverted one after another at each iteration. This is the great advantage of these techniques compared to MM when the entire huge matrix needs to be inverted at once since it has non-zero elements outside the diagonal blocks.

We use in the ALI-ARMS standard routines for linear equation solution ~~(Press et al., 2002)~~ (e.g. Press et al., 2002) ludcmp (LU decomposition), lubksb (backsubstitution) and mprove (iterative improvement) for matrix inversions. We found that for

these routines applied to the non-LTE problems studied here the coefficient between the number of operations and time for matrix inversion depends on the matrix dimension N and may be approximated by expression:

$$C = 1.0\text{e-7} \cdot (0.04 + 1.2/N). \tag{10}$$

One may see it the upper part of Table 2 that for night conditions the application of MM technique causes the matrix inversion be the most time-consuming calculation part at each iteration, although the number of iterations $N_{Iter} = 2$ is low. Applying LI,LBL techniques, provides strong reduction of the matrix inversion time per one iteration gives, however, only moderate reduction of total time (by a factor ~ 5) compared to MM,LBL due to a large number of iterations (60). The number of iterations for the LI/ALI techniques slightly depends on the atmospheric pressure/temperature distribution. The numbers, which are given in the table are mean values for a few hundreds of run for different atmospheric conditions. Applying ALI instead of LI significantly reduces the number iteration (5 instead of 60) providing additional acceleration of calculations by the factor $\gtrsim 10$. We note, that for the LI/ALI,LBL the most time-consuming part for each iteration is now the radiative transfer solution, which is more than 15 times slower than two other parts of calculation together. The ODF technique allows reducing T_{Rad} by a factor 50-60. This provides total additional acceleration by a factor $\gtrsim 10$. The last column in table gives the acceleration factor $K = T_{tot}/T_{tot,ALI,ODF}$, which shows how faster the ALI,ODF combination works compared to other techniques: it is about 900 and 160 time faster than MM,LBL and LI,LBL techniques, respectively.

The lower part of Table 2 shows the number of operations and times for various parts of calculations for the daytime non-LTE model described in ~~Sect.~~ section 4.1. Compared to nighttime, daytime calculations require about 2.5 times more time due to increased number of vibrational levels and bands accounted for. Nevertheless, main points discussed above in this section for the nighttime runs remain valid for daytime: (a) main decelerating factor for MM technique is the matrix inversion, notwithstanding the low number of iterations; (b) LI technique although reduces the matrix inversion time by a factor $\gtrsim 7000$, provides, however, only moderate decrease of total time (by a factor of ~ 10) because of the large number of iterations; (c) the ALI technique is more over 100 times faster than MM with the slowest part of calculations to be the LBL solution of RTE; (d) the ODF provides acceleration of RT calculations by a factor of 50. Finally, the ALI,ODF technique appears to be over 1000 times faster than the MM,LBL approach.

We measured the time the F98 routine requires at x86~~64-bit~~_64 Intel 2.2 GHz processors and found it to be around 3e-4 s. It means that for nighttime ~~KF2023~~ KF23 is about 300 times slower than F98. At daytime, when the solar heating parameterization of Ogibalov and Fomichev (2003)) is accounted for, our version of F98 requires about 30% more time. Still, it remains about 600 times faster than the daytime ~~KF2023~~ KF23 routine. In the next section we discuss in detail the accuracy of both routines. This study will help the user to choose between the accuracy and calculation speed depending on the errors his model may tolerate.

5 Accuracy of cooling/heating rate calculations

To estimate the calculations errors, we compared the outputs of our new ~~KF2023~~ KF23 routine and the F98 routine for the non-LTE CO_2 cooling calculations with ~~the reference model~~our non-LTE reference model, discussed in section 4.1. In these

355   tests, we used the CO_2 volume mixing ratio ~~profile~~ (VMR) profiles with 400 ppmv in ~~its~~ their "well mixed" part. We also tested the same profiles multiplied by factors of 2, 4, and 10. For the $CO_2(\nu_2)+O(^3P)$ quenching rate we used temperature-dependent coefficient $k = 3.0 \times 10^{-12}$ $s^{-1}cm^3 \times \sqrt{(T/300)}$ (see ~~Sect.~~ section 5.4 for more details). As we described ~~above in Sect.~~ before in section 4.1, the vibrations levels and bands accounted for in ~~KF2023~~ KF23 keep its accuracy of ~ 1 K/~~Day~~ day for any temperature profile, including those strongly disturbed by various tidal and gravity waves. Here, we show the errors of both

360   routines compared to the reference model only for "wavy" temperature profiles. For mean profiles with a smooth structure, the errors of ~~KF2023~~ KF23 were about 0.1-0.3 K/~~Day~~ day (for 400 ppmv of CO_2). For the F98 routine, the errors for smooth profiles were around 1-3 K/~~Day~~ day confirming the results of Fomichev et al. (1998).

5.1   ~~Nighttime~~The nighttime cooling/heating rates

+
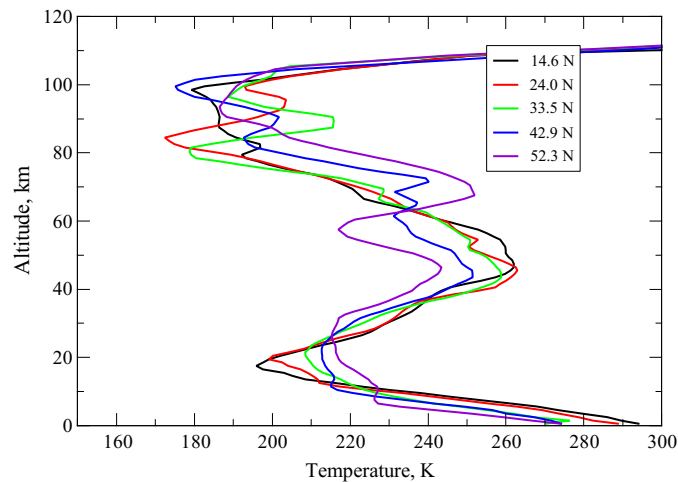
Figure 2. Temperature profiles used for testing the CO_2 15 μm cooling calculations

    In Figure 2, we show five ~~perturbed temperature profile for latitudes 0-55°N~~typical temperature profiles, which demon-

365   strate superposition of different meso-scale waves. These profiles, as well as corresponding pressure, $O(^3P)$ and CO_2 distribution (shown in Figure 3), and other constituents from the Whole Atmosphere Community Climate Model Version 6 (WACCM6~~CESM~~) (Gettelman et al., 2019) runs were kindly provided by Dan Marsh (private communications). For the 15 μm cooling calculations this model uses the F98 parameterization. We show below the calculation results for these atmospheric model inputs because WACCM is widely used by the community model. Generally, any pressure/temperature profiles disturbed

370   by strong waves, give similar results, as we observed in our tests. These may be both p/T distributions generated by modern GCMs, like in our case here, or those retrieved from ground base or space observations, or artificial wavy p/T distributions.
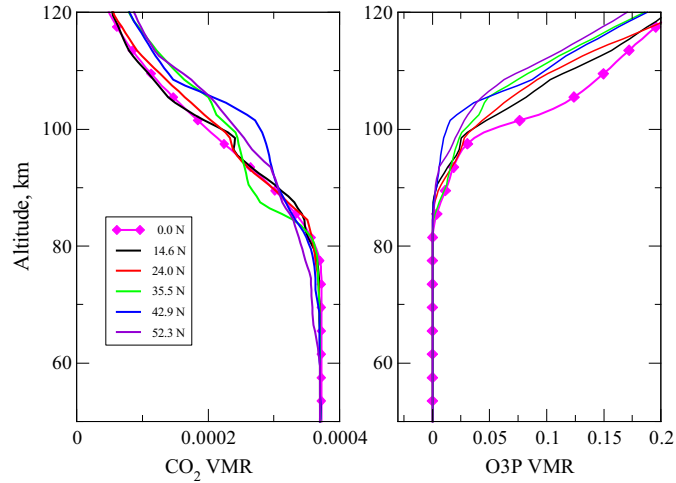
Figure 3. Volume mixing ratio profiles of CO_2 and $O(^3P)$ used for testing the CO_2 15 μm cooling calculations. Solid magenta line with diamonds for 0.0 N are data taken from Yudin et al. (2022) which were used for the simulations shown in Figure 9; ~~Solis~~ Solid lines for 14.6°N - 52.3°N correspond to the temperature profiles in Figure 2 and were used for simulations shown in Figures 4 - 6, see text for details.

.

Figure 4 shows the CO_2 15 μm cooling rates for the new ~~KF2023 routinean for~~ KF23 routine, for the F98 parameterization~~for~~, and for our reference model for temperatures in Figure 2 and the 400 ppmv CO_2 profiles. One may see in this figure that errors of new routine do not exceed 0.5 K/~~Day~~day. On the other hand the F98 routine errors reach up to 13 K/~~Day~~day. The altitude range, where the F98 routine demonstrates significant errors, is broad starting just above the altitude of 60 km. In Figure 5 we show same as Figure 4 cooling rates and their differences, however, for the twice higher CO_2 of 800 ppmv in the "well mixed" range. We note here that both maximal absolute values of cooling rates as well as the new- and the F98 routine errors are roughly twice higher compared to those of Figure 4. For the new routine they do not exceed 1 K/day, whereas for the F98 routine they reach up to 23 K/~~Day~~day.

Finally, in Figure 6 we show in panel (a) the cooling rates produced by the reference model and by ~~KF2023~~ KF23 routine for the CO_2 VMR of 4000 ppmv, which is 10 times higher then the reference one. The new routine errors are shown in panel (b). F98 routine was not tested at this inputs since it was not designed to work with the CO_2 VMRs higher than 720 ppmv. One may see in this figure that absolute cooling rates (maximal values) are approximately 10 times higher than those for 400 ppmv of CO_2. Same is roughly true for the new routine errors, which now reach in upper parts of tested region the values up to 8 K/~~Day~~day.

In Figure 7 we show for night the contributions of major and minor CO_2 isotopes, included in the model (see ~~Sect.~~ section 4.1), for temperature at 33.5°N for 400 and 1600 ppmv of CO_2. One may see in this figure that for the 400 CO_2 ppmv this
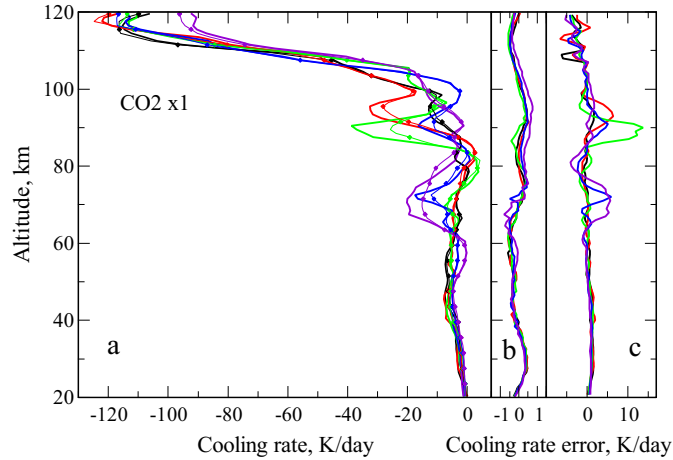
Figure 4. ~~Nighttime~~ The nighttime cooling rates in the CO_2 15 μm band and cooling rates errors for the CO_2 VMR of 400 ppmv for temperature distributions of Figure 2. Line colors correspond to the legend in Figure 2. (a) Cooling rates: thick solid lines - reference ~~data~~model; thin solid lines with diamonds - F98 routine; the ~~KF2023~~ KF23 results are not shown; (b) Cooling rate differences between the new routine ~~KF2023~~ KF23 and reference data; (c) Cooling rate differences between the F98 routine and reference data.
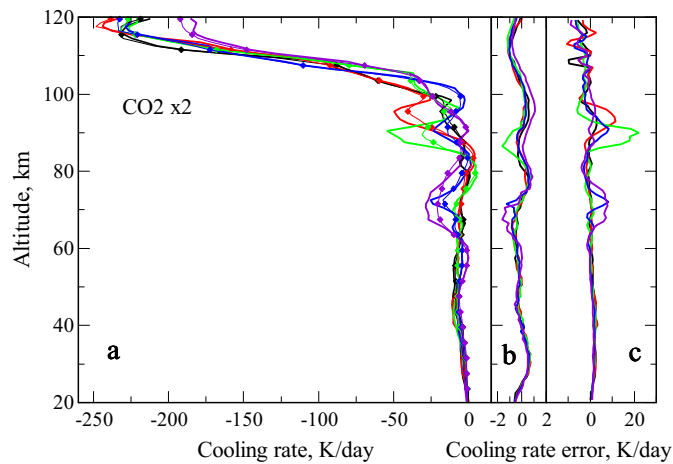
Figure 5. ~~Same~~ The same as in Figure 4, however, for 800 ppmv of CO_2.

contribution does not exceed $\sim$2 K/~~Day~~ day and $\sim$1 K/day for the 626 hot bands and for all minor isotope bands, respectively.
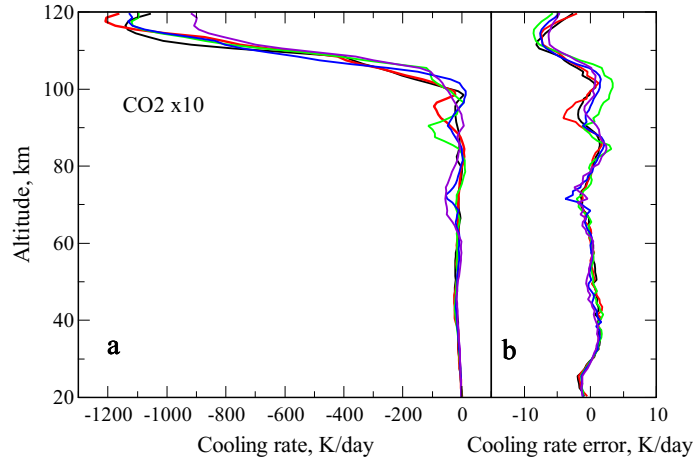
Figure 6. ~~Same~~ The same as ~~in~~ Figure 4, however, for 4000 ppmv of CO_2, no results for the F98 routine are shown.
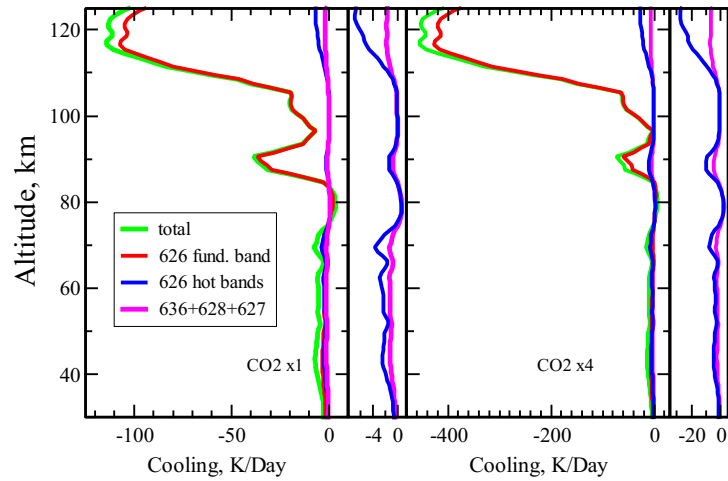
Figure 7. Contributions of various CO_2 bands to the total nighttime cooling at 33.5°N. ~~Narrow~~ The narrow sub-panels show re-scaled 626 isotope hot bands and minor isotope contributions.

This effect of hot bands and minor species is increasing with the CO_2 density, see the right panel of Figure 7 particularly for
390   altitudes affected by waves.

As we mentioned in the ~~Sect.~~section 4.1 we use all CO_2 bands available in the ~~HITRAN-16~~ HITRAN-2016 for the night set of levels in Table 1. This minimizes the errors compared to reference calculations to ≤ 1 K/day for 400 ppmv of CO_2. The routine allows ~~the user to reduce the number of~~ using less levels and bands to accelerate calculations, however, at the expense of error increase (see for more details Appendix A). For instance, ~~the test for the nighttime for roughly twice smaller set of bands, which does not include weak first and second~~ excluding (see Figure 1) weak first $(10001,02201,10002) \rightarrow 01101$ and second $(11101,03301,11102) \rightarrow (10001,02201,10002)$ hot bands of 626 and 636 isotopes ~~shows that the~~ makes the total number of bands twice lower. Our tests show that in this case the routine work only about 10% (see also Table 2) faster, however the maximal cooling rate error for 400 ppmv ~~may increase~~ increases up to 3 K/day~~, however, computing time becomes only 10% shorter (see also Table 2).~~.

5.2 ~~Daytime. Near-infrared~~ The daytime cooling/heating rates

At daytime the near-infrared heating due to the absorption of solar radiation in the CO_2 bands around 2.0-4.3 μm represents a small, however, non-negligible reduction of the total CO_2 cooling (up to 1-2 K/day for the current CO_2). The complex mechanisms of the absorbed solar energy assimilation into a heat were investigated in detail in a number of studies summarized by Lopez-Puertas and Taylor (2001). Ogibalov and Fomichev (2003) studied this heating for smooth temperatures for various CO_2 and solar zenith angles (SZAs) and suggested the look-up-table, which allows a quick estimate of this heating in GCMs. Due to its reasonable accuracy (~ 0.5 K/~~Day~~ day for current CO_2) this table has been used as a daytime supplement to the F98 nighttime cooling parameterization. Unfortunately, with increasing CO_2 density the errors of this table increase rapidly above ~ 70 km: for 720 ppmv CO_2 it underestimates the heating around the mesopause by more than 50% (see Figure 5 of Ogibalov and Fomichev (2003) for daily averaged heating). In Figure 8 the heating of the atmosphere due to the daytime absorption of
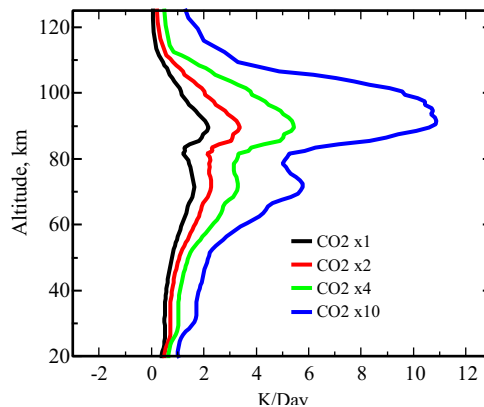
Figure 8. ~~Near~~ The near infra-red solar heating at 33.5° N for solar zenith angle 45° for various CO_2 densities.

solar radiation in the CO_2 bands at 2.0-4.3 μm for SZA=45° at the latitude 33.5°N produced by our new routine is shown. To prevent increasing errors for daytime due to an inadequate treatment of solar radiation absorption and assimilation, the

KF20223 utilises at daytime an extended non-LTE model which, compared to the nighttime, includes additionally 10 more CO_2 vibrations levels (see Table 1) and comprehensive system of radiative and collisional VT and VV energy exchanges as described by Shved et al. (1998); Ogibalov et al. (1998). Higher number of vibrational levels and more than twice higher number of bands leads to a 2.5-time longer time for the daytime cooling/heating calculation (see Table 2). However, the daytime errors were of the same order (less that 1 K/~~Day~~ day for 400 ppmv) as those for the nighttime (Fig. 4-6) even for strongly perturbed temperatures and increased CO_2. We do not present these comparisons. As in the night case removing a half of bands (various hot and combinational bands) in the daytime model gives only about 10% speed gain, however, maximal errors of cooling may reach for 400 ppmv 4 K/~~Day~~day.

5.3 ~~Diurnal~~ Cooling/heating rates for the diurnal tides at equator
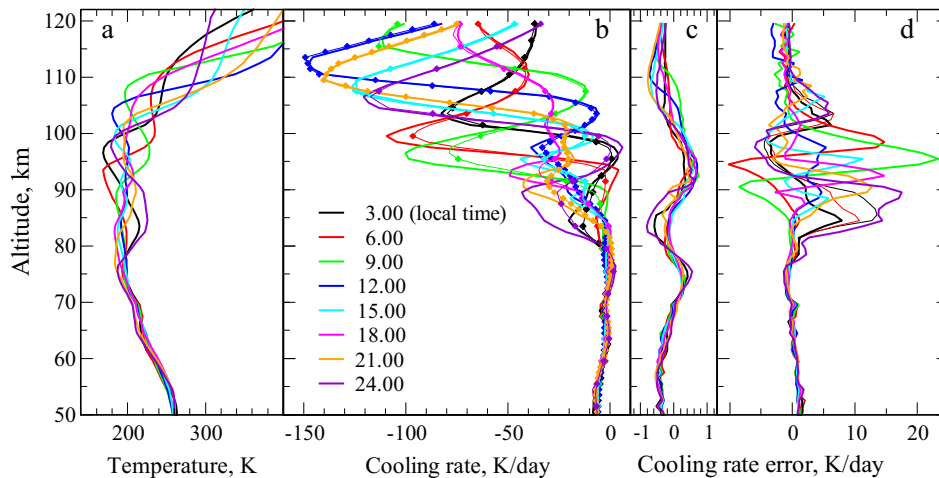
Figure 9. Comparisons of the CO_2 15 μm cooling rates. Diurnal tides at equator. (a) Temperature profiles for various local times; (b) Cooling rates: thick solid lines - reference model, thin solid lines with diamonds - F98 routine; (c) Cooling rate differences between new routine, presented in this study, and the reference model; (d) Cooling rate differences between the F98 routine and the reference model

In Figure 9, we compare the cooling rates obtained with the ~~KF2023~~ KF23 routine and with F98 parameterization with those produced by the reference model. For these tests, we used the temperature/pressure distributions affected by the diurnal tides at the equator. p, T and the atmospheric constituent densities as well as local zenith angles for local times at 1.0°N and 12.0°E (March 15, 2019) corresponds to the WACCM-X (Whole Atmosphere Community Climate Model extended in the thermosphere and ionosphere) equatorial simulations constrained by meteorological analyses of the NASA Goddard Earth Observing System version 5 (GEOS-5) below the stratopause, as discussed in Yudin et al. (2020, 2022). The temperature distributions at various local times are shown in panel (a). Panel (b) presents the CO_2 15 μm cooling rates calculated using

the reference model (thick solid lines) and the F98 routine (thin solid lines with diamonds). We do not show here the cooling rates obtained using the ~~KF2023~~ KF23 routine because the difference between them and the reference data does not exceed the
thickness of a curve. These differences do not exceed 1 K/day (Fig. 9c). Figure 9d shows the differences between the cooling produced by the F98 routine and the reference calculations. In contrast to Figure 9c, these differences exceed 20 K/day for some temperature profiles.

One may see in Figure 9 that the accuracy of the F98 routine is improving above 100 km and below 80 km. Above 100 km, the F98 parameterization uses the recursive expression, the accuracy of which increases with height (Kutepov, 1978). Below 80 km, the F98 routine is based on LTE matrix algorithm for cooling calculations. This algorithm accounts for the radiative interaction of the neighboring levels and the escape of radiation to above, and, therefore, provides a good accuracy of cooling in this optically thick layer. In the layer between 80 and 100 km, the F98 routine merges the cooling values calculated by the two methods outlined above. This merging works reasonably well for smooth temperature distributions tested by Fomichev et al. (1998), but it fails with "wavy" temperatures. One also needs to keep in mind that this layer is the transition region between the LTE and non-LTE state of the $CO_2(\nu_2)$ vibrations, where the physics of formation of the non-equilibrium vibrational distribution must be considered in all details (e.g. Kutepov et al. (2006)). Compared to the ~~KF2023~~ KF23 routine, which rigorously models the non-LTE, the F98 routine fails in this situation, what Fomichev et al. (1993) warned about when they presented the first version of this parameterization.

5.4 The $CO_2(\nu_2)$+O(^{3}P) quenching rate coefficient

The results above in section 5 were obtained for the temperature-dependent $CO_2(\nu_2)$+O(^{3}P) quenching rate coefficient $k = 3.0 \times 10^{-12}$ s^{-1}cm$^3 \times \sqrt{(T/300)}$. The multiplier in this expression is the median value of the rate coefficient from the range of (1.5 - 6.0)$\times 10^{-12}$ s^{-1}cm^3 which spans from the low laboratory data up to high data obtained from the space observations of the CO_2 15 μm emission, see ~~(Feofilov et al., 2012)~~ (e.g. Feofilov et al., 2012) and references therein. This value is currently accepted for usage in the GCMs for calculation of the 15 μm cooling. The dependence of MLT cooling on k was ~~studied~~ investigated in many previous ~~studies (e.g. Lopez-Puertas and Taylor (2001)~~ works summarized by Lopez-Puertas and Taylor (2001) , see also references therein). It is known that the maximum value of cooling, which is usually reached at the altitudes of 100-140 km, is roughly proportional to the k value used in calculations. The ~~KF2023~~ KF23 routine works well for any k from the range given above, and it also allows varying the temperature dependence of the rate coefficient (e.g. Castle et al. (2012)), see Appendix A. For our calculations, we used the O(^{3}P) densities shown Figure 3.

5.5 Upper and lower ~~boundary~~ boundaries

The accuracy tests of the ~~KF2023 routine above were performed for 1-km step grid~~ KF23 routine were performed with the upper boundary of atmosphere at 130 km boundary. The routine may work with any upper boundary in the upper ~~mesopshere~~ mesosphere and above. Putting the upper boundary below $\sim$ 110 km may cause, however, increasing cooling errors due to not accounting for the upper atmospheric layers. The lower boundary can be placed at any altitude below $\sim$ 50 km where all CO_2 15 μm bands are in LTE. This will justify the LTE lower boundary condition for the radiative transfer equation solution.

However, it is not recommended to use the routine results below ~ 20 km because of increasing errors by not accounting for the line overlapping in a current version of the ODF approach.

6   Conclusions

We present the new ~~KF2023~~ KF23 routine for calculating the non-LTE CO_2 15 μm radiative cooling/heating in the middle

465   and upper atmosphere. The routine provides high accuracy cooling rates above 20 km in a broad range of atmospheric input variations for any temperature distributions including those disturbed by strong micro- and meso-scale strictures and is the optimized version of the ALI-ARMS reference model and research code (Feofilov and Kutepov, 2012), which rigorously solves the non-LTE in CO_2, N_2, O_2 coupled by intensive vibrational-vibrational energy exchanges. ~~It~~ The routine relies on advanced techniques of exact non-LTE problem solution (ALI-algorithm) and the molecular band radiative transfer treatment

470   (ODF-technique). Using these methods, we achieved about ~ 1000 times acceleration compared to the standard matrix/line-by-line solution of the same non-LTE problem without sacrificing the accuracy. We show that the maximum error of calculations does not exceed 1 K/day for the current atmospheric CO_2 density and the median value of $CO_2(\nu_2)+O(^3P)$ quenching rate coefficient. This accuracy is ensured by a relatively large number of CO_2 levels and bands used in the ~~KF2023~~ KF23 routine. We also allow the user to choose between the accuracy and calculation speed by adding or removing certain bands and levels

475   (see Appendix A).

The ~~KF2023~~ KF23 routine provides accurate cooling calculations in a ~~very broad ranges of *k*,~~ vast range of the $CO_2(\nu_2)+O(^3P)$ quenching rate coefficient and $O(^3P)$ ~~variation~~ variations. It works also well for very broad ~~variation of~~ variations of the CO_2 VMR, both below and above the current density, up to 4000 ppmv. ~~This allows using this routine for modeling~~ Consequently, this allow to use this routine to model the Earth's ancient atmospheres and the climate changes caused by increasing CO_2.

480   Recently López-Puertas et al. (2023) presented an updated version of the F98 routine. Detailed analysis of this work is given by Kutepov (2023). The main improvement compared to F98 is an extended range of CO_2 abundances: whereas F98 routine covered the range of CO_2 concentrations with tropospheric values from 150 to 720 ppm the parameterization presented in this work goes up to 3000 ppm of tropospheric CO_2. Another minor improvement is the finer altitude grid of revised parameterization. The authors did not make revised routine available for users for its independent testing. They show numerous

485   tests of the routine accuracy, however, only for undisturbed individual temperature distributions, for which its error does not exceed 0.5 K/day. They also tested the revised routine for the temperatures retrieved from the MIPAS (Michelson Interferometer for Passive Atmospheric Sounding) observations, which demonstrate large variability. These individual profiles are the good inputs for the revised parameterization to show how it works for strongly disturbed temperature profiles. However, the authors do not show these results. Instead, they present only as the zonal means of the differences. Obviously, this averaging washes

490   out the errors obtained for individual profiles, for which we observed (see section 5) the F98 parameterization errors up to 25 K/day. Meanwhile these large errors in our study are generally concentrated in the altitude region around 90 km, exactly where the Root Mean Square Errors (RMSEs) in Figure 25 of López-Puertas et al. (2023) are maximized reaching 8-9 K/day. In section 5 we explain why F98 works badly in this altitude region. These large RMSEs allow to conclude that presented by

López-Puertas et al. (2023) revised routine has the same problems as the F98 parameterization and, therefore, works nothing better for the disturbed temperature distributions then the F98 parameterization.

Appendix A: The NLTE15μmCool-E ~~v~~1.0 routine ~~. Technical~~ (technical details~~.~~)

The routine source code is written in C. The routine is available at https://doi.org/10.5281/zenodo.8005028 and is ready for implementation into any General Circulation Models usually written in Fortran through a small "wrapper".

The routine has an interface, which allows efficiently receiving feed-backs from the model. These are inputs required for the cooling calculations such as pressure, temperature, CO_2, $O(^3P)$ and other atmospheric constituent densities. It return the CO_2 15 μm radiative cooling/heating at the altitude grid specified by the user. The routine works for day (SZA $\leq 110°$) and night (SZA $> 110°$) conditions.

Following the discussion in ~~Sect.~~ section 5 the routine may generally work with any upper and lower boundary, however it is nor recommended putting the upper boundary below $\sim$ 110 km since it causes increasing calculations errors due to not accounting for the upper atmospheric layers as well as placing the lower boundary below $\sim$ 20 km because of increasing errors caused by not accounting for the line overlapping in a current version of the ODF approach.

The module requires *geometrical altitudes* to calculate radiative transfer and an *equidistant altitude grid*, which guaranties exact solution of the radiative transfer equation. The user may define any grid step including very fine one, which allows resolving micro-scale temperature disturbances. ~~The calculation time of the routine~~ This is an advantage of our routine since its calculation time only linearly depends on the number of grid points N_D ~~compared to matrix algorithms, where the time~~. Compared to this the calculation time of matrix algorithms $\sim N_D^3$, see expressions (4 -10). ~~To account for the~~ Nevertheless, for those, who wants to account for additional cooling effect of the micro-scale sub-grid disturbances, we recommend to use ~~the~~ its parameterization described in ~~(Kutepov et al., 2007; ?). This parameterization is~~ (Kutepov et al., 2007; Kutepov et al., 2013b), which may be easily implemented in the routine~~and may be switched on and off by the user.~~.

The routine includes all inputs required for its proper performance, among them all collisional rate coefficient parameterizations as described by Shved et al. (1998) as well as the ~~HITRAN-16~~ HITRAN-2016 spectroscopic data for all bands available for the CO_2 level set in Table 1. The ~~letter~~ latter are presented as temperature dependent ~~A(T) and B(T)~~ $A(T)$ and $B(T)$ Einstein coefficients for each band branch calculated in accordance with (Kutepov et al., 1998; Gusev and Kutepov, 2003). We compared $A(T)$ and $B(T)$ with those calculated for 2 earlier HITRAN versions and found the differences less than 0.1-0.2% for bands included in our CO_2 night time model. For some hot 15, 4.3-μm, and combinational bands included in the daytime model, these differences are of the order of 0.5%, since data for these bands slightly vary from one HITRAN version to another.

The routine includes also the detailed table of basic ODF for a band branch in a broad ranges of temperature and pressure variations, which then re-scaled for calculating the radiative transfer in any individual band branch.

The supplied set of levels and spectral band information ensures the cooling/heating calculation errors for day and night to be below 1 K/day for any temperature disturbances. For smooth temperature profiles, the calculation errors are around 0.1-0.3 K/~~Day~~ day (for 400 ppmv of CO_2).

Finally, the routine allows the user to switch on ~~an~~ and off the vibrational levels and/or bands used in the model. This removing or adding vibrational levels will also automatically add (or removes) the bands related to these levels. If the user task can tolerate larger errors, the calculation speed can be increased at the cost of lowering the accuracy.

Code availability. The current version of the routine code is available at https://doi.org/10.5281/zenodo.8005028

Author contributions. Within more than 20 year of collaboration of both authors on the development of the ALI-ARMS code, which optimized version NLTE15μmCool-E is presented here, AK contributed most in the development of the ALI and ODF methodologies, he also wrote the manuscript draft supported by AF. AF contributed most to the development of the ALI-ARMS physical model, designed and implemented in the code the ODF based routines for radiative transfer treatment, performed all calculations presented in this paper as well as the detailed analysis of the routine computational performance.

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