



- 1 Soil related developments of the Biome-BGCMuSo v6.2
- terrestrial ecosystem model by integrating crop model
   components
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# 28 Abstract

Terrestrial biogeochemical models are essential tools to quantify climate-carbon cycle 29 feedback and plant-soil relations from local to global scale. In this study, theoretical basis is 30 provided for the latest version of Biome-BGCMuSo biogeochemical model (version 6.2). 31 32 Biome-BGCMuSo is a branch of the original Biome-BGC model with a large number of developments and structural changes. Earlier model versions performed poorly in terms of 33 34 soil water content (SWC) dynamics in different environments. Moreover, lack of detailed nitrogen cycle representation was a major limitation of the model. Since problems associated 35 36 with these internal drivers might influence the final results and parameter estimation, additional structural improvements were necessary. During the developments we took 37 38 advantage of experiences from the crop modeller community where internal process representation has a long history. In this paper the improved soil hydrology and soil 39 carbon/nitrogen cycle calculation methods are described in detail. Capabilities of the 40 Biome-BGCMuSo v6.2 model are demonstrated via case studies focusing on soil hydrology 41 42 and soil organic carbon content estimation. Soil hydrology related results are compared to observation data from an experimental lysimeter station. The results indicate improved 43 performance for Biome-BGCMuSo v6.2 compared to v4.0 (explained variance increased from 44 0.121 to 0.8 for SWC, and from 0.084 to 0.46 for soil evaporation; bias changed from -0.047 45 to -0.007 m<sup>3</sup> m<sup>-3</sup> for SWC, and from -0.68 mm day<sup>-1</sup> to -0.2 mm day<sup>-1</sup> for soil evaporation). 46 Sensitivity analysis and optimization of the decomposition scheme is presented to support 47 practical application of the model. The improved version of Biome-BGCMuSo has the ability 48 49 to provide more realistic soil hydrology representation and nitrification/denitrification process estimation which represents a major milestone. 50

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# 53 1. Introduction

54 The construction and development of biogeochemical models (BGM) is the response of the scientific community to address challenges related to climate change and human 55 induced global environmental change. BGMs can be used to quantify future climate-56 57 vegetation interaction including climate-carbon cycle feedback, and as they simulate plant production, they can be used to study a variety of ecosystem services that are related to human 58 59 nutrition and resource availability (Asseng et al., 2013; Bassu et al., 2014; Huntzinger et al., 2013). Similarly to the models describing various and complex environmental proscesses, the 60 61 structure of biogeochemical models reflects our current knowledge about a complex system with many internal processes and interactions. 62

63 Processes of the atmosphere-plant-soil system take place on different temporal (subdaily to centennial) scales and are driven by markedly different mechanisms that are 64 quantified by a large diversity of modeling tools (Schwalm et al., 2019). Plant photosynthesis 65 is an enzyme-driven biochemical process that has its own mathematical equation set and 66 67 related parameters (and a large literature; e.g. Farquhar et al., 1980; Medlyn et al. 2002; Smith and Dukes, 2013; Dietze, 2013). Allocation of carbohydrates in the different plant 68 compartments is studied extensively and also has a large literature and mathematical tool set 69 (Friedlingstein et al., 1999; Olin et al., 2015; Merganičová et al., 2019). Plant phenology is 70 71 quantified by specific algorithms that are rather uncertain components of the models 72 (Richardson et al., 2013; Hufkens et al., 2018; Peaucelle et al., 2019). Soil biogeochemistry is driven by microbial and fungal activity and also has its own methodology and a vast literature 73 74 (Zimmermann et al 2007; Kuzyakov, 2011; Koven et al., 2013; Berardi et al., 2020). 75 Emerging scientific areas like the quantification of the dynamics of non-structural carbohydrates (NSC) in plants has a separate methodology that claims for mathematical 76 77 representation in models (Martínez-Vilalta et al., 2016). Simulation of land surface hydrology including evapotranspiration is typically handled by some variant of the Penman-Monteith 78 equation that is widely studied thus represents a separate scientific field (McMahon et al., 79 80 2013; Doležal et al., 2018).

Putting all together, if we are about to construct and further improve a biogeochemical model to consider novel findings and track global changes, we need a comprehensive knowledge that integrates many, almost disjunct scientific fields. Clearly, transparent and well-documented development of a biogeochemical model is of high priority but challenging





85 from the very beginning that claims for cooperation of researchers from various scientific

86 fields.

87 Continuous model development is inevitable but it has to be supported by extensive comparison with observations and some kind of implementation of the model-data fusion 88 approach (Keenan et al., 2011). It is well documented that structural problems might trigger 89 incorrect parameter estimation that might be associated with distorted internal processes 90 91 (Sándor et al., 2017; Martre et al., 2015). In other words, one major issue with BGMs (and in 92 fact with all models using many parameters) is the possibility to get good simulation results for wrong reasons (which means incorrect parameterization) due to compensation of errors 93 (Martre et al., 2015). In order to avoid this issue, any model developer team has to make an 94 effort to focus also internal ecosystem conditions (e.g. soil volumetric water content (SWC), 95 nutrient availability, stresses, etc.) and other processes (e.g. decomposition) rather than the 96 97 main simulated processes (e.g. photosynthesis, evapotranspiration).

98 Historically, biogeochemical models have been developed to simulate the processes of undisturbed ecosystems with simple representation of the vegetation (Levis, 2010). As the 99 100 focus was on the carbon cycle, water and nitrogen cycles and related soil processes were not well represented. Incorrect representation of SWC dynamics is still an issue with the models 101 especially in drought-prone ecosystems (Sándor et al., 2017). Additionally, human 102 103 intervention representation (management) was missing in many cases and it seems that some 104 state-of-the-art BGMs still lack the representation of e.g. thinning, grass mowing, grazing, fertilization, planting or harvest (Table A1 in Friedlingstein et al., 2010). 105

106 In contrast, crop models with different complexity were used for about 50 years or so to simulate the processes of managed vegetation (Jones et al., 2017; Franke et al., 2020). As 107 108 the focus of the crop models is on final yield due to economic reasons, the carbon balance, or the full greenhouse gas balance was not, or was just partially addressed originally. Crop 109 models typically have a sophisticated representation of soil water balance with a multilayer 110 111 soil module that usually calculates plant response to water stress as well. Nutrient stress, soil 112 conditions during planting, consideration of multiple phenological phases, heat stress during anthesis, vernalization, manure application, fertilization, harvest, and many other processes 113 have been implemented during the decades (Ewert et al., 2015). Therefore, it seems to be 114 115 straightforward to exploit the benefits of crop models and implement sound and well-tested algorithms into the BGMs. 116

117 Our group has been developing Biome-BGCMuSo for 15 years. Starting from the 118 well-known Biome-BGC model originally developed to simulate undisturbed forests and





119 grasslands, using a simple single layer soil submodel (Running and Hunt, 1993; Thornton and Rosenbloom, 2005), we developed a complex, more sophisticated model (Hidy et al., 2012; 120 121 2016). Biome-BGCMuSo v4.0 (Biome-BGC with Multilayer Soil module) uses a 7-layer soil module and is capable of simulating different ecosystems from natural grassland to cropland 122 including several management options, taking into account many environmental effects (Hidy 123 et al., 2016). The developments included improvements regarding both soil and plant 124 processes. In a nutshell, the most important, soil related developments were the improvement 125 126 of the soil water balance module by implementing routines for estimating percolation, diffusion, pond water formation and runoff; the introduction of multilayer simulation for 127 belowground processes in a simplified way. The most important, plant related developments 128 involved the implementation of a routine for estimating the effect of drought on vegetation 129 growth and senescence; the improvement of stomatal conductance calculation considering 130 atmospheric CO<sub>2</sub> concentration; the integration of selected management modules; the 131 implementation of new plant compartments (e.g. yield); the implementation of C4 132 photosynthesis routine; the implementation of photosynthesis and respiration acclimation of 133 134 plants and temperature-dependent Q10; and empirical estimation of methane and nitrous 135 oxide soil efflux.

Problems found with the Biome-BGCMuSo v4.0 simulation result (such as the poor representation of soil water content (Hidy et al., 2016; Sándor et al., 2017) or the lack of sophisticated, layer-specific soil nitrogen dynamics representation) and the model structure related problems (such as the lubber parameterization of the model) marked the path for further developments.

The aim of the present study is to provide detailed documentation on the current, improved version of Biome-BGCMuSo v6.2, which has many new features and facilitates various in-depth investigations of ecosystem functioning. Due to large number of developments, this paper focuses only on the soil related model improvements. Case studies are also presented to demonstrate the capabilities of the new model version and to provide guidance for the model user community.

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## 148 2. The original Biome-BGC model

Biome-BGC was developed from the Forest-BGC mechanistic model family in orderto simulate vegetation types other than forests. Biome-BGC was one of the earliest





biogeochemical models that included explicit carbon and nitrogen cycle modules. Biome-BGC simulates the storages and fluxes of water, carbon, and nitrogen within and between the vegetation, litter, and soil components of terrestrial ecosystems. It uses a daily time step, and is driven by daily values of maximum and minimum temperatures, precipitation, solar radiation, and vapor pressure deficit (Running and Hunt, 1993). The model calculations apply to a unit ground area that is considered to be homogeneous.

The three most important components of the model are the phenological, the carbon 157 158 uptake and release, and the soil flux modules. The core logic that is described below in this section remained intact during the developments. The phenological module calculates foliage 159 development that affects the accumulation of C and N in leaf, stem (if present), root and 160 consequently the amount of litter. In the carbon flux module gross primary production (GPP) 161 of the biome is calculated using Farquhar's photosynthesis routine (Farquhar et al., 1980) and 162 163 the enzyme kinetics model based on Woodrow and Berry (2003). Autotrophic respiration is 164 separated into maintenance and growth respiration. Maintenance respiration is calculated as the function of the N content of living plant pools, while growth respiration is an adjustable 165 166 but fixed proportion of the daily GPP. The single-layer soil module simulates the decomposition of dead plant material (litter) and soil organic matter, N mineralization and N 167 balance in general (Running and Gower, 1991). The soil module uses the so-called 168 converging cascade method (Thornton and Rosenbloom, 2005) to simulate decomposition, 169 carbon and nitrogen turnover, and related soil CO<sub>2</sub> efflux. 170

The simulation has two basic steps. During the first (optional) spinup simulation the 171 available climate data series is repeated as many times as it is required to reach a dynamic 172 equilibrium in the soil organic matter content to estimate the initial values of the carbon and 173 nitrogen pools. The second, normal simulation uses the results of the spinup simulation as 174 initial conditions and runs for a given, predefined time period (Running and Gower 1991). So-175 called transient simulation option (which is the extension of the spinup routine) is a novel 176 177 feature in Biome-BGCMuSo in order to ensure smooth transition between the spinup and 178 normal phase (Hidy et al., 2021).

In Biome-BGC, the main parts of the simulated ecosystem are defined as plant, litter and soil. The most important pools include leaf (C, N and intercepted water), root (C, N), stem (C, N), soil (C, N and water) and litter (C, N). Plant C and N pools have sub-pools (actual pools, storage pools and transfer pools). The actual sub-pools store C and N for the current year growth. The storage sub-pools (essentially the non-structural carbohydrate pool, the source for the cores or buds) contain the amount of C and N that will be active during the





next growing season. The transfer sub-pools inherit the entire content of the storage pools at
the end of every simulation year. Soil C also has sub-pools representing various organic
matter forms characterized by considerably different decomposition rates.

In spite of its popularity and proven applicability, the development of Biome-BGC was temporarily stopped (the latest official NTSG version is Biome-BGC 4.2; https://www.ntsg.umt.edu). One major drawback of the model was its relatively poor performance in modelling managed ecosystems, and the simplistic soil water balance submodel using a single soil layer only.

Our team started to develop the Biome-BGC model further in 2006. According to the logic of the team, the new model branch was planned to be the continuation of the Biome-BGC model with regard to the original concept of the developers (keeping the model code open source, providing detailed documentation, and providing support for the users).

197 The starting point of our model development was Biome-BGC v4.1.1 that was a result 198 of the model improvement activities of the Max Planck Institute (Vetter et al., 2007). Development of the Biome-BGCMuSo model branch has a long history by now. Previous 199 200 model developments were documented in Hidy et al. (2012) and Hidy et al. (2016). Below, we provide detailed description of the new developments that are included in Biome-201 BGCMuSo v6.2 which is the latest version released in September, 2021. A comprehensive 202 203 review of the input data requirement of the model together with explanation on the input data structure is available in the User's Guide (Hidy et al., 2021). In this paper we refer to some 204 input files (e.g. soil file, plant file) that are described in the User's Guide in detail. 205

One of the most important novelty and advantage of the new model version (Biome-BGCMuSo v6.2) compared to any previous versions that due to the extensive and detailed soil parameter set (current version has 79, MuSo 4.0 has 39 and original model version has only 6 adjustable soil related parameters) the parameterization of the model is much more flexible. But this might be of course a challenging task to define all of the input parameters. In order to support practical application of the model, the User's Guide contains proposed values for most of the new parameters (Hidy et al., 2021).

### 213 **3. Soil hydrology related developments**

In Biome-BGCMuSo v6.2 a 10-layer soil submodel was implemented. Previous model versions included a 7-layer submodel, which turned out to be insufficient to capture hydrological events like drying of the topsoil layers with sufficient accuracy. The thicknesses





of the layers from the surface to the bottom are 3, 7, 20, 30, 30, 30, 30, 50, 200 and 600 cm. The centre of the given layer represents the depth of each soil layer. Soil texture can be defined by the percentage of sand and silt for each layer separately along with the most important physical and chemical parameters (pH, bulk density, characteristic SWC values, drainage coefficient, hydraulic conductivity) in the soil input file (Hidy et al., 2021).

The water balance module of Biome-BGCMuSo has five major components to describe soil water related processes in daily resolution (listed here following the order of calculation): pond water accumulation and runoff; infiltration and downward gravitational flow (percolation); water potential gradient driven water movement within the soil (diffusion); evaporation and transpiration (root water uptake); and the downward/upward fluxes to/from groundwater. In the following subsections these five major components are described.

#### 228 **3.1 Pond water accumulation and runoff**

Precipitation can reach the surface as rain or snow (below 0 °C snow accumulation is
assumed). Snow water melts from the snowpack as a function of temperature and radiation
and added to the precipitation input.

The canopy can intercept rain. The intercepted volume goes into the *canopy water* pool, which can evaporate. No canopy interception of snow is assumed. The throughfall (complemented with the amount of melted snow) gives the potential infiltration.

Important novelty of Biome-BGCMuSo v6.2 is that maximum infiltration is calculated 235 236 based on the saturated hydraulic conductivity and the SWC of the top soil layers. If the potential infiltration exceeds the maximum infiltration, pond water can be formed. If the sum 237 of the precipitation and the actual pond height minus the maximum infiltration rate is greater 238 than the maximum pond height, the excess water is added to surface runoff detailed below 239 (Balsamo et al., 2009). The maximum pond height is an input parameter. Water from the pond 240 241 can infiltrate into the soil at a rate the top soil layer can absorb it. Evaporation of the pond water is assumed equal to the potential evaporation. 242

Surface runoff is the water flow occurring on the surface when a portion of the precipitation cannot infiltrate into the soil. Two types of surface runoff processes can be distinguished: Hortonian and Dunne. Hortonian runoff is unsaturated overland flow that occurs when the rate of precipitation exceeds the rate at which water can infiltrate. The other type of surface runoff is the Dunne runoff (also known as the saturation overland flow) which occurs when the entire soil is saturated but the rain continues to fall. In this case the rainfall immediately triggers pond water formation and (above the maximum pond water height)





surface runoff. The handling of these processes is presented in the soil hydrological module of

- 251 Biome-BGCMuSo v6.2.
- Calculation of Hortonain runoff (in kg  $H_2O \text{ m}^{-2} \text{ day}^{-1}$ ) is based on a semi-empirical method and uses the precipitation amount (in cm day<sup>-1</sup>), the unitless runoff curve number (*RCN*), and the actual moisture content status of the topsoil (Rawls et al., 1980; this method is known as the SCS runoff curve number method). This type of runoff simulation can be turned off by setting *RCN* to zero. The detailed description can be found in the Supplementary material, Section 1. The amount of runoff as a function of the soil type and the actual SWC is presented in Figure 1.



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Figure 1: Hortonian runoff as the function of rainfall intensity, soil type and actual soil water content of the top soil layer. Sand soil means 92% sand, 4% silt and 4% clay; silt soil means 8% sand, 86% silt and 6% clay; clay soil means

262 20% sand, 20% silt and 60% clay. SWC means soil water content; SAT means saturation.

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#### 264 **3.2 Infiltration, percolation and diffusion**

There are two optional methods in Biome-BGCMuSo v6.2 to calculate soil water movement between soil layers and actual SWC layer by layer. The first one is a cascade method (also known as tipping bucket method), and the second is a Richards equation based physical method. The tipping bucket method has a long history in crop modelling and is considered as a successful, well-evaluated algorithm that can accurately simulate downward water flow in the soil.

The cascade method uses a semi-empirical input parameter (DC: drainage coefficient 271 in day<sup>-1</sup>) to calculate downward water flow rate. When the SWC of a soil layer exceeds field 272 capacity (FC), a fraction (equal to DC) of the water amount above FC goes to the layer next 273 below. If DC is not set in the soil input file, it is estimated from the saturated hydraulic 274 conductivity:  $DC = 0.1122 \cdot K_{SAT}^{0.339}$  ( $K_{SAT}$ : saturated hydraulic conductivity in cm day<sup>-1</sup>; 275 the user can set its value or the model based on soil texture estimates it internally; see Hidy et 276 al., 2016). The detailed description of the method can be found in the Supplementary material, 277 Section 2. Drainage from the bottom layer is a net loss for the soil profile. 278

Water diffusion that is the capillary water flow between the soil layers is calculated to account for the relatively slow movement of water. The flow rate is the function of the water content difference of two adjacent layers and the soil water diffusivity at the boundary of the layers, which is determined based on the average water content of the two layers. The detailed mathematical description of the method can be found in the Supplementary material, Section 3.

The detailed description of the Richards method can be found in Hidy et al. (2012). To support efficient and robust calculations of soil water fluxes a dynamically changing time step was introduced in version 4.0 (Hidy et al., 2016). An enhancement of this method in Biome-BGCMuSo v6.2 is the finer vertical discretisation of the soil profile that is used during the numerical solution of the equation. The implementation of the Richards-equation is still in an experimental phase requiring rigorous testing and validation in the future.

## 291 **3.3 Evapotranspiration**

Biome-BGCMuSo, such as its predecessor Biome-BGC, estimates evaporation of leaf intercepted water, bare soil evaporation, and transpiration to estimate the total evapotranspiration in a daily level. The potential rates of all three processes are calculated based on the Penman-Monteith (PM) method. PM equation requires net radiation (minus soil





heat flux) and conductance values by definition using different parameterization for the different processes. The model calculates leaf- and canopy-level conductances of water vapour and sensible heat fluxes, to be used in Penman-Monteith calculations of canopy evaporation and canopy transpiration. Note that in the Biome-BGC model family the direct wind effect is ignored but can be considered indirectly by adjusting boundary layer conductance to site-specific conditions. A possible future direction might be the extension of the model logic to consider wind effect directly.

#### 303 *3.3.1 Canopy evaporation*

304 If there is intercepted water, this portion of evaporation is calculated using the canopy 305 resistance (reciprocal of conductance) to evaporated water and the resistance to sensible heat. 306 The time required for the water to evaporate based on the average daily conditions is calculated, and subtracted from the day length to get the effective day length for 307 evapotranspiration. Combined resistance to convective and radiative heat transfer is calculated 308 based on canopy conductance of vapour and leaf conductance of sensible heat both of which 309 are assumed to be equal to the boundary layer conductance. Besides the 310 conductance/resistance parameters the canopy absorbed shortwave radiation drives the 311 calculation. Note that the canopy evaporation routine was not modified significantly in 312 313 Biome-BGCMuSo.

#### 314 *3.3.2 Soil evaporation*

In order to estimate soil evaporation, first the potential evaporation is calculated, 315 assuming that the resistance to vapour is equal to the resistance to sensible heat and assuming 316 no additional resistance component. Both resistances are assumed to be equal to the actual 317 aerodynamic resistance. Actual aerodynamic resistance is the function of the actual air 318 pressure and air temperature and the potential aerodynamic resistance ( $potR_{air}$  in s m<sup>-1</sup>). 319  $potR_{air}$  was a fixed value in the previous model versions (107 s m<sup>-1</sup>). Its value was derived 320 from observations over bare soil in tiger-bush in south-west Niger (Wallace and Holwill, 321 322 1997). In Biome-BGCMuSo v6.2, the  $potR_{air}$  is an input parameter that can be adjusted by the user (Hidy et al., 2021). Another new development in Biome-BGCMuSo v6.2 is the 323 324 introduction of an upper limit for daily potential evaporation  $(evap_{limit})$  that is determined by the available energy (incident shortwave flux that reaches the soil surface): 325

$$326 \quad evap_{limit} = \frac{irad \cdot dayl}{LH_{vap}} \tag{1}$$





(3)

where *irad* is the incident shortwave flux density in W m<sup>-2</sup>, *dayl* is the length of the day in seconds,  $LH_{vap}$  is the latent heat of vaporization (the amount of energy that must be added to liquid to transform into gas) in J kg<sup>-1</sup>. This feature was missing from previous model versions resulting in considerable overestimation of evaporation on certain days that was caused by the missing energy limitation on evaporation.

An important novelty in Biome-BGCMuSo v6.2 is the calculation of the actual evaporation from the potential evaporation and the square root of time elapsed since the last precipitation (expressed by days; Ritchie, 1998). This is another method that has been used by the crop modeller community for many years. Detailed description of the algorithm can be found in the Supplementary material, Section 4.

A major novel feature in Biome-BGCMuSo v6.2 is the simulation of the reducing effect of surface residue or mulch cover on bare soil evaporation. Here we use the term 'mulch' to quantify surface residue cover in general keeping in mind that mulch is typically a human-induced coverage. Surface residue includes aboveground litter and coarse woody debris as well.

342 The evaporation reduction effect (evapREDmulch; unitless) is a variable between 0 and 1 (0 means full limitation, and 1 means no limitation) estimated based on a power 343 344 function of the surface coverage (*mulchCOV* in %) and a soil specific constant set by the user (pREDmulch; see Hidy et al., 2021). If variable mulchCOV reaches 100% it means that the 345 346 surface is completely covered. If *mulchCOV* is greater than 100% it means the surface is covered by more than one layers. Surface coverage is a power function of the amount of 347 mulch (*mu* in kgC m<sup>-2</sup>) with parameters  $p1_{mulch}$ ,  $p2_{mulch}$ , and  $p3_{mulch}$  (soil parameters) based 348 on the method of Rawls et al. (1991): 349

350

351 
$$mulchCOV = p1_{mulch} \cdot (mu/p2_{mulch})^{p3_{mulch}}$$
 (2)

$$352 \quad evapREdmulch = pREDmulch \frac{mulchCOV}{100}$$

Another simulated effect of surface residue cover is the homogenization of soil temperature between 0 and 30 cm depth (layers 1, 2 and 3). The functional forms of surface coverage and evaporation reduction factor are presented in Figure 2.







356

Figure 2: Surface coverage as a function of the amount of surface residue or mulch (upper plot) and the evaporation
 reduction factor (evapREDmulch) as the function of mulch coverage (lower plot) using different mulch specific soil
 parameters (pREDmulch). See text for details.

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#### 361 *3.3.3 Transpiration*

In order to simulate transpiration, first transpiration demand (TD in kg H<sub>2</sub>O m<sup>-2</sup> day<sup>-1</sup>) is calculated using the Penman-Monteith equation separately for sunlit and shaded leaves. TDis the function of leaf-scale conductance to water vapor, which is derived from stomatal, cuticular and leaf boundary layer conductances. A novelty in Biome-BGCMuSo v6.2 is that potential evapotranspiration is also calculated using the maximal stomatal conductance instead of the actual stomatal conductance, which means that stomatal aperture is not affected by the soil moisture status (in contrast to the actual one).

*TD* is distributed across the soil layers according to the actual root distribution using an improved method (the logic was changed since Biome-BGCMuSo v4.0). From the plant specific root parameters and the actual root weight Biome-BGCMuSo calculates the number of the layers where roots can be found together with the root mass distribution across the layers. If there is not enough water in a given soil layer to fulfil the transpiration demand, the transpiration flux from that layer is limited, and below wilting point (WP) it is set to zero. The sum of layer-specific transpiration fluxes across the root zone gives the actual transpiration





376 flux. The detailed description of the algorithm can be found in the Supplementary material,

377 Section 5.

## 378 **3.4 Effect of groundwater**

Simulation of groundwater effect was introduced in Biome-BGCMuSo v4.0 (Hidy et al., 2016), but the method has been significantly improved, and the new algorithm it is now available in Biome-BGCMuSo v6.2. In the recent model version there is an option to provide an additional input file with the daily values of the groundwater table depth (*GW depth* in m).

Groundwater may affect soil hydrological and plant physiological processes if the water table is closer to the root zone than the thickness of the capillary fringe (that is the region saturated from groundwater via capillary effect). The thickness of the capillary fringe (*CF* in m) is estimated using literature data and depends on the soil type (Johnson and Ettinger model; Tillman and Weaver, 2006). Groundwater table distance (*GWdist* in m) for a given layer is defined as the difference between *GWdepth* and the depth of the midpoint of the layer.

390 The layers completely below the groundwater table are assumed to be fully saturated. In case of layers within the capillary fringe (GWdist < CF), the calculation of water balance 391 changes: the field capacity rises, thus the difference between saturation (SAT) and FC 392 decreases and the layer charges gradually, till the increased FC value is reached. The FC-393 rising effect of groundwater for the layers above the water table is calculated based on the 394 395 ratio of the groundwater distance and the capillary fringe thickness, but only after the water 396 content of the layers below have reached their modified FC values. Detailed description of the groundwater effect can be found in Supplementary material, Section 6. 397

#### 398 **3.5 Soil moisture stress**

In the original Biome-BGC model the effect of changing soil water content on photosynthesis and decomposition of soil organic matter is expressed in terms of soil water potential ( $\Psi$ ). Instead of  $\Psi$ , the volumetric SWC is also widely used to calculate the limitation of stomatal conductance and decomposition. A practical advantage of using SWC as a factor in stress function is that it is easier to measure in the field and the changes of the driving function are much smoother than in case of  $\Psi$ . The disadvantage is that SWC is not comparable among different soil types (in contrast to  $\Psi$ ).





The maximum of SWC is the saturation value; the minimum is the wilting point or the hygroscopic water depending on the type of the simulated process. Novelty of Biome-BGCMuSo v6.2 is that the hygroscopic water, the wilting point, the field capacity and the saturation values are calculated internally by the model based on the soil texture data, or can be defined in the input file layer by layer.

In Biome-BGCMuSo v6.2 the so-called soil moisture stress index (SMSI) is calculated 411 to represent overall soil stress conditions. SMSI is affected by the length of the drought event 412 413 (SMSE: extent of soil stress), the severity of the drought event (SMSL: length of soil stress), aggravated by the extreme temperature (extremT: effect of extreme heat). SMSI is equal to 414 415 zero if no soil moisture limitation occurs and equal to 1 in case of full soil moisture limitation. SMSI is used by the model for plant senescence calculations (presentation of plant related 416 417 processes is the subject of a forthcoming publication)). The members of SMSI are explained detailed below. 418

419

420  $SMSI = 1 - SMSE \cdot SMSL \cdot extremT$ 

(4)

421 Magnitude of soil moisture stress (*SMSE*) is calculated layer by layer based on SWC. 422 Regarding soil moisture stress two different processes are distinguished: drought (i.e. low 423 SWC close to or below WP) and anoxic condition (i.e. after large precipitation events or in 424 the presence of high groundwater table; Bond-Lamberty et al., 2007). An important novelty of 425 Biome-BGCMuSo v6.2 is the soil curvature parameters (q) which is introduced to provide 426 mechanism for soil texture dependent drought stress as it can affect the shape of the soil stress 427 function (which means possibility for non-linear ramp function):

428

429 
$$SMSE^{i} = 0$$
 ;  $SWC^{i} < SWC_{WP}^{i}$   
430  $SMSE^{i} = \left(\frac{SWC^{i} - SWC_{WP}^{i}}{SWC_{drought}^{i} - SWC_{WP}^{i}}\right)^{q}$  ;  $SWC_{WP}^{i} \le SWC < SWC_{drought}^{i}$  (5)  
431  $SMSE^{i} = 1$  ;  $SWC_{drought}^{i} \le SWC \le SWC_{anoxic}^{i}$ 

432 
$$SMSE^{i} = \frac{SWC_{SAT}^{i} - SWC^{i}}{SWC_{SAT}^{i} - SWC_{anoxic}^{i}}$$
;  $SWC^{i} > SWC_{anoxic}^{i}$ 

where q is the curvature of soil stress function, SWC<sup>i</sup><sub>drought</sub> and SWC<sup>i</sup><sub>anoxic</sub> are critical SWC
values for calculating soil stress.
In order to make the SWC values comparable between different soil types,

436  $SWC_{drought}^{i}$  and  $SWC_{anoxic}^{i}$  can be set in normalized form (such as in Eq. 4)) as part of the





- ecophysiological parameterization of the model. More details about the adjustment of thecritical SWC values can be found in Hidy et al. (2021).
- 439 The layer specific soil moisture stress extent values are summed across the root zone 440 using the relative amount of roots in the layers ( $RP^{i}$ ) as weighting factors to obtain the overall 441 soil moisture stress extent (*SMSE*):

442 
$$SMSE = \sum_{i=0}^{i=nr} SMSE^i \cdot RP^i$$
 (6)

443 
$$RP^{i} = RD \frac{z^{i}}{RL} \cdot e^{-RD \cdot (mid^{i}/RL)}$$
(7)

where nr is the number of the soil layers where roots can be found, RL is the actual length of 444 445 roots, RD is rooting distribution parameter (ecophysiological parameter; see details in the User's Guide; Hidy et al., 2021). In the current model version SMSE can also affect the entire 446 photosynthetic machinery by the introduction of an empirical parameter. This mechanism is 447 448 responsible to account for the non-stomatal effect of drought on photosynthesis (details about this algorithm will be published in a separate paper). Since there is no mechanistic 449 450 representation behind this empirical down-regulation of photosynthesis, further test are needed for the correct setting of this parameter using preferentially eddy covariance data. 451

452 The soil moisture stress length related factor (SMSL) is the ratio of the critical soil moisture stress length (ecophysiological parameter) and the sum of the daily (1 - SMSE)453 values. This cumulated value restarts if SMSE is equal to one (no stress). Extreme heat 454 (extremT) is also considered and is taken into account in the final stress function (see above) 455 by using a ramp function. Its parameterization thus requires the setting of two critical 456 temperature limits that defines the ramp function (set by the ecophysiological 457 parameterization; see Hidy et al., 2021). Its characteristic temperature values can be set by 458 459 parameterization (ecophysiological input file).

### 460 **4. Soil carbon and nitrogen cycles**

#### 461 **4.1 Soil-litter module**

We made substantial changes in the soil biogeochemistry module of the Biome-BGC model. Previous model versions already offered solutions for multilayer simulations (Hidy et al., 2012, 2016), but some pools still inherited the single-layer logic of the original model. In the new model version all relevant soil processes are separated layer by layer which is a major step forward.





467 Instead of defining a single litter, soil organic carbon (SOC) and nitrogen pool, we implemented separate carbon and nitrogen pools for each soil layer in the form of soil organic 468 469 matter (SOM) and litter in Biome-BGCMuSo v6.2. The changes of the mass of the carbon and nitrogen pools are calculated layer by layer. Mortality fluxes (whole plant mortality, 470 senescence, litterfall) of aboveground plant material are transferred into the litter pools of the 471 top soil layers (0-10 cm, layers 1-2). Mortality fluxes of belowground plant material are 472 transferred into the corresponding soil layers based on their location within the root zone. Due 473 474 to ploughing and leaching, carbon and nitrogen can also be relocated to deeper layers. The 475 plant material turning into the litter compartment is divided between the different types of litter pools (labile, unshielded cellulose, shielded cellulose and lignin) according to the 476 parameterization. Litter and soil decomposition fluxes (carbon and nitrogen fluxes from litter 477 to soil pools) are calculated layer by layer, depending on the actual temperature and SWC of 478 479 the corresponding layers. Vertical mixing of soil organic matter between the soil layers (e.g. 480 bioturbation) is not implemented in the current model version.

Figure 3 shows the most important simulated soil and litter processes. N-fixation (Nf) 481 482 is the N input from the atmosphere to soil layers in the root zone by microorganisms. The user can set its annual value as an input parameter. N-deposition (Nd) is the N input from the 483 484 atmosphere to the top soil layers (see below). The user can set its annual value as a sitespecific parameter in the initialization input file. Nitrogen deposition can be provided by 485 486 annually varying values as well. Plant uptake (PU) is the absorption of mineral N by plants from the soil layers in the root zone. Mineralization (MI) is the release of plant-available 487 488 nitrogen (flux from soil organic matter to mineralized nitrogen). Immobilization (IM) is the consumption of inorganic nitrogen by microorganisms (flux from mineralized nitrogen to soil 489 490 organic matter). Nitrification (NI) is the biological oxidation of ammonium to nitrate through 491 nitrifying bacteria. Denitrification (DN) is a microbial process where nitrate  $(NO_3)$  is reduced and converted to nitrogen gas  $(N_2)$  through intermediate nitrogen oxide gases. Leaching (L) is 492 the loss of water-soluble mineral nitrogen from the soil layers. If leaching occurs in the 493 lowermost soil layer that means loss of N from the simulated system. Litterfall (Ll) is the 494 plant material transfer from plant compartments to litter. Decomposition is the C and N 495 transfer from litter to soil pools and between soil pools. In case of woody vegetation coarse 496 woody debris (CWD) contains the woody plant material after litterfall before physical 497 498 fragmentation. Litter has also four sub-pools based on their composition: labile (L1), unshielded and shielded cellulose (L2, L3) and lignin (L4). Soil organic matter has also four 499





- sub-pools based on their turnover rate: labile (S1), medium (S2), slow (S3) and passive
- 501 (recalcitrant; S4) SOM pool. Soil mineralized nitrogen pool contains the inorganic N-forms of
- 502 the soil: ammonium and nitrate.



503

504Figure 3: Soil and litter related simulated carbon/nitrogen fluxes (arrows) and pools (rectangles) in Biome-BGCMuSo505v6.2. HR: heterotrophic respiration, IM: immobilization, MI: mineralization, PU: plant uptake, LI: litterfall, NI:506nitrification, D: decomposition ( $D_L$ : decomposition of litter,  $D_S$ : decomposition of SOM,  $D_C$ : fragmentation of coarse507woody debris), L: leaching, Nf: nitrogen fixation, Nd: nitrogen deposition, DN: denitrification. L represents loss of C508and N from the simulated system.

509

## 510 4.2 Decomposition

511 In the decomposition module (i.e. converging cascade scheme; Thornton, 1998) the 512 fluxes between litter and soil pools are calculated layer by layer. The potential fluxes are 513 modified in case of N limitation when the potential gross immobilization is greater than the 514 potential gross mineralization.

515 To explain the decomposition processes implemented in Biome-BGCMuSo v6.2 the 516 main carbon/nitrogen pools and fluxes between litter and soil organic and inorganic 517 (mineralized) matter are presented on Figure 4.







518

519Figure 4: Overview of the converging cascade model of litter and soil organic matter decomposition that is520implemented in Biome-BGCMuSo v6.2. rf represents the respiration fraction of the different transformation fluxes,  $\tau$ 521is the residence time (reciprocal of the rate constants that is the turnover rate), IM/MI: immobilization/mineralization522fluxes, HR: heterotrophic respiration. Note that both the respiration fraction and the turnover rate parameters can be523adjusted through parameterization.

524

525

526 For the calculation of nitrogen mineralization first respiration cost (respiration 527 fraction) is estimated. Mineralization than is the function of the remaining part of the pool and its C:N ratio. The nitrogen mineralization fluxes of the SOM pools are functions of the 528 529 potential rate constant (reciprocal of residence time), and the integrated response function that accounts for the impact of multiple environmental factors. The integrated response function of 530 531 decomposition is a product of the response functions of depth, soil temperature and SWC  $(F_r(d)_{D_r}, F_r(T)_{D_r}, F_r(SWC)_{D_r})$ ; Figure 5). Its detailed description can be found in the 532 533 Supplementary material, Section 7. The dependence of the three different factors on depth, temperature and SWC with default parameters are presented in Figure 5. 534







535

Figure 5: The dependence of the individual factors that form the complex environmental response function of decomposition on depth  $(Fr(d)_D)$ , temperature  $(Fr(T)_D)$  and SWC in case of different soil types  $(Fr(SWC)_D)$ . ED is the e-folding depth which is one of the adjustable soil parameters of the model. Sand soil means 92% sand, 4% silt and 4% clay; silt soil means 8% sand, 86% silt and 6% clay; clay soil means 20% sand, 20% silt and 60% clay.

540

#### 541 4.3 Soil nitrogen processes

In Biome-BGCMuSo v6.2 separate ammonium (*sNH4*) and nitrate (*sNO3*) soil pools
are implemented instead of a general mineralized nitrogen pool. This was a necessary step for





the realistic representation of many internal processes like plant nitrogen uptake, nitrification,
denitrification, consideration of the effect of different mineral and organic fertilizers and N<sub>2</sub>O
emission.

It is important to introduce the *availability* concept that Biome-BGCMuSo uses and is associated with the ammonium and nitrate pools. We use the logic proposed by Thomas et al. (2013) which means that the plant has access only to a part of the given inorganic nitrogen pool. Unavailable part is buffered as it is associated with soil aggregates and is unavailable for plant uptake. The available part of ammonium is calculated based on  $NH_4$  mobilen proportion (that is a soil parameter set to 10% according to Thomas et al., 2013; Hidy et al., 2021) and the actual pool. The available part of nitrate is assumed to be 100%.

The amount of ammonium and nitrate are determined layer by layer controlled by input and output fluxes (F in kg N m<sup>-2</sup> day<sup>-1</sup>) listed below:

556 
$$F_{sNH4}^{i} = IN_{sNH4}^{i} - L_{sNH4}^{i} + L_{sNH4}^{i-1} - PU_{sNH4}^{i} - IM_{sNH4}^{i} + MI_{sNH4}^{i} - NI_{sNH4}^{i}$$
(8)

557 
$$F_{sN03}^{i} = IN_{sN03}^{i} - L_{sN03}^{i} + L_{sN03}^{i-1} - PU_{sN03}^{i} - IM_{sN03}^{i} + MI_{sN03}^{i} - DN_{sN03}^{i}$$
(9)

where  $IN_{sNH4}^{i}$  and  $IN_{sNO3}^{i}$  are the input fluxes to the ammonium and nitrate pools, respectively;  $L_{sNH4}^{i}$ ,  $L_{sNH4}^{i-1}$ ,  $L_{sNO3}^{i}$ ,  $L_{sNO3}^{i-1}$  are the amount of leached mineralized ammonium and nitrate from a layer (*i*) or from the upper layer (*i*-1), respectively;  $PU_{sNH4}^{i}$  and  $PU_{sNO3}^{i}$  are the plant uptake fluxes of ammonium and nitrate, respectively;  $IM_{sNH4}^{i}$  and  $IM_{sNO3}^{i}$  are the immobilization fluxes of ammonium and nitrate, respectively;  $MI_{sNH4}^{i}$  and  $MI_{sNO3}^{i}$  are the mineralization fluxes of ammonium and nitrate, respectively;  $NI_{sNH4}^{i}$  and  $MI_{sNO3}^{i}$  are the mineralization fluxes of ammonium and nitrate, respectively;  $NI_{sNH4}^{i}$  is the nitrification flux of ammonium and  $DN_{sNO3}^{i}$  is the denitrification flux of nitrate.

565 In the following subsections the different terms of the equations are described in 566 detail.

567 Input to the sNH4 and sNO3 pools (IN in Eq. 6 and 7)

According to the model logic N-fixation occurs in the root zone layers. Its distribution between sNH4 and sNO3 pools is calculated based on their actual available proportion in the actual layer ( $NH4prop^i$ ):

571  $NH4prop^{i} = sNH4avail^{i} + sNO3avail^{i}$  (10)

where *sNH4avail<sup>i</sup>* and *sNO3avail<sup>i</sup>* are the available part of the sNH4 and sNO3 pools in the
actual layer.

N-deposition related nitrogen input is associated with the 0-10 cm soil layers assuming
uniform distribution across layers 1-2 in the model, and the distribution between sNH4 and





576	sNO3 pools is calculated based on the proportion of NH <sub>4</sub> flux of N-deposition soil parameter
577	(Hidy et al., 2021).
578	Organic and inorganic fertilization is also an optional nitrogen input. The amount and
579	composition $(NH_4^+ \text{ and } NO_3^- \text{ content})$ can be set in the fertilization input file.
580	
	Loophing downword movement of minoralized N (Lin Eq. ( and 7)
581	Leaching - downward movement of mineralized N (L in Eq. 6 and 7)
582	The amount of leached mineralized N (mobile part of the given N pool) from a layer is
583	directly proportional to the amount of drainage and the available part of the sNH4 and sNO3
584	pools. Leaching from the layer above is a net gain, while leaching from actual layer is a net
585	loss for the actual layer. Leaching is described in Section 4.5.
586	
587	Plant uptake by roots (PU in Eq. 6 and 7)
588	N uptake required for plant growth is estimated in the photosynthesis calculations and
589	the amount is distributed across the layers in the root zone. The partition of the N uptake
590	between sNH4 and sNO3 pools is calculated based on their actual available proportion in each
591	layer.
592	
593	Mineralization and immobilization (MI and IM Eq. 6 and 7)
594	Mineralization and immobilization calculations are detailed in Section 4.2. The
595	distribution of these N fluxes between sNH4 and sNO3 pools is calculated based on their
596	actual available proportion in each layer.
597	
598	Nitrification (NI Eq. 6 and 7)
599	Nitrification is a function of the soil ammonium content, the net mineralization and the
600	response functions of temperature, soil pH and SWC $(F_r(pH)_{NI}, F_r(T)_{NI})$ , and $F_r(SWC)_{NI}$ ,
601	respectively) based on the method of Parton et al. (2001) and Thomas et al. (2013). Its
602	detailed mathematical description can be found in the Supplementary material, Section 8. The
603	response functions with proposed parameters are shown in Figure 6.







(11)



604

Figure 6: The dependence of the individual factors of the environmental response function of nitrification on soil pH  $(F_r(pH)_{NI})$ , temperature  $(F_r(T)_{NI})$  and SWC  $F_r(SWC)_{NI}$  in case of different soil types. pH and temperature response functions are independent of the soil texture.

608

## 609 Denitrification (DN Eq. 6 and 7)

610 Denitrification flux is estimated with a simple formula (Thomas et al., 2013):

611  $DN^{i} = DNcoeff \cdot SOMresp^{i} \cdot sNO3avail^{i} \cdot WFPS^{i}$ 

612 where DN of the actual layer is the product of the available nitrate content (sN03avail in

 $kg N m^{-2}$ ), *SOMresp<sup>i</sup>* in g C m<sup>-2</sup> day<sup>-1</sup> is the SOM decomposition related respiration cost, the

614  $WFPS^i$  is the water-filled pore space and DNcoeff is the soil respiration related

615 *denitrification rate* in g  $C^{-1}$ , which is an input soil parameter (Hidy et al., 2021). The unitless





- water-filled pore space is the ratio of the actual and the saturated SWC. SOM decomposition
  associated respiration is the sum of the heterotrophic respiration fluxes of the four soil
  compartments (S1-S4, Figure 4.).
- 619

## 620 4.4 N<sub>2</sub>O-emission and N-emission

621

622During both nitrification and denitrification  $N_2O$ -emission occurs which (added to the623 $N_2O$ -flux originated from grazing processes if applicable) contributes to the total  $N_2O$ -624emission of the examined ecosystem.

In Biome-BGCMuSo v6.2 a fixed part (set by the *coefficient of*  $N_2O$  *emission of nitrification* input soil parameter; Hidy et al., 2021) of nitrification flux is lost as N<sub>2</sub>O and not converted to NO<sub>3</sub>.

During denitrification, nitrate is transformed into  $N_2$  and  $N_2O$  gas depending on the environmental conditions:  $NO_3$  availability, total soil respiration (proxy for microbial activity), SWC and pH. The *denitrification related*  $N_2/N_2O$  *ratio* input soil parameter is used to represent the effect of the soil type on the  $N_2/N_2O$  ratio (del Grosso et al., 2000; Hidy et al., 2021). Detailed mathematical description of the algorithm can be found in the Supplementary material, Section 9.

634

#### 635 4.5 Leaching of dissolved matter

Leaching of nitrate, ammonium, and dissolved organic carbon and nitrogen (DOC and 636 DON) content from the actual layer is calculated as the product of the concentration of the 637 dissolved component in the soil water and the amount of water (drainage plus diffusion) 638 leaving the given layer either downward or upward. The dissolved component (concentration) 639 of organic carbon is calculated from the SOC pool contents and the corresponding fraction of 640 dissolved part of SOC soil parameters. The dissolved component of organic nitrogen content 641 of the given soil pool is calculated from the carbon content and the corresponding C:N ratio. 642 The downward leaching is net loss from the actual layer and net gain for the layer next below; 643 644 the upward flux is net loss for the actual layer and net gain for the layer next up. The downward leaching of the bottom active layer (9<sup>th</sup>) is net loss for the system. The upward 645 movement of dissolved substance from the passive (10<sup>th</sup>) layer is net gain for the system. 646





# 647 5. Case studies

#### 648 5.1 Evaluation of soil hydrological simulation

In order to evaluate the functioning of the new model version (and to compare 649 simulation results made by the current and the previously published model version), a case 650 study is presented regarding soil water content and soil evaporation simulations. The results 651 of a bare soil simulation (i.e. no plant is assumed to be present) are compared to observation 652 data of a weighing lysimeter station installed at Martonvásár, Hungary (47°18'57.6"N, 653 654 18°47'25.6"E) in 2017. The station consists of twelve 2 meter deep scientific lysimeter columns with 1 m diameter (Meter Group Inc., USA) with soil temperature, SWC and soil 655 656 water potential sensors installed at 5, 10, 30, 50, 70, 100 and 150 cm depth. Observation data for 2020 from six columns without vegetation cover (i.e. bare soil) was used to validate the 657 658 model.

Raw lysimeter observation data were processed using standard methods. Bare soil 659 660 evaporation values were derived based on changes of the mass of the soil columns also considering the mass change of the drainage water. Additionally, experience has shown that 661 wind speed is related to the high frequency mass change of the soil column mass. To reduce 662 663 noise, 5-point (5-min) moving averages were used based on Marek et al. (2014). After quality control of the data, the corrected and smoothed lysimeter mass values were used for the 664 calculations. SWC observations were averaged to daily resolution to match the time step of 665 the model. 666

667 Observed local meteorology was used to drive the models for year 2020. Soil physical 668 model input parameters (field capacity, wilting point, bulk density, etc.) were determined in 669 the laboratory using 100 cm<sup>3</sup> undisturbed soil samples taken from various depths during the 670 installation of the lysimeter station. Regarding other soil parameters the proposed values were 671 used. Detailed description of the input soil parameters and their proposed values are presented 672 in the User's Guide (Hidy et al., 2021).

In Figure 7 the simulated and the observed time series of soil evaporation are presented for Martonvásár, for 2020. The figure shows that the soil evaporation simulation by v6.2 is more realistic than by v4.0. Biome-BGCMuSo v4.0 provides very low values during summer in some days which is not in accordance with the observations. Biome-BGCMuSo v6.2 provides more realistic values during this time period.

25







Figure 7: The simulated (blue line: v4.0; red line: v6.2) and the observed (grey dots) daily soil evaporation values at
 Martonvásár during 2020. Vertical grey lines associated with the observations represent standard deviation of the
 observation from 6 columns. The improved model clearly outperforms the earlier version.

683

678

In Figure 8 the simulated and the observed SWC at 10 cm depth are presented with the 684 685 daily sum of precipitation representing the bare soil simulation in Martonvásár, for 2020. The soil water balance simulation seems to be realistic using v6.2, since the annual course 686 captures the low and high end of the observed values. In contrast, Biome-BGCMuSo v4.0 687 underestimates the range of SWC and provides overestimations during the growing season 688 (from spring to autumn). With a couple of exceptions, the simulated values using v6.2 fall 689 into the uncertainty range of the measured values defined by the standard deviation of the six 690 691 parallel measurements. This is not the case for the simulations with the 4.0 version.







692

Figure 8: The simulated (blue line: v4.0; red line: v6.2) and the observed (gray dots) soil water content values at 10 cm
 depth (right y axis) with the daily sums of precipitation (left axis; black columns) during 2020 at Martonvásár
 lysimeter station. Vertical grey lines associated with the observations represent +/- one standard deviation of the
 observation. Simulated SWC using v6.2 is more consistent with the observations than using v4.0.



698

Figure 9: Comparison of the simulated (left: v4.0; right: v6.2) and observed daily soil evaporation (right) representing
 the means of measured data obtained from six weighing lysimeter columns with bare soil at Martonvásár in 2020. R<sup>2</sup>,
 MAE and MSE denote the square of the linear correlation coefficient, mean absolute error and mean signed error
 (bias) of the simulated values, respectively.

703 704

Model performance was evaluated by quantitative measures such as square of linear correlation coefficient ( $R^2$ ), mean absolute error (MAE) and mean signed error (MSE). In Figure 9 the comparison of the simulated and the observed daily evaporation is presented.





- Based on the performance indicators it is obvious that the simulation with new model version
  (v6.2) is much closer to observations than the old version (v4.0). Biome-BGCMuSo v6.2
  slightly underestimated the observations.
- In Figure 10 the comparison of the simulated and the observed daily SWC from the lysimeter experiment is presented. Based on the model evaluation it seems that the simulation with new model version is much closer to observation than with old version (4.0). The results obtained from v4.2 are consistent with earlier findings about the incorrect representation of the annual SWC cycle (Hidy et al., 2016; Sándor et al., 2017).
- Throughout validation of the improved model based on observed SWC and ETdatasets from eddy covariance sites is under way.
- 718



Figure 10: Comparison of the simulated (left: v4.0; right: v6.2) and observed daily SWC representing the means of
 measured data obtained from six weighing lysimeter columns with bare soil at Martonvásár in 2020. R<sup>2</sup>, MAE and
 MSE denote the square of the linear correlation coefficient, mean absolute error and mean signed error (bias) of the
 simulated values, respectively.

725

719

### 726 5.2 Sensitivity analysis and optimization of the soil biogeochemistry scheme

727

Here we present another case study that provides insight into the functioning of the converging cascade scheme that is implemented in Biome-BGCMuSo v6.2. A large scale experiment is also presented where the main aim was to perform model self-initialization (i.e. spinup) at the country scale (for the entire area of Hungary) where the resulting soil organic matter pools are expected to be consistent with the observations.





733 The observation based, gridded, multi-layer SOC database of Hungary (DOSoReMI database; Pásztor et al., 2020) as well as the FORESEE meteorological database (Kern et al., 734 735 2016) was used for the sensitivity analysis of the soil scheme as well as for optimizing the most important soil parameters referring to SOC simulation. As a first step, the area of the 736 country was divided into 1104 grid cells (regular grid with 0.1° by 0.1° resolution). The 1104 737 grid cells of the DOSoReMI database were grouped based on their dominant land-use type 738 (cropland, grassland, forest based on CORINE-2012 database; EEA, 2021) as well as the soil 739 texture class (12 classes according to the USDA system; USDA, 1987) and SOC content (high 740 741 and low; high is greater than the group mean while low is less than the mean) of the topsoil (0-30 cm layer). As some of the theoretically possible 72 groups had no members (e.g. there is 742 no soil in Hungary with sandy-clay texture) soils of the 1104 grid cells were categorized into 743 744 51 groups. For each group one single cell (so-called representative cell) was selected based on the topsoil SOC content. The representative cell was the one with the smallest absolute 745 746 deviation from the group mean SOC content.

Grassland ecophysiological parameterization without management was used for 747 748 croplands for the spinup phase, and with fertilization, harvest and ploughing settings in the transient phase. In case of grasslands, both during the spinup and transient phases grassland 749 parameterization was used, and in the transient phase mowing was assumed (once a year in 750 case of forests generic deciduous broadleaf forest parameterization was used for both spinup 751 and transient phases, and in the transient phase thinning was set. Parameterization was 752 753 performed based on generic, plant functional type specific ecophysiological parameters that were created based on the original parameterization of White et al. (2000). Biome-BGCMuSo 754 specific parameter sets are available at the website of the model<sup>1</sup>. 755

Soil parameters in Biome-BGCMuSo 6.2 were classified into six groups: (1) 4 generic
soil parameters, (2) 24 decomposition-nitrification-denitrification related parameters, (3) 14
rate scalars for the converging cascade scheme, (4) 19 soil moisture related parameters, (5) 7
methane related parameters and (6) 11 soil composition and characteristic values (can be set
layer by layer). Detailed description and proposed value of each soil parameters can be found
in the User's Guide (Hidy et al., 2021).

- 762
- 763

<sup>&</sup>lt;sup>1</sup> http://nimbus.elte.hu/bbgc/files/generic\_EPC\_set\_6.1.zip





764 765 766 Table 1: Soil parameters of Biome-BGCMuSo v6.2 (referring to SOC simulation) that were used during the sensitivity

analysis. The first column contains the group, the second contains the name of the parameter, the third contains the abbreviation, and the fourth contains original proposed values (Hidy et al., 2021). See Figure 4 for explanation on the compartment names. The parameters that were included in the  $2^{nd}$  phase of the sensitivity analysis are marked with 767

768 bold letters (see text).

GROUP	NAME	ABBREVIATION	VALUE
a : 1	C:N ratio of stable soil pool (soil4)	soil4CN	12
Generic soil parameters	NH4 mobilen proportion	amMP	0.1
parameters	aerodynamic resistance	potRair	107
	parameter 1 for temperature response function of decomp.	Tp1decomp	1.75
	parameter 2 for temperature response function of decomp.	Tp2decomp	17
	parameter 3 for temperature response function of decomp.	Tp3decomp	2.6
	parameter 4 for temperature response function of decomp.	Tp4decomp	40
	minimum T for decomposition and nitrification	Tp5decomp	-5
	e-folding depth of decomposition rate's depth scalar	EFD	10
	net mineralization proportion of nitrification	NITRnetMINER	0.2
	maximum nitrification rate	NITRmaxRATE	0.1
	coefficient of N2O emission of nitrification	NITRratioN2O	0.02
	parameter 1 for pH response function of nitrification	pHp1nitrif	0.15
Decomposition,	parameter 2 for pH response function of nitrification	pHp2nitrif	1
nitrification,	parameter 3 for pH response function of nitrification	pHp3nitrif	5.2
denitrification	parameter 4 for pH response function of nitrification	pHp4nitrif	0.55
parameters	parameter 1 for Tsoil response function of nitrification	Tp1nitrif	1
	parameter 2 for Tsoil response function of nitrification	Tp2nitrif	12
	parameter 3 for Tsoil response function of nitrification	Tp3nitrif	2.6
	parameter 4 for Tsoil response function of nitrification	Tp4nitrif	2.6
	minimum WFPS for scalar of nitrification calculation	minWFPS	0.1
	lower optimum WFPS for scalar of nitrification	opt1WFPS	0.45
	higher optimum WFPS for scalar of nitrification	opt2WFPS	0.55
	minimum value for saturated WFPS scalar of nitrification	minWFPSscalar	0.2
	soil respiration related denitrification rate	DENITcoeff	0.05
	denitrification related N2/N2O ratio multiplier	DNratioN2O	2
	critical WFPS value for denitrification	critWFPSdenitr	0.50
	respiration fractions for fluxes between compartments (l1s1)	RFl1s1	0.39
	respiration fractions for fluxes between compartments (l2s2)	RFl2s2	0.55
	respiration fractions for fluxes between compartments (l4s3)	RFl4s3	0.29
	respiration fractions for fluxes between compartments (s1s2)	RFs1s2	0.28
	respiration fractions for fluxes between compartments (s2s3)	RFs2s3	0.46
	respiration fractions for fluxes between compartments (s3s4)	RFs3s4	0.55
	potential rate constant of labile litter pool	RCS1	0.7
	potential rate constant of cellulose litter pool	RCS2	0.07
	potential rate constant of lignin litter pool	RCS3	0.014
	potential rate constant of fast microbial recycling pool	RCS4	0.07
	potential rate constant of medium microbial recycling pool	RCS5	0.014
	potential rate constant of slow microbial recycling pool	RCS6	0.0014
Rate scalars	potential rate constant of recalcitrant SOM (humus) pool	RCS7	0.0001
	potential rate constant of physical fragmentation of wood	RCS8	0.001
	maximum height of pond water	MP	5
	curvature of soil stress function	q	1
	fraction of dissolved part of S1 organic matter	fD1	0.005
	fraction of dissolved part of S2 organic matter	fD2	0.004
	fraction of dissolved part of S3 organic matter	fD3	0.003
	fraction of dissolved part of S4 organic matter	fD4	0.002
	mulch parameter: critical amount	CAmulch	1
	parameter 1 for mulch function	p1mulch	100
	parameter 2 for mulch function	p2mulch	0.75
	parameter 3 for mulch function	p3mulch	0.75
	mulch parameter: evaporation reduction	ERmulch	0.5





As methane simulation was not the subject of the present case study we neglected the related parameters. Regarding to the soil composition and characteristic values we used the DOSoReMI database (Pásztor et al., 2020). From the remaining 61 parameters soil depth, runoff curve number, the three soil moisture related parameters (tipping bucket method) were not included into analysis. Groundwater parameters were inactive in this case (no groundwater is assumed) which means that those parameters were not studied. The remaining 53 parameters are used in sensitivity analysis and are listed in Table 1.

776 As a first step sensitivity analysis was carried out for the selected 53 soil parameters by running the Biome-BGCMuSo v6.2 model in spinup mode until a quasi-equilibrium in the 777 total SOC is reached (that is the usual logic of the spinup run). The model was run for each 778 representative cell 2000 times with varying model parameters using Monte-Carlo method. 779 Each model parameters were varied randomly within the  $\pm 10\%$  range of their initial values 780 781 that were inherited from the Biome-BGC model or were set according to the literature. The 782 least square linearization (LSL) method (Verbeeck et al., 2006) was used for dividing output uncertainty into its input parameter related variability. As result of the LSL method, the total 783 784 variance of the model output and the sensitivity coefficient of each parameter can be determined. Sensitivity coefficients show the percent of total variance for which the given 785 parameter is responsible. 786

In order to simplify the workflow and decrease the degree of freedom another sensitivity analysis was performed. In this second step, the sensitive parameters (sensitivity coefficient > 1% for at least one land use type; a total of 18 parameters) were used in the following sensitivity analysis with 6000 iteration steps. These 18 parameters are marked with bold letters in Table 1.

Figure 10 shows the summary of the second sensitivity analysis where the overall 792 793 importance of the parameters are calculated as the mean of all selected pixels in a given land 794 use category. It can be seen in Figure 10 that from the 18 parameters (selected during the first 795 phase) soil carbon ratio of the recalcitrant pool (soil4CN), the temperature dependence 796 parameters of decomposition function (Tp1decomp, Tp2decomp, Tp3decomp, Tp4\_decomp) and the respiration fraction of S2-S3 and S3-S4 decomposition process (RFs2s3 and RFs3s4), 797 the curvature of soil stress function (q<sub>soilstress</sub>) and the fraction of dissolved part of S4 organic 798 799 matter (fD4) are the most important for all land use types. Among the other parameters the 800 critical WFPS of denitrification (critWFPSdentir) for grasslands has a remarkably high sensitivity (greater that 35%). It means that in case of grasslands the nitrogen availability 801 802 seems to be an important limitation of the primary production, probably because there are





- 803 only natural sources of nitrogen (no fertilization is assumed here), and the rooting zone is shallower than in case of forest which involves limited mineralized N access. Thus, in case of 804 higher values of critical WFPS of denitrification, the simulated production of the grassland 805
- 806 (and therefore the final SOC) seems to be significantly underestimated.



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Figure 10: The sensitivity coefficients of the soil parameters as the result of the sensitivity analysis. Black columns 809 refer to the crop, light grey to the grass and dark grey to the forest simulations. The sensitivity coefficients are 810 calculated as the mean pixel level sensitivity coefficient for the given land use type. Horizontal line indicates the 5% 811 threshold that was used to select the final parameter set that is subject to optimization.

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813 The selected ten, soil biogeochemistry related parameters were optimized for each of the 51 groups separately, using maximum likelihood estimation. For each group, the 814 parameter set providing the smallest deviation between the simulated and the observed values 815 816 of the weighted average SOC content (weight factor of 5 is used for the 0-30 cm, and weight 817 factor of 1 is used for the 30-60 cm soil layers) was considered to be the final (optimized) 818 model parameter set.

The differences of the simulated and observed SOC content for the 0-30 cm layer 819 820 (SOC0-30) using the initial (Table 1) and final soil parameters (not shown here) are presented in Figure 11. On the upper plot the signed relative error of SOC0-30 simulation before 821 822 optimization, while on the lower figure the signed relative error of SOC0-30 simulation after optimization can be seen. It is clearly visible that because of optimization the overestimation 823 of the SOC0-30 simulation significantly decreased. 824







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Figure 11: Differences between the simulated and observed SOC data for the 0-30 layer (SOC0-30) using the initial
(upper map) and optimized (lower map) soil parameters. The maps present the signed relative error in percent.
Visual comparison of the maps reveals the success of the optimization in terms of capturing the overall SOC for the
country area.

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We do not claim of course that the optimized parameters have universal value. Site history is neglected during the spin up simulations, and we use many simplifications like nonexistent land use change, present-day ecosphysiological parameterization etc. In this sense, the optimized parameter set can be best considered as a pragmatic solution to provide initial conditions (equilibrium SOC pools) for the model at the country scale that is consistent with the observations.





# 837 6. Concluding remarks

In this paper, we presented a detailed description of the soil hydrology and 838 carbon/nitrogen budget related developments of the Biome-BGCMuSo v6.2 terrestrial 839 840 ecosystem model. We mostly focused on changes relative to the previously published Biome-841 BGCMuSo v4.0 (Hidy et al., 2016), but our intention was also to provide a complete, standalone reference for the modelling community with mathematical equations (detailed in 842 843 the Supplementary Material). Table 2 summarizes the structural changes that we made during the developments starting from Biome-BGC v4.1.1 also including the previously published 844 Biome-BGCMuSo v4.0 (Hidy et al., 2016). 845

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 Table 2. Comparison of model structural solutions for Biome-BGC 4.1.1, Biome-BGCMuSo v4.0 and Biome-BGCMuSo v6.2.

 848
 BGCMuSo v6.2.

Routine	original Biome-BGC	Biome-BGCMuSo v4.0	Biome-BGCMuSo v6.2
Runoff	no	based on simple, empirical	distinguishing Hortonian and
Kulloli		formulation	Dunne runoff
	no	simple solution	development of pond water
Pond water			formation (based on infiltration
	Based on Penman-Monteith	Based on Penman-Monteith	capacity) Based on Penman-Monteith
	equation	equation	equation
	Calculation of the actual	Calculation of the actual	Parameterization possibility of
	evaporation from the potential	evaporation from the potential	actual aerodynamic resistance.
	evaporation and the square root	evaporation and the square root	Introduction of an upper limit for
	of time elapsed since the last	of time elapsed since the last	daily potential evaporation that is
Soil evaporation	precipitation.	precipitation.	determined by the available
Son evaporation			energy.
			Calculation of the actual
			evaporation is based on the method Ritche (1981).
			Simulation of the reducing effect
			of surface residue or mulch cover
			on bare soil evaporation
н. : <i>:</i> :	Transpiration from one-layer	Transpiration from 7-layers soil	Transpiration from 10-layers soil
Transpiration	bucket soil	based on soil stress	based on available water
	no	Simple groundwater simulation.	Improvement of the simulation of
			groundwater effect (using
Groundwater			capillary fringe). Introduction of two different
			methods.
	no	Relative SWC data is used to	The hygroscopic water, the
	10	calculate soil water stress.	wilting point, the field capacity
		The hygroscopic water, the	and the saturation values of the
		wilting point, the field capacity	soil layers can be defined in the
		and the saturation values of the	input file layer by layer.
		soil layers can be defined in the	The soil moisture stress index is
Soil moisture		input file layer by layer.	affected by the length and the
stress		The soil moisture stress index is	severity of the drought event,
		affected by the length and the day since the drought event	aggravated by the extreme temperature.
		lasted.	Introduction of the soil curvature
		- asteal	parameters to provide mechanism
			for soil texture dependent
			drought stress since it can affect
			the shape of the soil stress
			function.





			Normalized SWC data are used to calculate soil moisture stress index.
Organic carbon and nitrogen	One layer soil module with one organic carbon and nitrogen pool.	Multi-layered soil module without soil carbon and nitrogen profile.	Instead of defining a single litter, soil organic carbon and nitrogen pool, separate carbon and nitrogen pools for each soil layer in the form of soil organic matter and litter were implemented. Separation of above- and belowground litter pools. Litter and soil decomposition fluxes (carbon and nitrogen fluxes from litter to soil pools) are calculated layer by layer, depending on the actual temperature and SWC of the corresponding layers. Leaching of dissolved organic carbon and nitrogen.
Inorganic nitrogen	One layer soil module with one mineralized N pool.	Multi-layer soil module with an empirical inorganic N-profile (no layer-by-layer calculations, only estimation of the subpools in the different soil layer based on the rootlenght proportion).	Separation of ammonium (sNH4) and nitrate (sNO3) soil pools instead of a general mineralized nitrogen pool. Nitrification fluxes are calculated layer by layer, depending on the actual pH, temperature and SWC of the given layers. Denitrification fluxes are calculated layer by layer, depending on the depth, actual temperature and SWC of the given layers.

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851 Earlier model versions used a soil hydrology scheme based on the Richards equation, but the results were not satisfactory. Sándor et al. (2017) presented results from the first major 852 grassland model intercomparison project (executed within the frame of FACCE MACSUR) 853 854 where Biome-BGCMuSo 2.2 was used. That study demonstrated the problems associated with proper representation of soil water content that was a common shortcoming of all included 855 856 models. In the Hidy et al. (2016) paper, where the focus was on Biome-BGCMuSo v4.0, the SWC related figures clearly indicated problems with the simulations compared to 857 observations. The SWC amplitude was not captured well which clearly influences drought 858 stress, decomposition, and other SWC driven processes like nitrification and denitrification. 859 860 For the latter two processes this is especially critical as they are associated with contrasting SWC regimes (nitrification is an aerobic, while denitrification is an anaerobic process). This 861 is a good example for erroneous internal process representation that may lead to improper 862 results. Note that the currently used functions for nitrification/denitrification are also subject 863 864 to uncertainty that needs to be addressed in the future (Heinen, 2006). Nevertheless, the





presented model developments might contribute to a more realistic soil process simulations and improved results.

867 Algorithm ensemble approach is already implemented in Biome-BGCMuSo. Algorithm ensemble means that the user has more than one option for the representation of 868 some processes. Biome-BGCMuSo v6.2 has alternative phenology routines (Hidy et al., 869 2012), two alternative methods for soil temperature (Hidy et al., 2016), soil hydrology 870 (described in this study), photosynthesis and soil moisture stress calculation. We plan to 871 872 extend the algorithm ensemble by providing alternative decomposition schemes to the model. One possibility is the implementation of a CENTURY-like structure (Koven et al., 2013) that 873 is a promising direction and might improve the quality of the equilibrium (spin-up) 874 simulations and the simulated N mineralization related to SOM decomposition. Reported 875 problems related to the rapid decomposition of litter in the current model structure (Bonan et 876 al., 2013) needs to be addressed in future model versions as well. 877

Plant growth and allocation related developments were not addressed in this study but of course has many inferences with the presented model logic (i.e. parameterization and related primary production defines the amount and quality of litter, etc.). A forthcoming publication will provide a comprehensive overview on the plant growth and senescence related model modifications where elements from crop models are also included.

Biome-BGCMuSo is still an open source model that can be freely downloaded from its website with a detailed User's Guide and other supplementary files. We also encourage users to test the so-called RBBGCMuso package (available at GitHub) that has many advanced features to support model application and optimization. A graphical environment, called AgroMo (also available at GitHub) was also developed around Biome-BGCMuSo to help users in carrying out simulations either with site specific plot scale data or with gridded databases representing large regions.

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#### 892 Code and data availability

The current version of Biome-BGCMuSo, together with sample input files and detailed User's Guide are available from the website of the model: http://nimbus.elte.hu/bbgc/download.html under the GPL-2 licence. Biome-BGCMuSo v6 is also available at GitHub: https://github.com/bpbond/Biome-BGC/tree/Biome-BGCMuSo\_v6. The exact version of the model (v6.2 alpha) used to produce the results used in this paper is archived on Zenodo





- 898 (https://doi.org/10.5281/zenodo.5761202). Experimental data and model parameterization used
- in the study are available from the corresponding author upon request.

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# 902 Authors' Contributions

Hidy developed Biome-BGCMuSo, maintained the source code and executed the sample 903 simulations. The study was conceived and designed by Hidy, Barcza and Fodor, with 904 905 assistance from Acs, Dobor and Hollós. It was directed by Hidy and Barcza . Acs and Dobor contributed with model benchmarking. Hollós participated with the construction of a 906 907 modeling framework for Biome-BGCMuSo. Filep, Incze, Zacháry and Pásztor contributed with experimental data. Hidy, Barcza, Fodor and Merganičová prepared the manuscript and 908 the supplement with contributions from all co-authors. All authors reviewed and approved the 909 present article and the supplement. 910

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