

1 **Soil related developments of the Biome-BGCMuSo v6.2**

2 **terrestrial ecosystem model**

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29 **Abstract**

30 Terrestrial biogeochemical models are essential tools to quantify climate-carbon cycle
31 feedback and plant-soil relations from local to global scale. In this study, theoretical basis is
32 provided for the latest version of Biome-BGCMuSo biogeochemical model (version 6.2).
33 Biome-BGCMuSo is a branch of the original Biome-BGC model with a large number of
34 developments and structural changes. Earlier model versions performed poorly in terms of
35 soil water content (SWC) dynamics in different environments. Moreover, lack of detailed
36 nitrogen cycle representation was a major limitation of the model. Since problems associated
37 with these internal drivers might influence the final results and parameter estimation,
38 additional structural improvements were necessary. In this paper the improved soil hydrology
39 and soil carbon/nitrogen cycle calculation methods are described in detail. Capabilities of the
40 Biome-BGCMuSo v6.2 model are demonstrated via case studies focusing on soil hydrology,
41 soil nitrogen cycle and soil organic carbon content estimation. Soil hydrology related results
42 are compared to observation data from an experimental lysimeter station. The results indicate
43 improved performance for Biome-BGCMuSo v6.2 compared to v4.0 (explained variance
44 increased from 0.121 to 0.8 for SWC, and from 0.084 to 0.46 for soil evaporation; bias
45 changed from -0.047 to $-0.007 \text{ m}^3 \text{ m}^{-3}$ for SWC, and from $-0.68 \text{ mm day}^{-1}$ to -0.2 mm day^{-1}
46 for soil evaporation). Nitrogen balance and soil CO_2 efflux related simulations were evaluated
47 based on observations made in a long-term field experiment under crop rotation. The results
48 indicated that the model is able to provide realistic nitrate content estimation for the topsoil.
49 Soil nitrous oxide (N_2O) efflux and soil respiration simulations were also realistic with overall
50 correspondence with the observations (for the N_2O efflux simulation bias was between -0.13
51 and $-0.1 \text{ mg N m}^{-2} \text{ day}^{-1}$, NRMSE was 32.4% – 37.6%; for CO_2 efflux simulations bias was
52 0.04 – $0.17 \text{ g C m}^{-2} \text{ day}^{-1}$, while NRMSE was 34.1% – 40.1%). Sensitivity analysis and
53 optimization of the decomposition scheme is presented to support practical application of the
54 model. The improved version of Biome-BGCMuSo has the ability to provide more realistic
55 soil hydrology representation and nitrification/denitrification process estimation which
56 represents a major milestone.

57

58

59 **1. Introduction**

60 The construction and development of biogeochemical models (BGM) is the response
61 of the scientific community to address challenges related to climate change and human
62 induced global environmental change. BGMs can be used to quantify future climate-
63 vegetation interaction including climate-carbon cycle feedback, and as they simulate plant
64 production, they can be used to study a variety of ecosystem services that are related to human
65 nutrition and resource availability (Asseng et al., 2013; Bassu et al., 2014; Huntzinger et al.,
66 2013). Similarly to the models describing various and complex environmental processes, the
67 structure of biogeochemical models reflects our current knowledge about a complex system
68 with many internal processes and interactions.

69 Processes of the atmosphere-plant-soil system take place on different temporal (sub-
70 daily to centennial) scales and are driven by markedly different mechanisms that are
71 quantified by a large diversity of modeling tools (Schwalm et al., 2019). Plant photosynthesis
72 is an enzyme-driven biochemical process that has its own mathematical equation set and
73 related parameters (and a large literature; e.g. Farquhar et al., 1980; Medlyn et al. 2002; Smith
74 and Dukes, 2013; Dietze, 2013). Allocation of carbohydrates in the different plant
75 compartments is studied extensively and also has a large literature and mathematical tool set
76 (Friedlingstein et al., 1999; Olin et al., 2015; Merganičová et al., 2019). Plant phenology is
77 quantified by specific algorithms that are rather uncertain components of the models
78 (Richardson et al., 2013; Hufkens et al., 2018; Peaucelle et al., 2019). Soil biogeochemistry is
79 driven by microbial and fungal activity and also has its own methodology and a vast literature
80 (Zimmermann et al 2007; Kuzyakov, 2011; Koven et al., 2013; Berardi et al., 2020).
81 Emerging scientific areas like the quantification of the dynamics of non-structural
82 carbohydrates (NSC) in plants has a separate methodology that claims for mathematical
83 representation in models (Martínez-Vilalta et al., 2016). Simulation of land surface hydrology
84 including evapotranspiration is typically handled by some variant of the Penman-Monteith
85 equation that is widely studied thus represents a separate scientific field (McMahon et al.,
86 2013; Doležal et al., 2018).

87 Putting all together, if we are about to construct and further improve a biogeochemical
88 model to consider novel findings and track global changes, we need a comprehensive
89 knowledge that integrates many, almost disjunct scientific fields. Clearly, transparent and
90 well-documented development of a biogeochemical model is of high priority but challenging

91 from the very beginning that claims for cooperation of researchers from various scientific
92 fields.

93 Continuous model development is inevitable but it has to be supported by extensive
94 comparison with observations and some kind of implementation of the model-data fusion
95 approach (Keenan et al., 2011). It is well documented that structural problems might trigger
96 incorrect parameter estimation that might be associated with distorted internal processes
97 (Sándor et al., 2017; Martre et al., 2015). In other words, one major issue with BGMs (and in
98 fact with all models using many parameters) is the possibility to get good simulation results
99 for wrong reasons (which means incorrect parameterization) due to compensation of errors
100 (Martre et al., 2015). In order to avoid this issue, any model developer team has to make an
101 effort to focus also on internal ecosystem conditions (e.g. soil volumetric water content
102 (SWC), nutrient availability, stresses, etc.) and other processes (e.g. decomposition) rather
103 than the main simulated processes (e.g. photosynthesis, evapotranspiration).

104 Historically, biogeochemical models have been developed to simulate the processes of
105 undisturbed ecosystems with simple representation of the vegetation (Levis, 2010). As the
106 focus was on the carbon cycle, water and nitrogen cycles and related soil processes were not
107 well represented. Incorrect representation of SWC dynamics is still an issue with the models
108 especially in drought-prone ecosystems (Sándor et al., 2017). Additionally, human
109 intervention representation (management) is still incomplete in some state-of-the-art BGMs,
110 e.g. thinning, grass mowing, grazing, tillage or irrigation is missing in some models (see
111 Table A1 in Friedlingstein et al., 2020).

112 In contrast, crop models with different complexity were used for about 50 years or so
113 to simulate the processes of managed vegetation (Jones et al., 2017; Franke et al., 2020). As
114 the focus of the crop models is on final yield due to economic reasons, the carbon balance, or
115 the full greenhouse gas balance was not, or was just partially addressed originally. Crop
116 models typically have a sophisticated representation of soil water balance with a multilayer
117 soil module that usually calculates plant response to water stress as well. Nutrient stress, soil
118 conditions during planting, consideration of multiple phenological phases, heat stress during
119 anthesis, vernalization, manure application, fertilization, harvest, and many other processes
120 have been implemented during the decades (Ewert et al., 2015). Therefore, it seems to be
121 straightforward to exploit the benefits of crop models and implement sound and well-tested
122 algorithms into the BGMs.

123 Starting from the well-known Biome-BGC model originally developed to simulate
124 undisturbed forests and grasslands, using a simple single layer soil submodel (Running and

125 Hunt, 1993; Thornton and Rosenbloom, 2005), we developed a complex, more sophisticated
126 model (Hidy et al., 2012; 2016). Biome-BGCMuSo v4.0 (Biome-BGC with Multilayer Soil
127 module) uses a 7-layer soil module and is capable of simulating different ecosystems from
128 natural grassland to cropland including several management options (mowing, grazing,
129 thinning, planting and harvest), taking into account many environmental effects (Hidy et al.,
130 2016). The developments included improvements regarding both soil and plant processes. In a
131 nutshell, the most important, soil related developments were the improvement of the soil
132 water balance module by implementing routines for estimating percolation, diffusion, pond
133 water formation and runoff; the introduction of multilayer simulation for belowground
134 processes in a simplified way. The most important, plant related developments involved the
135 implementation of a routine for estimating the effect of drought on vegetation growth and
136 senescence; the improvement of stomatal conductance calculation considering atmospheric
137 CO₂ concentration; the integration of selected management modules; the implementation of
138 new plant compartments (e.g. yield); the implementation of C4 photosynthesis routine; the
139 implementation of photosynthesis and respiration acclimation of plants and temperature-
140 dependent Q10; and empirical estimation of methane and nitrous oxide soil efflux.

141 Problems found with the Biome-BGCMuSo v4.0 simulation result (namely the poor
142 representation of soil water content; or the lack of sophisticated, layer-specific soil nitrogen
143 dynamics representation; or the model structure related problems, such as the lubber
144 parameterization of the model) marked the path for further developments.

145 The aim of the present study is to provide detailed documentation on the current,
146 improved version of Biome-BGCMuSo v6.2, which has many new features and facilitates
147 various in-depth investigations of ecosystem functioning. Due to large number of
148 developments, this paper focuses only on the soil related model improvements. Case studies
149 are also presented to demonstrate the capabilities of the new model version and to provide
150 guidance for the model user community.

151 **2. The original Biome-BGC model**

152 Biome-BGC was developed from the Forest-BGC mechanistic model family in order
153 to simulate vegetation types other than forests. Biome-BGC was one of the earliest
154 biogeochemical models that included explicit carbon and nitrogen cycle modules. Biome-
155 BGC simulates the storages and fluxes of water, carbon, and nitrogen within and between the
156 vegetation, litter, and soil components of terrestrial ecosystems. It uses a daily time step, and

157 is driven by daily values of maximum and minimum temperatures, precipitation, solar
158 radiation, and vapor pressure deficit (Running and Hunt, 1993). The model calculations apply
159 to a unit ground area that is considered to be homogeneous.

160 The three most important components of the model are the phenological, the carbon
161 uptake and release, and the soil flux modules. The core logic that is described below in this
162 section remained intact during the developments. The phenological module calculates foliage
163 development that affects the accumulation of C and N in leaf, stem (if present), root and
164 consequently the amount of litter. In the carbon flux module gross primary production (GPP)
165 of the biome is calculated using Farquhar's photosynthesis routine (Farquhar et al., 1980) and
166 the enzyme kinetics model based on Woodrow and Berry (2003). Autotrophic respiration is
167 separated into maintenance and growth respiration. Maintenance respiration is calculated as
168 the function of the N content of living plant pools, while growth respiration is an adjustable
169 but fixed proportion of the daily GPP. The single-layer soil module simulates the
170 decomposition of dead plant material (litter) and soil organic matter, N mineralization and N
171 balance in general (Running and Gower, 1991). The soil module uses the so-called
172 converging cascade method (Thornton and Rosenbloom, 2005) to simulate decomposition,
173 carbon and nitrogen turnover, and related soil CO₂ efflux.

174 The simulation has two basic steps. During the first (optional) spinup simulation the
175 available climate data series is repeated as many times as it is required to reach a dynamic
176 equilibrium in the soil organic matter content to estimate the initial values of the carbon and
177 nitrogen pools. The second, normal simulation uses the results of the spinup simulation as
178 initial conditions and runs for a given, predefined time period (Running and Gower 1991). So-
179 called transient simulation option (which is the extension of the spinup routine) is a novel
180 feature in Biome-BGCMuSo v6.2 relative to the previous versions in order to ensure smooth
181 transition between the spinup and normal phase (Hidy et al., 2021).

182 In Biome-BGC, the main parts of the simulated ecosystem are defined as plant, litter
183 and soil. The most important pools include leaf (C, N and intercepted water), root (C, N),
184 stem (C, N), soil (C, N and water) and litter (C, N). Plant C and N pools have sub-pools
185 (actual pools, storage pools and transfer pools). The actual sub-pools store C and N for the
186 current year growth. The storage sub-pools (essentially the non-structural carbohydrate pool,
187 the source for the cores or buds) contain the amount of C and N that will be active during the
188 next growing season. The transfer sub-pools inherit the entire content of the storage pools at
189 the end of every simulation year. Soil C also has sub-pools representing various organic
190 matter forms characterized by considerably different decomposition rates.

191 In spite of its popularity and proven applicability, the development of Biome-BGC
192 was temporarily stopped (the latest official NTSG version is Biome-BGC 4.2;
193 <https://www.ntsug.umd.edu>). One major drawback of the model was its relatively poor
194 performance in modelling managed ecosystems, and the simplistic soil water balance
195 submodel using a single soil layer only.

196 Our team started to develop the Biome-BGC model further in 2006. According to the
197 logic of the team, the new model branch was planned to be the continuation of the Biome-
198 BGC model with regard to the original concept of the developers (keeping the model code
199 open source, providing detailed documentation, and providing support for the users).

200 The starting point of our model development was Biome-BGC v4.1.1 that was a result
201 of the model improvement activities of the Max Planck Institute (Vetter et al., 2007).
202 Development of the Biome-BGCMuSo model branch has a long history by now. Previous
203 model developments were documented in Hidy et al. (2012) and Hidy et al. (2016). Below,
204 we provide detailed description of the new developments that are included in Biome-
205 BGCMuSo v6.2 which is the latest version released in September, 2021. A comprehensive
206 review of the input data requirement of the model together with explanation on the input data
207 structure is available in the User's Guide (Hidy et al., 2021). In this paper we refer to some
208 input files (e.g. soil file, plant file) that are described in the User's Guide in detail.

209 One of the most important novelty and advantage of the new model version (Biome-
210 BGCMuSo v6.2) compared to any previous versions that due to the extensive and detailed
211 soil parameter set (current version has 79, MuSo 4.0 has 39 and original model version has
212 only 6 adjustable soil related parameters) the parameterization of the model is much more
213 flexible. But this might be of course a challenging task to define all of the input parameters. In
214 order to support practical application of the model, the User's Guide contains proposed values
215 for most of the new parameters (Hidy et al., 2021).

216 **3. Soil hydrology related developments**

217 In Biome-BGCMuSo v6.2 a 10-layer soil submodel was implemented. Previous model
218 versions included a 7-layer submodel, which turned out to be insufficient to capture
219 hydrological events like drying of the topsoil layers with sufficient accuracy. The thicknesses
220 of the layers from the surface to the bottom are 3, 7, 20, 30, 30, 30, 30, 50, 200 and 600 cm.
221 The centre of the given layer represents the depth of each soil layer. Soil texture can be
222 defined by the percentage of sand and silt for each layer separately along with the most

223 important physical and chemical parameters (pH, bulk density, characteristic SWC values,
224 drainage coefficient, hydraulic conductivity) in the soil input file (Hidy et al., 2021).

225 The water balance module of Biome-BGCMuSo has five major components to
226 describe soil water related processes in daily resolution (listed here following the order of
227 calculation): pond water accumulation and runoff; infiltration and downward gravitational
228 flow (percolation); water potential gradient driven water movement within the soil (diffusion);
229 evaporation and transpiration (root water uptake); and the downward/upward fluxes to/from
230 groundwater. In the following subsections these five major components are described.

231 **3.1 Pond water accumulation and runoff**

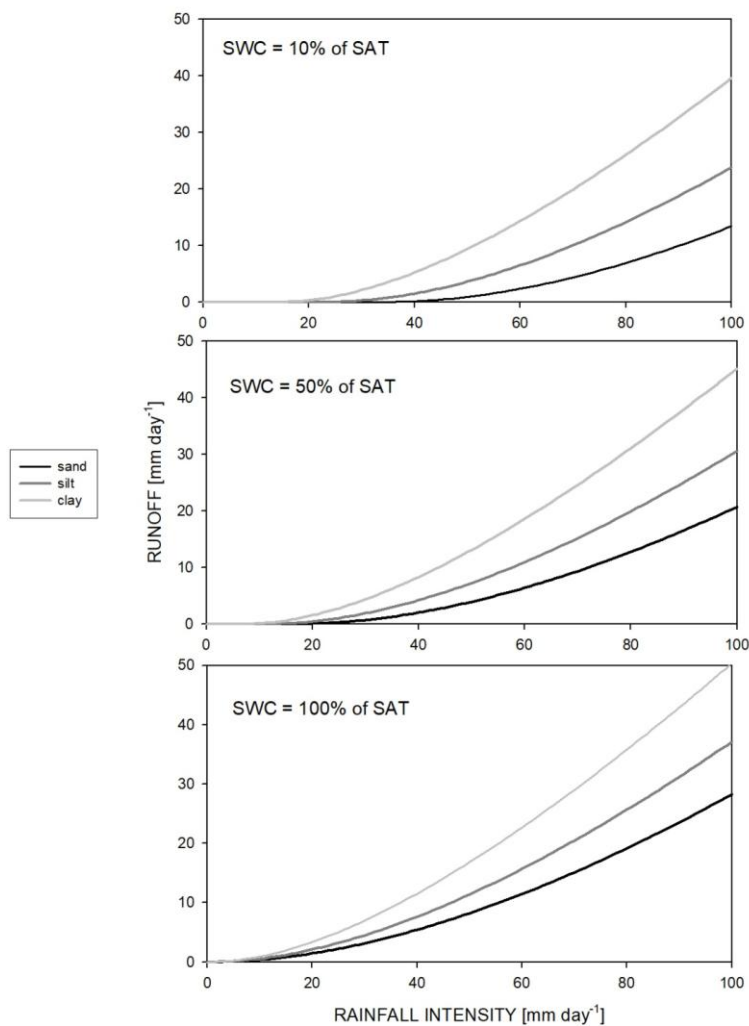
232 Precipitation can reach the surface as rain or snow (below 0 °C snow accumulation is
233 assumed). Snow water melts from the snowpack as a function of temperature and radiation
234 and added to the precipitation input.

235 The canopy can intercept rain. The intercepted volume goes into the *canopy water*
236 pool, which can evaporate. No canopy interception of snow is assumed. The throughfall
237 (complemented with the amount of melted snow) gives the potential infiltration.

238 A new development in Biome-BGCMuSo v6.2 is that maximum infiltration is
239 calculated based on the saturated hydraulic conductivity and the SWC of the top soil layers. If
240 the potential infiltration exceeds the maximum infiltration, pond water can be formed. If the
241 sum of the precipitation and the actual pond height minus the maximum infiltration rate is
242 greater than the maximum pond height, the excess water is added to surface runoff detailed
243 below (Balsamo et al., 2009). The maximum pond height is an input parameter. Water from
244 the pond can infiltrate into the soil at a rate the top soil layer can absorb it. Evaporation of the
245 pond water is assumed equal to the potential evaporation.

246 Surface runoff is the water flow occurring on the surface when a portion of the
247 precipitation cannot infiltrate into the soil. Two types of surface runoff processes can be
248 distinguished: Hortonian and Dunne. Hortonian runoff is unsaturated overland flow that
249 occurs when the rate of precipitation exceeds the rate at which water can infiltrate. The other
250 type of surface runoff is the Dunne runoff (also known as the saturation overland flow) which
251 occurs when the entire soil is saturated but the rain continues to fall. In this case the rainfall
252 immediately triggers pond water formation and (above the maximum pond water height)
253 surface runoff. The handling of these processes is presented in the soil hydrological module of
254 Biome-BGCMuSo v6.2.

255 Calculation of Hortonian runoff (in $\text{kg H}_2\text{O m}^{-2} \text{ day}^{-1}$) is based on a semi-empirical
 256 method and uses the precipitation amount (in cm day^{-1}), the unitless runoff curve number
 257 (RCN), and the actual moisture content status of the topsoil (Rawls et al., 1980; this method is
 258 known as the SCS runoff curve number method). This type of runoff simulation can be turned
 259 off by setting RCN to zero. The detailed description can be found in the Supplementary
 260 material, Section 1. The amount of runoff as a function of the soil type and the actual SWC is
 261 presented in Figure 1.



262
 263 **Figure 1: Hortonian runoff as the function of rainfall intensity, soil type and actual soil water content of the top soil**
 264 **layer. Sand soil means 92% sand, 4% silt and 4% clay; silt soil means 8% sand, 86% silt and 6% clay; clay soil means**
 265 **20% sand, 20% silt and 60% clay. SWC and SAT denote soil water content and saturation, respectively.**

266
 267 **3.2 Infiltration, percolation and diffusion**

268 There are two optional methods in Biome-BGCMuSo v6.2 to calculate soil water
 269 movement between soil layers and actual SWC layer by layer. The first one is a cascade
 270 method (also known as tipping bucket method), and the second is a Richards equation based

271 physical method. The tipping bucket method has a long history in crop modelling and is
272 considered as a successful, well-evaluated algorithm that can accurately simulate downward
273 water flow in the soil.

274 The cascade method uses a semi-empirical input parameter (*DC*: drainage coefficient
275 in day⁻¹) to calculate downward water flow rate. When the *SWC* of a soil layer exceeds field
276 capacity (*FC*), a fraction (equal to *DC*) of the water amount above *FC* goes to the layer next
277 below. If *DC* is not set in the soil input file, it is estimated from the saturated hydraulic
278 conductivity: $DC = 0.1122 \cdot K_{SAT}^{0.339}$ (K_{SAT} : saturated hydraulic conductivity in cm day⁻¹;
279 the user can set its value or the model based on soil texture estimates it internally; see Hidy et
280 al., 2016). The detailed description of the method can be found in the Supplementary material,
281 Section 2. Drainage from the bottom layer is a net loss for the soil profile.

282 Water diffusion that is the capillary water flow between the soil layers is calculated to
283 account for the relatively slow movement of water. The flow rate is the function of the water
284 content difference of two adjacent layers and the soil water diffusivity at the boundary of the
285 layers, which is determined based on the average water content of the two layers. The detailed
286 mathematical description of the method can be found in the Supplementary material, Section
287 3.

288 The detailed description of the Richards-method can be found in Hidy et al. (2012). To
289 support efficient and robust calculations of soil water fluxes a dynamically changing time step
290 was introduced in version 4.0 (Hidy et al., 2016). The implementation of the more
291 sophisticated Richards-method is still in an experimental phase requiring rigorous testing and
292 validation in the future.

293 **3.3 Evapotranspiration**

294 Biome-BGCMuSo, such as its predecessor Biome-BGC, estimates evaporation of leaf
295 intercepted water, bare soil evaporation, and transpiration to estimate the total
296 evapotranspiration in a daily level. The potential rates of all three processes are calculated
297 based on the Penman-Monteith (PM) method. PM equation requires net radiation (minus soil
298 heat flux) and conductance values by definition using different parameterization for the
299 different processes. The model calculates leaf- and canopy-level conductances of water
300 vapour and sensible heat fluxes, to be used in Penman-Monteith calculations of canopy
301 evaporation and canopy transpiration. Note that in the Biome-BGC model family the direct
302 wind effect is ignored but can be considered indirectly by adjusting boundary layer

303 conductance to site-specific conditions. A possible future direction might be the extension of
304 the model logic to consider wind effect directly.

305 3.3.1 Canopy evaporation

306 If there is intercepted water, this portion of evaporation is calculated using the canopy
307 resistance (reciprocal of conductance) to evaporated water and the resistance to sensible heat.
308 The time required for the water to evaporate based on the average daily conditions is
309 calculated, and subtracted from the day length to get the effective day length for
310 evapotranspiration. Combined resistance to convective and radiative heat transfer is calculated
311 based on canopy conductance of vapour and leaf conductance of sensible heat both of which
312 are assumed to be equal to the boundary layer conductance. Besides the
313 conductance/resistance parameters the canopy absorbed shortwave radiation drives the
314 calculation. Note that the canopy evaporation routine was not modified significantly in
315 Biome-BGCMuSo.

316 3.3.2 Soil evaporation

317 In order to estimate soil evaporation, first the potential evaporation is calculated,
318 assuming that the resistance to vapour is equal to the resistance to sensible heat and assuming
319 no additional resistance component. Both resistances are assumed to be equal to the actual
320 aerodynamic resistance. Actual aerodynamic resistance is the function of the actual air
321 pressure and air temperature and the potential aerodynamic resistance ($potR_{air}$ in $s\ m^{-1}$).
322 $potR_{air}$ was a fixed value in the previous model versions ($107\ s\ m^{-1}$). Its value was derived
323 from observations over bare soil in tiger-bush in south-west Niger (Wallace and Holwill,
324 1997). In Biome-BGCMuSo v6.2, the $potR_{air}$ is an input parameter that can be adjusted by the
325 user (Hidy et al., 2021). Another new development in Biome-BGCMuSo v6.2 is the
326 introduction of an upper limit for daily potential evaporation ($evap_{limit}$) that is determined by
327 the available energy (incident shortwave flux that reaches the soil surface):

$$328\ evap_{limit} = \frac{irad \cdot dayl}{LH_{vap}} \quad (1)$$

329 where $irad$ is the incident shortwave flux density in $W\ m^{-2}$, $dayl$ is the length of the day in
330 seconds, LH_{vap} is the latent heat of vaporization (the amount of energy that must be added to
331 liquid to transform into gas) in $J\ kg^{-1}$. This feature was missing from previous model versions
332 resulting in considerable overestimation of evaporation on certain days that was caused by the
333 missing energy limitation on evaporation.

334 A new feature in Biome-BGCMuSo v6.2 is the calculation of the actual evaporation
335 from the potential evaporation and the square root of time elapsed since the last precipitation
336 (expressed by days; Ritchie, 1998). This is another method that has been used by the crop
337 modeller community for many years. Detailed description of the algorithm can be found in the
338 Supplementary material, Section 4.

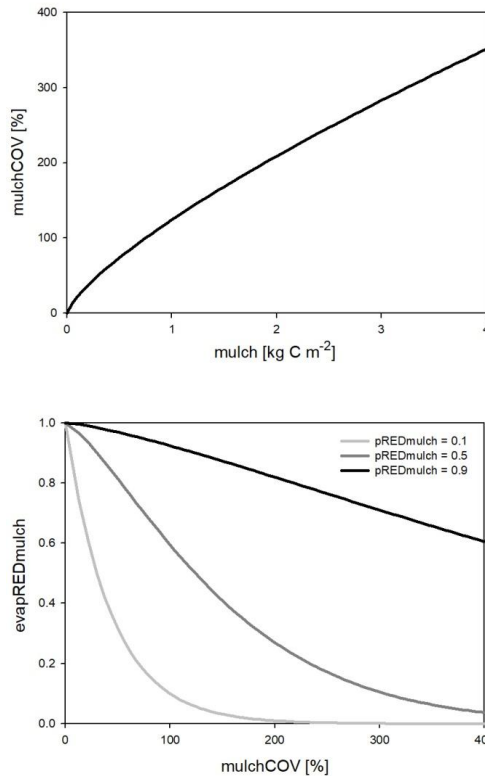
339 One major new development in Biome-BGCMuSo v6.2 is the simulation of the
340 reducing effect of surface residue or mulch cover on bare soil evaporation. Here we use the
341 term ‘mulch’ to quantify surface residue cover in general keeping in mind that mulch is
342 typically a human-induced coverage. Surface residue includes aboveground litter and coarse
343 woody debris as well.

344 The evaporation reduction effect (*evapREDmulch*; unitless) is a variable between 0
345 and 1 (0 means full limitation, and 1 means no limitation) estimated based on a power
346 function of the surface coverage (*mulchCOV* in %) and a soil specific constant set by the user
347 (*pREDmulch*; see Hidy et al., 2021). If variable *mulchCOV* reaches 100% it means that the
348 surface is completely covered. If *mulchCOV* is greater than 100% it means the surface is
349 covered by more than one layers. Surface coverage is a power function of the amount of
350 mulch (*mu* in kgC m⁻²) with parameters *p1_{mulch}*, *p2_{mulch}*, and *p3_{mulch}* (soil parameters) based
351 on the method of Rawls et al. (1991):

$$352 \quad mulchCOV = p1_{mulch} \cdot (mu/p2_{mulch})^{p3_{mulch}} \quad (2)$$

$$353 \quad evapREDmulch = pREDmulch^{\frac{mulchCOV}{100}} \quad (3)$$

354 Another simulated effect of surface residue cover is the homogenization of soil
355 temperature between 0 and 30 cm depth (layers 1, 2 and 3). The functional forms of surface
356 coverage and evaporation reduction factor are presented in Figure 2.



357

358 **Figure 2: Surface coverage as a function of the amount of surface residue or mulch (upper plot) and the evaporation**
 359 **reduction factor (evapREDmulch) as the function of mulch coverage (lower plot) using different mulch specific soil**
 360 **parameters (pREDmulch). See text for details.**

361

362 3.3.3 Transpiration

363 In order to simulate transpiration, first transpiration demand (TD in $\text{kg H}_2\text{O m}^{-2} \text{ day}^{-1}$)
 364 is calculated using the Penman-Monteith equation separately for sunlit and shaded leaves. TD
 365 is the function of leaf-scale conductance to water vapor, which is derived from stomatal,
 366 cuticular and leaf boundary layer conductances. A novelty in Biome-BGCMuSo v6.2 is that
 367 potential evapotranspiration is also calculated using the maximal stomatal conductance
 368 instead of the actual stomatal conductance, which means that stomatal aperture is not affected
 369 by the soil moisture status (in contrast to the actual one).

370 TD is distributed across the soil layers according to the actual root distribution using
 371 an improved method (the logic was changed since Biome-BGCMuSo v4.0). From the plant
 372 specific root parameters and the actual root weight Biome-BGCMuSo calculates the number
 373 of the layers where roots can be found together with the root mass distribution across the
 374 layers (Jarvis, 1989; Hidy et al., 2016). If there is not enough water in a given soil layer to
 375 fulfil the transpiration demand, the transpiration flux from that layer is limited, and below
 376 wilting point (WP) it is set to zero. The sum of layer-specific transpiration fluxes across the

377 root zone gives the actual transpiration flux. The detailed description of the algorithm can be
378 found in the Supplementary material, Section 5.

379 **3.4 Effect of groundwater**

380 Simulation of groundwater effect was introduced in Biome-BGCMuSo v4.0 (Hidy et
381 al., 2016), but the method has been significantly improved, and the new algorithm it is now
382 available in Biome-BGCMuSo v6.2. In the recent model version there is an option to provide
383 an additional input file with the daily values of the groundwater table depth (*GWdepth* in m).

384 Groundwater may affect soil hydrological and plant physiological processes if the
385 water table is closer to the root zone than the thickness of the capillary fringe (that is the
386 region saturated from groundwater via capillary effect). The thickness of the capillary fringe
387 (*CF* in m) is estimated using literature data and depends on the soil type (Johnson and Ettinger
388 model; Tillman and Weaver, 2006). Groundwater table distance (*GWdist* in m) for a given
389 layer is defined as the difference between *GWdepth* and the depth of the midpoint of the
390 layer.

391 The layers completely below the groundwater table are assumed to be fully saturated.
392 In case of layers within the capillary fringe ($GWdist < CF$), the calculation of water balance
393 changes: the FC rises, thus the difference between saturation (SAT) and FC decreases and the
394 layer charges gradually, till the increased FC value is reached. The FC-rising effect of
395 groundwater for the layers above the water table is calculated based on the ratio of the
396 groundwater distance and the capillary fringe thickness, but only after the water content of the
397 layers below have reached their modified FC values. Detailed description of the groundwater
398 effect can be found in Supplementary material, Section 6.

399 **3.5 Soil moisture stress**

400 In the original Biome-BGC model the effect of changing soil water content on
401 photosynthesis and decomposition of soil organic matter is expressed in terms of soil water
402 potential (Ψ). Instead of Ψ , the SWC is also widely used to calculate the limitation of stomatal
403 conductance and decomposition. A practical advantage of using SWC as a factor in stress
404 function is that it is easier to measure in the field and the changes of the driving function are
405 much smoother than in case of Ψ . The disadvantage is that SWC is not comparable among
406 different soil types (in contrast to Ψ).

407 The maximum of SWC is the saturation value; the minimum is the wilting point or the
408 hygroscopic water depending on the type of the simulated process. Novelty of Biome-

409 BGCMuSo v6.2 is that the hygroscopic water, the wilting point, the field capacity and the
 410 saturation values are calculated internally by the model based on the soil texture data, or can
 411 be defined in the input file layer by layer.

412 In Biome-BGCMuSo v6.2 the so-called soil moisture stress index (*SMSI*) is calculated
 413 to represent overall soil stress conditions. *SMSI* is affected by the length of the drought event
 414 (*SMSE*: extent of soil stress), the severity of the drought event (*SMSL*: length of soil stress),
 415 aggravated by the extreme temperature (*extremT*: effect of extreme heat). *SMSI* is equal to
 416 zero if no soil moisture limitation occurs and equal to 1 in case of full soil moisture limitation.
 417 *SMSI* is used by the model for plant senescence calculations (presentation of plant related
 418 processes is the subject of a forthcoming publication)). The members of *SMSI* are explained
 419 detailed below.

$$420 \quad SMSI = 1 - SMSE \cdot SMSL \cdot extremT \quad (4)$$

421 Magnitude of soil moisture stress (*SMSE*) is calculated layer by layer based on SWC.
 422 Regarding soil moisture stress two different processes are distinguished: drought (i.e. low
 423 SWC close to or below WP) and anoxic condition (i.e. after large precipitation events or in
 424 the presence of high groundwater table; Bond-Lamberty et al., 2007). An important novelty of
 425 Biome-BGCMuSo v6.2 is the soil curvature parameters (*q*) which is introduced to provide
 426 mechanism for soil texture dependent drought stress as it can affect the shape of the soil stress
 427 function (which means possibility for non-linear ramp function):

$$428 \quad SMSE^i = 0 \quad ; SWC^i < SWC_{WP}^i$$

$$429 \quad SMSE^i = \left(\frac{SWC^i - SWC_{WP}^i}{SWC_{drought}^i - SWC_{WP}^i} \right)^q \quad ; SWC_{WP}^i \leq SWC < SWC_{drought}^i \quad (5)$$

$$430 \quad SMSE^i = 1 \quad ; SWC_{drought}^i \leq SWC \leq SWC_{anoxic}^i$$

$$431 \quad SMSE^i = \frac{SWC_{SAT}^i - SWC^i}{SWC_{SAT}^i - SWC_{anoxic}^i} \quad ; SWC^i > SWC_{anoxic}^i$$

432 where *q* is the curvature of soil stress function, $SWC_{drought}^i$ and SWC_{anoxic}^i are critical SWC
 433 values for calculating soil stress.

434 In order to make the SWC values comparable between different soil types,
 435 $SWC_{drought}^i$ and SWC_{anoxic}^i can be set in normalized form (such as in Eq. 4)) as part of the
 436 ecophysiological parameterization of the model. More details about the adjustment of the
 437 critical SWC values can be found in Hidy et al. (2021).

438 The layer specific soil moisture stress extent values are summed across the root zone
 439 using the relative amount of roots in the layers (RP^i) as weighting factors to obtain the overall
 440 soil moisture stress extent (*SMSE*):

441 $SMSE = \sum_{i=0}^{i=nr} SMSE^i \cdot RP^i$ (6)

442 $RP^i = RD \frac{z^i}{RL} \cdot e^{-RD \cdot (mid^i / RL)}$ (7)

443 where nr is the number of the soil layers where roots can be found, RL is the actual length of
 444 roots, RD is rooting distribution parameter (ecophysiological parameter; see details in the
 445 User's Guide; Hidy et al., 2021). In the current model version $SMSE$ can also affect the entire
 446 photosynthetic machinery by the introduction of an empirical parameter. This mechanism is
 447 responsible to account for the non-stomatal effect of drought on photosynthesis (details about
 448 this algorithm will be published in a separate paper). Since there is no mechanistic
 449 representation behind this empirical down-regulation of photosynthesis, further test are
 450 needed for the correct setting of this parameter using preferentially eddy covariance data.

451 The soil moisture stress length related factor ($SMSL$) is the ratio of the critical soil
 452 moisture stress length (ecophysiological parameter) and the sum of the daily $(1 - SMSE)$
 453 values. This cumulated value restarts if $SMSE$ is equal to one (no stress). Extreme heat
 454 ($extremT$) is also considered and is taken into account in the final stress function (see above)
 455 by using a ramp function. Its parameterization thus requires the setting of two critical
 456 temperature limits that defines the ramp function (set by the ecophysiological
 457 parameterization; see Hidy et al., 2021). Its characteristic temperature values can be set by
 458 parameterization (ecophysiological input file).

459 **4. Soil carbon and nitrogen cycles**

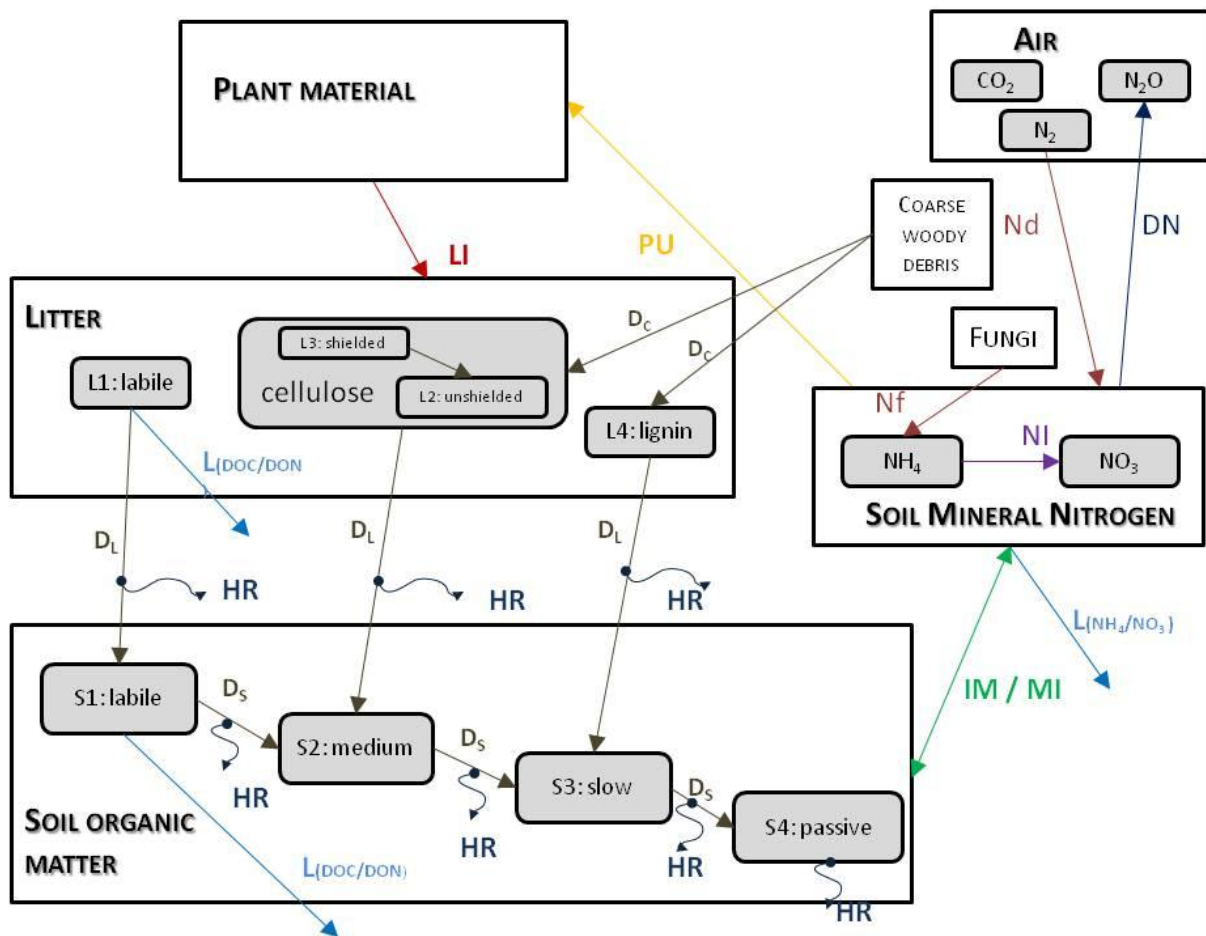
460 **4.1 Soil-litter module**

461 We made substantial changes in the soil biogeochemistry module of the Biome-BGC
 462 model. Previous model versions already offered solutions for multilayer simulations (Hidy et
 463 al., 2012, 2016), but some pools still inherited the single-layer logic of the original model. In
 464 the new model version all relevant soil processes are separated layer by layer which is a major
 465 step forward.

466 Instead of defining a single litter, soil organic carbon (SOC) and nitrogen pool, we
 467 implemented separate carbon and nitrogen pools for each soil layer in the form of soil organic
 468 matter (SOM) and litter in Biome-BGCMuSo v6.2. The changes of the mass of the carbon and
 469 nitrogen pools are calculated layer by layer. Mortality fluxes (whole plant mortality,
 470 senescence, litterfall) of aboveground plant material are transferred into the litter pools of the
 471 top soil layers (0-10 cm, layers 1-2). Mortality fluxes of belowground plant material are

472 transferred into the corresponding soil layers based on their location within the root zone. Due
473 to ploughing and leaching, carbon and nitrogen can also be relocated to deeper layers. The
474 plant material turning into the litter compartment is divided between the different types of
475 litter pools (labile, unshielded cellulose, shielded cellulose and lignin) according to the
476 parameterization. Litter and soil decomposition fluxes (carbon and nitrogen fluxes from litter
477 to soil pools) are calculated layer by layer, depending on the actual temperature and SWC of
478 the corresponding layers. Vertical mixing of soil organic matter between the soil layers (e.g.
479 bioturbation) is not implemented in the current model version.

480 Figure 3 shows the most important simulated soil and litter processes. N-fixation (Nf)
481 is the N input from the atmosphere to soil layers in the root zone by microorganisms. The user
482 can set its annual value as an input parameter. N-deposition (Nd) is the N input from the
483 atmosphere to the top soil layers (see below). The user can set its annual value as a site-
484 specific parameter in the initialization input file. Nitrogen deposition can be provided by
485 annually varying values as well. Plant uptake (PU) is the absorption of mineral N by plants
486 from the soil layers in the root zone. Mineralization (M) is the release of plant-available
487 nitrogen (flux from soil organic matter to mineralized nitrogen). Immobilization (IM) is the
488 consumption of inorganic nitrogen by microorganisms (flux from mineralized nitrogen to soil
489 organic matter). Nitrification (N) is the biological oxidation of ammonium to nitrate through
490 nitrifying bacteria. Denitrification (DM) is a microbial process where nitrate (NO_3^-) is reduced
491 and converted to nitrogen gas (N_2) through intermediate nitrogen oxide gases. Leaching (L) is
492 the loss of water-soluble mineral nitrogen from the soil layers. If leaching occurs in the
493 lowermost soil layer that means loss of N from the simulated system. Litterfall (LI) is the
494 plant material transfer from plant compartments to litter. Decomposition is the C and N
495 transfer from litter to soil pools and between soil pools. In case of woody vegetation coarse
496 woody debris (CWD) contains the woody plant material after litterfall before physical
497 fragmentation. Litter has also four sub-pools based on their composition: labile (L1),
498 unshielded and shielded cellulose (L2, L3) and lignin (L4). Soil organic matter has also four
499 sub-pools based on their turnover rate: labile (S1), medium (S2), slow (S3) and passive
500 (recalcitrant; S4) SOM pool. Soil mineralized nitrogen pool contains the inorganic N-forms of
501 the soil: ammonium and nitrate.



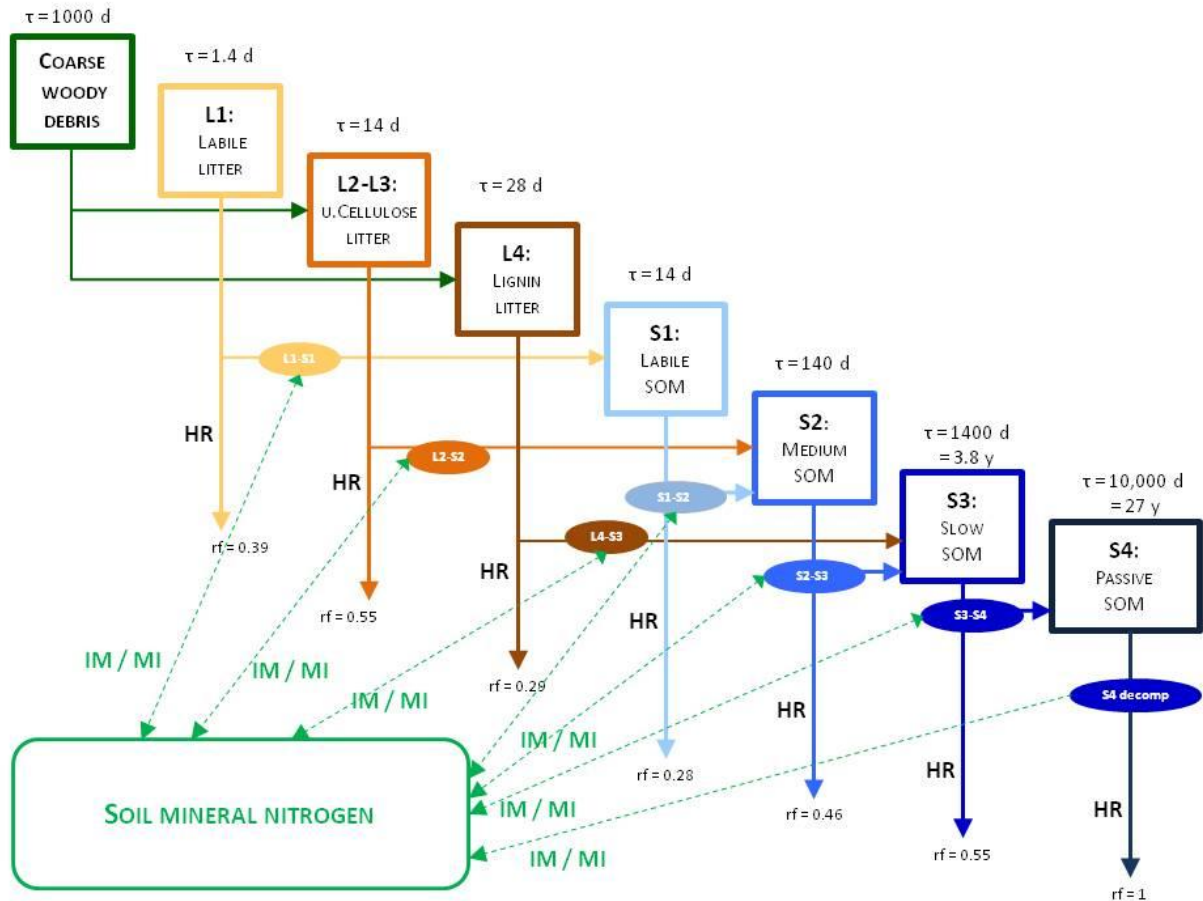
502
 503 **Figure 3: Soil and litter related simulated carbon/nitrogen fluxes (arrows) and pools (rectangles) in Biome-BGCMuSo**
 504 **v6.2. HR: heterotrophic respiration, IM: immobilization, MI: mineralization, PU: plant uptake, LI: litterfall, NI:**
 505 **nitrification, D: decomposition (D_L : decomposition of litter, D_s : decomposition of SOM, D_c : fragmentation of coarse**
 506 **woody debris), L: leaching, Nf: nitrogen fixation, Nd: nitrogen deposition, DN: denitrification. L represents loss of C**
 507 **and N from the simulated system.**

508

509 4.2 Decomposition

510 In the decomposition module (i.e. converging cascade scheme; Thornton, 1998) the
 511 fluxes between litter and soil pools are calculated layer by layer. The potential fluxes are
 512 modified in case of N limitation when the potential gross immobilization is greater than the
 513 potential gross mineralization.

514 To explain the decomposition processes implemented in Biome-BGCMuSo v6.2 the
 515 main carbon/nitrogen pools and fluxes between litter and soil organic and inorganic
 516 (mineralized) matter are presented on Figure 4.



517

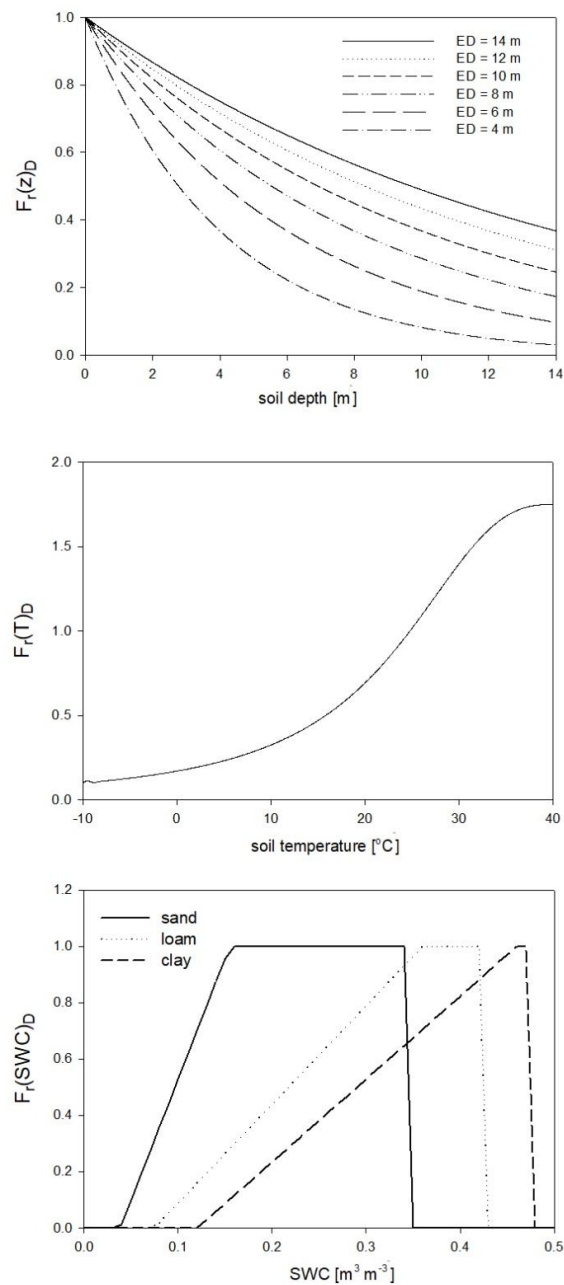
518 Figure 4: Overview of the converging cascade model of litter and soil organic matter decomposition that is
 519 implemented in Biome-BGCMuSo v6.2. rf represents the respiration fraction of the different transformation fluxes, τ
 520 is the residence time (reciprocal of the rate constants that is the turnover rate), IM/MI: immobilization/mineralization
 521 fluxes, HR: heterotrophic respiration. Note that both the respiration fraction and the turnover rate parameters can be
 522 adjusted through parameterization.

523

524 In the original Biome-BGC and in previous Biome-BGCMuSo versions the C:N ratio
 525 (CN) of the soil pools were fixed in the model code. One of the new features in
 526 Biome-BGCMuSo v6.2 is that the CN of the passive soil pool (S4 in Figure 4; recalcitrant soil
 527 organic matter) can be set by the user as a soil parameter. The CN of the other soil pools
 528 (labile, medium and slow; S1, S2 and S3) are calculated based on the proportion of fixed CN
 529 values of the original Biome-BGC ($CN_{\text{labile}} / CN_{\text{passive}} = 1.2$, $CN_{\text{medium}} / CN_{\text{passive}} = 1.2$, $CN_{\text{slow}} /$
 530 $CN_{\text{passive}} = 1$). Note that the CN of the donor and acceptor pools are used in decomposition
 531 calculations (see details in Supplement Material, Section 7), and as a result these parameters
 532 set the C:N ratio of the soil pools. The donor and acceptor pools can be seen in Figure 3 and
 533 Figure 4.

534 For the calculation of nitrogen mineralization first respiration cost (respiration
 535 fraction) is estimated. Mineralization then is the function of the remaining part of the pool and

536 its C:N ratio. The nitrogen mineralization fluxes of the SOM pools are functions of the
 537 potential rate constant (reciprocal of residence time), and the integrated response function that
 538 accounts for the impact of multiple environmental factors. The integrated response function of
 539 decomposition is a product of the response functions of depth, soil temperature and SWC
 540 ($F_r(d)_D$, $F_r(T)_D$, $F_r(SWC)_D$; Figure 5). Its detailed description can be found in the
 541 Supplementary material, Section 7. The dependence of the three different factors on depth,
 542 temperature and SWC with default parameters are presented in Figure 5.



543
 544 **Figure 5: The dependence of the individual factors that form the complex environmental response function of**
 545 **decomposition on depth ($F_r(d)_D$), temperature ($F_r(T)_D$) and SWC in case of different soil types ($F_r(SWC)_D$).** ED is the
 546 **e-folding depth which is one of the adjustable soil parameters of the model. For the definition of sand, silt and clay see**
 547 **Figure 1.**

548 4.3 Soil nitrogen processes

549 In Biome-BGCMuSo v6.2 separate ammonium (sNH_4) and nitrate (sNO_3) soil pools
 550 are implemented instead of a general mineralized nitrogen pool. This was a necessary step for
 551 the realistic representation of many internal processes like plant nitrogen uptake, nitrification,
 552 denitrification, consideration of the effect of different mineral and organic fertilizers and N_2O
 553 emission.

554 It is important to introduce the *availability* concept that Biome-BGCMuSo uses and is
 555 associated with the ammonium and nitrate pools. We use the logic proposed by Thomas et al.
 556 (2013) which means that the plant has access only to a part of the given inorganic nitrogen
 557 pool. Unavailable part is buffered as it is associated with soil aggregates and is unavailable for
 558 plant uptake. The available part of ammonium is calculated based on NH_4 *mobilen proportion*
 559 (that is a soil parameter set to 10% according to Thomas et al., 2013; Hidy et al., 2021) and
 560 the actual pool. The available part of nitrate is assumed to be 100%.

561 The amount of ammonium and nitrate are determined layer by layer controlled by
 562 input and output fluxes (F in $kg\ N\ m^{-2}\ day^{-1}$) listed below:

$$563 F_{sNH_4}^i = IN_{sNH_4}^i - L_{sNH_4}^i + L_{sNH_4}^{i-1} - PU_{sNH_4}^i - IM_{sNH_4}^i + MI_{sNH_4}^i - NI_{sNH_4}^i \quad (8)$$

$$564 F_{sNO_3}^i = IN_{sNO_3}^i - L_{sNO_3}^i + L_{sNO_3}^{i-1} - PU_{sNO_3}^i - IM_{sNO_3}^i + MI_{sNO_3}^i - DN_{sNO_3}^i \quad (9)$$

565 where $IN_{sNH_4}^i$ and $IN_{sNO_3}^i$ are the input fluxes to the ammonium and nitrate pools, respectively;
 566 $L_{sNH_4}^i, L_{sNH_4}^{i-1}, L_{sNO_3}^i, L_{sNO_3}^{i-1}$ are the amount of leached mineralized ammonium and nitrate from
 567 a layer (i) or from the upper layer ($i-1$), respectively; $PU_{sNH_4}^i$ and $PU_{sNO_3}^i$ are the plant uptake
 568 fluxes of ammonium and nitrate, respectively; $IM_{sNH_4}^i$ and $IM_{sNO_3}^i$ are the immobilization
 569 fluxes of ammonium and nitrate, respectively; $MI_{sNH_4}^i$ and $MI_{sNO_3}^i$ are the mineralization
 570 fluxes of ammonium and nitrate, respectively; $NI_{sNH_4}^i$ is the nitrification flux of ammonium
 571 and $DN_{sNO_3}^i$ is the denitrification flux of nitrate.

572 In the following subsections the different terms of the equations are described in
 573 detail.

574 Input to the sNH_4 and sNO_3 pools (IN in Eq. 6 and 7)

575 According to the model logic N-fixation occurs in the root zone layers. Its distribution
 576 between sNH_4 and sNO_3 pools is calculated based on their actual available proportion in the
 577 actual layer (NH_4prop^i):

$$578 NH_4prop^i = sNH_4avail^i + sNO_3avail^i \quad (10)$$

579 where sNH_4avail^i and sNO_3avail^i are the available part of the sNH_4 and sNO_3 pools in the
 580 actual layer.

581 N-deposition related nitrogen input is associated with the 0-10 cm soil layers assuming
582 uniform distribution across layers 1-2 in the model, and the distribution between sNH₄ and
583 sNO₃ pools is calculated based on the *proportion of NH₄ flux of N-deposition* soil parameter
584 (Hidy et al., 2021).

585 Organic and inorganic fertilization is also an optional nitrogen input. The amount and
586 composition (NH₄⁺ and NO₃⁻ content) can be set in the fertilization input file.

587

588 Leaching - downward movement of mineralized N (L in Eq. 6 and 7)

589 The amount of leached mineralized N (mobile part of the given N pool) from a layer is
590 directly proportional to the amount of drainage and the available part of the sNH₄ and sNO₃
591 pools. Leaching from the layer above is a net gain, while leaching from actual layer is a net
592 loss for the actual layer. Leaching is described in Section 4.5.

593

594 Plant uptake by roots (PU in Eq. 6 and 7)

595 N uptake required for plant growth is estimated in the photosynthesis calculations and
596 the amount is distributed across the layers in the root zone. The partition of the N uptake
597 between sNH₄ and sNO₃ pools is calculated based on their actual available proportion in each
598 layer.

599

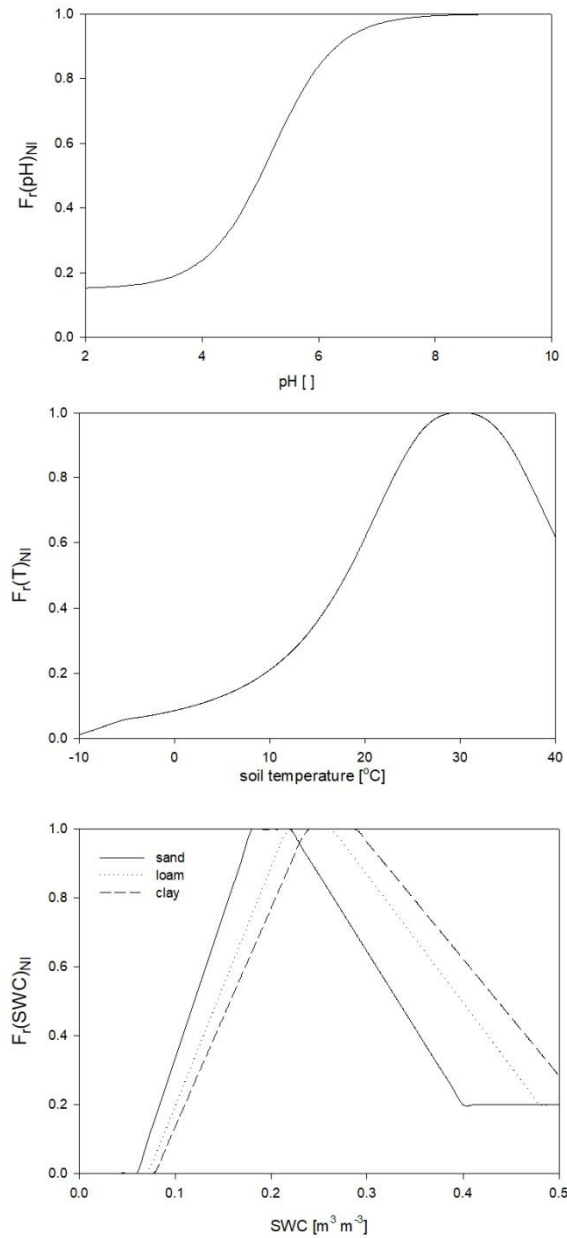
600 Mineralization and immobilization (MI and IM Eq. 6 and 7)

601 Mineralization and immobilization calculations are detailed in Section 4.2. The
602 distribution of these N fluxes between sNH₄ and sNO₃ pools is calculated based on their
603 actual available proportion in each layer.

604

605 Nitrification (NI Eq. 6 and 7)

606 Nitrification is a function of the soil ammonium content, the net mineralization and the
607 response functions of temperature, soil pH and SWC ($F_r(pH)_{NI}$, $F_r(T)_{NI}$, and $F_r(SWC)_{NI}$,
608 respectively) based on the method of Parton et al. (2001) and Thomas et al. (2013). Its
609 detailed mathematical description can be found in the Supplementary material, Section 8. The
610 response functions with proposed parameters are shown in Figure 6.



611

612 **Figure 6: The dependence of the individual factors of the environmental response function of nitrification on soil pH**
 613 **($F_r(\text{pH})_{\text{NI}}$), temperature ($F_r(\text{T})_{\text{NI}}$) and SWC $F_r(\text{SWC})_{\text{NI}}$ in case of different soil types. pH and temperature response**
 614 **functions are independent of the soil texture.**

615

616 Denitrification (DN Eq. 6 and 7)

617 Denitrification flux is estimated with a simple formula (Thomas et al., 2013):

618
$$DN^i = DNcoeff \cdot SOMresp^i \cdot sNO3avail^i \cdot WFPS^i \quad (11)$$

619 where DN of the actual layer is the product of the available nitrate content ($sNO3avail$ in
 620 kg N m^{-2}), $SOMresp^i$ in $\text{g C m}^{-2} \text{ day}^{-1}$ is the SOM decomposition related respiration cost, the
 621 $WFPS^i$ is the water-filled pore space and $DNcoeff$ is the *soil respiration related*
 622 *denitrification rate* in g C^{-1} , which is an input soil parameter (Hidy et al., 2021). The unitless

623 water-filled pore space is the ratio of the actual and the saturated SWC. SOM decomposition
624 associated respiration is the sum of the heterotrophic respiration fluxes of the four soil
625 compartments (S1-S4, Figure 4.).

626 **4.4 N₂O-emission and N-emission**

627 During both nitrification and denitrification N₂O-emission occurs which (added to the
628 N₂O-flux originated from grazing processes if applicable) contributes to the total N₂O-
629 emission of the examined ecosystem.

630 In Biome-BGCMuSo v6.2 a fixed part (set by the *coefficient of N₂O emission of*
631 *nitrification* input soil parameter; Hidy et al., 2021) of nitrification flux is lost as N₂O and not
632 converted to NO₃.

633 During denitrification, nitrate is transformed into N₂ and N₂O gas depending on the
634 environmental conditions: NO₃ availability, total soil respiration (proxy for microbial
635 activity), SWC and pH. The *denitrification related N₂/N₂O ratio* input soil parameter is used
636 to represent the effect of the soil type on the N₂/N₂O ratio (del Grosso et al., 2000; Hidy et al.,
637 2021). Detailed mathematical description of the algorithm can be found in the Supplementary
638 material, Section 9.

639 **4.5 Leaching of dissolved matter**

640 Leaching of nitrate, ammonium, and dissolved organic carbon and nitrogen (DOC and
641 DON) content from the actual layer is calculated as the product of the concentration of the
642 dissolved component in the soil water and the amount of water (drainage plus diffusion)
643 leaving the given layer either downward or upward. The dissolved component (concentration)
644 of organic carbon is calculated from the SOC pool contents and the corresponding *fraction of*
645 *dissolved part of SOC* soil parameters. The dissolved component of organic nitrogen content
646 of the given soil pool is calculated from the carbon content and the corresponding C:N ratio.
647 The downward leaching is net loss from the actual layer and net gain for the layer next below;
648 the upward flux is net loss for the actual layer and net gain for the layer next up. The
649 downward leaching of the bottom active layer (9th) is net loss for the system. The upward
650 movement of dissolved substance from the passive (10th) layer is net gain for the system.

651 **5. Case studies**

652 **5.1 Evaluation of soil hydrological simulation**

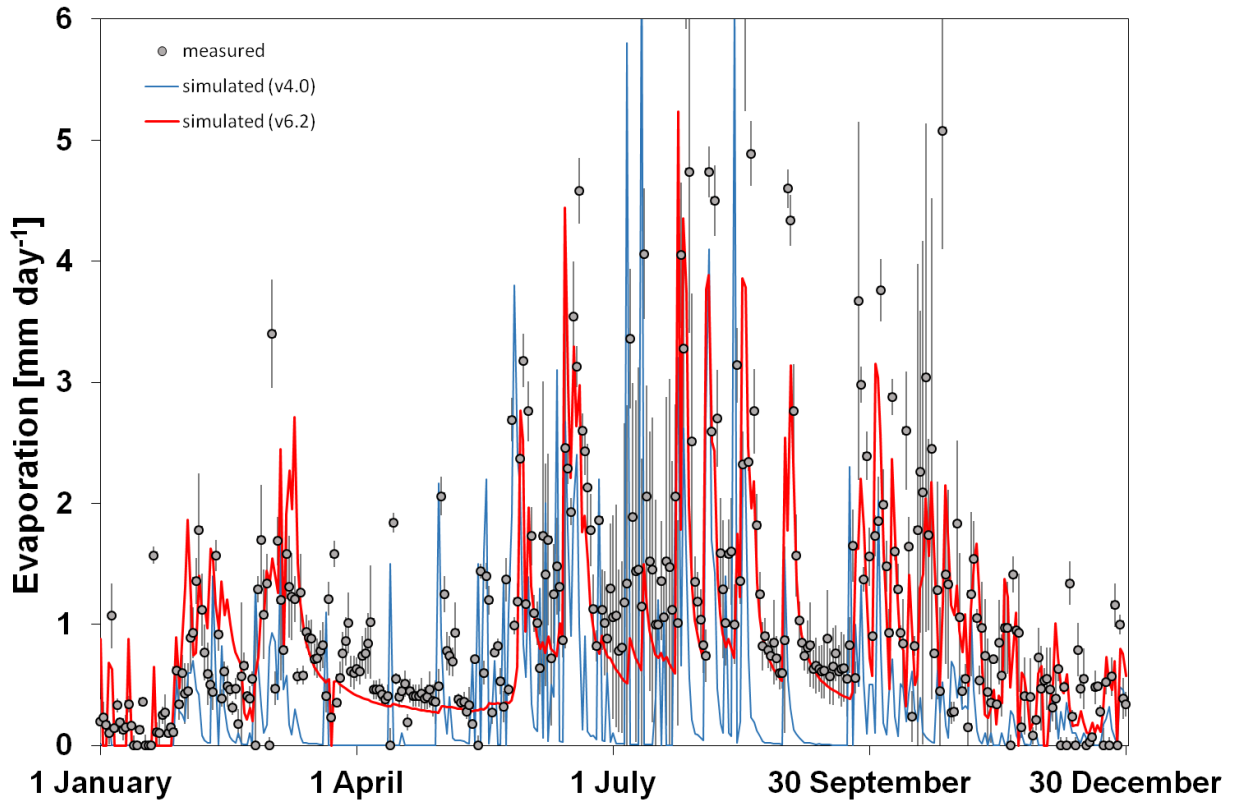
653 In order to evaluate the functioning of the new model version (and to compare
654 simulation results made by the current and the previously published model version), a case
655 study is presented regarding soil water content and soil evaporation simulations. The results
656 of a bare soil simulation (i.e. no plant is assumed to be present) are compared to observation
657 data of a weighing lysimeter station installed at Martonvásár, Hungary (47°18'57.6"N,
658 18°47'25.6"E) in 2017. The climate of the area is continental with a 30-year average
659 temperature of 11.0 °C (−1 °C in January and 21.2 °C in July) and annual rainfall of 548 mm,
660 based on data of the on-site weather station.

661 The station consists of twelve 2 meter deep scientific lysimeter columns with 1 m
662 diameter (Meter Group Inc., USA) with soil temperature, SWC and soil water potential
663 sensors installed at 5, 10, 30, 50, 70, 100 and 150 cm depth. Observation data for 2020 from
664 six columns without vegetation cover (i.e. bare soil) was used to validate the model.

665 Raw lysimeter observation data were processed using standard methods. Bare soil
666 evaporation values were derived based on changes of the mass of the soil columns also
667 considering the mass change of the drainage water. Additionally, experience has shown that
668 wind speed is related to the high frequency mass change of the soil column mass. To reduce
669 noise, 5-point (5-min) moving averages were used based on Marek et al. (2014). After quality
670 control of the data, the corrected and smoothed lysimeter mass values were used for the
671 calculations. SWC observations were averaged to daily resolution to match the time step of
672 the model.

673 Observed local meteorology was used to drive the models for year 2020. Soil physical
674 model input parameters (field capacity, wilting point, bulk density, etc.) were determined in
675 the laboratory using 100 cm³ undisturbed soil samples taken from various depths during the
676 installation of the lysimeter station. Regarding other soil parameters the proposed values were
677 used. Detailed description of the input soil parameters and their proposed values are presented
678 in the User's Guide (Hidy et al., 2021).

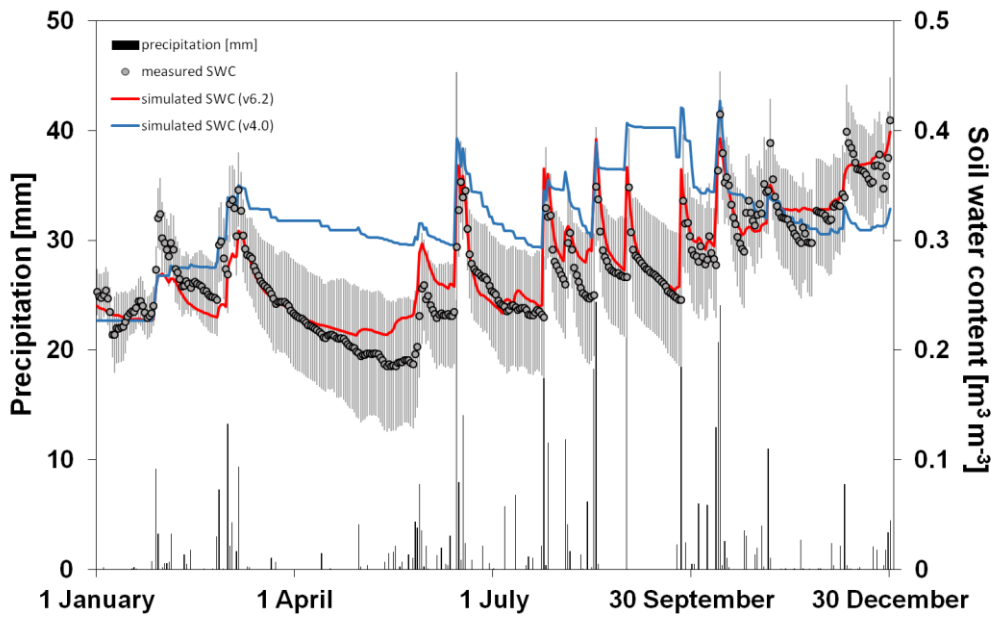
679 In Figure 7 the simulated and the observed time series of soil evaporation are
680 presented for Martonvásár, for 2020. The figure shows that the soil evaporation simulation by
681 v6.2 is more realistic than by v4.0. Biome-BGCMuSo v4.0 provides very low values during
682 summer in some days which is not in accordance with the observations. Biome-BGCMuSo
683 v6.2 provides more realistic values during this time period.



684
 685 **Figure 7: The simulated (blue line: v4.0; red line: v6.2) and the observed (grey dots) daily soil evaporation values at**
 686 **Martonvásár during 2020. Vertical grey lines associated with the observations represent standard deviation of the**
 687 **observations from 6 lysimeter columns. The improved model clearly outperforms the earlier version.**
 688

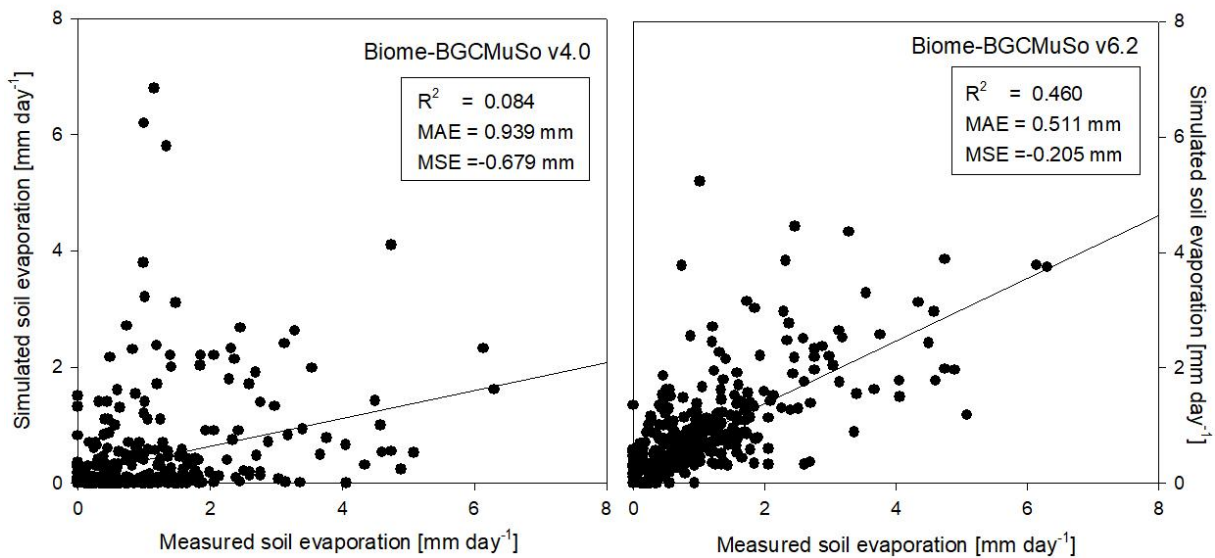
689

690 In Figure 8 the simulated and the observed SWC at 10 cm depth are presented with the
 691 daily sum of precipitation representing the bare soil simulation in Martonvásár, for 2020. The
 692 soil water balance simulation seems to be realistic using v6.2, since the annual course
 693 captures the low and high end of the observed values. In contrast, Biome-BGCMuSo v4.0
 694 underestimates the range of SWC and provides overestimations during the growing season
 695 (from spring to autumn). With a couple of exceptions, the simulated values using v6.2 fall
 696 into the uncertainty range of the measured values defined by the standard deviation of the six
 697 parallel measurements. This is not the case for the simulations with the 4.0 version.



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Figure 8: The simulated (blue line: v4.0; red line: v6.2) and the observed (grey dots) soil water content values at 10 cm depth (right y axis) with the daily sums of precipitation (left axis; black columns) during 2020 at Martonvásár lysimeter station. Vertical grey lines associated with the observations represent +/- one standard deviation around the observations. The improved model clearly outperforms the earlier version in simulating soil water balance.



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Figure 9: Comparison of the simulated (left: v4.0; right: v6.2) and observed daily soil evaporation representing the means of measured data obtained from six weighing lysimeter columns with bare soil at Martonvásár in 2020. R^2 , MAE and MSE denote the coefficient of determination, mean absolute error and mean signed error (bias) of the simulated values, respectively.

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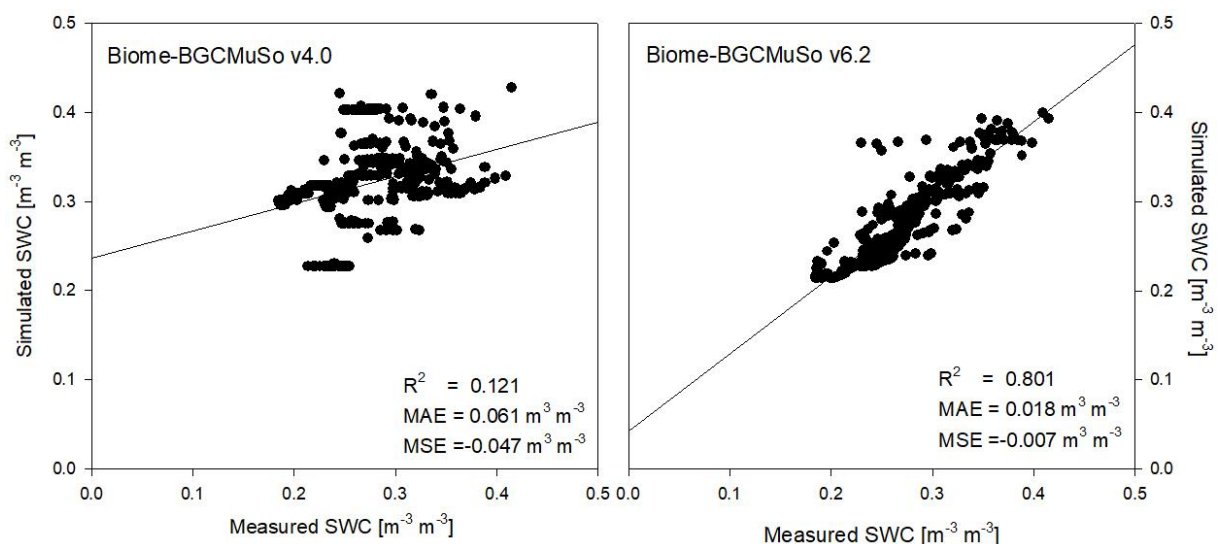
Model performance was evaluated by quantitative measures such as coefficient of determination (R^2), mean absolute error (MAE) and mean signed error (MSE). In Figure 9 the comparison of the simulated and the observed daily evaporation is presented. Based on the

714 performance indicators it is obvious that the simulation with new model version (v6.2) is
 715 much closer to observations than the old version (v4.0). Biome-BGCMuSo v6.2 slightly
 716 underestimated the observations.

717 In Figure 10 the comparison of the simulated and the observed daily SWC from the
 718 lysimeter experiment is presented. Based on the model evaluation it seems that the simulation
 719 with new model version is much closer to observation than with old version (4.0). The results
 720 obtained from v4.0 are consistent with earlier findings about the incorrect representation of
 721 the annual SWC cycle (Hidy et al., 2016; Sándor et al., 2017).

722 Throughout validation of the improved model based on observed SWC and ET
 723 datasets from eddy covariance sites is planned to be published in an upcoming paper about the
 724 plant related improvements.

725



726

727 **Figure 10: Comparison of the simulated (left: v4.0; right: v6.2) and observed daily SWC representing the means of**
 728 **measured data obtained from six weighing lysimeter columns with bare soil at Martonvásár in 2020. R^2 , MAE and**
 729 **MSE denote the coefficient of determination, mean absolute error and mean signed error (bias) of the simulated**
 730 **values, respectively.**

731

732 5.2 Evaluation of the soil nitrogen balance module and the simulated soil respiration

733 Soil related developments were evaluated with a case study focusing on topsoil nitrate
 734 content, soil N_2O efflux and soil respiration.

735 Experimental data were collected in a long-term fertilization experiment that was set
 736 up in 1959 at Martonvásár, Hungary (N 47°18'41", E 18°46'50"). According to the FAO-
 737 WRB classification system (IUSS Working Group, 2015), the soil is a Haplic Chernozem,
 738 with 51.4% sand, 34% silt and 14.6% clay content. Bulk density is 1.47 g cm^{-3} , $\text{pH}(\text{H}_2\text{O})$ is

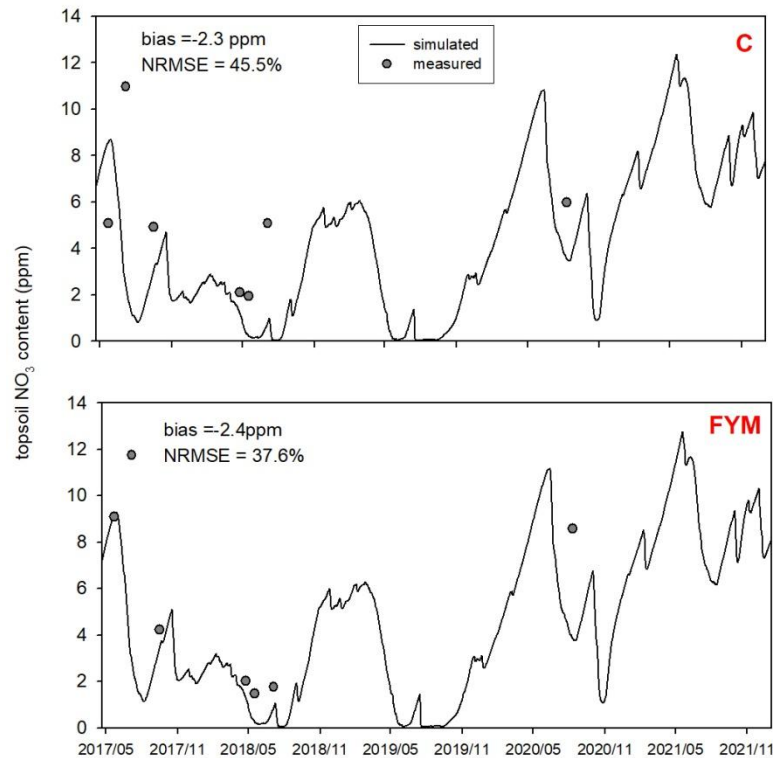
739 7.3, CaCO₃ content is 0–1%, and the mean soil organic matter content in the topsoil is 3.2%.
740 The plant-available macronutrient supply in the soil was poor for Phosphorus and medium to
741 good for Potassium, based on the ProPlanta plant nutrition advisory system (Fodor et al.,
742 2011). In the long-term fertilization experiment the treatments were arranged in a random
743 block design with 6×8 m plots in four replicates. Eight different treatments were set up:
744 control (zero artificial fertilizer applied), only N, only P and NPK – with farmyard manure;
745 absolute control (zero nutrient supply), only N, only P, NPK – without farmyard manure. The
746 crops in the four-year fertilizer cycles were maize in the 1st and 2nd years and winter wheat in
747 the 3rd and 4th years. Here we used data from the absolute control and from the farmyard
748 manure (FYM) treatments only. FYM was applied once every four years at a rate of 35 t ha⁻¹
749 in autumn.

750 Topsoil nitrate content was measured during 2017, 2018 and 2020 on a few occasions
751 by wet chemical reactions using a stream distillation method after KCl extraction of soil
752 samples (Hungarian Standards Institution MSZ 20135:1999; Akhtar et al., 2011).

753 Dynamic chamber based soil N₂O efflux observations were available from 2020 and
754 2021. The N₂O efflux measurements with a gas incubation time of 10 minutes were
755 performed by using a Picarro G2508 (Picarro, USA) cavity ring down spectrometer
756 (Christiansen et al. 2015; Zhen et al. 2021). The cylinder shaped transparent gas incubation
757 chamber was 16.5 cm in diameter and its height was 30 cm. N₂O flux measurements were
758 executed in 6 replicates per treatment on a biweekly (2020) and precipitation event-related
759 (2021) basis. Soil respiration was measured with the same Picarro gas analyser. Sampling
760 numbers and points were identical with those of the N₂O efflux measurements. CO₂ and N₂O
761 effluxes were calculated by linear equation (Widen and Lindroth, 2003) based on gas
762 concentration data.

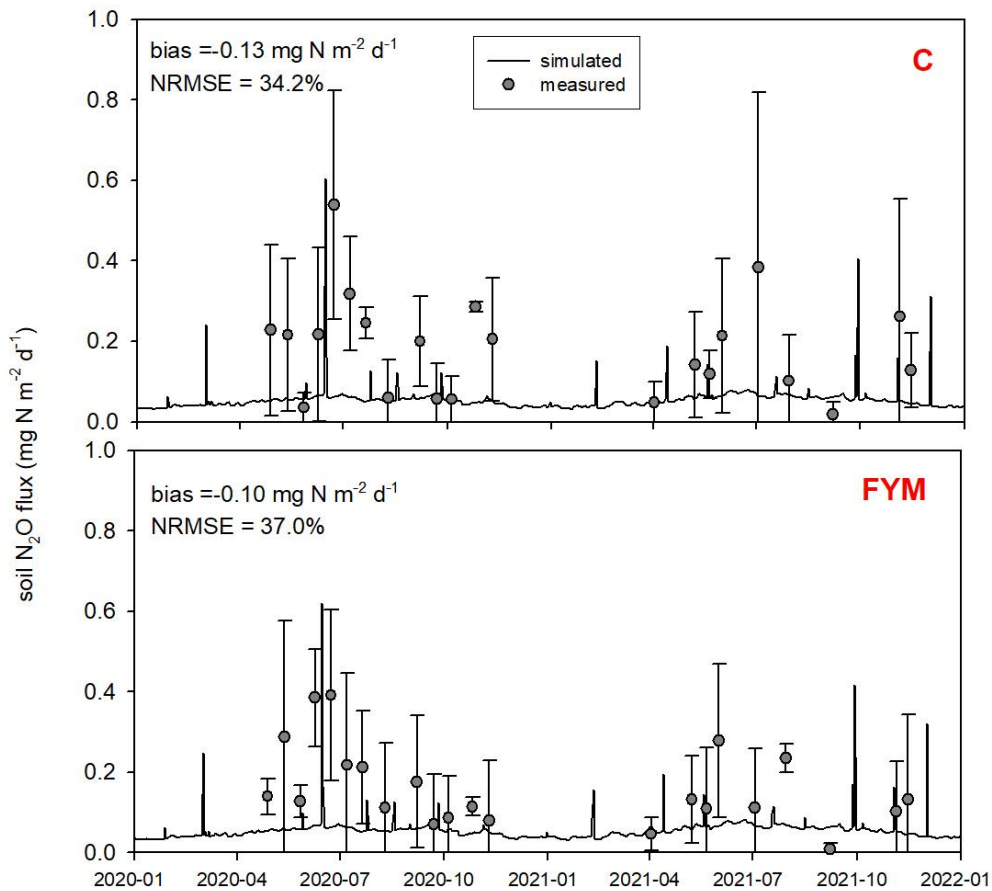
763 For the simulations we used maize parameterization from previous studies (Fodor et
764 al., 2021). Winter wheat parameterization was constructed based on a country-scale
765 optimization using the AgroMo software package (<https://github.com/hollorol/AgroMo>) and
766 the NUTS 3 level long-term (1991-2020) yield database of the Hungarian Central Statistical
767 Office. For nitrogen cycle related parameters we mainly used the values presented in the
768 User's Guide (Hidy et al., 2021). Two soil parameters were adjusted (coefficient of N₂O
769 emission for nitrification and N₂/N₂O ratio multiplier for denitrification related N gas flux;
770 Del Grosso et al., 2000; Parton et al., 2001; Thomas et al., 2013; Hidy et al., 2021) to match
771 the simulated N₂O efflux to the observations.

772 Figure 11 shows the comparison of the simulated and observed NO₃ content of the
 773 topsoil for the two selected treatments. The results indicate that the model underestimate the
 774 topsoil NO₃ content both in the case of C and FYM (bias is -2.3 ppm and -2.4 ppm,
 775 respectively) treatments, but the simulation error is in an acceptable range (NRMSE is 45.5%
 776 and 37.6% for C and FYM, respectively).



777
 778 **Figure 11: Comparison of the simulated and observed NO₃ content of the topsoil for the absolute control (C; upper)**
 779 **and for the farmyard manure (FYM; bottom) treatment between May 2017 and November 2021 at Martonvásár.**
 780

781 Figure 12 shows the comparison of the observed and simulated N₂O efflux for the
 782 2020-2021 time period. Measurement uncertainties are also indicated on the plot. Note that
 783 the uncertainty of the observations (e.g. due to spatial heterogeneity and sample number, soil
 784 disturbance, improper chamber design, methods of sample analysis) is remarkable due to
 785 known features of the chamber technique (Chadwick et al. 2014; Pavelka et al. 2018). The
 786 model captured more of the magnitude of N₂O efflux peaks and less of their timing. Overall
 787 the model underestimated the observed values in both cases (bias is -0.13 mg N m⁻² day⁻¹ and
 788 -0.1 mg N m⁻² day⁻¹ for C and FYM, respectively), with NRMSE of 32.4% and 37.6% for C
 789 and FYM, respectively.



790

791 **Figure 12: Comparison of the simulated and observed soil N₂O efflux for two treatments: absolute control (C; upper)**
 792 **and application of farmyard manure (FYM; bottom) between January 2020 and December 2021 at Martonvásár.**
 793 **Whiskers indicate the uncertainty (\pm one standard deviation) of the measurements.**

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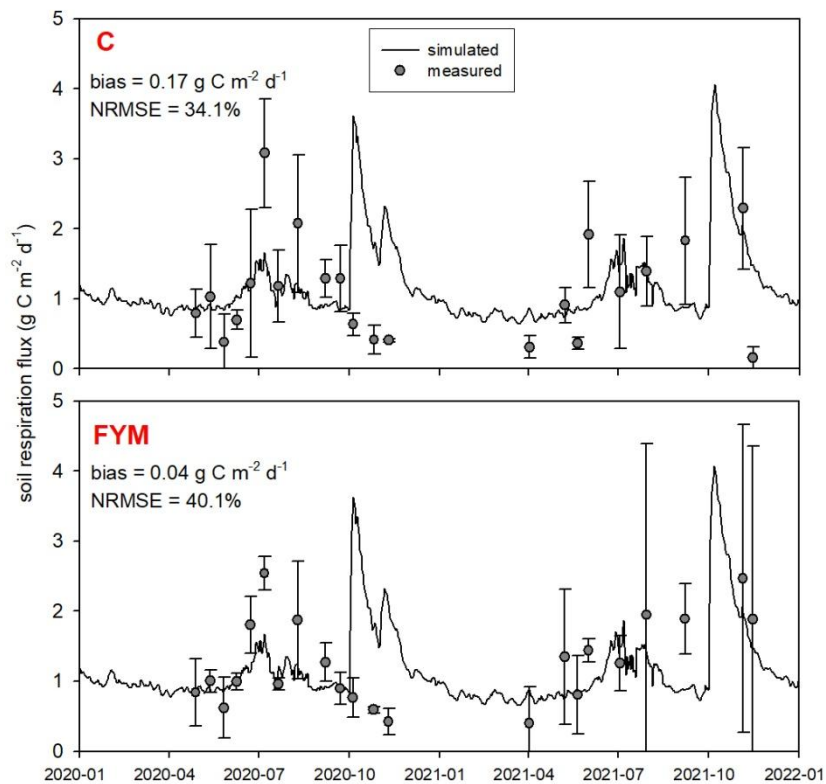
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Figure 13 presents the comparison of the observed and simulated soil respiration for the same time period as for the soil N₂O efflux. Observation uncertainty is indicated that represents one standard deviation of the replicates. The model mostly captured the magnitude and variability of soil respiration flux. The model overestimated the observed values in both cases with bias of 0.17 g C m⁻² day⁻¹ and 0.04 g C m⁻² day⁻¹ for C and FYM, respectively. The NRMSE is 34.1% and 40.1% for C and FYM, respectively. It is interesting to note that the observations and the simulations are particularly different after harvest time in both years (i.e. beginning of October). The simulated respiration have peaks are corresponding to harvest when the amount of litter sharply increases due to the byproducts left behind (decomposition of residues left on the site after harvest are accounted for in the model). The chamber based CO₂ efflux data did not really show similar peaks likely because of methodological issues (litter is removed from the soil surface before placing of the chambers).



807
 808 **Figure 13: Comparison of the simulated and observed soil respiration flux for two treatments: absolute control (C;**
 809 **upper) and application of farmyard manure (FYM; bottom) between January 2020 and December 2021 at**
 810 **Martonvásár. Whiskers indicate the uncertainty (\pm one standard deviation) of the measurements.**
 811

812 Overall, the model provided nitrate content, N_2O emission and soil respiration
 813 simulation results that are consistent with the observations. The model was capable of
 814 estimating the observed values with a comparable efficiency reported in similar studies
 815 (Gabrielle et al., 2002; Andrews et al., 2020).

816 5.3 Sensitivity analysis and optimization of the soil biogeochemistry scheme

817 Here we present another case study that provides insight into the functioning of the
 818 converging cascade (decomposition) scheme that is implemented in Biome-BGCMuSo v6.2.
 819 A large scale in silico experiment is also presented where the main aim was to perform model
 820 self-initialization (i.e. spinup) at country scale (for the entire area of Hungary) where the
 821 resulting soil organic matter pools are expected to be consistent with the observations.

822 The observation based, gridded, multi-layer SOC database of Hungary (DOSoReMI
 823 database; Pásztor et al., 2020; see Supplementary material Figures S3-S4) as well as the
 824 FORESEE meteorological database (Kern et al., 2016) was used for the sensitivity analysis of
 825 the soil scheme as well as for optimizing the most important soil parameters when the model

826 was calibrated to the observation based SOC values. As a first step, the area of the country
827 was divided into 1104 grid cells (regular grid with 0.1° by 0.1° resolution, corresponding to
828 an approximately 10 km resolution). The 1104 grid cells of the DOSoReMI database were
829 grouped based on their dominant land-use type (cropland, grassland, forest based on
830 CORINE-2018 database; EEA, 2021; Supplementary material Figures S1-S2) as well as the
831 soil texture class (12 classes according to the USDA system; USDA, 1987) and SOC content
832 (high and low; high is greater than the group mean while low is less than the mean) of the
833 topsoil (0-30 cm layer). As some of the theoretically possible 72 groups had no members (e.g.
834 there is no soil in Hungary with sandy-clay texture) soils of the 1104 grid cells were
835 categorized into 51 groups. For each group one single cell (so-called representative cell) was
836 selected based on the topsoil SOC content. The representative cell was the one with the
837 smallest absolute deviation from the group mean SOC content. (Land use maps for Hungary
838 are presented in the Supplementary Material Section 10: Figure S1-S2).

839 Grassland ecophysiological parameterization without management was used in the
840 spinup phase to initialize SOC pools for croplands. For the transient phase cropland
841 parameterization was used with fertilization, ploughing, planting and harvest settings. In case
842 of grasslands, both during the spinup and transient phases grassland parameterization was
843 used, and in the transient phase mowing was assumed once a year. In case of forests generic
844 deciduous broadleaf forest parameterization was used for both spinup and transient phases
845 with thinning in the latter phase. For our parameterization presented in the MS the generic,
846 plant functional type specific ecophysiological parameter sets published by White et al.
847 (2000) served as starting points. These Biome-BGCMuSo specific parameter sets are
848 available at the website of the model¹.

849 Soil parameters in Biome-BGCMuSo v6.2 were classified into six groups: (1) 4
850 generic soil parameters, (2) 24 decomposition-nitrification-denitrification related parameters,
851 (3) 14 rate scalars for the converging (decomposition) cascade scheme, (4) 19 soil moisture
852 related parameters, (5) 7 methane related parameters and (6) 11 soil composition and
853 characteristic values (can be set layer by layer). Detailed description and proposed value of
854 each soil parameters can be found in the User's Guide (Hidy et al., 2021).

855

856

¹ http://nimbus.elte.hu/bbgc/files/generic_EPC_set_6.2.zip

857 **Table 1: Soil parameters of Biome-BGCMuSo v6.2 (referring to SOC simulation) that were used during the sensitivity**
858 **analysis. The VALUE column shows the originally proposed values (Hidy et al., 2021). See Figure 4 for explanation on**
859 **the compartment names. The parameters that were included in the 2nd phase of the sensitivity analysis are marked**
860 **with bold letters (see text).**

GROUP	PARAMETER NAME	ABBREVIATION	VALUE
Generic soil parameters	C:N ratio of stable soil pool (soil4)	soil4CN	12
	NH4 mobilen proportion	amMP	0.1
	aerodynamic resistance	potRair	107
Decomposition, nitrification, denitrification parameters	parameter 1 for temperature response function of decomp.	Tp1decomp	1.75
	parameter 2 for temperature response function of decomp.	Tp2decomp	17
	parameter 3 for temperature response function of decomp.	Tp3decomp	2.6
	parameter 4 for temperature response function of decomp.	Tp4decomp	40
	minimum T for decomposition and nitrification	Tp5decomp	-5
	e-folding depth of decomposition rate's depth scalar	EFD	10
	net mineralization proportion of nitrification	NITRnetMINER	0.2
	maximum nitrification rate	NITRmaxRATE	0.1
	coefficient of N2O emission of nitrification	NITRratioN2O	0.02
	parameter 1 for pH response function of nitrification	pHp1nitrif	0.15
	parameter 2 for pH response function of nitrification	pHp2nitrif	1
	parameter 3 for pH response function of nitrification	pHp3nitrif	5.2
	parameter 4 for pH response function of nitrification	pHp4nitrif	0.55
	parameter 1 for Tsoil response function of nitrification	Tp1nitrif	1
	parameter 2 for Tsoil response function of nitrification	Tp2nitrif	12
	parameter 3 for Tsoil response function of nitrification	Tp3nitrif	2.6
	parameter 4 for Tsoil response function of nitrification	Tp4nitrif	2.6
	minimum WFPS for scalar of nitrification calculation	minWFPS	0.1
	lower optimum WFPS for scalar of nitrification	opt1WFPS	0.45
	higher optimum WFPS for scalar of nitrification	opt2WFPS	0.55
	minimum value for saturated WFPS scalar of nitrification	minWFPSscalar	0.2
	soil respiration related denitrification rate	DENITcoeff	0.05
	denitrification related N2/N2O ratio multiplier	DNratioN2O	2
critical WFPS value for denitrification	critWFPSdenitr	0.50	
Rate scalars	respiration fractions for fluxes between compartments (11s1)	RF11s1	0.39
	respiration fractions for fluxes between compartments (12s2)	RF12s2	0.55
	respiration fractions for fluxes between compartments (14s3)	RF14s3	0.29
	respiration fractions for fluxes between compartments (s1s2)	RFs1s2	0.28
	respiration fractions for fluxes between compartments (s2s3)	RFs2s3	0.46
	respiration fractions for fluxes between compartments (s3s4)	RFs3s4	0.55
	potential rate constant of labile litter pool	RCS1	0.7
	potential rate constant of cellulose litter pool	RCS2	0.07
	potential rate constant of lignin litter pool	RCS3	0.014
	potential rate constant of fast microbial recycling pool	RCS4	0.07
	potential rate constant of medium microbial recycling pool	RCS5	0.014
	potential rate constant of slow microbial recycling pool	RCS6	0.0014
	potential rate constant of recalcitrant SOM (humus) pool	RCS7	0.0001
	potential rate constant of physical fragmentation of wood	RCS8	0.001
	maximum height of pond water	MP	5
	curvature of soil stress function	q	1
	fraction of dissolved part of S1 organic matter	fD1	0.005
	fraction of dissolved part of S2 organic matter	fD2	0.004
	fraction of dissolved part of S3 organic matter	fD3	0.003
	fraction of dissolved part of S4 organic matter	fD4	0.002
	mulch parameter: critical amount	CAmulch	1
	parameter 1 for mulch function	p1mulch	100
	parameter 2 for mulch function	p2mulch	0.75
	parameter 3 for mulch function	p3mulch	0.75
	mulch parameter: evaporation reduction	ERmulch	0.5

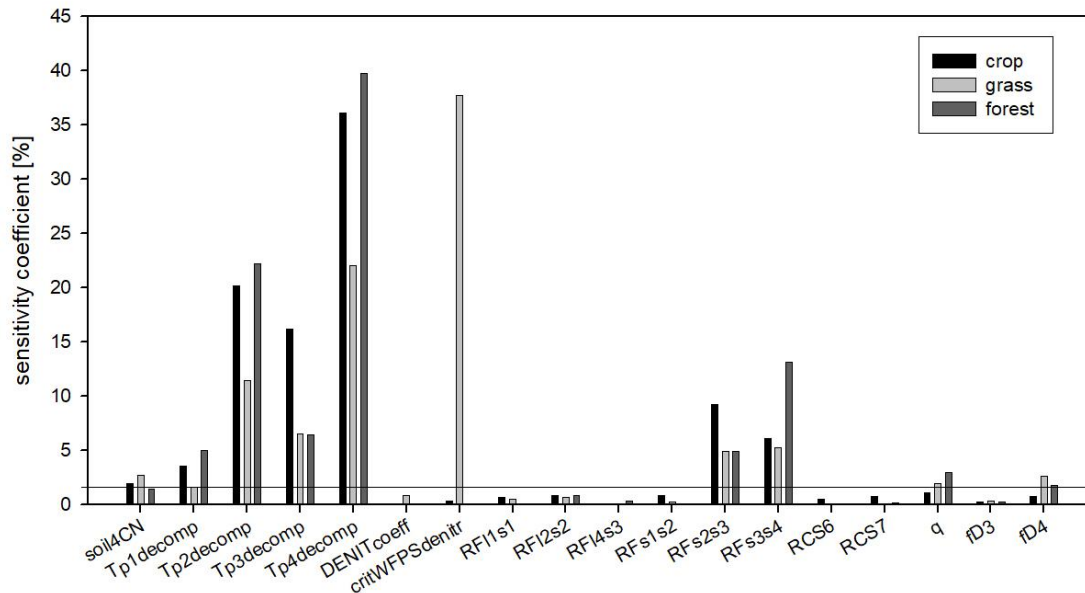
861 As methane simulation was not the subject of the present case study we neglected the
862 related parameters. Regarding to the soil composition and characteristic values we used the
863 DOSoReMI database (Pásztor et al., 2020). From the remaining 61 parameters soil depth,
864 runoff curve number, the three soil moisture related parameters (tipping bucket method) were
865 not included in the analysis. The groundwater module was switched off in this case (no
866 groundwater is assumed) and the related parameters were not studied. The remaining 53
867 parameters were used in the sensitivity analysis and are listed in Table 1.

868 As a first step sensitivity analysis was carried out for the selected 53 soil parameters
869 by running the Biome-BGCMuSo v6.2 model in spinup mode until a quasi-equilibrium in the
870 total SOC is reached (that is the usual logic of the spinup run). The model was run for each
871 representative cell 2000 times with varying model parameters using Monte-Carlo method.
872 Each model parameters were varied randomly within the $\pm 10\%$ range of their initial values
873 that were inherited from the Biome-BGC model or were set according to the literature. The
874 least square linearization (LSL) method (Verbeeck et al., 2006) was used for dividing output
875 uncertainty into its input parameter related variability. As result of the LSL method, the total
876 variance of the model output and the sensitivity coefficient of each parameter can be
877 determined. Sensitivity coefficients show the percent of total variance for which the given
878 parameter is responsible.

879 In order to simplify the workflow and decrease the degree of freedom another
880 sensitivity analysis was performed. In this second step, the sensitive parameters (sensitivity
881 coefficient $> 1\%$ for at least one land use type; a total of 18 parameters) were used in the
882 following sensitivity analysis with 6000 iteration steps. These 18 parameters are marked with
883 bold letters in Table 1.

884 Figure 14 shows the summary of the second sensitivity analysis where the overall
885 importance of the parameters is calculated as the mean of all selected pixels in a given land
886 use category. It can be seen in Figure 4 that from the 18 parameters (selected during the first
887 phase) soil carbon ratio of the recalcitrant pool (soil4CN), the temperature dependence
888 parameters of decomposition function (Tp1decomp, Tp2decomp, Tp3decomp, Tp4_decomp)
889 and the respiration fraction of S2-S3 and S3-S4 decomposition process (RFs2s3 and RFs3s4),
890 the curvature of soil stress function ($q_{\text{soilstress}}$) and the fraction of dissolved part of S4 organic
891 matter (fD4) are the most important for all land use types. Among the other parameters the
892 critical WFPS of denitrification (critWFPSdentir) for grasslands has a remarkably high
893 sensitivity (greater than 35%). It means that in case of grasslands the nitrogen availability
894 seems to be an important limitation of the primary production, probably because there are

895 only natural sources of nitrogen (no fertilization is assumed here), and the rooting zone is
 896 shallower than in case of forest which involves limited mineralized N access. Thus, in case of
 897 higher values of critical WFPS of denitrification, the simulated production of the grassland
 898 (and therefore the final SOC) seems to be significantly underestimated.

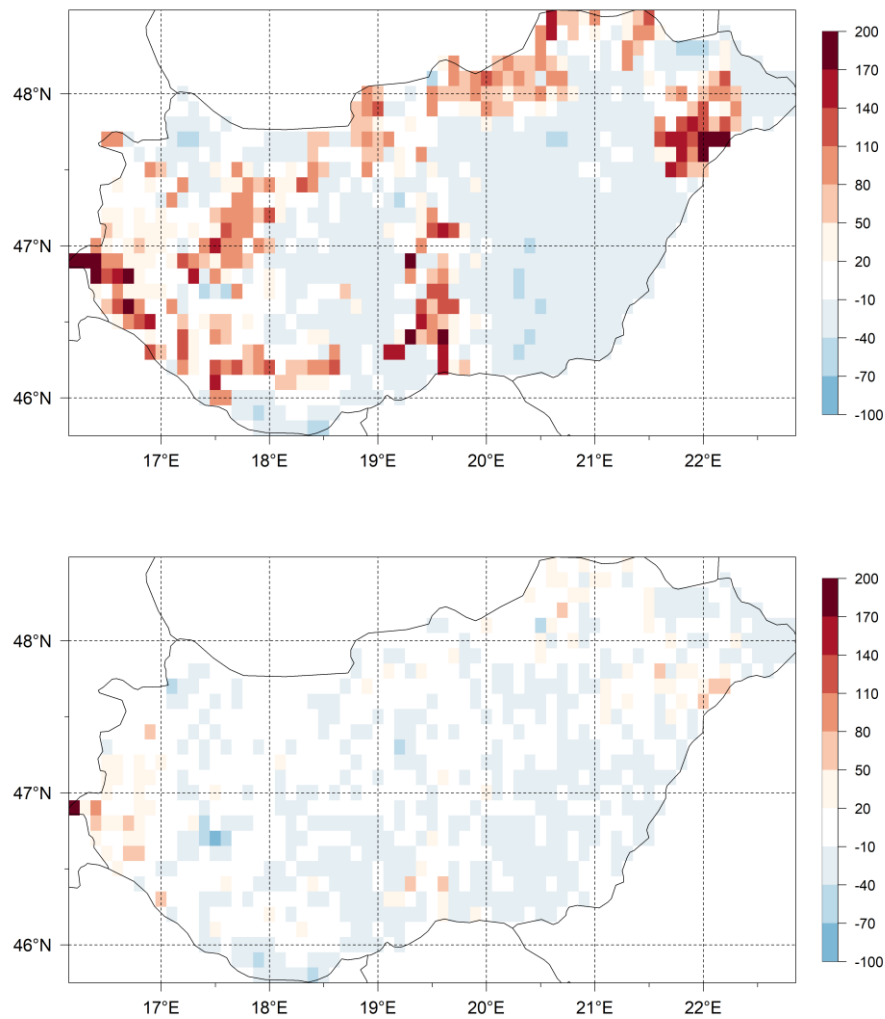


899 **Figure 14: The sensitivity coefficients of the soil parameters as the result of the sensitivity analysis. Black columns**
 900 **refer to the crop, light grey to the grass and dark grey to the forest simulations. The sensitivity coefficients are**
 901 **calculated as the mean pixel level sensitivity coefficient for the given land use type. Horizontal line indicates the 5%**
 902 **threshold that was used to select the final parameter set for optimization.**
 903

904

905 The selected ten, soil biogeochemistry related parameters were optimized for each of
 906 the 51 groups separately, using maximum likelihood estimation. For each group, the
 907 parameter set providing the smallest deviation between the simulated and the observed values
 908 of the weighted average SOC content (weight factor of 5 is used for the 0-30 cm, and weight
 909 factor of 1 is used for the 30-60 cm soil layers) was considered to be the final (optimized)
 910 model parameter set.

911 The differences of the simulated and observed SOC content for the 0-30 cm layer
 912 (SOC0-30) using the initial (Table 1) and final soil parameters (not shown here) are presented
 913 in Figure 15. On the upper plot the signed relative error of SOC0-30 simulation before
 914 optimization, while on the lower figure the signed relative error of SOC0-30 simulation after
 915 optimization can be seen. It is clearly visible that because of optimization the overestimation
 916 of the SOC0-30 simulation significantly decreased.



917

918 **Figure 15: Differences (expressed as signed relative error, %) between the simulated and observed SOC data for the**
 919 **0-30 layer (SOC0-30) using the initial (upper map) and optimized (lower map) soil parameters. Visual comparison of**
 920 **the maps reveals the success of the optimization in terms of capturing the overall SOC for the whole country area.**

921

922 We do not claim of course that the optimized parameters have universal value. Site
 923 history is neglected during the spin up simulations, and we use many simplifications like
 924 disregarding land use change, present-day ecophysiological parameterization etc. In this
 925 sense, the optimized parameter set can be best considered as a pragmatic solution to provide
 926 initial conditions (equilibrium SOC pools) for the model at country scale that is consistent
 927 with the observations.

928 **6. Concluding remarks**

929 In this paper, we presented a detailed description of the soil hydrology and
 930 carbon/nitrogen budget related developments of the Biome-BGCMuSo v6.2 terrestrial
 931 ecosystem model. We mostly focused on changes relative to the previously published Biome-
 932 BGCMuSo v4.0 (Hidy et al., 2016), but our intention was also to provide a complete,
 933 standalone reference for the modelling community with mathematical equations (detailed in
 934 the Supplementary Material). Table 2 summarizes the structural changes that we made during
 935 the developments starting from Biome-BGC v4.1.1 also including the previously published
 936 Biome-BGCMuSo v4.0 (Hidy et al., 2016).

937

938 **Table 2. Comparison of the internal processes simulated in Biome-BGC 4.1.1, Biome-BGCMuSo v4.0 and in Biome-**
 939 **BGCMuSo v6.2.**

Routine	original Biome-BGC	Biome-BGCMuSo v4.0	Biome-BGCMuSo v6.2
Runoff	no	based on simple, empirical formulation	distinguishing Hortonian and Dunne runoff
Pond water	no	simple solution	development of pond water formation (based on infiltration capacity)
Soil evaporation	Based on Penman-Monteith equation Calculation of the actual evaporation from the potential evaporation and the square root of time elapsed since the last precipitation.	Based on Penman-Monteith equation Calculation of the actual evaporation from the potential evaporation and the square root of time elapsed since the last precipitation.	Based on Penman-Monteith equation Parameterization possibility of actual aerodynamic resistance. Introduction of an upper limit for daily potential evaporation that is determined by the available energy. Calculation of the actual evaporation is based on the method Ritchie (1981). Simulation of the reducing effect of surface residue or mulch cover on bare soil evaporation
Transpiration	Transpiration from one-layer bucket soil	Transpiration from 7-layers soil based on soil stress	Transpiration from 10-layers soil based on available water
Groundwater	no	Simple groundwater simulation.	Improvement of the simulation of groundwater effect (using capillary fringe). Introduction of two different methods.
Soil moisture stress	no	Relative SWC data is used to calculate soil water stress. The hygroscopic water, the wilting point, the field capacity and the saturation values of the soil layers can be defined in the input file layer by layer. The soil moisture stress index is affected by the length and the day since the drought event lasted.	The hygroscopic water, the wilting point, the field capacity and the saturation values of the soil layers can be defined in the input file layer by layer. The soil moisture stress index is affected by the length and the severity of the drought event, aggravated by the extreme temperature. Introduction of the soil curvature parameters to provide mechanism for soil texture dependent drought stress since it can affect the shape of the soil stress function.

			Normalized SWC data are used to calculate soil moisture stress index.
Organic carbon and nitrogen	One layer soil module with one organic carbon and nitrogen pool.	Multi-layered soil module without soil carbon and nitrogen profile.	Instead of defining a single litter, soil organic carbon and nitrogen pool, separate carbon and nitrogen pools for each soil layer in the form of soil organic matter and litter were implemented. Separation of above- and belowground litter pools. Litter and soil decomposition fluxes (carbon and nitrogen fluxes from litter to soil pools) are calculated layer by layer, depending on the actual temperature and SWC of the corresponding layers. Leaching of dissolved organic carbon and nitrogen.
Inorganic nitrogen	One layer soil module with one mineralized N pool.	Multi-layer soil module with an empirical inorganic N-profile (no layer-by-layer calculations, only estimation of the subpools in the different soil layer based on the rootlength proportion).	Separation of ammonium (sNH ₄) and nitrate (sNO ₃) soil pools instead of a general mineralized nitrogen pool. Nitrification fluxes are calculated layer by layer, depending on the actual pH, temperature and SWC of the given layers. Denitrification fluxes are calculated layer by layer, depending on the depth, actual temperature and SWC of the given layers.

940

941

942 Earlier model versions used a soil hydrology scheme based on the Richards equation,
943 but the results were not satisfactory. Sándor et al. (2017) presented results from the first major
944 grassland model intercomparison project (executed within the frame of FACCE MACSUR)
945 where Biome-BGCMuSo v2.2 was used. That study demonstrated the problems associated
946 with proper representation of soil water content that was a common shortcoming of all
947 included models. In the Hidy et al. (2016) paper, where the focus was on Biome-BGCMuSo
948 v4.0, the SWC related figures clearly indicated problems with the simulations compared to
949 observations. The SWC amplitude was not captured well which clearly influences drought
950 stress, decomposition, and other SWC driven processes like nitrification and denitrification.
951 For the latter two processes this is especially critical as they are associated with contrasting
952 SWC regimes (nitrification is an aerobic, while denitrification is an anaerobic process). This
953 is a good example for erroneous internal process representation that may lead to improper
954 results. Note that the currently used functions for nitrification/denitrification are also subject
955 to uncertainty that needs to be addressed in the future (Heinen, 2006). Nevertheless, the

956 presented model developments might contribute to a more realistic soil process simulations
957 and improved results.

958 Algorithm ensemble approach is already implemented in Biome-BGCMuSo.
959 Algorithm ensemble means that the user has more than one option for the representation of
960 some processes. Biome-BGCMuSo v6.2 has alternative phenology routines (Hidy et al.,
961 2012), two alternative methods for soil temperature (Hidy et al., 2016), soil hydrology
962 (described in this study), photosynthesis and soil moisture stress calculation. We plan to
963 extend the algorithm ensemble by providing alternative decomposition schemes to the model.
964 One possibility is the implementation of a CENTURY-like structure (Koven et al., 2013) that
965 is a promising direction and might improve the quality of the equilibrium (spin-up)
966 simulations and the simulated N mineralization related to SOM decomposition. Reported
967 problems related to the rapid decomposition of litter in the current model structure (Bonan et
968 al., 2013) needs to be addressed in future model versions as well.

969 Plant growth and allocation related developments were not addressed in this study but
970 of course has many inferences with the presented model logic (i.e. parameterization and
971 related primary production defines the amount and quality of litter, etc.). A forthcoming
972 publication will provide a comprehensive overview on the plant growth and senescence
973 related model modifications where elements from crop models are also included.

974 Biome-BGCMuSo is still an open source model that can be freely downloaded from
975 its website with a detailed User's Guide and other supplementary files. We also encourage
976 users to test the so-called RBBGCMuso package (available at GitHub) that has many
977 advanced features to support model application and optimization. A graphical environment,
978 called AgroMo (also available at GitHub: <https://github.com/hollorol/AgroMo>) was also
979 developed around Biome-BGCMuSo to help users in carrying out simulations either with site
980 specific plot scale data or with gridded databases representing large regions.

981

982

983 **Code and data availability**

984 The current version of Biome-BGCMuSo, together with sample input files and detailed User's
985 Guide are available from the website of the model: <http://nimbus.elte.hu/bbgc/download.html>
986 under the GPL-2 licence. Biome-BGCMuSo v6 is also available at GitHub:
987 https://github.com/bpbond/Biome-BGC/tree/Biome-BGCMuSo_v6. The exact version of the
988 model (v6.2 alpha) used to produce the results used in this paper is archived on Zenodo

989 (<https://doi.org/10.5281/zenodo.5761202>). Experimental data and model parameterization
990 used in the study are available from the corresponding author upon request.

991

992

993 **Authors' Contributions**

994 Hidy developed Biome-BGCMuSo, maintained the source code and executed the sample
995 simulations. The study was conceived and designed by Hidy, Barcza and Fodor, with
996 assistance from Ács, Dobor and Hollós. It was directed by Hidy and Barcza. Ács and Dobor
997 contributed with model benchmarking. Hollós participated with the construction of a
998 modeling framework for Biome-BGCMuSo. Filep, Incze, Zacháry and Pásztor contributed
999 with experimental data. Hidy, Barcza, Fodor and Merganičová prepared the manuscript and
1000 the supplement with contributions from all co-authors. All authors reviewed and approved the
1001 present article and the supplement.

1002

1003

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