# Soil related developments of the Biome-BGCMuSo v6.2 terrestrial ecosystem model by integrating crop model components

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# 32 Abstract

Terrestrial biogeochemical models are essential tools to quantify climate-carbon cycle 33 34 feedback and plant-soil relations from local to global scale. In this study, theoretical basis is provided for the latest version of Biome-BGCMuSo biogeochemical model (version 6.2). 35 Biome-BGCMuSo is a branch of the original Biome-BGC model with a large number of 36 developments and structural changes. Earlier model versions performed poorly in terms of 37 soil water content (SWC) dynamics in different environments. Moreover, lack of detailed 38 nitrogen cycle representation was a major limitation of the model. Since problems associated 39 40 with these internal drivers might influence the final results and parameter estimation, additional structural improvements were necessary. During the developments we took 41 42 advantage of experiences from the crop modeller community where internal process representation has a long history. In this paper the improved soil hydrology and soil 43 carbon/nitrogen cycle calculation methods are described in detail. Capabilities of the 44 Biome-BGCMuSo v6.2 model are demonstrated via case studies focusing on soil hydrology, 45 soil nitrogen and soil organic carbon cyclecontent estimation. Soil hydrology related results 46 are compared to observation data from an experimental lysimeter station. The results indicate 47 improved performance for Biome-BGCMuSo v6.2 compared to v4.0 (explained variance 48 increased from 0.121 to 0.8 for SWC, and from 0.084 to 0.46 for soil evaporation; bias 49 changed from -0.047 to -0.007 m<sup>3</sup> m<sup>-3</sup> for SWC, and from -0.68 mm day<sup>-1</sup> to -0.2 mm day<sup>-1</sup> 50 for soil evaporation). Nitrogen balance and soil CO2 efflux related simulations were evaluated 51 based on observations made in a long-term field experiment under crop rotation. The results 52 indicated that the model is able to provide realistic nitrate content estimation for the topsoil. 53 Soil nitrous oxide (N<sub>2</sub>O) efflux and soil respiration simulations were also realistic with overall 54 correspondence with the observations (for the N<sub>2</sub>O efflux simulation bias was between -0.13 55 and -0.1 mg N m<sup>-2</sup> day<sup>-1</sup>, NRMSE was 32.4% - 37.6%; for CO<sub>2</sub> efflux simulations bias was 56  $0.04 - 0.17 \text{ g C m}^{-2} \text{ day}^{-1}$ , while RMSE was 34.1% - 40.1%). Sensitivity analysis and 57 optimization of the decomposition scheme is presented to support practical application of the 58 model. The improved version of Biome-BGCMuSo has the ability to provide more realistic 59 soil hydrology representation and nitrification/denitrification process estimation which 60 61 represents a major milestone.

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# 64 **1. Introduction**

The construction and development of biogeochemical models (BGM) is the response 65 66 of the scientific community to address challenges related to climate change and human induced global environmental change. BGMs can be used to quantify future climate-67 68 vegetation interaction including climate-carbon cycle feedback, and as they simulate plant production, they can be used to study a variety of ecosystem services that are related to human 69 70 nutrition and resource availability (Asseng et al., 2013; Bassu et al., 2014; Huntzinger et al., 71 2013). Similarly to the models describing various and complex environmental 72 processes<del>proscesses</del>, the structure of biogeochemical models reflects our current knowledge about a complex system with many internal processes and interactions. 73

74 Processes of the atmosphere-plant-soil system take place on different temporal (subdaily to centennial) scales and are driven by markedly different mechanisms that are 75 quantified by a large diversity of modeling tools (Schwalm et al., 2019). Plant photosynthesis 76 77 is an enzyme-driven biochemical process that has its own mathematical equation set and related parameters (and a large literature; e.g. Farquhar et al., 1980; Medlyn et al. 2002; Smith 78 and Dukes, 2013; Dietze, 2013). Allocation of carbohydrates in the different plant 79 compartments is studied extensively and also has a large literature and mathematical tool set 80 (Friedlingstein et al., 1999; Olin et al., 2015; Merganičová et al., 2019). Plant phenology is 81 quantified by specific algorithms that are rather uncertain components of the models 82 (Richardson et al., 2013; Hufkens et al., 2018; Peaucelle et al., 2019). Soil biogeochemistry is 83 84 driven by microbial and fungal activity and also has its own methodology and a vast literature (Zimmermann et al 2007; Kuzyakov, 2011; Koven et al., 2013; Berardi et al., 2020). 85 Emerging scientific areas like the quantification of the dynamics of non-structural 86 carbohydrates (NSC) in plants has a separate methodology that claims for mathematical 87 representation in models (Martínez-Vilalta et al., 2016). Simulation of land surface hydrology 88 including evapotranspiration is typically handled by some variant of the Penman-Monteith 89 equation that is widely studied thus represents a separate scientific field (McMahon et al., 90 2013; Doležal et al., 2018). 91

Putting all together, if we are about to construct and further improve a biogeochemical model to consider novel findings and track global changes, we need a comprehensive knowledge that integrates many, almost disjunct scientific fields. Clearly, transparent and well-documented development of a biogeochemical model is of high priority but challenging

96 from the very beginning that claims for cooperation of researchers from various scientific97 fields.

Continuous model development is inevitable but it has to be supported by extensive 98 comparison with observations and some kind of implementation of the model-data fusion 99 approach (Keenan et al., 2011). It is well documented that structural problems might trigger 100 incorrect parameter estimation that might be associated with distorted internal processes 101 (Sándor et al., 2017; Martre et al., 2015). In other words, one major issue with BGMs (and in 102 fact with all models using many parameters) is the possibility to get good simulation results 103 104 for wrong reasons (which means incorrect parameterization) due to compensation of errors (Martre et al., 2015). In order to avoid this issue, any model developer team has to make an 105 106 effort to focus also on internal ecosystem conditions (e.g. soil volumetric water content (SWC), nutrient availability, stresses, etc.) and other processes (e.g. decomposition) rather 107 108 than the main simulated processes (e.g. photosynthesis, evapotranspiration).

Historically, biogeochemical models have been developed to simulate the processes of 109 110 undisturbed ecosystems with simple representation of the vegetation (Levis, 2010). As the focus was on the carbon cycle, water and nitrogen cycles and related soil processes were not 111 112 well represented. Incorrect representation of SWC dynamics is still an issue with the models especially in drought-prone ecosystems (Sándor et al., 2017). Additionally, human 113 intervention representation (management) is still incomplete inwas missing in many cases and 114 it seems that some state-of-the-art BGMs, still lack the representation of e.g. thinning, grass 115 mowing, grazing, tillagefertilization, planting or irrigation is missing in some models (see 116 harvest (Table A1 in Friedlingstein et al., 20202010). 117

In contrast, crop models with different complexity were used for about 50 years or so 118 to simulate the processes of managed vegetation (Jones et al., 2017; Franke et al., 2020). As 119 the focus of the crop models is on final yield due to economic reasons, the carbon balance, or 120 the full greenhouse gas balance was not, or was just partially addressed originally. Crop 121 models typically have a sophisticated representation of soil water balance with a multilayer 122 123 soil module that usually calculates plant response to water stress as well. Nutrient stress, soil conditions during planting, consideration of multiple phenological phases, heat stress during 124 anthesis, vernalization, manure application, fertilization, harvest, and many other processes 125 have been implemented during the decades (Ewert et al., 2015). Therefore, it seems to be 126 straightforward to exploit the benefits of crop models and implement sound and well-tested 127 algorithms into the BGMs. 128

Our group has been developing Biome BGCMuSo for 15 years. Starting from the 129 well-known Biome-BGC model originally developed to simulate undisturbed forests and 130 grasslands, using a simple single layer soil submodel (Running and Hunt, 1993; Thornton and 131 Rosenbloom, 2005), we developed a complex, more sophisticated model (Hidy et al., 2012; 132 2016). Biome-BGCMuSo v4.0 (Biome-BGC with Multilayer Soil module) uses a 7-layer soil 133 module and is capable of simulating different ecosystems from natural grassland to cropland 134 including several management options (mowing, grazing, thinning, planting and harvest),, 135 taking into account many environmental effects (Hidy et al., 2016). The developments 136 137 included improvements regarding both soil and plant processes. In a nutshell, the most important, soil related developments were the improvement of the soil water balance module 138 139 by implementing routines for estimating percolation, diffusion, pond water formation and runoff; the introduction of multilayer simulation for belowground processes in a simplified 140 141 way. The most important, plant related developments involved the implementation of a routine for estimating the effect of drought on vegetation growth and senescence; the 142 143 improvement of stomatal conductance calculation considering atmospheric  $CO_2$ concentration; the integration of selected management modules; the implementation of new 144 plant compartments (e.g. yield); the implementation of C4 photosynthesis routine; the 145 implementation of photosynthesis and respiration acclimation of plants and temperature-146 dependent Q10; and empirical estimation of methane and nitrous oxide soil efflux. 147

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Problems found with the Biome-BGCMuSo v4.0 simulation result (namelysuch as the poor representation of soil water content; (Hidy et al., 2016; Sándor et al., 2017) or the lack of 149 sophisticated, layer-specific soil nitrogen dynamics representation; or) and the model structure 150 related problems, -(such as the lubber parameterization of the model) marked the path for 151 further developments. 152

The aim of the present study is to provide detailed documentation on the current, 153 improved version of Biome-BGCMuSo v6.2, which has many new features and facilitates 154 various in-depth investigations of ecosystem functioning. Due to large number of 155 156 developments, this paper focuses only on the soil related model improvements. Case studies are also presented to demonstrate the capabilities of the new model version and to provide 157 158 guidance for the model user community.

# 160 **2. The original Biome-BGC model**

Biome-BGC was developed from the Forest-BGC mechanistic model family in order 161 to simulate vegetation types other than forests. Biome-BGC was one of the earliest 162 biogeochemical models that included explicit carbon and nitrogen cycle modules. Biome-163 164 BGC simulates the storages and fluxes of water, carbon, and nitrogen within and between the vegetation, litter, and soil components of terrestrial ecosystems. It uses a daily time step, and 165 166 is driven by daily values of maximum and minimum temperatures, precipitation, solar 167 radiation, and vapor pressure deficit (Running and Hunt, 1993). The model calculations apply 168 to a unit ground area that is considered to be homogeneous.

The three most important components of the model are the phenological, the carbon 169 170 uptake and release, and the soil flux modules. The core logic that is described below in this section remained intact during the developments. The phenological module calculates foliage 171 development that affects the accumulation of C and N in leaf, stem (if present), root and 172 173 consequently the amount of litter. In the carbon flux module gross primary production (GPP) of the biome is calculated using Farquhar's photosynthesis routine (Farquhar et al., 1980) and 174 the enzyme kinetics model based on Woodrow and Berry (2003). Autotrophic respiration is 175 separated into maintenance and growth respiration. Maintenance respiration is calculated as 176 the function of the N content of living plant pools, while growth respiration is an adjustable 177 but fixed proportion of the daily GPP. The single-layer soil module simulates the 178 179 decomposition of dead plant material (litter) and soil organic matter, N mineralization and N 180 balance in general (Running and Gower, 1991). The soil module uses the so-called converging cascade method (Thornton and Rosenbloom, 2005) to simulate decomposition, 181 carbon and nitrogen turnover, and related soil CO<sub>2</sub> efflux. 182

183 The simulation has two basic steps. During the first (optional) spinup simulation the available climate data series is repeated as many times as it is required to reach a dynamic 184 185 equilibrium in the soil organic matter content to estimate the initial values of the carbon and nitrogen pools. The second, normal simulation uses the results of the spinup simulation as 186 initial conditions and runs for a given, predefined time period (Running and Gower 1991). So-187 called transient simulation option (which is the extension of the spinup routine) is a novel 188 189 feature in Biome-BGCMuSo v6.2 relative to the previous versions in order to ensure smooth transition between the spinup and normal phase (Hidy et al., 2021). 190

191 In Biome-BGC, the main parts of the simulated ecosystem are defined as plant, litter 192 and soil. The most important pools include leaf (C, N and intercepted water), root (C, N), stem (C, N), soil (C, N and water) and litter (C, N). Plant C and N pools have sub-pools (actual pools, storage pools and transfer pools). The actual sub-pools store C and N for the current year growth. The storage sub-pools (essentially the non-structural carbohydrate pool, the source for the cores or buds) contain the amount of C and N that will be active during the next growing season. The transfer sub-pools inherit the entire content of the storage pools at the end of every simulation year. Soil C also has sub-pools representing various organic matter forms characterized by considerably different decomposition rates.

In spite of its popularity and proven applicability, the development of Biome-BGC was temporarily stopped (the latest official NTSG version is Biome-BGC 4.2; https://www.ntsg.umt.edu). One major drawback of the model was its relatively poor performance in modelling managed ecosystems, and the simplistic soil water balance submodel using a single soil layer only.

Our team started to develop the Biome-BGC model further in 2006. According to the logic of the team, the new model branch was planned to be the continuation of the Biome-BGC model with regard to the original concept of the developers (keeping the model code open source, providing detailed documentation, and providing support for the users).

209 The starting point of our model development was Biome-BGC v4.1.1 that was a result 210 of the model improvement activities of the Max Planck Institute (Vetter et al., 2007). Development of the Biome-BGCMuSo model branch has a long history by now. Previous 211 model developments were documented in Hidy et al. (2012) and Hidy et al. (2016). Below, 212 we provide detailed description of the new developments that are included in Biome-213 214 BGCMuSo v6.2 which is the latest version released in September, 2021. A comprehensive review of the input data requirement of the model together with explanation on the input data 215 structure is available in the User's Guide (Hidy et al., 2021). In this paper we refer to some 216 217 input files (e.g. soil file, plant file) that are described in the User's Guide in detail.

One of the most important novelty and advantage of the new model version (Biome-BGCMuSo v6.2) compared to any previous versions that due to the extensive and detailed soil parameter set (current version has 79, MuSo 4.0 has 39 and original model version has only 6 adjustable soil related parameters) the parameterization of the model is much more flexible. But this might be of course a challenging task to define all of the input parameters. In order to support practical application of the model, the User's Guide contains proposed values for most of the new parameters (Hidy et al., 2021).

# **3. Soil hydrology related developments**

In Biome-BGCMuSo v6.2 a 10-layer soil submodel was implemented. Previous model 226 versions included a 7-layer submodel, which turned out to be insufficient to capture 227 hydrological events like drying of the topsoil layers with sufficient accuracy. The thicknesses 228 229 of the layers from the surface to the bottom are 3, 7, 20, 30, 30, 30, 30, 50, 200 and 600 cm. The centre of the given layer represents the depth of each soil layer. Soil texture can be 230 231 defined by the percentage of sand and silt for each layer separately along with the most 232 important physical and chemical parameters (pH, bulk density, characteristic SWC values, 233 drainage coefficient, hydraulic conductivity) in the soil input file (Hidy et al., 2021).

The water balance module of Biome-BGCMuSo has five major components to describe soil water related processes in daily resolution (listed here following the order of calculation): pond water accumulation and runoff; infiltration and downward gravitational flow (percolation); water potential gradient driven water movement within the soil (diffusion); evaporation and transpiration (root water uptake); and the downward/upward fluxes to/from groundwater. In the following subsections these five major components are described.

#### 240 **3.1 Pond water accumulation and runoff**

Precipitation can reach the surface as rain or snow (below 0 °C snow accumulation is assumed). Snow water melts from the snowpack as a function of temperature and radiation and added to the precipitation input.

The canopy can intercept rain. The intercepted volume goes into the *canopy water* pool, which can evaporate. No canopy interception of snow is assumed. The throughfall (complemented with the amount of melted snow) gives the potential infiltration.

A new development in <u>Important novelty of</u> Biome-BGCMuSo v6.2 is that 247 maximum infiltration is calculated based on the saturated hydraulic conductivity and the SWC 248 of the top soil layers. If the potential infiltration exceeds the maximum infiltration, pond water 249 250 can be formed. If the sum of the precipitation and the actual pond height minus the maximum 251 infiltration rate is greater than the maximum pond height, the excess water is added to surface runoff detailed below (Balsamo et al., 2009). The maximum pond height is an input 252 parameter. Water from the pond can infiltrate into the soil at a rate the top soil layer can 253 absorb it. Evaporation of the pond water is assumed equal to the potential evaporation. 254

Surface runoff is the water flow occurring on the surface when a portion of the precipitation cannot infiltrate into the soil. Two types of surface runoff processes can be

distinguished: Hortonian and Dunne. Hortonian runoff is unsaturated overland flow that occurs when the rate of precipitation exceeds the rate at which water can infiltrate. The other type of surface runoff is the Dunne runoff (also known as the saturation overland flow) which occurs when the entire soil is saturated but the rain continues to fall. In this case the rainfall immediately triggers pond water formation and (above the maximum pond water height) surface runoff. The handling of these processes is presented in the soil hydrological module of Biome-BGCMuSo v6.2.

Calculation of Hortonain runoff (in kg  $H_2O m^{-2} day^{-1}$ ) is based on a semi-empirical method and uses the precipitation amount (in cm day<sup>-1</sup>), the unitless runoff curve number (*RCN*), and the actual moisture content status of the topsoil (Rawls et al., 1980; this method is known as the SCS runoff curve number method). This type of runoff simulation can be turned off by setting *RCN* to zero. The detailed description can be found in the Supplementary material, Section 1. The amount of runoff as a function of the soil type and the actual SWC is presented in Figure 1.

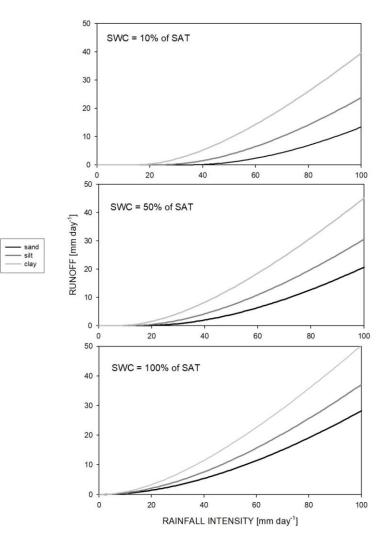


Figure 1: Hortonian runoff as the function of rainfall intensity, soil type and actual soil water content of the top soil layer. Sand soil means 92% sand, 4% silt and 4% clay; silt soil means 8% sand, 86% silt and 6% clay; clay soil means 20% sand, 20% silt and 60% clay. SWC and SAT denotemeans soil water content and; SAT means saturation, respectively.

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### 277 **3.2 Infiltration, percolation and diffusion**

There are two optional methods in Biome-BGCMuSo v6.2 to calculate soil water movement between soil layers and actual SWC layer by layer. The first one is a cascade method (also known as tipping bucket method), and the second is a Richards equation based physical method. The tipping bucket method has a long history in crop modelling and is considered as a successful, well-evaluated algorithm that can accurately simulate downward water flow in the soil.

The cascade method uses a semi-empirical input parameter (DC: drainage coefficient 284 in day<sup>-1</sup>) to calculate downward water flow rate. When the SWC of a soil layer exceeds field 285 286 capacity (FC), a fraction (equal to DC) of the water amount above FC goes to the layer next below. If DC is not set in the soil input file, it is estimated from the saturated hydraulic 287 conductivity:  $DC = 0.1122 \cdot K_{SAT}^{0.339}$  ( $K_{SAT}$ : saturated hydraulic conductivity in cm day<sup>-1</sup>; 288 289 the user can set its value or the model based on soil texture estimates it internally; see Hidy et 290 al., 2016). The detailed description of the method can be found in the Supplementary material, 291 Section 2. Drainage from the bottom layer is a net loss for the soil profile.

Water diffusion that is the capillary water flow between the soil layers is calculated to account for the relatively slow movement of water. The flow rate is the function of the water content difference of two adjacent layers and the soil water diffusivity at the boundary of the layers, which is determined based on the average water content of the two layers. The detailed mathematical description of the method can be found in the Supplementary material, Section 3.

The detailed description of the Richards\_-method can be found in Hidy et al. (2012). To support efficient and robust calculations of soil water fluxes a dynamically changing time step was introduced in version 4.0 (Hidy et al., 2016). An enhancement of this method in Biome BGCMuSo v6.2 is the finer vertical discretisation of the soil profile that is used during the numerical solution of the equation. The implementation of the more sophisticated Richards-methodequation is still in an experimental phase requiring rigorous testing and validation in the future.

# 305 **<u>3.3</u> Evapotranspiration**

306 Biome-BGCMuSo, such as its predecessor Biome-BGC, estimates evaporation of leaf intercepted water, bare soil evaporation, and transpiration to estimate the total 307 308 evapotranspiration in a daily level. The potential rates of all three processes are calculated based on the Penman-Monteith (PM) method. PM equation requires net radiation (minus soil 309 310 heat flux) and conductance values by definition using different parameterization for the different processes. The model calculates leaf- and canopy-level conductances of water 311 312 vapour and sensible heat fluxes, to be used in Penman-Monteith calculations of canopy evaporation and canopy transpiration. Note that in the Biome-BGC model family the direct 313 314 wind effect is ignored but can be considered indirectly by adjusting boundary layer conductance to site-specific conditions. A possible future direction might be the extension of 315 316 the model logic to consider wind effect directly.

#### 317 *3.3.1 Canopy evaporation*

If there is intercepted water, this portion of evaporation is calculated using the canopy 318 resistance (reciprocal of conductance) to evaporated water and the resistance to sensible heat. 319 The time required for the water to evaporate based on the average daily conditions is 320 calculated, and subtracted from the day length to get the effective day length for 321 322 evapotranspiration. Combined resistance to convective and radiative heat transfer is calculated based on canopy conductance of vapour and leaf conductance of sensible heat both of which 323 324 are assumed to be equal to the boundary layer conductance. Besides the conductance/resistance parameters the canopy absorbed shortwave radiation drives the 325 326 calculation. Note that the canopy evaporation routine was not modified significantly in Biome-BGCMuSo. 327

#### 328 *3.3.2 Soil evaporation*

In order to estimate soil evaporation, first the potential evaporation is calculated, 329 assuming that the resistance to vapour is equal to the resistance to sensible heat and assuming 330 no additional resistance component. Both resistances are assumed to be equal to the actual 331 aerodynamic resistance. Actual aerodynamic resistance is the function of the actual air 332 pressure and air temperature and the potential aerodynamic resistance ( $potR_{air}$  in s m<sup>-1</sup>). 333  $potR_{air}$  was a fixed value in the previous model versions (107 s m<sup>-1</sup>). Its value was derived 334 from observations over bare soil in tiger-bush in south-west Niger (Wallace and Holwill, 335 336 1997). In Biome-BGCMuSo v6.2, the  $potR_{air}$  is an input parameter that can be adjusted by the user (Hidy et al., 2021). Another new development in Biome-BGCMuSo v6.2 is the 337

introduction of an upper limit for daily potential evaporation  $(evap_{limit})$  that is determined by the available energy (incident shortwave flux that reaches the soil surface):

$$340 \quad evap_{limit} = \frac{irad \cdot dayl}{LH_{vap}} \tag{1}$$

where *irad* is the incident shortwave flux density in W m<sup>-2</sup>, *dayl* is the length of the day in seconds,  $LH_{vap}$  is the latent heat of vaporization (the amount of energy that must be added to liquid to transform into gas) in J kg<sup>-1</sup>. This feature was missing from previous model versions resulting in considerable overestimation of evaporation on certain days that was caused by the missing energy limitation on evaporation.

A new feature An important novelty in Biome-BGCMuSo v6.2 is the calculation of the actual evaporation from the potential evaporation and the square root of time elapsed since the last precipitation (expressed by days; Ritchie, 1998). This is another method that has been used by the crop modeller community for many years. Detailed description of the algorithm can be found in the Supplementary material, Section 4.

351 <u>OneA major new developmentnovel feature</u> in Biome-BGCMuSo v6.2 is the 352 simulation of the reducing effect of surface residue or mulch cover on bare soil evaporation. 353 Here we use the term 'mulch' to quantify surface residue cover in general keeping in mind 354 that mulch is typically a human-induced coverage. Surface residue includes aboveground 355 litter and coarse woody debris as well.

The evaporation reduction effect (evapREDmulch; unitless) is a variable between 0 356 and 1 (0 means full limitation, and 1 means no limitation) estimated based on a power 357 function of the surface coverage (mulchCOV in %) and a soil specific constant set by the user 358 359 (pREDmulch; see Hidy et al., 2021). If variable mulchCOV reaches 100% it means that the surface is completely covered. If *mulchCOV* is greater than 100% it means the surface is 360 covered by more than one layers. Surface coverage is a power function of the amount of 361 mulch (*mu* in kgC m<sup>-2</sup>) with parameters  $p1_{mulch}$ ,  $p2_{mulch}$ , and  $p3_{mulch}$  (soil parameters) based 362 on the method of Rawls et al. (1991): 363

365 
$$mulchCOV = p1_{mulch} \cdot (mu/p2_{mulch})^{p3_{mulch}}$$
(2)

$$366 \quad evapREdmulch = pREDmulch \frac{mulchCOV}{100}$$
(3)

Another simulated effect of surface residue cover is the homogenization of soil temperature between 0 and 30 cm depth (layers 1, 2 and 3). The functional forms of surface coverage and evaporation reduction factor are presented in Figure 2.

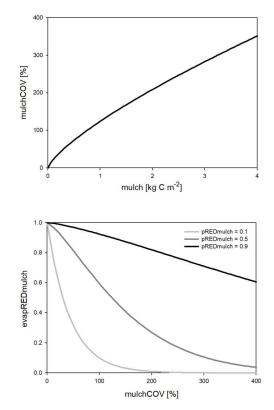


Figure 2: Surface coverage as a function of the amount of surface residue or mulch (upper plot) and the evaporation
 reduction factor (evapREDmulch) as the function of mulch coverage (lower plot) using different mulch specific soil
 parameters (pREDmulch). See text for details.

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#### 375 *3.3.3 Transpiration*

In order to simulate transpiration, first transpiration demand (TD in kg H<sub>2</sub>O m<sup>-2</sup> day<sup>-1</sup>) is calculated using the Penman-Monteith equation separately for sunlit and shaded leaves. TDis the function of leaf-scale conductance to water vapor, which is derived from stomatal, cuticular and leaf boundary layer conductances. A novelty in Biome-BGCMuSo v6.2 is that potential evapotranspiration is also calculated using the maximal stomatal conductance instead of the actual stomatal conductance, which means that stomatal aperture is not affected by the soil moisture status (in contrast to the actual one).

383 *TD* is distributed across the soil layers according to the actual root distribution using 384 an improved method (the logic was changed since Biome-BGCMuSo v4.0). From the plant 385 specific root parameters and the actual root weight Biome-BGCMuSo calculates the number 386 of the layers where roots can be found together with the root mass distribution across the 387 layers (Jarvis, 1989; Hidy et al., 2016).- If there is not enough water in a given soil layer to 388 fulfil the transpiration demand, the transpiration flux from that layer is limited, and below 389 wilting point (WP) it is set to zero. The sum of layer-specific transpiration fluxes across the root zone gives the actual transpiration flux. The detailed description of the algorithm can befound in the Supplementary material, Section 5.

#### **392 3.4 Effect of groundwater**

Simulation of groundwater effect was introduced in Biome-BGCMuSo v4.0 (Hidy et al., 2016), but the method has been significantly improved, and the new algorithm it is now available in Biome-BGCMuSo v6.2. In the recent model version there is an option to provide an additional input file with the daily values of the groundwater table depth (*GWdepth* in m).

Groundwater may affect soil hydrological and plant physiological processes if the water table is closer to the root zone than the thickness of the capillary fringe (that is the region saturated from groundwater via capillary effect). The thickness of the capillary fringe (*CF* in m) is estimated using literature data and depends on the soil type (Johnson and Ettinger model; Tillman and Weaver, 2006). Groundwater table distance (*GWdist* in m) for a given layer is defined as the difference between *GWdepth* and the depth of the midpoint of the layer.

404 The layers completely below the groundwater table are assumed to be fully saturated. In case of layers within the capillary fringe (GWdist < CF), the calculation of water balance 405 changes: the FCfield capacity rises, thus the difference between saturation (SAT) and FC 406 407 decreases and the layer charges gradually, till the increased FC value is reached. The FCrising effect of groundwater for the layers above the water table is calculated based on the 408 409 ratio of the groundwater distance and the capillary fringe thickness, but only after the water content of the layers below have reached their modified FC values. Detailed description of the 410 411 groundwater effect can be found in Supplementary material, Section 6.

# 412 **3.5 Soil moisture stress**

In the original Biome-BGC model the effect of changing soil water content on photosynthesis and decomposition of soil organic matter is expressed in terms of soil water potential ( $\Psi$ ). Instead of  $\Psi$ , the volumetric SWC is also widely used to calculate the limitation of stomatal conductance and decomposition. A practical advantage of using SWC as a factor in stress function is that it is easier to measure in the field and the changes of the driving function are much smoother than in case of  $\Psi$ . The disadvantage is that SWC is not comparable among different soil types (in contrast to  $\Psi$ ).

The maximum of SWC is the saturation value; the minimum is the wilting point or the hygroscopic water depending on the type of the simulated process. Novelty of BiomeBGCMuSo v6.2 is that the hygroscopic water, the wilting point, the field capacity and the
saturation values are calculated internally by the model based on the soil texture data, or can
be defined in the input file layer by layer.

In Biome-BGCMuSo v6.2 the so-called soil moisture stress index (SMSI) is calculated 425 to represent overall soil stress conditions. SMSI is affected by the length of the drought event 426 (SMSE: extent of soil stress), the severity of the drought event (SMSL: length of soil stress), 427 428 aggravated by the extreme temperature (*extremT*: effect of extreme heat). SMSI is equal to zero if no soil moisture limitation occurs and equal to 1 in case of full soil moisture limitation. 429 SMSI is used by the model for plant senescence calculations (presentation of plant related 430 processes is the subject of a forthcoming publication)). The members of SMSI are explained 431 detailed below. 432

433

434

#### $SMSI = 1 - SMSE \cdot SMSL \cdot extremT \tag{4}$

435 Magnitude of soil moisture stress (*SMSE*) is calculated layer by layer based on SWC. 436 Regarding soil moisture stress two different processes are distinguished: drought (i.e. low 437 SWC close to or below WP) and anoxic condition (i.e. after large precipitation events or in 438 the presence of high groundwater table; Bond-Lamberty et al., 2007). An important novelty of 439 Biome-BGCMuSo v6.2 is the soil curvature parameters (q) which is introduced to provide 440 mechanism for soil texture dependent drought stress as it can affect the shape of the soil stress 441 function (which means possibility for non-linear ramp function):

442

$$443 \quad SMSE^{i} = 0 \qquad ; SWC^{i} < SWC_{WP}^{i}$$

$$444 \quad SMSE^{i} = \left(\frac{SWC^{i} - SWC_{WP}^{i}}{SWC_{drought}^{i} - SWC_{WP}^{i}}\right)^{q} \qquad ; SWC_{WP}^{i} \le SWC < SWC_{drought}^{i} \qquad (5)$$

$$445 \quad SMSE^{i} = 1 \qquad ; SWC_{drought}^{i} \le SWC \le SWC_{anoxic}^{i}$$

$$446 \quad SMSE^{i} = \frac{SWC_{SAT}^{i} - SWC_{anoxic}^{i}}{SWC_{SAT}^{i} - SWC_{anoxic}^{i}} \qquad ; SWC^{i} > SWC_{anoxic}^{i}$$

447 where *q* is the curvature of soil stress function,  $SWC^{i}_{drought}$  and  $SWC^{i}_{anoxic}$  are critical SWC 448 values for calculating soil stress.

In order to make the SWC values comparable between different soil types,  $SWC^{i}_{drought}$  and  $SWC^{i}_{anoxic}$  can be set in normalized form (such as in Eq. 4) ) as part of the ecophysiological parameterization of the model. More details about the adjustment of the critical SWC values can be found in Hidy et al. (2021). The layer specific soil moisture stress extent values are summed across the root zone using the relative amount of roots in the layers ( $RP^{i}$ ) as weighting factors to obtain the overall soil moisture stress extent (*SMSE*):

456 
$$SMSE = \sum_{i=0}^{i=nr} SMSE^i \cdot RP^i$$
 (6)

457 
$$RP^{i} = RD \frac{z^{i}}{RL} \cdot e^{-RD \cdot (mid^{i}/RL)}$$
(7)

where nr is the number of the soil layers where roots can be found, RL is the actual length of 458 459 roots, RD is rooting distribution parameter (ecophysiological parameter; see details in the User's Guide; Hidy et al., 2021). In the current model version SMSE can also affect the entire 460 photosynthetic machinery by the introduction of an empirical parameter. This mechanism is 461 462 responsible to account for the non-stomatal effect of drought on photosynthesis (details about this algorithm will be published in a separate paper). Since there is no mechanistic 463 464 representation behind this empirical down-regulation of photosynthesis, further test are needed for the correct setting of this parameter using preferentially eddy covariance data. 465

466 The soil moisture stress length related factor (SMSL) is the ratio of the critical soil moisture stress length (ecophysiological parameter) and the sum of the daily (1 - SMSE)467 values. This cumulated value restarts if SMSE is equal to one (no stress). Extreme heat 468 (*extremT*) is also considered and is taken into account in the final stress function (see above) 469 by using a ramp function. Its parameterization thus requires the setting of two critical 470 temperature limits that defines the ramp function (set by the ecophysiological 471 472 parameterization; see Hidy et al., 2021). Its characteristic temperature values can be set by parameterization (ecophysiological input file). 473

# 474 **4. Soil carbon and nitrogen cycles**

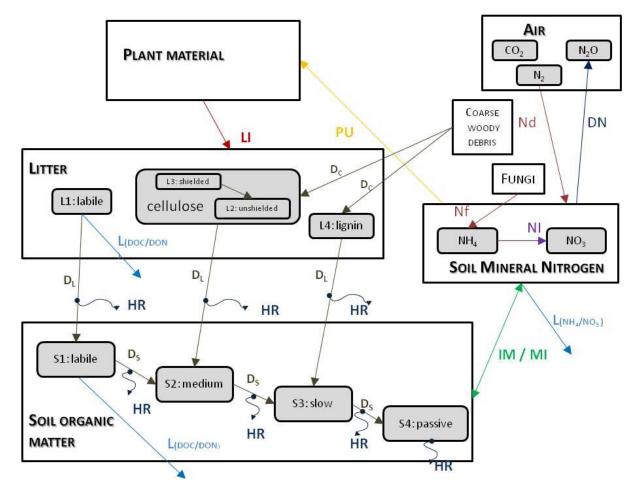
#### 475 **4.1 Soil-litter module**

We made substantial changes in the soil biogeochemistry module of the Biome-BGC model. Previous model versions already offered solutions for multilayer simulations (Hidy et al., 2012, 2016), but some pools still inherited the single-layer logic of the original model. In the new model version all relevant soil processes are separated layer by layer which is a major step forward.

Instead of defining a single litter, soil organic carbon (SOC) and nitrogen pool, we implemented separate carbon and nitrogen pools for each soil layer in the form of soil organic matter (SOM) and litter in Biome-BGCMuSo v6.2. The changes of the mass of the carbon and

nitrogen pools are calculated layer by layer. Mortality fluxes (whole plant mortality, 484 senescence, litterfall) of aboveground plant material are transferred into the litter pools of the 485 top soil layers (0-10 cm, layers 1-2). Mortality fluxes of belowground plant material are 486 487 transferred into the corresponding soil layers based on their location within the root zone. Due to ploughing and leaching, carbon and nitrogen can also be relocated to deeper layers. The 488 plant material turning into the litter compartment is divided between the different types of 489 litter pools (labile, unshielded cellulose, shielded cellulose and lignin) according to the 490 parameterization. Litter and soil decomposition fluxes (carbon and nitrogen fluxes from litter 491 492 to soil pools) are calculated layer by layer, depending on the actual temperature and SWC of the corresponding layers. Vertical mixing of soil organic matter between the soil layers (e.g. 493 494 bioturbation) is not implemented in the current model version.

495 Figure 3 shows the most important simulated soil and litter processes. N-fixation (*Nf*) 496 is the N input from the atmosphere to soil layers in the root zone by microorganisms. The user can set its annual value as an input parameter. N-deposition (Nd) is the N input from the 497 atmosphere to the top soil layers (see below). The user can set its annual value as a site-498 specific parameter in the initialization input file. Nitrogen deposition can be provided by 499 annually varying values as well. Plant uptake (PU) is the absorption of mineral N by plants 500 501 from the soil layers in the root zone. Mineralization (MI) is the release of plant-available 502 nitrogen (flux from soil organic matter to mineralized nitrogen). Immobilization (IM) is the consumption of inorganic nitrogen by microorganisms (flux from mineralized nitrogen to soil 503 organic matter). Nitrification (NI) is the biological oxidation of ammonium to nitrate through 504 nitrifying bacteria. Denitrification (*DN*) is a microbial process where nitrate ( $NO_3^{-}$ ) is reduced 505 506 and converted to nitrogen gas  $(N_2)$  through intermediate nitrogen oxide gases. Leaching (L) is 507 the loss of water-soluble mineral nitrogen from the soil layers. If leaching occurs in the 508 lowermost soil layer that means loss of N from the simulated system. Litterfall (LI) is the 509 plant material transfer from plant compartments to litter. Decomposition is the C and N transfer from litter to soil pools and between soil pools. In case of woody vegetation coarse 510 woody debris (CWD) contains the woody plant material after litterfall before physical 511 512 fragmentation. Litter has also four sub-pools based on their composition: labile (L1), 513 unshielded and shielded cellulose (L2, L3) and lignin (L4). Soil organic matter has also four sub-pools based on their turnover rate: labile (S1), medium (S2), slow (S3) and passive 514 515 (recalcitrant; S4) SOM pool. Soil mineralized nitrogen pool contains the inorganic N-forms of the soil: ammonium and nitrate. 516



517

518Figure 3: Soil and litter related simulated carbon/nitrogen fluxes (arrows) and pools (rectangles) in Biome-BGCMuSo519v6.2. HR: heterotrophic respiration, IM: immobilization, MI: mineralization, PU: plant uptake, LI: litterfall, NI:520nitrification, D: decomposition ( $D_L$ : decomposition of litter,  $D_S$ : decomposition of SOM,  $D_C$ : fragmentation of coarse521woody debris), L: leaching, Nf: nitrogen fixation, Nd: nitrogen deposition, DN: denitrification. L represents loss of C522and N from the simulated system.

#### 524 **4.2 Decomposition**

In the decomposition module (i.e. converging cascade scheme; Thornton, 1998) the fluxes between litter and soil pools are calculated layer by layer. The potential fluxes are modified in case of N limitation when the potential gross immobilization is greater than the potential gross mineralization.

To explain the decomposition processes implemented in Biome-BGCMuSo v6.2 the main carbon/nitrogen pools and fluxes between litter and soil organic and inorganic (mineralized) matter are presented on Figure 4.

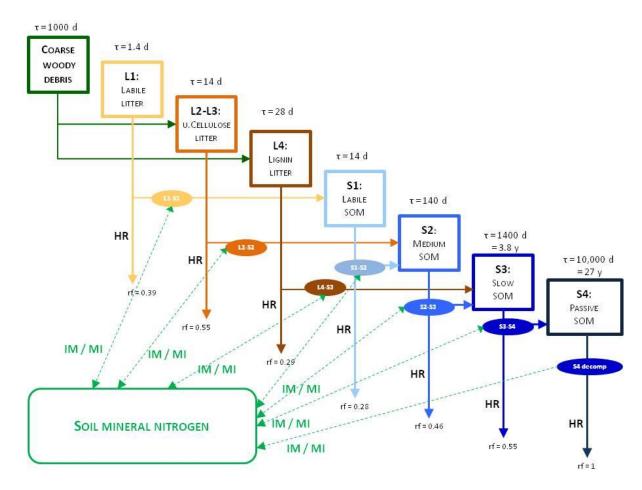


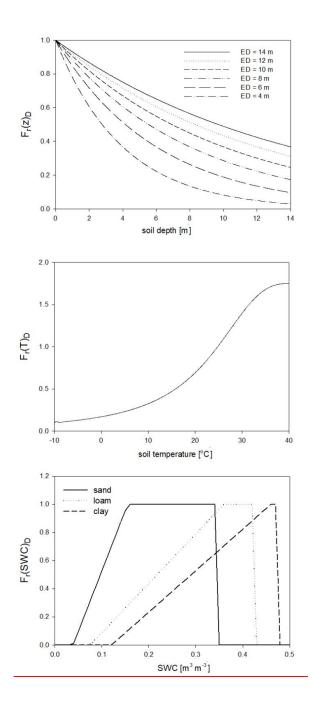
Figure 4: Overview of the converging cascade model of litter and soil organic matter decomposition that is
 implemented in Biome-BGCMuSo v6.2. rf represents the respiration fraction of the different transformation fluxes, τ
 is the residence time (reciprocal of the rate constants that is the turnover rate), IM/MI: immobilization/mineralization
 fluxes, HR: heterotrophic respiration. Note that both the respiration fraction and the turnover rate parameters can be
 adjusted through parameterization.

538

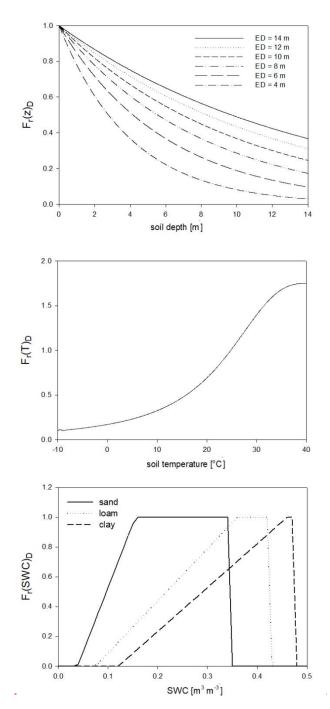
In the original Biome-BGC and in previous Biome-BGCMuSo versions the C:N ratio 539 (CN) of the soil pools were fixed in the model code. One of the new features in 540 Biome-BGCMuSo v6.2 is that the CN of the passive soil pool (S4 in Figure 4; recalcitrant soil 541 organic matter) can be set by the user as a soil parameter. The CN of the other soil pools 542 (labile, medium and slow; S1, S2 and S3) are calculated based on the proportion of fixed CN 543 values of the original Biome-BGC ( $CN_{labile} / CN_{passive} = 1.2, CN_{medium} / CN_{passive} = 1.2, CN_{slow} / CN_{slow}$ 544  $CN_{passive} = 1$ ). Note that the CN of the donor and acceptor pools are used in decomposition 545 calculations (see details in Supplement Material, Section 7), and as a result these parameters 546 set the C:N ratio of the soil pools. The donor and acceptor pools can be seen in Figure 3 and 547 Figure 4. 548

549For the calculation of nitrogen mineralization first respiration cost (respiration550fraction) is estimated. Mineralization thenthan is the function of the remaining part of the pool

and its C:N ratio. The nitrogen mineralization fluxes of the SOM pools are functions of the potential rate constant (reciprocal of residence time), and the integrated response function that accounts for the impact of multiple environmental factors. The integrated response function of decomposition is a product of the response functions of depth, soil temperature and SWC  $(F_r(d)_D, F_r(T)_D, F_r(SWC)_D)$ ; Figure 5). Its detailed description can be found in the Supplementary material, Section 7. The dependence of the three different factors on depth, temperature and SWC with default parameters are presented in Figure 5.



558





560Figure 5: The dependence of the individual factors that form the complex environmental response function of<br/>decomposition on depth  $(Fr(d)_D)$ , temperature  $(Fr(T)_D)$  and SWC in case of different soil types  $(Fr(SWC)_D)$ . ED is the<br/>e-folding depth which is one of the adjustable soil parameters of the model. For the definition of sand, silt and clay see<br/>Figure 1Sand soil means 92% sand, 4% silt and 4% clay; silt soil means 8% sand, 86% silt and 6% clay; clay soil<br/>means 20% sand, 20% silt and 60% clay.

### 566 **4.3 Soil nitrogen processes**

In Biome-BGCMuSo v6.2 separate ammonium (*sNH4*) and nitrate (*sNO3*) soil pools are implemented instead of a general mineralized nitrogen pool. This was a necessary step for the realistic representation of many internal processes like plant nitrogen uptake, nitrification, denitrification, consideration of the effect of different mineral and organic fertilizers and  $N_2O$ emission.

It is important to introduce the *availability* concept that Biome-BGCMuSo uses and is associated with the ammonium and nitrate pools. We use the logic proposed by Thomas et al. (2013) which means that the plant has access only to a part of the given inorganic nitrogen pool. Unavailable part is buffered as it is associated with soil aggregates and is unavailable for plant uptake. The available part of ammonium is calculated based on  $NH_4$  mobilen proportion (that is a soil parameter set to 10% according to Thomas et al., 2013; Hidy et al., 2021) and the actual pool. The available part of nitrate is assumed to be 100%.

579 The amount of ammonium and nitrate are determined layer by layer controlled by 580 input and output fluxes (F in kg N m<sup>-2</sup> day<sup>-1</sup>) listed below:

581 
$$F_{SNH4}^{i} = IN_{SNH4}^{i} - L_{SNH4}^{i} + L_{SNH4}^{i-1} - PU_{SNH4}^{i} - IM_{SNH4}^{i} + MI_{SNH4}^{i} - NI_{SNH4}^{i}$$
(8)

582 
$$F_{sNO3}^{i} = IN_{sNO3}^{i} - L_{sNO3}^{i} + L_{sNO3}^{i-1} - PU_{sNO3}^{i} - IM_{sNO3}^{i} + MI_{sNO3}^{i} - DN_{sNO3}^{i}$$
(9)

where  $IN_{sNH4}^{i}$  and  $IN_{sNO3}^{i}$  are the input fluxes to the ammonium and nitrate pools, respectively;  $L_{sNH4}^{i}$ ,  $L_{sNH4}^{i-1}$ ,  $L_{sNO3}^{i}$ ,  $L_{sNO3}^{i-1}$  are the amount of leached mineralized ammonium and nitrate from a layer (*i*) or from the upper layer (*i-1*), respectively;  $PU_{sNH4}^{i}$  and  $PU_{sNO3}^{i}$  are the plant uptake fluxes of ammonium and nitrate, respectively;  $IM_{sNH4}^{i}$  and  $IM_{sNO3}^{i}$  are the immobilization fluxes of ammonium and nitrate, respectively;  $MI_{sNH4}^{i}$  and  $MI_{sNO3}^{i}$  are the mineralization fluxes of ammonium and nitrate, respectively;  $MI_{sNH4}^{i}$  and  $MI_{sNO3}^{i}$  are the mineralization and  $DN_{sNO3}^{i}$  is the denitrification flux of nitrate.

590 In the following subsections the different terms of the equations are described in 591 detail.

# 592 Input to the sNH4 and sNO3 pools (IN in Eq. 6 and 7)

According to the model logic N-fixation occurs in the root zone layers. Its distribution between sNH4 and sNO3 pools is calculated based on their actual available proportion in the actual layer ( $NH4prop^i$ ):

596 
$$NH4prop^{i} = sNH4avail^{i} + sNO3avail^{i}$$
 (10)

597 where  $sNH4avail^i$  and  $sNO3avail^i$  are the available part of the sNH4 and sNO3 pools in the 598 actual layer.

599 N-deposition related nitrogen input is associated with the 0-10 cm soil layers assuming 600 uniform distribution across layers 1-2 in the model, and the distribution between sNH4 and

601	sNO3 pools is calculated based on the proportion of NH <sub>4</sub> flux of N-deposition soil parameter
602	(Hidy et al., 2021).
603	Organic and inorganic fertilization is also an optional nitrogen input. The amount and
604	composition (NH <sub>4</sub> <sup>+</sup> and NO <sub>3</sub> <sup>-</sup> content) can be set in the fertilization input file.
605	
606	Leaching - downward movement of mineralized N (L in Eq. 6 and 7)
607	The amount of leached mineralized N (mobile part of the given N pool) from a layer is
608	directly proportional to the amount of drainage and the available part of the sNH4 and sNO3
609	pools. Leaching from the layer above is a net gain, while leaching from actual layer is a net
610	loss for the actual layer. Leaching is described in Section 4.5.
611	
612	Plant uptake by roots (PU in Eq. 6 and 7)
613	N uptake required for plant growth is estimated in the photosynthesis calculations and
614	the amount is distributed across the layers in the root zone. The partition of the N uptake
615	between sNH4 and sNO3 pools is calculated based on their actual available proportion in each
616	layer.
617	
618	Mineralization and immobilization (MI and IM Eq. 6 and 7)
619	Mineralization and immobilization calculations are detailed in Section 4.2. The
620	distribution of these N fluxes between sNH4 and sNO3 pools is calculated based on their
621	actual available proportion in each layer.
622	
623	Nitrification (NI Eq. 6 and 7)
624	Nitrification is a function of the soil ammonium content, the net mineralization and the
625	response functions of temperature, soil pH and SWC $(F_r(pH)_{NI}, F_r(T)_{NI}, and F_r(SWC)_{NI},$
626	respectively) based on the method of Parton et al. (2001) and Thomas et al. (2013). Its
627	detailed mathematical description can be found in the Supplementary material, Section 8. The
628	response functions with proposed parameters are shown in Figure 6.

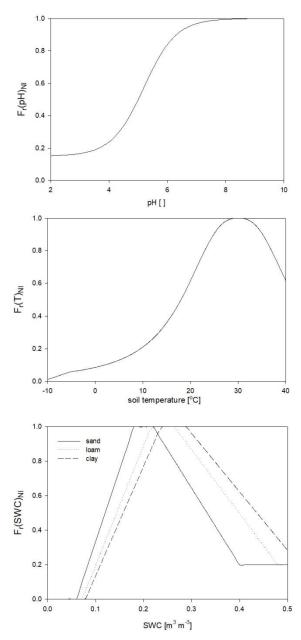


Figure 6: The dependence of the individual factors of the environmental response function of nitrification on soil pH ( $F_r(pH)_{NI}$ ), temperature ( $F_r(T)_{NI}$ ) and SWC  $F_r(SWC)_{NI}$  in case of different soil types. pH and temperature response functions are independent of the soil texture.

629

### 634 <u>Denitrification (DN Eq. 6 and 7)</u>

635 Denitrification flux is estimated with a simple formula (Thomas et al., 2013):

$$636 \quad DN^{i} = DNcoeff \cdot SOMresp^{i} \cdot sNO3avail^{i} \cdot WFPS^{i}$$

$$(11)$$

637 where DN of the actual layer is the product of the available nitrate content (sNO3avail in

638 kg N m<sup>-2</sup>), *SOMresp<sup>i</sup>* in g C m<sup>-2</sup> day<sup>-1</sup> is the SOM decomposition related respiration cost, the

639  $WFPS^i$  is the water-filled pore space and DNcoeff is the *soil respiration related* 640 *denitrification rate* in g C<sup>-1</sup>, which is an input soil parameter (Hidy et al., 2021). The unitless

water-filled pore space is the ratio of the actual and the saturated SWC. SOM decomposition 641 associated respiration is the sum of the heterotrophic respiration fluxes of the four soil 642 compartments (S1-S4, Figure 4.). 643

- 644
- 645

# 4.4 N<sub>2</sub>O-emission and N-emission

646

During both nitrification and denitrification N<sub>2</sub>O-emission occurs which (added to the 647 N<sub>2</sub>O-flux originated from grazing processes if applicable) contributes to the total N<sub>2</sub>O-648 emission of the examined ecosystem. 649

In Biome-BGCMuSo v6.2 a fixed part (set by the coefficient of  $N_2O$  emission of 650 nitrification input soil parameter; Hidy et al., 2021) of nitrification flux is lost as N<sub>2</sub>O and not 651 converted to NO<sub>3</sub>. 652

During denitrification, nitrate is transformed into N<sub>2</sub> and N<sub>2</sub>O gas depending on the 653 environmental conditions: NO<sub>3</sub> availability, total soil respiration (proxy for microbial 654 activity), SWC and pH. The denitrification related N<sub>2</sub>/N<sub>2</sub>O ratio input soil parameter is used 655 to represent the effect of the soil type on the  $N_2/N_2O$  ratio (del Grosso et al., 2000; Hidy et al., 656 657 2021). Detailed mathematical description of the algorithm can be found in the Supplementary material, Section 9. 658

659

#### 4.5 Leaching of dissolved matter 660

661 Leaching of nitrate, ammonium, and dissolved organic carbon and nitrogen (DOC and DON) content from the actual layer is calculated as the product of the concentration of the 662 dissolved component in the soil water and the amount of water (drainage plus diffusion) 663 leaving the given layer either downward or upward. The dissolved component (concentration) 664 of organic carbon is calculated from the SOC pool contents and the corresponding *fraction of* 665 dissolved part of SOC soil parameters. The dissolved component of organic nitrogen content 666 of the given soil pool is calculated from the carbon content and the corresponding C:N ratio. 667 The downward leaching is net loss from the actual layer and net gain for the layer next below; 668 669 the upward flux is net loss for the actual layer and net gain for the layer next up. The downward leaching of the bottom active layer (9<sup>th</sup>) is net loss for the system. The upward 670 movement of dissolved substance from the passive (10<sup>th</sup>) layer is net gain for the system. 671

# **5. Case studies**

### 673 **5.1 Evaluation of soil hydrological simulation**

674 In order to evaluate the functioning of the new model version (and to compare 675 simulation results made by the current and the previously published model version), a case 676 study is presented regarding soil water content and soil evaporation simulations. The results 677 of a bare soil simulation (i.e. no plant is assumed to be present) are compared to observation data of a weighing lysimeter station installed at Martonvásár, Hungary (47°18'57.6"N, 678 18°47'25.6"E) in 2017. The climate of the area is continental with a 30-year average 679 temperature of 11.0 °C (-1 °C in January and 21.2 °C in July) and annual rainfall of 548 mm, 680 681 based on data of the on-site weather station.

The station consists of twelve 2 meter deep scientific lysimeter columns with 1 m diameter (Meter Group Inc., USA) with soil temperature, SWC and soil water potential sensors installed at 5, 10, 30, 50, 70, 100 and 150 cm depth. Observation data for 2020 from six columns without vegetation cover (i.e. bare soil) was used to validate the model.

Raw lysimeter observation data were processed using standard methods. Bare soil 686 evaporation values were derived- based on changes of the mass of the soil columns also 687 considering the mass change of the drainage water. Additionally, experience has shown that 688 wind speed is related to the high frequency mass change of the soil column mass. To reduce 689 690 noise, 5-point (5-min) moving averages were used based on Marek et al. (2014). After quality control of the data, the corrected and smoothed lysimeter mass values were used for the 691 692 calculations. SWC observations were averaged to daily resolution to match the time step of 693 the model.

Observed local meteorology was used to drive the models for year 2020. Soil physical model input parameters (field capacity, wilting point, bulk density, etc.) were determined in the laboratory using 100 cm<sup>3</sup> undisturbed soil samples taken from various depths during the installation of the lysimeter station. Regarding other soil parameters the proposed values were used. Detailed description of the input soil parameters and their proposed values are presented in the User's Guide (Hidy et al., 2021).

In Figure 7 the simulated and the observed time series of soil evaporation are presented for Martonvásár, for 2020. The figure shows that the soil evaporation simulation by v6.2 is more realistic than by v4.0. Biome-BGCMuSo v4.0 provides very low values during summer in some days which is not in accordance with the observations. Biome-BGCMuSo v6.2 provides more realistic values during this time period.

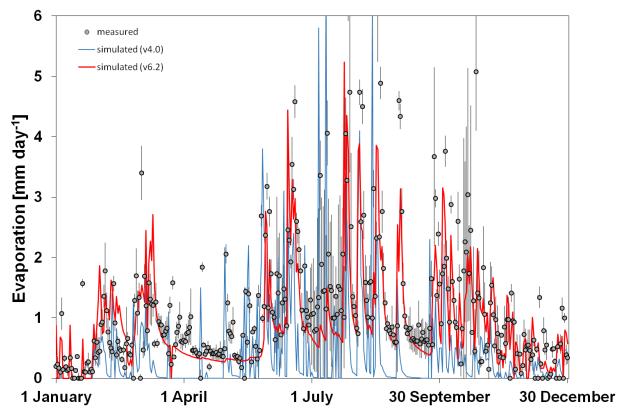


 Figure 7: The simulated (blue line: v4.0; red line: v6.2) and the observed (grey dots) daily soil evaporation values at Martonvásár during 2020. Vertical grey lines associated with the observations represent standard deviation of the observationsobservation from 6 lysimeter columns. The improved model clearly outperforms the earlier version.

705

In Figure 8 the simulated and the observed SWC at 10 cm depth are presented with the 711 daily sum of precipitation representing the bare soil simulation in Martonvásár, for 2020. The 712 soil water balance simulation seems to be realistic using v6.2, since the annual course 713 captures the low and high end of the observed values. In contrast, Biome-BGCMuSo v4.0 714 underestimates the range of SWC and provides overestimations during the growing season 715 (from spring to autumn). With a couple of exceptions, the simulated values using v6.2 fall 716 into the uncertainty range of the measured values defined by the standard deviation of the six 717 718 parallel measurements. This is not the case for the simulations with the 4.0 version.

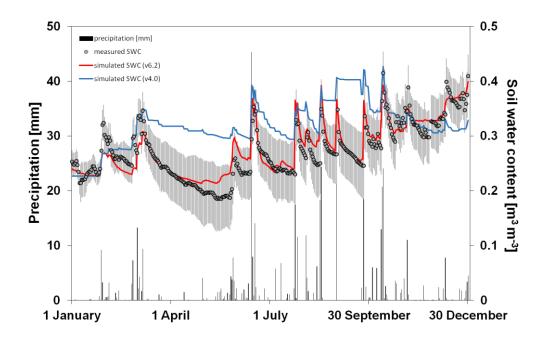




Figure 8: The simulated (blue line: v4.0; red line: v6.2) and the observed (greygray dots) soil water content values at 10 cm depth (right y axis) with the daily sums of precipitation (left axis; black columns) during 2020 at Martonvásár
lysimeter station. Vertical grey lines associated with the observations represent +/- one standard deviation aroundof
the observation. Simulated SWC using v6.2 is more consistent with the observations. The improved model clearly
outperforms the earlier version in simulating soil water balance. than using v4.0.



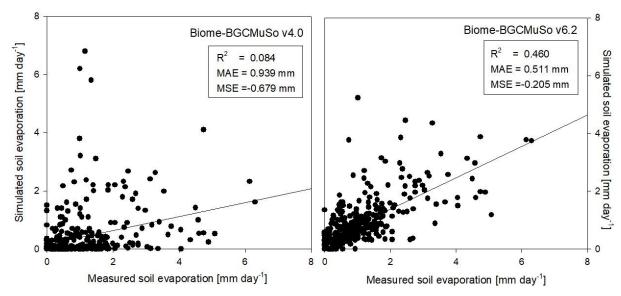


Figure 9: Comparison of the simulated (left: v4.0; right: v6.2) and observed daily soil evaporation (right) representing
 the means of measured data obtained from six weighing lysimeter columns with bare soil at Martonvásár in 2020. R<sup>2</sup>,
 MAE and MSE denote the square of the linear correlation coefficient of determination, mean absolute error and
 mean signed error (bias) of the simulated values, respectively.





Model performance was evaluated by quantitative measures such as square of linear
 correlation coefficient of determination (R<sup>2</sup>), mean absolute error (MAE) and mean signed
 error (MSE). In Figure 9 the comparison of the simulated and the observed daily evaporation

is presented. Based on the performance indicators it is obvious that the simulation with new
model version (v6.2) is much closer to observations than the old version (v4.0). BiomeBGCMuSo v6.2 slightly underestimated the observations.

In Figure 10 the comparison of the simulated and the observed daily SWC from the lysimeter experiment is presented. Based on the model evaluation it seems that the simulation with new model version is much closer to observation than with old version (4.0). The results obtained from v4.02 are consistent with earlier findings about the incorrect representation of the annual SWC cycle (Hidy et al., 2016; Sándor et al., 2017).

Throughout validation of the improved model based on observed SWC and ET
datasets from eddy covariance sites is planned to be published in an upcoming paper about the
plant related improvements.under way.

747

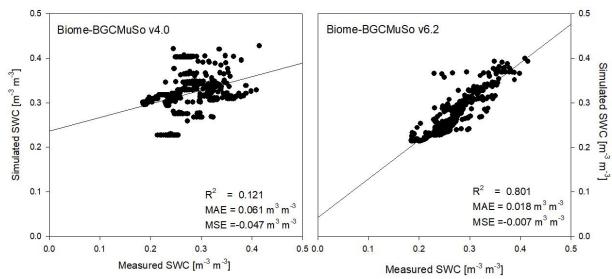




Figure 10: Comparison of the simulated (left: v4.0; right: v6.2) and observed daily SWC representing the means of measured data obtained from six weighing lysimeter columns with bare soil at Martonvásár in 2020. R<sup>2</sup>, MAE and MSE denote the square of the linear correlation coefficient of determination, mean absolute error and mean signed error (bias) of the simulated values, respectively.

754	5.2 Evaluation of the soil nitrogen balance module and the simulated soil respiration
755	Soil related developments were evaluated with a case study focusing on topsoil nitrate
756	content, soil $N_2O$ efflux and soil respiration.
757	Experimental data were collected in a long-term fertilization experiment that was set
758	up in 1959 at Martonvásár, Hungary (N 47°18'41", E 18°46'50"). According to the FAO-
759	WRB classification system (IUSS Working Group, 2015), the soil is a Haplic Chernozem,
760	with 51.4% sand, 34% silt and 14.6% clay content. Bulk density is 1.47 g cm <sup>-3</sup> , pH(H <sub>2</sub> O) is

7.3, CaCO<sub>3</sub> content is 0–1%, and the mean soil organic matter content in the topsoil is 3.2%.
The plant-available macronutrient supply in the soil was poor for Phosphorus and medium to
good for Potassium, based on the ProPlanta plant nutrition advisory system (Fodor et al.,
2011). In the long-term fertilization experiment the treatments were arranged in a random
block design with 6×8 m plots in four replicates. Eight different treatments were set up:
control (zero artificial fertilizer applied), only N, only P and NPK – with farmyard manure;
absolute control (zero nutrient supply), only N, only P, NPK – without farmyard manure. The
crops in the four-year fertilizer cycles were maize in the 1<sup>st</sup> and 2<sup>nd</sup> years and winter wheat in
the 3<sup>rd</sup> and 4<sup>th</sup> years. Here we used data from the absolute control and from the farmyard
manure (FYM) treatments only. FYM was applied once every four years at a rate of 35 t ha<sup>-1</sup>
in autumn.

Topsoil nitrate content was measured during 2017, 2018 and 2020 on a few occasions by wet chemical reactions using a stream distillation method after KCl extraction of soil samples (Hungarian Standards Institution MSZ 20135:1999; Akhtar et al., 2011).

Dynamic chamber based soil  $N_2O$  efflux observations were available from 2020 and 2021. The N<sub>2</sub>O efflux measurements with a gas incubation time of 10 minutes were performed by using a Picarro G2508 (Picarro, USA) cavity ring down spectrometer (Christiansen et al. 2015; Zhen et al. 2021). The cylinder shaped transparent gas incubation chamber was 16.5 cm in diameter and its height was 30 cm. N<sub>2</sub>O flux measurements were executed in 6 replicates per treatment on a biweekly (2020) and precipitation event-related (2021) basis. Soil respiration was measured with the same Picarro gas analyser. Sampling numbers and points were identical with those of the N<sub>2</sub>O efflux measurements. CO<sub>2</sub> and N<sub>2</sub>O effluxes were calculated by linear equation (Widen and Lindroth, 2003) based on gas concentration data.

For the simulations we used maize parameterization from previous studies (Fodor et al., 2021). Winter wheat parameterization was constructed based on a country-scale optimization using the AgroMo software package (https://github.com/hollorol/AgroMo) and the NUTS 3 level long-term (1991-2020) yield database of the Hungarian Central Statistical Office. For nitrogen cycle related parameters we mainly used the values presented in the User's Guide (Hidy et al., 2021). Two soil parameters were adjusted (coefficient of N<sub>2</sub>O emission for nitrification and N<sub>2</sub>/N<sub>2</sub>O ratio multiplier for denitrification related N gas flux; Del Grosso et al., 2000; Parton et al., 2001; Thomas et al., 2013; Hidy et al., 2021) to match the simulated N<sub>2</sub>O efflux to the observations.

Figure 11 shows the comparison of the simulated and observed NO<sub>3</sub> content of the 794 topsoil for the two selected treatments. The results indicate that the model underestimate the topsoil NO<sub>3</sub> content both in the case of C and FYM (bias is -2.3 ppm and -2.4 ppm, respectively) treatments, but the simulation error is in an acceptable range (NRMSE is 45.5% 798 and 37.6% for C and FYM, respectively).

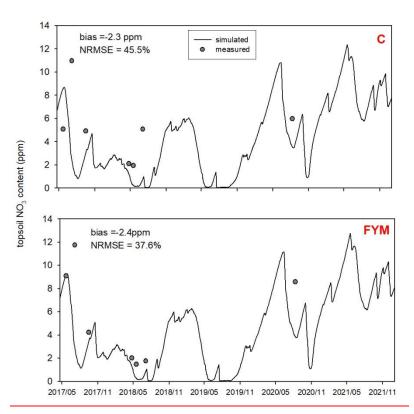


Figure 11: Comparison of the simulated and observed NO3 content of the topsoil for the absolute control (C; upper) and for the farmyard manure (FYM; bottom) treatment between May 2017 and November 2021 at Martonvásár.

Figure 12 shows the comparison of the observed and simulated N<sub>2</sub>O efflux for the 803 2020-2021 time period. Measurement uncertainties are also indicated on the plot. Note that 804 the uncertainty of the observations (e.g. due to spatial heterogeneity and sample number, soil 805 disturbance, improper chamber design, methods of sample analysis) is remarkable due to 806 known features of the chamber technique (Chadwick et al. 2014; Pavelka et al. 2018). The 807 model captured more of the magnitude of N<sub>2</sub>O efflux peaks and less of their timing. Overall 808 the model underestimated the observed values in both cases (bias is  $-0.13 \text{ mg N m}^{-2} \text{ dav}^{-1}$  and 809 -0.1 mg N m<sup>-2</sup> dav<sup>-1</sup> for C and FYM, respectively), with NRMSE of 32.4% and 37.6% for C 810 811 and FYM, respectively.

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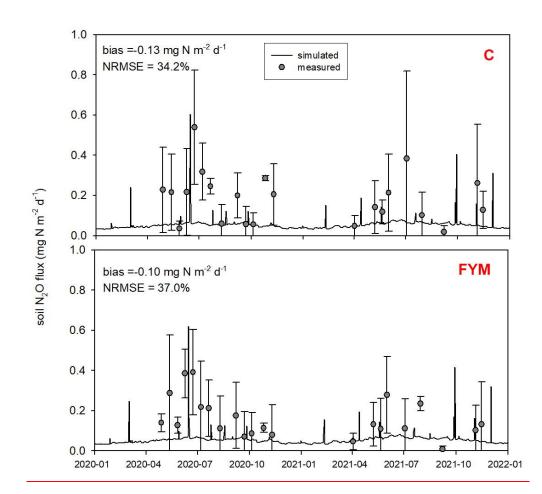




Figure 12: Comparison of the simulated and observed soil  $N_2O$  efflux for two treatments: absolute control (C; upper) and application of farmyard manure (FYM; bottom) between January 2020 and December 2021 at Martonvásár. Whiskers indicate the uncertainty (± one standard deviation) of the measurements.

Figure 13 presents the comparison of the observed and simulated soil respiration for the same time period as for the soil  $N_2O$  efflux. Observation uncertainty is indicated that represents one standard deviation of the replicates. The model mostly captured the magnitude and variability of soil respiration flux. The model overestimated the observed values in both cases with bias of 0.17 g C m<sup>-2</sup> day<sup>-1</sup> and 0.04 g C m<sup>-2</sup> day<sup>-1</sup> for C and FYM, respectively. The NRMSE is 34.1% and 40.1% for C and FYM, respectively. It is interesting to note that the observations and the simulations are particularly different after harvest time in both years (i.e. beginning of October). The simulated respiration have peaks are corresponding to harvest when the amount of litter sharply increases due to the byproducts left behind (decomposition of residues left on the site after harvest are accounted for in the model). The chamber based CO<sub>2</sub> efflux data did not really show similar peaks likely because of methodological issues (litter is removed from the soil surface before placing of the chambers).

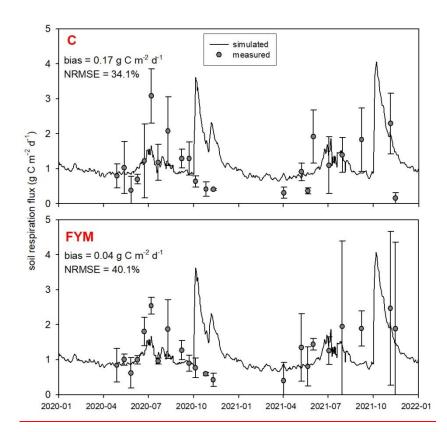


Figure 13: Comparison of the simulated and observed soil respiration flux for two treatments: absolute control (C; upper) and application of farmyard manure (FYM; bottom) between January 2020 and December 2021 at Martonyásár, Whiskers indicate the uncertainty  $(\pm$  one standard deviation) of the measurements.

Overall, the model provided nitrate content, N<sub>2</sub>O emission and soil respiration simulation results that are consistent with the observations. The model was capable of estimating the observed values with a comparable efficiency reported in similar studies (Gabrielle et al., 2002; Andrews et al., 2020).

<u>5.3</u>

# 5.2 Sensitivity analysis and optimization of the soil biogeochemistry scheme

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Here we present another case study that provides insight into the functioning of the 842 converging cascade (decomposition) scheme that is implemented in Biome-BGCMuSo v6.2. A large scale in silico experiment is also presented where the main aim was to perform model 843 self-initialization (i.e. spinup) at the country scale (for the entire area of Hungary) where the 844 resulting soil organic matter pools are expected to be consistent with the observations. 845

The observation based, gridded, multi-layer SOC database of Hungary (DOSoReMI 846 database; Pásztor et al., 2020; see Supplementary material Figures S3-S42020) as well as the 847

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FORESEE meteorological database (Kern et al., 2016) was used for the sensitivity analysis of 848 849 the soil scheme as well as for optimizing the most important soil parameters when the model 850 was calibratedreferring to the observation based SOC valuessimulation. As a first step, the area of the country was divided into 1104 grid cells (regular grid with 0.1° by 0.1° resolution, 851 corresponding to an approximately 10 km resolution)... The 1104 grid cells of the DOSoReMI 852 853 database were grouped based on their dominant land-use type (cropland, grassland, forest based on CORINE-20182012 database; EEA, 2021; Supplementary material Figures S1-S2) 854 as well as the soil texture class (12 classes according to the USDA system; USDA, 1987) and 855 856 SOC content (high and low; high is greater than the group mean while low is less than the 857 mean) of the topsoil (0-30 cm layer). As some of the theoretically possible 72 groups had no 858 members (e.g. there is no soil in Hungary with sandy-clay texture) soils of the 1104 grid cells were categorized into 51 groups. For each group one single cell (so-called representative cell) 859 860 was selected based on the topsoil SOC content. The representative cell was the one with the 861 smallest absolute deviation from the group mean SOC content. (Land use maps for Hungary 862 are presented in the Supplementary Material Section 10: Figure S1-S2).

Grassland ecophysiological parameterization without management was used in the 863 864 spinup phase to initialize SOC pools for croplands. For for the transientspinup phase cropland 865 parameterization was used, and with fertilization, harvest and ploughing, planting and harvest settings-in the transient phase. In case of grasslands, both during the spinup and transient 866 phases grassland parameterization was used, and in the transient phase mowing was assumed 867 (once a year. In-in case of forests generic deciduous broadleaf forest parameterization was 868 869 used for both spinup and transient phases with thinning, and in the lattertransient phase. For our parameterization presented in the MS the thinning was set. Parameterization was 870 871 performed based on generic, plant functional type specific ecophysiological parameter sets 872 published by<del>parameters that were created based on the original parameterization of</del> White et 873 al. (2000) served as starting points. These). Biome-BGCMuSo specific parameter sets are available at the website of the model<sup>1</sup>. 874

Soil parameters in Biome-BGCMuSo v66.2 were classified into six groups: (1) 4
generic soil parameters, (2) 24 decomposition-nitrification-denitrification related parameters,
(3) 14 rate scalars for the converging (decomposition) cascade scheme, (4) 19 soil moisture
related parameters, (5) 7 methane related parameters and (6) 11 soil composition and

<sup>&</sup>lt;sup>1</sup> http://nimbus.elte.hu/bbgc/files/generic\_EPC\_set\_6.24.zip

- 879 characteristic values (can be set layer by layer). Detailed description and proposed value of
- each soil parameters can be found in the User's Guide (Hidy et al., 2021).

Table 1: Soil parameters of Biome-BGCMuSo v6.2 (referring to SOC simulation) that were used during the sensitivity analysis. <u>The VALUE column shows the originallyThe first column contains the group, the second contains the name of the parameter, the third contains the abbreviation, and the fourth contains original proposed values (Hidy et al., 2021). See Figure 4 for explanation on the compartment names. The parameters that were included in the 2<sup>nd</sup> phase of the sensitivity analysis are marked with bold letters (see text).</u> 

GROUP	PARAMETER NAME	ABBREVIATION	VALUE
~	C:N ratio of stable soil pool (soil4)	soil4CN	12
Generic soil parameters	NH4 mobilen proportion	amMP	0.1
parameters	aerodynamic resistance	potRair	107
	parameter 1 for temperature response function of decomp.	Tp1decomp	1.75
	parameter 2 for temperature response function of decomp.	Tp2decomp	17
	parameter 3 for temperature response function of decomp.	Tp3decomp	2.6
	parameter 4 for temperature response function of decomp.	Tp4decomp	40
	minimum T for decomposition and nitrification	Tp5decomp	-5
	e-folding depth of decomposition rate's depth scalar	EFD	10
	net mineralization proportion of nitrification	NITRnetMINER	0.2
	maximum nitrification rate	NITRmaxRATE	0.1
	coefficient of N2O emission of nitrification	NITRratioN2O	0.02
	parameter 1 for pH response function of nitrification	pHp1nitrif	0.15
Decomposition,	parameter 2 for pH response function of nitrification	pHp2nitrif	1
nitrification,	parameter 3 for pH response function of nitrification	pHp3nitrif	5.2
denitrification	parameter 4 for pH response function of nitrification	pHp4nitrif	0.55
parameters	parameter 1 for Tsoil response function of nitrification	Tp1nitrif	1
	parameter 2 for Tsoil response function of nitrification	Tp2nitrif	12
	parameter 3 for Tsoil response function of nitrification	Tp3nitrif	2.6
	parameter 4 for Tsoil response function of nitrification	Tp4nitrif	2.6
	minimum WFPS for scalar of nitrification calculation	minWFPS	0.1
	lower optimum WFPS for scalar of nitrification	opt1WFPS	0.45
	higher optimum WFPS for scalar of nitrification	opt2WFPS	0.55
	minimum value for saturated WFPS scalar of nitrification	minWFPSscalar	0.2
	soil respiration related denitrification rate	DENITcoeff	0.05
	denitrification related N2/N2O ratio multiplier	DNratioN2O	2
	critical WFPS value for denitrification	critWFPSdenitr	0.50
	respiration fractions for fluxes between compartments (l1s1)	RFl1s1	0.39
	respiration fractions for fluxes between compartments (12s2)	RF12s2	0.55
	respiration fractions for fluxes between compartments (14s3)	RFl4s3	0.29
	respiration fractions for fluxes between compartments (s1s2)	RFs1s2	0.29
	respiration fractions for fluxes between compartments (s2s2)	RFs2s3	0.46
	respiration fractions for fluxes between compartments (5250)	RFs3s4	0.55
	potential rate constant of labile litter pool	RCS1	0.7
	potential rate constant of rabile litter pool	RCS2	0.07
	potential rate constant of centrolse inter pool	RCS3	0.014
	potential rate constant of fast microbial recycling pool	RCS4	0.014
	potential rate constant of rast incrobial recycling pool	RCS5	0.014
Rate scalars	potential rate constant of includin incrobial recycling pool	RCS6	0.014
	potential rate constant of slow incrobial recycling pool potential rate constant of recalcitrant SOM (humus) pool	RCS0 RCS7	0.0014
Rate scalars	potential rate constant of recarcinal solve (numus) poor	RCS8	0.001
	maximum height of pond water	MP	5
			1
	curvature of soil stress function fraction of dissolved part of \$1 organic matter	<b>q</b> fD1	0.005
	fraction of dissolved part of S2 organic matter	fD2	0.004
	fraction of dissolved part of S3 organic matter	fD3	0.003
	fraction of dissolved part of S4 organic matter	fD4	0.002
	mulch parameter: critical amount	CAmulch	1
	parameter 1 for mulch function	p1mulch	100
	parameter 2 for mulch function	p2mulch	0.75
	parameter 3 for mulch function	p3mulch	0.75
	mulch parameter: evaporation reduction	ERmulch	0.5

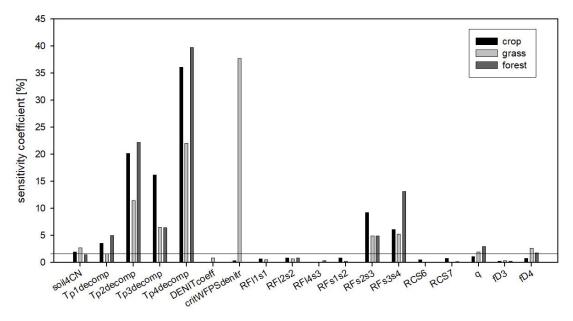
As methane simulation was not the subject of the present case study we neglected the 888 889 related parameters. Regarding to the soil composition and characteristic values we used the DOSoReMI database (Pásztor et al., 2020). From the remaining 61 parameters soil depth, 890 runoff curve number, the three soil moisture related parameters (tipping bucket method) were 891 not included in theinto analysis. The groundwater module was switched off-Groundwater 892 parameters were inactive in this case (no groundwater is assumed) and the relatedwhich 893 means that those parameters were not studied. The remaining 53 parameters wereare used in 894 895 the sensitivity analysis and are listed in Table 1.

896 As a first step sensitivity analysis was carried out for the selected 53 soil parameters 897 by running the Biome-BGCMuSo v6.2 model in spinup mode until a quasi-equilibrium in the 898 total SOC is reached (that is the usual logic of the spinup run). The model was run for each representative cell 2000 times with varying model parameters using Monte-Carlo method. 899 900 Each model parameters were varied randomly within the  $\pm 10\%$  range of their initial values that were inherited from the Biome-BGC model or were set according to the literature. The 901 902 least square linearization (LSL) method (Verbeeck et al., 2006) was used for dividing output 903 uncertainty into its input parameter related variability. As result of the LSL method, the total 904 variance of the model output and the sensitivity coefficient of each parameter can be 905 determined. Sensitivity coefficients show the percent of total variance for which the given parameter is responsible. 906

In order to simplify the workflow and decrease the degree of freedom another sensitivity analysis was performed. In this second step, the sensitive parameters (sensitivity coefficient > 1% for at least one land use type; a total of 18 parameters) were used in the following sensitivity analysis with 6000 iteration steps. These 18 parameters are marked with bold letters in Table 1.

912 Figure 1410 shows the summary of the second sensitivity analysis where the overall 913 importance of the parameters is are calculated as the mean of all selected pixels in a given land use category. It can be seen in Figure 410 that from the 18 parameters (selected during the 914 915 first phase) soil carbon ratio of the recalcitrant pool (soil4CN), the temperature dependence 916 parameters of decomposition function (Tp1decomp, Tp2decomp, Tp3decomp, Tp4\_decomp) 917 and the respiration fraction of S2-S3 and S3-S4 decomposition process (RFs2s3 and RFs3s4), the curvature of soil stress function (q<sub>soilstress</sub>) and the fraction of dissolved part of S4 organic 918 919 matter (fD4) are the most important for all land use types. Among the other parameters the critical WFPS of denitrification (critWFPSdentir) for grasslands has a remarkably high 920 sensitivity (greater thanthat 35%). It means that in case of grasslands the nitrogen availability 921

922 seems to be an important limitation of the primary production, probably because there are 923 only natural sources of nitrogen (no fertilization is assumed here), and the rooting zone is 924 shallower than in case of forest which involves limited mineralized N access. Thus, in case of 925 higher values of critical WFPS of denitrification, the simulated production of the grassland 926 (and therefore the final SOC) seems to be significantly underestimated.

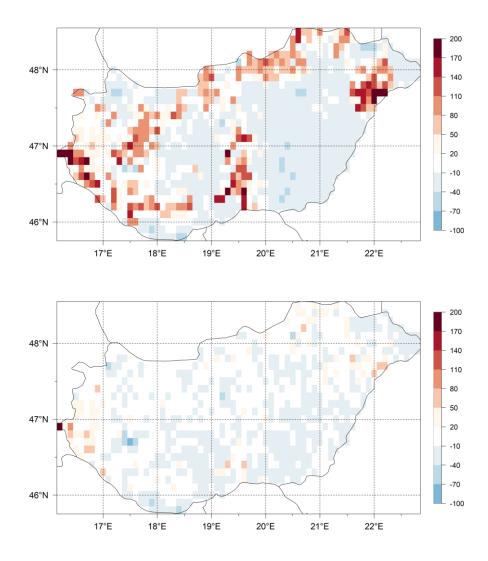


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928 Figure <u>1410</u>: The sensitivity coefficients of the soil parameters as the result of the sensitivity analysis. Black columns refer to the crop, light grey to the grass and dark grey to the forest simulations. The sensitivity coefficients are calculated as the mean pixel level sensitivity coefficient for the given land use type. Horizontal line indicates the 5%
931 threshold that was used to select the final parameter set <u>forthat is subject to</u> optimization.

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The selected ten, soil biogeochemistry related parameters were optimized for each of the 51 groups separately, using maximum likelihood estimation. For each group, the parameter set providing the smallest deviation between the simulated and the observed values of the weighted average SOC content (weight factor of 5 is used for the 0-30 cm, and weight factor of 1 is used for the 30-60 cm soil layers) was considered to be the final (optimized) model parameter set.

The differences of the simulated and observed SOC content for the 0-30 cm layer (SOC0-30) using the initial (Table 1) and final soil parameters (not shown here) are presented in Figure <u>1544</u>. On the upper plot the signed relative error of SOC0-30 simulation before optimization, while on the lower figure the signed relative error of SOC0-30 simulation after optimization can be seen. It is clearly visible that because of optimization the overestimation of the SOC0-30 simulation significantly decreased.



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Figure <u>1511</u>: Differences (expressed as signed relative error, %) between the simulated and observed SOC data for the 0-30 layer (SOC0-30) using the initial (upper map) and optimized (lower map) soil parameters. The maps present the signed relative error in percent. Visual comparison of the maps reveals the success of the optimization in terms of capturing the overall SOC for the whole country area.

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We do not claim of course that the optimized parameters have universal value. Site history is neglected during the spin up simulations, and we use many simplifications like disregardingnon-existent land use change, present-day ecosphysiological parameterization etc. In this sense, the optimized parameter set can be best considered as a pragmatic solution to provide initial conditions (equilibrium SOC pools) for the model at the country scale that is consistent with the observations.

## 957 6. Concluding remarks

958 In this paper, we presented a detailed description of the soil hydrology and carbon/nitrogen budget related developments of the Biome-BGCMuSo v6.2 terrestrial 959 ecosystem model. We mostly focused on changes relative to the previously published Biome-960 BGCMuSo v4.0 (Hidy et al., 2016), but our intention was also to provide a complete, 961 standalone reference for the modelling community with mathematical equations (detailed in 962 the Supplementary Material). Table 2 summarizes the structural changes that we made during 963 the developments starting from Biome-BGC v4.1.1 also including the previously published 964 Biome-BGCMuSo v4.0 (Hidy et al., 2016). 965

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Routine	original Biome-BGC	Biome-BGCMuSo v4.0	Biome-BGCMuSo v6.2
Runoff	no	based on simple, empirical formulation	distinguishing Hortonian and Dunne runoff
Pond water	no	simple solution	development of pond water formation (based on infiltration capacity)
Soil evaporation	Based on Penman-Monteith equation Calculation of the actual evaporation from the potential evaporation and the square root of time elapsed since the last precipitation.	Based on Penman-Monteith equation Calculation of the actual evaporation from the potential evaporation and the square root of time elapsed since the last precipitation.	Based on Penman-Monteith equation Parameterization possibility of actual aerodynamic resistance. Introduction of an upper limit for daily potential evaporation that determined by the available energy. Calculation of the actual evaporation is based on the method <u>RitchieRitche</u> (1981). Simulation of the reducing effect of surface residue or mulch cover on bare soil evaporation
Transpiration	Transpiration from one-layer bucket soil	Transpiration from 7-layers soil based on soil stress	Transpiration from 10-layers so based on available water
Groundwater	no	Simple groundwater simulation.	Improvement of the simulation of groundwater effect (using capillary fringe). Introduction of two different methods.
Soil moisture stress	no	Relative SWC data is used to calculate soil water stress. The hygroscopic water, the wilting point, the field capacity and the saturation values of the soil layers can be defined in the input file layer by layer. The soil moisture stress index is affected by the length and the day since the drought event lasted.	The hygroscopic water, the wilting point, the field capacity and the saturation values of the soil layers can be defined in the input file layer by layer. The soil moisture stress index is affected by the length and the severity of the drought event, aggravated by the extreme temperature. Introduction of the soil curvatur parameters to provide mechanis for soil texture dependent drought stress since it can affect the shape of the soil stress function.

967Table 2. Comparison of the internal processes simulated in model structural solutions forBiome-BGC 4.1.1, Biome-968BGCMuSo v4.0 and in Biome-BGCMuSo v6.2.

			Normalized SWC data are used to calculate soil moisture stress index.
Organic carbon and nitrogen	One layer soil module with one organic carbon and nitrogen pool.	Multi-layered soil module without soil carbon and nitrogen profile.	Instead of defining a single litter, soil organic carbon and nitrogen pool, separate carbon and nitrogen pools for each soil layer in the form of soil organic matter and litter were implemented. Separation of above- and belowground litter pools. Litter and soil decomposition fluxes (carbon and nitrogen fluxes from litter to soil pools) are calculated layer by layer, depending on the actual temperature and SWC of the corresponding layers. Leaching of dissolved organic carbon and nitrogen.
Inorganic nitrogen	One layer soil module with one mineralized N pool.	Multi-layer soil module with an empirical inorganic N-profile (no layer-by-layer calculations, only estimation of the subpools in the different soil layer based on the rootlenght proportion).	Separation of ammonium (sNH4) and nitrate (sNO3) soil pools instead of a general mineralized nitrogen pool. Nitrification fluxes are calculated layer by layer, depending on the actual pH, temperature and SWC of the given layers. Denitrification fluxes are calculated layer by layer, depending on the depth, actual temperature and SWC of the given layers.

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971 Earlier model versions used a soil hydrology scheme based on the Richards equation, but the results were not satisfactory. Sándor et al. (2017) presented results from the first major 972 973 grassland model intercomparison project (executed within the frame of FACCE MACSUR) where Biome-BGCMuSo v22.2 was used. That study demonstrated the problems associated 974 975 with proper representation of soil water content that was a common shortcoming of all included models. In the Hidy et al. (2016) paper, where the focus was on Biome-BGCMuSo 976 977 v4.0, the SWC related figures clearly indicated problems with the simulations compared to 978 observations. The SWC amplitude was not captured well which clearly influences drought 979 stress, decomposition, and other SWC driven processes like nitrification and denitrification. For the latter two processes this is especially critical as they are associated with contrasting 980 981 SWC regimes (nitrification is an aerobic, while denitrification is an anaerobic process). This is a good example for erroneous internal process representation that may lead to improper 982 results. Note that the currently used functions for nitrification/denitrification are also subject 983 to uncertainty that needs to be addressed in the future (Heinen, 2006). Nevertheless, the 984

presented model developments might contribute to a more realistic soil process simulationsand improved results.

Algorithm ensemble approach is already implemented in Biome-BGCMuSo. 987 Algorithm ensemble means that the user has more than one option for the representation of 988 some processes. Biome-BGCMuSo v6.2 has alternative phenology routines (Hidy et al., 989 2012), two alternative methods for soil temperature (Hidy et al., 2016), soil hydrology 990 (described in this study), photosynthesis and soil moisture stress calculation. We plan to 991 extend the algorithm ensemble by providing alternative decomposition schemes to the model. 992 993 One possibility is the implementation of a CENTURY-like structure (Koven et al., 2013) that is a promising direction and might improve the quality of the equilibrium (spin-up) 994 995 simulations and the simulated N mineralization related to SOM decomposition. Reported problems related to the rapid decomposition of litter in the current model structure (Bonan et 996 997 al., 2013) needs to be addressed in future model versions as well.

998 Plant growth and allocation related developments were not addressed in this study but 999 of course has many inferences with the presented model logic (i.e. parameterization and 1000 related primary production defines the amount and quality of litter, etc.). A forthcoming 1001 publication will provide a comprehensive overview on the plant growth and senescence 1002 related model modifications where elements from crop models are also included.

Biome-BGCMuSo is still an open source model that can be freely downloaded from its website with a detailed User's Guide and other supplementary files. We also encourage users to test the so-called RBBGCMuso package (available at GitHub) that has many advanced features to support model application and optimization. A graphical environment, called AgroMo (also available at GitHub: https://github.com/hollorol/AgroMo) was also developed around Biome-BGCMuSo to help users in carrying out simulations either with site specific plot scale data or with gridded databases representing large regions.

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### 1012 Code and data availability

1013 The current version of Biome-BGCMuSo, together with sample input files and detailed User's 1014 Guide are available from the website of the model: http://nimbus.elte.hu/bbgc/download.html 1015 under the GPL-2 licence. Biome-BGCMuSo v6 is also available at GitHub: 1016 https://github.com/bpbond/Biome-BGC/tree/Biome-BGCMuSo\_v6. The exact version of the 1017 model (v6.2 alpha) used to produce the results used in this paper is archived on Zenodo 1018 (https://doi.org/10.5281/zenodo.5761202). Experimental data and model parameterization
1019 used in the study are available from the corresponding author upon request.

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## 1022 Authors' Contributions

Hidy developed Biome-BGCMuSo, maintained the source code and executed the sample 1023 1024 simulations. The study was conceived and designed by Hidy, Barcza and Fodor, with assistance from Ács, Dobor and Hollós. It was directed by Hidy and Barcza-. Ács and Dobor 1025 contributed with model benchmarking. Hollós participated with the construction of a 1026 1027 modeling framework for Biome-BGCMuSo. -Filep, Incze, Zacháry and Pásztor contributed 1028 with experimental data. Hidy, Barcza, Fodor and Merganičová prepared the manuscript and the supplement with contributions from all co-authors. All authors reviewed and approved the 1029 1030 present article and the supplement.

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