SYNERGY BETWEEN SATELLITE OBSERVATIONS OF SOIL MOISTURE AND WATER STORAGE ANOMALIES FOR RUNOFF ESTIMATION

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ABSTRACT

This paper presents an innovative approach, STREAM - SaTellite based Runoff Evaluation And Mapping - to derive daily river discharge and runoff estimates from satellite soil moisture, precipitation and ~~terrestrial~~ total water storage anomalies observations. Within a very simple model structure, precipitation and soil moisture data~~the first two variables (precipitation and soil moisture)~~ are used to estimate the *quick-flow* river discharge component while the ~~terrestrial~~ total water storage anomalies are used for obtaining its complementary part, i.e., the *slow-flow* river discharge component. The two are then summed up to obtain river discharge ~~and runoff~~ estimates.

The method is tested over the Mississippi river basin for the period 2003-2016 by using Tropical Rainfall Measuring Mission (TRMM) Multi-satellite Precipitation Analysis (TMPA) precipitation data, European Space Agency Climate Change Initiative (ESA CCI) soil moisture data and Gravity Recovery and Climate Experiment (GRACE) ~~terrestrial~~ total water storage data. Despite the model simplicity, relatively high-performance scores are obtained in river discharge ~~simulations~~estimates, with a Kling-Gupta efficiency index greater than 0.~~65~~ 64 both at the basin outlet and over several inner stations used for model calibration highlighting the high information content of satellite observations on surface processes. Potentially useful for multiple operational and scientific applications, ~~(~~from flood warning systems to the understanding of water cycle~~)~~, the added-value of the STREAM approach is twofold: 1) a simple modelling framework, potentially suitable for global runoff monitoring, at daily time scale when forced with satellite observations only, 2) increased knowledge on the natural processes, human activities and on their interactions on the land.

Key words: satellite products, soil moisture, water storage variations, conceptual hydrological modelling, rainfall-runoff modelling, Mississippi.

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1. INTRODUCTION

Spatial and temporal continuous river discharge monitoring is paramount for improving the understanding of the hydrological cycle, for planning human activities related to water use as well as to prevent or ~~/~~mitigate the losses due to extreme flood events. To accomplish these tasks, runoff and river discharge data, which represents the aggregated signal of runoff (Fekete et al., 2012), should be available at adequate spatial and ~~/~~temporal resolution.~~, i.~~e For water resources management and drought monitoring monthly time series over basin area larger than 10’000 km^2 are sufficient whereas observations up to grid scale of few km and daily or sub-daily time step are required for flood prediction~~., at basin scale (basin area larger than 10’000 km^2) and at monthly time step for water resources management and drought monitoring up to grid scale~~ of ~~(few km)/(su~~ and ~~b-) daily~~ or sub-daily ~~time step for flood prediction~~. The accurate spatio-temporally continuous ~~(in space and time)~~ runoff and river discharge estimation at finer spatial~~/~~ or temporal resolution is still a big challenge for hydrologists.

Traditional in situ observations of river discharge, even if generally characterized by high temporal resolution (up to sub-hourly time step), typically offer little information on the spatial distribution of runoff within a watershed. Moreover, river discharge observation networks suffer from many limitations such as low station density and often incomplete temporal coverage, substantial delay in data access and large decline in monitoring capacity (Vörösmarty et al., 2002). Paradoxically, this latter issue is exacerbated in developing nations (Crochemore et al., 2020), where the knowledge of the terrestrial water dynamics deserves greater attention due to huge damages to settlements and especially the loss of human lives that occurs regularly.

This precarious situation has led to growing interest in finding alternative solutions, i.e., model-based or observation-based approaches, for runoff and river discharge monitoring. Model-based approaches, based on the mathematical description of the main hydrological processes (e.g., water balance models, WBMs, global hydrological models, GHMs, e.g., Döll et al., 2003 or, increasing in complexity, land surface models, LSM, e.g., Balsamo et al., 2009; Schellekens et al., 2017), are able to provide comprehensive information on a large number of relevant variables of the hydrological cycle including runoff and river discharge at very high temporal and spatial resolution (up to hourly sampling and 0.05° grid scale). However, the values of ~~simulated~~ modelled water balance components rely on a massive parameterization of the soil, vegetation and land parameters,~~,~~ which is not always realistic, and are strongly dependent on the GHM or ~~/~~LSM models used, analysis periods (Wisser et al., 2010) and climate forcings selected (e.g Haddeland et al., 2012; Gudmundsson et al., 2012a, b; Prudhomme et al., 2014; Müller Schmied et al., 2016).

Alternatively, the observation-based approaches exploit machine learning techniques and a considerable amount of data to describe the physics of the system (~~i.e. hydraulic and/or hydrologic phenomena,~~ Solomatine and Ostfeld, 2008) with only a limited number of assumptions. Besides being simpler than model-based approaches, these approaches still present some limitations. For example, ~~At first, as~~ they rely on a considerable amount of data describing the modelled system's physics and ~~s,~~ the spatial/temporal extent and the uncertainty of the resulting dataset is determined by both the spatial and ~~/~~temporal coverage and the accuracy of the forcing data (e.g., see E-RUN dataset, Gudmundsson and Seneviratne, 2016; GRUN dataset, Ghiggi et al., 2019; FLO1K dataset, Barbarossa et al., 2018). Additional limitations stem from the employed method to estimate runoff. Indeed, random forests such as employed in Gudmundsson and Seneviratne~~,~~ (2016)~~,~~ like other machine learning techniques, are powerful tools for data driven modeling, but they are prone to overfitting, implying that noise in the data can obscure possible signals (Hastie et al., 2009). Moreover, the influence of land parameters on continental-scale runoff dynamics is not ~~taken into account~~considered as the underlying hypothesis is that the hydrological response of a basin exclusively ~~depend~~depends on present and past atmospheric forcing. It is easy to understand that this assumption will only be valid in certain circumstances and might lead to problems, e.g., over complex terrain (Orth and Seneviratne, 2015) or in cases of human river flow regulation (Ghiggi et al., 2019).

Remote sensing can provide estimates of nearly all the climate variables of the global hydrological cycle including soil moisture (e.g., Wagner et al., 2007; Seneviratne et al., 2010), precipitation (Huffman et al., 2014) and total terrestrial water storage (e.g., Houborg et al., 2012; Landerer and Swenson, 2012; Famiglietti and Rodell, 2013). It has undeniably changed and improved dramatically the ability to monitor the global water cycle and, hence, runoff. By taking advantage of satellite information, some studies tried to develop methodologies able to optimally produce multivariable datasets from the fusion of in situ and satellite-based observations (e.g., Rodell et al., 2015; Zhang et al., 2018; Pellet et al., 2019). Other studies exploited satellite observations of hydrological variables, e.g., precipitation (Hong et al, 2007), soil moisture (Massari et al., 2014), and geodetic variables (e.g., Sneeuw e~~a~~t~~.~~ al., 2014; Tourian et al., 2018) to monitor single components of the water cycle in an independent way.

Although the majority of these studies provide runoff and river discharge data at basin scale and monthly time step, they deserve to be recalled here as important for the purpose of the present study. In particular, Hong et al. (2007) presented a first attempt to obtain an approximate but quasi-global annual streamflow dataset~~,~~ by incorporating satellite precipitation data in a relatively simple rainfall-runoff simulation approach. Driven by the multiyear (1998-2006) Tropical Rainfall Measuring Mission Multi-satellite Precipitation Analysis, runoff was independently computed for each global land surface grid cell through the Natural Resources Conservation Service (NRCS) runoff curve number (CN) method (NRCS, 1986) and subsequently routed to the watershed outlet to ~~simulate~~ predict streamflow. The results, compared to the in situ observed river discharge data, demonstrated the potential of using satellite precipitation data for diagnosing river discharge values both at global scale and for medium to large river basins. If, on the one hand, the work of Hong et al. (2007) can be considered as a pioneer study, on the other hand it presents a serious drawback within the NRCS-CN method that lacks a realistic definition of the soil moisture conditions of the catchment before flood events. This aspect is not negligible~~,~~ as it is well established that soil moisture is paramount in the partitioning of precipitation into surface runoff and infiltration inside a catchment (Brocca et al., 2008). In particular, for the same rainfall amount but different values of initial soil moisture conditions, different flooding effects can occur (see e.g. Crow et al., 2005; Brocca et al., 2008; Berthet et al., 2009; Merz and Bloschl, 2009; Tramblay et al., 2010). On this line following Brocca et al. (2009), Massari et al. (2016) presented a very first attempt to estimate global streamflow data by using satellite Soil Moisture Active and Passive (SMAP, Entekhabi et al.~~,~~, 2010) and Global Precipitation Measurement (GPM, Huffman et al., 2019) products. Although the validation was carried out by routing the monthly surface runoff only in a single basin in Central Italy, the obtained results suggested to dedicate additional efforts in this direction.

Among the studies that use satellite observations of hydrological variables for runoff estimation, the hydro-geodetic approaches are undoubtedly worth mentioning, see e.g., Sneeuw et al.~~,~~ (2014) for a comprehensive overview or Lorenz et al. (2014) for an analysis of satellite-based water balance misclosures with discharge as closure term. In particular, the satellite mission Gravity Recovery And Climate Experiment (GRACE), which observed the temporal changes in the gravity field, has given a strong impetus to satellite-driven hydrology research (Tapley et al., 2019). Since temporal gravity field variations over the continents imply water storage change, GRACE was the first remote sensing system to provide observational access to deeper groundwater storage. GRACE and its successor mission GRACE-FO provide monthly snapshots of the Earth's gravity field. The temporal variation is therefore relative to the temporally mean gravity field and, hence, the time variations of water storage are fundamentally relative to the mean storage. This relative water storage variation is termed Total Water Storage Anomaly (TSWA).

The relation between GRACE-derived ~~groundwater storage change~~TWSA and runoff was characterized by Riegger and Tourian (2014), which even allowed the quantification of absolute drainable water storage over the Amazon (Tourian et al., 2018). In essence, the storage-runoff relation describes the gravity-driven drainage of a basin and, hence, the slow-flow processes. Due to GRACE’s spatial-temporal resolution, runoff and river discharge are generally available for large basins (>160’000 km^2) and at monthly time step.

Based on the above discussion, it is clear that each approach presents strengths and limitations that enable or hamper the runoff and river discharge monitoring at finer spatial and temporal resolutions. In this context, this study presents an attempt to find an alternative method to derive daily river discharge and runoff estimates at ~~¼~~ 0.25° degree spatial resolution exploiting satellite observations and the knowledge of the key mechanisms and processes that act in the formation of runoff, i.e., the role of soil moisture in determining the response of a catchment to precipitation. For that, soil moisture, precipitation and ~~terrestrial water storage anomalies (~~TWSA~~)~~ observations are used as input into a simple modelling framework named ~~STREAM v1.3~~STREAM v1.3 (SaTellite based Runoff Evaluation And Mapping, version 1.3, hereafter referred to as STREAM). Unlike classical ~~land surface models~~LSMs, STREAM exploits the knowledge of the system states (i.e., soil moisture and TWSA) to derive river discharge and runoff, and thus it 1) skips the modelling of the evapotranspiration fluxes which are known to be a non-negligible source of uncertainty (Long et al. 2014), 2) limits the uncertainty associated with the over-parameterization of soil and land parameters and 3) implicitly takes into account processes, mainly human-driven (e.g., irrigation, change in the land use), that might have a large impact on the hydrological cycle and hence on runoff.

The detailed description of the STREAM ~~v1.3~~ model is given in ~~section~~ paragraph 4. The collected datasets and the experimental design for the Mississippi River Basin (~~section~~ paragraph 2) are described in paragraph ~~sections~~ 3 and 5, respectively. Results, discussion and conclusions are drawn in paragraph ~~section~~ 6, 7 and 8, respectively.

2. STUDY AREA

The STREAM ~~v1.3~~ model presented here has been tested and validated over the Mississippi River basin (Figure 1a). With a drainage area of about 3.3 million km^2, the Mississippi River basin is the fourth largest watershed in the world, bordered to the West by the crest of the Rocky Mountains and to the East by the crest of the Appalachian Mountains. According to the Köppen climate classification, the climate is subtropical humid over the southern part of the basin, continental humid with hot

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summer over the central part, continental humid with warm summer over the eastern and northern parts, whereas a semiarid cold climate affects the western part. The average annual air temperature across the watershed ranges from 4°C in the West to 6°C in the East. On average, the watershed receives about 900 mm/year of precipitation (77% as rainfall and 23% as snowfall), more concentrated in the eastern and southern portions of the basin with respect to its northern and western part (Vose et al., 2014).

The river flow has a clear natural seasonality mainly controlled by spring snowmelt (coming from the Missouri and the Upper Mississippi, the eastern and the upper part of the basin, respectively, Dyer 2008) and by heavy precipitation exceeding the soil moisture storage capacity (mostly occurring in the eastern and southern part of the basin, Berghuijs et al., 2016). The basin is also heavily regulated by the presence of large dams (Global Reservoir and Dam Database GRanD, Lehner et al., 2011) most of them located on the Missouri river, over the Great Plains. In particular, the river reach between Garrison and Gavins Point dams is the portion of the Missouri river where the large main-channel dams have the greatest impact on river discharge providing a substantial reduction in the annual peak floods, an increase on low flows and a reduction on the overall variability of intra-annual discharges (Alexander et al., 2012). The annual average of Mississippi river discharge at ~~the~~ Vicksburg, the ~~-~~ outlet river cross-section of the basin, is equal to 17’500 m^3/s (see Table 1). Given the variety of climate and topography across the Mississippi River basin, it is a good candidate to test the suitability of the STREAM ~~v1.3~~ model for river discharge and runoff simulation.

3. DATASETS

The datasets used in this study include in situ observations, satellite products and ~~model outputs~~runoff verification data. The first two datasets ~~have been~~are used as input data to the STREAM ~~v1.3~~ model. Conversely, the runoff verification data ~~model outputs~~ are used as a benchmark to validate the performance of the STREAM ~~v1.3~~ model in simulating the runoff.

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3.1 In situ Observations

In situ observations comprise air temperature ~~(T_{air})~~ and river discharge data ~~(Q)~~.

For ~~T_{air}~~ air temperature data the Climate Prediction Center (CPC) Global Temperature data developed by the American National Oceanic and Atmospheric Administration (NOAA) using the optimal interpolation of quality-controlled gauge records of the Global Telecommunication System (GTS) network (Fan et al., 2008) have been used. The dataset~~,~~ ~~downloadable at (https://psl.noaa.gov/data/gridded/data.cpc.globaltemp.html)~~ is available on a global regular 0.5°×0.5° grid~~,~~ and provides daily maximum (T_{max}) and minimum (T_{min}) air temperature data from 1979 to present (2022). The daily average air temperature data have been generated as the mean of T_{max} and T_{min} of each day.

Daily river discharge ~~Q~~ data over the study basin~~s~~ have been taken from the Global Runoff Data Center (GRDC, https://www.bafg.de/GRDC/EN/Home/homepage_node.html). In particular, –11 gauging stations located along the main river network of the Mississippi River basin have been selected to represent the spatial distribution of ~~runoff~~ river discharge over the basin. The location of these gauging stations along with relevant characteristics (e.g., the upstream basin area, the mean annual river discharge and the presence of upstream dams) are summarized in Table 1. ~~As it can be noted, m~~Mean annual river discharge ranges from 141 to 17’500 m^3/s, and 3 ~~out~~ of 11 ~~sections~~ gages are located downstream of big dams (Lehner et al., 2011). In particular, gages 1, 2 and 5 are located downstream of Garrison (the fifth-largest earthen dam in the world), Gavins Point and Kanopolis dams, ~~located downstream section 1, 2 and 5~~ respectively (see Figure ~~3~~ 1a and Table 1). The related reservoirs ~~, are three large dams~~ have ~~with~~ a maximum storage of 29~~.~~383×10^9 m^3, 0.607×10^9 m^3, and 1.058×10^9 m^3, respectively.

3.2 Satellite Products

Satellite products include observations of precipitation ~~(P)~~, soil moisture and TWSA.

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The satellite precipitation ~~*P*~~ dataset used in this study is the Multi-satellite Precipitation Analysis 3B42 Version 7 (her after referred to as TMPA~~TMPA 3B42 V7~~) estimate produced by the National Aeronautics and Space Administration (NASA) as the 0.25°×0.25° quasi-global (50°~~N~~S-50°~~S~~N) gridded dataset. The TMPA ~~3B42 V7~~ is a gauged-corrected satellite product, with a latency period of two months~~ after the end of the month of record~~, available at 3h sampling interval from 1998 to present~~ (2020)~~. Major details about the *P* dataset, downloadable from http://pmm.nasa.gov/data-access/downloads/trmm, can be found in Huffman et al. (2007).

Soil moisture data have been taken from the European Space Agency Climate Change Initiative (ESA CCI) Soil Moisture project (https://esa-soilmoisture-cci.org/) that provides a surface soil moisture product (referred to first 2~~-~~3 ~~centimeters~~ cm of soil) ~~that is~~ continuously updated in terms of spatial-temporal coverage, sensors and retrieval algorithms (Dorigo et al., 2017). In this study, the daily combined ESA CCI soil moisture product v4.2 is used. ~~and, that~~ It is available at global scale with a grid spacing of 0.25°, for the period 1978 ~~-2016~~to present.

TWSA have been obtained from the Gravity Recovery And Climate Experiment (GRACE) satellite mission. Here we employ the NASA Goddard Space Flight Center (GSFC) global mascon model, i.e., Release v02.4, (Luthcke et al. 2013). It has been produced based on the mass concentration (mascon) approach. The model provides surface mass densities on a monthly basis. Each monthly solution represents the average of surface mass densities within the month, referenced at the middle of the corresponding month. The model has been developed directly from GRACE level-1b K-Band Ranging (KBR) data. It is computed and delivered as surface mass densities per patch over blocks of approximately 1°×1° or about 12’000 km^2. Although the mascon size is smaller than the inherent spatial resolution of GRACE of about 2.5°×2.5° or 64’~~’~~000 km^2 (Vishwakarma et al., 2018), the model exhibits a relatively high spatial resolution. This is attributed to a statistically optimal Wiener filtering, which uses signal and noise full covariance matrices. This allows the filter to fine tune the smoothing in line with the signal-to-noise ratio in different areas. That is, the less smoothing, the higher signal-to-noise ratio in a particular area and vice versa. This ensures that the filtering is

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minimal and aggressive smoothing is avoided when unnecessary. Further details of such a filter can be found in Klees et~~.~~ al.~~,~~ (2008). Importantly, the coloured ~~(frequency-dependent)~~ noise characteristic of KBR data was taken in to account when compiling the GRACE model, which has allowed for a reliable computation of the aforementioned noise full covariance matrices. The coloured ~~(frequency-dependent)~~ noise characteristic of KBR data was taken into account when compiling the model, which has allowed for a reliable computation of these noise and signal covariance matrices. They play a crucial role when filtering and allow ~~to achieve~~ a higher spatial resolution compared to commonly applied GRACE filtering methods such as Gaussian smoothing and/or destriping filters. The GRACE data used here are available from January 2003 to July 2016, which suffices to demonstrate the STREAM capabilities. With its successor mission GRACE Follow-On (GRACE-FO), launched early 2018, the time series of time-variable gravity has reached a nearly uninterrupted time span of about 20 years, thus allowing a continued and operational use of STREAM. The existing interruptions, short ones due to mission operations or technical failures, but also the one-year gap between GRACE and GRACE-FO can be dealt with in various ways, e.g. by data driven gap filling (Yi and Sneeuw, 2021).~~GRACE data are available for the period 01 January 2003 to 15 July 2016.~~

3.3 ~~Model Outputs~~Runoff Verification Data

To establish the quality of the STREAM ~~v1.3~~ model in runoff simulation, monthly runoff ~~(*R*)~~ data obtained from the Global Runoff Reconstruction (GRUN_v1, https://doi.org/10.3929/ethz-b-000324386) have been used for comparison. The GRUN dataset (Ghiggi et al., 2019) is a global monthly runoff ~~*R*~~ dataset derived through the use of a machine learning algorithm trained with in situ river discharge ~~*Q*~~ observations of relatively small catchments (<2500 km^2) and gridded precipitation and temperature derived from the Global Soil Wetness Project Phase 3 (GSWP3) dataset (Kim et al., 2017). The dataset covers the period from 1902 to 2014 and it is provided on a 0.5° ×0.5° regular grid.

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4. METHOD

~~4.~~ 4.1 STREAM Model: the Concept

~~4.1 STREAM Model: the Concept~~

The ~~concept behind the STREAM v1.3~~STREAM model ~~is that~~ conceives river discharge ~~is~~ as a combination of hydrological responses operating at diverse time scales (Blöschl et al., 2013; Rakovec et al., 2016). In particular, river discharge can be considered made up of a *slow-flow* ~~-~~component, produced as outflow of the groundwater storage and of a *quick-flow* component, i.e. mainly related to the surface and shallow-subsurface runoff components (Hu and Li, 2018).

While the high spatial and temporal ~~(i.e., intermittence)~~ variability of precipitation and the highly changing land cover spatial distribution significantly impact the variability of the *quick-flow* river discharge component (with scales ranging from hours to days and ~~meters~~ metres to ~~kilometres~~ kilometres depending on the basin size), *slow-flow* river discharge reacts to precipitation inputs more slowly ~~(i.e., months)~~ as water infiltrates, is stored, mixed and is eventually released in times spanning from weeks to months. Therefore, the two components can be estimated by relying upon two different approaches that involve different types of observations. Based on that, within the ~~STREAM v1.3~~STREAM model, satellite soil moisture, precipitation and TWSA will be used for deriving river discharge and runoff estimates. The first two variables are used as proxy of the *quick-flow* river discharge component while TWSA is exploited for obtaining its complementary part, i.e., the *slow-flow* river discharge component. Firstly, we exploit the role of the soil moisture in determining the response of the catchment to the precipitation inputs, which have been soundly demonstrated in more than ten years of literature studies (see e.g., Brocca et al., 2017 for a comprehensive discussion on the topic). Secondly, we consider the important role of ~~terrestrial~~ total water storage in determining the *slow-flow* river discharge component as modelled in several hydrological models (e.g., Sneeuw et al., 2014).

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It is worth noting that -modeling the *quick-flow* and *slow-flow* river discharge components ~~this *modus operandi*, i.e. to model the *quick-flow* and *slow-flow* discharge component separately exploring their process controls~~ independently~~,~~ has been largely applied and tested in recent and past studies, e.g., for the estimation of the flow duration curve (see e.g, Botter et al., 2007a, b; Yokoo and Sivapalan 2011; Muneepeerakul et al., 2010; Ghotbi et al., 2020).

4.2 STREAM Model~~: the Laws~~

The STREAM model is a semi-distributed conceptual hydrological model that uses gridded satellite-derived inputs of precipitation, soil moisture, TWSA and air temperature to ~~simulate~~estimate daily values of gridded runoff and river discharge time series at select basin outlets.

To set up the model, the catchment is divided into *b* sub-catchments, each one representing either a tributary draining area with outlet along the main channel or an area draining directly into the main channel (see Figure ~~1~~2). Each sub-catchment, assumed homogeneous, is further divided into an array N_b of individual cells assumed as the unit basis for the runoff generation. Note that t~~T~~he number N_b differs for each sub-catchment~~,~~ as, for a fixed cell grid size, it ~~depends~~varies with ~~both on~~ the sub-catchment area~~ and the cell grid size~~. Once estimated at cell scale and aggregated at the sub-basin scale (see paragraph 4.2.1 for details), the runoff is routed at each sub-catchment outlet (~~–~~see paragraph 4.2.2) and then transferred through the channels and the rivers for the computation of the river discharge at intermediate outlets or at ~~the~~ the outlet of the entire basin (see paragraph 4.2.3).

Based on that, hereinafter we refer to river discharge, Q, to indicate the amount of water passing a particular point of a river (in m^3 s^{-1}) whereas runoff, R, is regarded as the depth of water produced from a drainage area during a particular time interval (in mm). The difference between the two quantities is related to the routing processes that allow to transform the runoff into river discharge~~The STREAM v1.3 model is a conceptual hydrological model that, by using as input observation of *P*, soil moisture, TWSA and T_{air} data, simulates continuous *R* and *Q* time series.~~ .

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4.2.1 Runoff generation at cell scale

The soil zone of each cell *i* of the basin is divided into two layers, the upper and lower soil storages allowing to ~~simulate~~ model the related runoff responses, $R_{q,i}$ ~~Rsu~~ [mm] and $R_{s,i}$ ~~Rsl~~ [mm], as illustrated in Figure ~~1~~2b.

~~-~~The upper cell storage receives inputs from precipitation (P_i ~~P~~), released through a snow module (Cislaghi et al., 2020) as rainfall (r_i) or stored as snow water equivalent (SWE_i) within the snowpack and on the glaciers. In particular, according to Cislaghi et al. (2020), SWE_i ~~$SWEi$~~ is modelled by using as input air temperature ($T_{\mathrm{air},\,i}$) and a degree-day coefficient, C_{m}, to be estimated by calibration. ~~We have to acknowledge that, even though this rain/snow differentiation method works quite efficiently at a large grid size like the one used in the study (25 x 25 km), the topographic complexity of higher elevations can be lost. A different differentiation scheme based e.g., on the wet bulb temperature like in IMERG (Wang et al., 2019; Arabzadeh and Behrangi, 2021), is another possibility.~~

Once precipitation is partitioned by the snow model, the rainfall output r_i contributes to $R_{q,i}$ ~~Rsu~~ while the SWE_i ~~$SWEi$~~ (like other fluxes contributing to modify the soil water content into *Su*) is neglected as already considered in the satellite TWSA. Therefore, the first key point of the STREAM model is that the water content in the upper storage of soil zone, *Su* (Figure ~~1~~2b), is directly provided by the satellite soil moisture observations and the loss processes like ~~infiltration~~percolation or evaporation do not need to be explicitly modelled to ~~simulate~~estimate the evolution in time of soil moisture. Consequently, for each cell i, $R_{q,i}$ ~~Rsu~~ can be computed following the formulation proposed by Georgakakos and Baumer (1996), as in equation (1):

$$R_{q,i}\,(t) = r_i(t)\;SWI_i(t,T)^{\alpha} \qquad (1)$$

where:

- t [days] represents the time;
- r_i [mm] is the rainfall, obtained as an output from the snow module;

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- SWI_i [-] is the Soil Water Index (Wagner et al., 1999), i.e., the root-zone soil moisture product referred to the first layer of the model (representative of the first 5–30 cm of soil), derived by the surface satellite soil moisture product, θ_i, by applying the exponential filtering approach in its recursive formulation (Albergel et al., 2009):

$$SWI_{i,n} = SWI_{i,n-1} + K_n(\theta_i(t_n) - SWI_{i,n-1}) \qquad (2)$$

with the gain K_n at the time t_n given by:

$$K_n = \frac{K_{n-1}}{K_{n-1} + e^{\left(\frac{t_n - t_{n-1}}{T}\right)}} \qquad (3)$$

- T [days] is a parameter, named characteristic time length, that characterizes the temporal variation of soil moisture within the root-zone profile and the gain K_n ranges between 0 and 1;
- α[-] is a coefficient linked to the non-linearity of the infiltration process and it ~~takes into account~~considers the characteristics of the soil;
- for the initialization of the filter $K_1 = 1$ and $SWI_1 = \theta(t_1)$.

The second key point of STREAM model concerns the estimation of $R_{s,i}$, i.e., the *slow*~~-~~*runoff* response related to the lower storage of the soil zone. The hypothesis here, shared also with other studies (e.g., Rakovec et al., 2016), is that the dynamic of R_s ~~Rsl~~ can be represented by the monthly TWSA data. Indeed, the time scale of R_s is typically in the range of seasons to years and it can be assumed almost independent of the water that is contained in the upper storage. For that, for each cell i, $R_{s,i}$ can be computed following the formulation proposed by Famiglietti and Wood (1994), through equation (4) as follows:

$$R_{s,i}(t) = \beta\,(TWSA_i^*(t))^m \qquad (4)$$

where:

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- $TWSA_i^*$ [-] is the TWSA estimated by GRACE over the cell i normalized by its minimum and maximum values. The assumption behind this equation is that TWSA can be assumed as a proxy of the evolution in time of the Sl, i.e., the water amount in the lower storage of the soil zone.
- β [mm h^{-1}] and m [-] are two parameters describing the nonlinearity between lower storage runoff component and $TWSA^*$.

Note that we made the hypothesis that soil moisture and TWSA observations are independent (whereas in reality soil moisture can be responsible both for the generation of R_q (mainly) and for the R_s contribution) given the different temporal (and spatial) scales at which the upper and lower runoff responses act.

By neglecting any lateral flow, the runoff responses at cell scale are averaged at sub-catchment scale to obtain~~ed~~ b runoff responses, one for each sub-catchment. Specifically, by considering N_b cells for each sub-catchment, the following equation are used:

$$R_{q,b}(t) = \frac{\sum_{i=1}^{N_b} R_{q,i}(t)}{N_b} \quad (5)$$

$$R_{s,b}(t) = \frac{\sum_{i=1}^{N_b} R_{s,i}(t)}{N_b} \quad (6)$$

~~By neglecting any lateral flow, the runoff responses at cell scale are averaged at sub-catchment scale to obtained b runoff responses. Specifically, by considering N_b cells for each sub-catchment, the following equation are used:~~

$$\cancel{R_{q,b}(t) = \frac{\sum_{i=1}^{N_b} R_{q,i}(t)}{N_b}} \quad \cancel{(5)}$$

$$\cancel{R_{s,b}(t) = \frac{\sum_{i=1}^{N_b} R_{s,i}(t)}{N_b}} \quad \cancel{(6)}$$

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4.2.2 Sub-catchment river discharge calculation

~~By neglecting any lateral flow, the runoff responses at cell scale are averaged at sub-catchment scale to obtained b runoff responses. Specifically, by considering N_b cells for each sub-catchment, the following equation are used:~~

$$\cancel{R_{q,b}(t) = \frac{\sum_{i=1}^{N_b} R_{q,i}(t)}{N_b}} \qquad \cancel{(5)}$$

$$\cancel{R_{s,b}(t) = \frac{\sum_{i=1}^{N_b} R_{s,i}(t)}{N_b}} \qquad \cancel{(6)}$$

For each sub-catchment b, the runoff component $R_{q,b}$ is routed to ~~the~~ its outlet by the Geomorphological Instantaneous Unit Hydro-graph (GIUH, Gupta et al., 1980) for tributary draining areas or through a linear reservoir approach (Nash, 1957) for directly draining areas. The $R_{s,b}$ runoff component is transferred to the sub-catchment outlet by a linear reservoir approach. These processes are controlled by a parameter lag time, L [days], evaluated as (Corradini et al., 2002):

$$L = \gamma 1.19\, A_b^{0.33} \qquad (7)$$

where A_b [km^2] is the sub-catchment area and γ [-] is a parameter to be calibrated.

By routing the $R_{q,b}$ and $R_{s,b}$ components ~~we obtain~~ the *quick-flow*, $Q_{q,b}$ [m^3/s], and the *slow-flow*, $Q_{s,b}$ [m^3/s] river discharge components at each sub-catchment outlet are obtained (see Figure ~~1~~2c).

4.2.3 River discharge routing through river networks

A diffusive linear approach (controlled by the parameters C [km h^{-1}] and D [km^2 h^{-1}] ~~C and D~~, i.e., Celerity and Diffusivity, Troutman and Karlinger, 1985) is applied to route the two river discharge components, $Q_{q,b}$ and $Q_{s,b}$ trough the river network from the sub-catchment outlet to intermediate outlets along the river or to the outlet of the entire basin (Brocca et al., 2011). In this way the *quick-*

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Formattato: Tipo di carattere: Non Corsivo, Non Apice / Pedice *flow*, Q_q [m^3/s], and the *slow-flow*, Q_s [m^3/s] river discharge components at the catchment outlet are obtained (see Figure 2d).

~~The model entails three main components (Figure 1): 1) a snow module to separate precipitation into snowfall and rainfall, 2) a soil module to simulate the evolution in time *t* of the quick and slow runoff responses, Qf [mm] and Qsl [mm], and 3) a routing module that transfers these components through the basins and the rivers for the simulation of the *quick-flow* river discharge, *QF* [m^3/s], and the *slow-flow* river discharge, *SF* [m^3/s] components. The soil module is composed of two storages, Su and Sl as illustrated in Figure 1. The upper storage receives inputs from *P*, released through a snow module (Cislaghi et al., 2020) as rainfall (*r*) or stored as snow water equivalent (*SWE*) within the snowpack and on the glaciers. In particular, according to Cislaghi et al. (2020), *SWE* is modelled by using as input T_{air} and a degree-day coefficient, C_m, to be estimated by calibration. We have to acknowledge that, even though this rain/snow differentiation method works quite efficiently at a large grid size like the one used in the study (25 x 25 km), the topographic complexity of higher elevations can be lost. A different differentiation scheme based e.g., on the wet bulb temperature like in IMERG (Wang et al., 2019; Arabzadeh and Behrangi, 2021), would be preferable but is out of the purpose study.~~

~~Once separated, *r* input contributes to the *quick* runoff response while the *SWE* (like other fluxes contributing to modify the soil water content into *Su*) is neglected as already considered in the satellite TWSA. Therefore, the first key point of the STREAM v1.3 model is that the water content in the upper storage is directly provided by the satellite soil moisture observations and the loss processes like infiltration or evaporation do not need to be explicitly modelled to simulate the evolution in time *t* of soil moisture. Consequently, the quick runoff response, Qfu from the first storage can be computed following the formulation proposed by Georgakakos and Baumer (1996), as in equation (1):~~

$$Qfu(t) = r(t)\, SWI(t,T)^{\alpha} \qquad (1)$$

~~where:~~

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- ~~SWI is the Soil Water Index (Wagner et al., 1999), i.e., the root-zone soil moisture product referred to the first layer of the model (representative of the first 5-30 centimeters of soil), derived by the surface satellite soil moisture product, θ, by applying the exponential filtering approach in its recursive formulation (Albergel et al., 2009):~~

$$\cancel{SWI_n = SWI_{n-1} + K_n(\theta(t_n) - SWI_{n-1})} \qquad \cancel{(2)}$$

~~with the gain K_n at the time t_n given by:~~

$$\cancel{K_n = \frac{K_{n-1}}{K_{n-1} + e^{\left(\frac{t_n - t_{n-1}}{T}\right)}}} \qquad \cancel{(3)}$$

- ~~T [days] is a parameter, named characteristic time length, that characterizes the temporal variation of soil moisture within the root-zone profile and the gain K_n ranges between 0 and 1;~~
- ~~α[-] is a coefficient linked to the non-linearity of the infiltration process and it takes into account the characteristics of the soil;~~
- ~~for the initialization of the filter $K_1 = 1$ and $SWI_1 = \theta(t_1)$.~~

~~The second key point of STREAM v1.3 model concerns the estimation of the slow runoff response, Qsl, from the second storage. The hypothesis here, shared also with other studies (e.g., Rakovec et al., 2016), is that the dynamic of the slow runoff component can be represented by the monthly TWSA data. Indeed, the time scale of slow runoff response is typically in the range of seasons to years and it can be assumed almost independent upon the water that is contained in that upper storage. For that, the slow runoff response Qsl, from the second storage, can be computed following the formulation proposed by Famiglietti and Wood (1994), through equation (4) as follows:~~

$$\cancel{Qsl(t) = \beta\,(TWSA^*(t))^m} \qquad \cancel{(4)}$$

~~where:~~

~~$TWSA^*$ [ ] is the TWSA estimated by GRACE normalized by its minimum and maximum values. The assumption behind this equation is that TWSA can be assumed as a proxy of the evolution in time, t, of the Sl, i.e., the storage of the lower storage.~~

~~β [mm h^{-1}] and m [-] are two parameters describing the nonlinearity between slow runoff component and $TWSA^*$.~~

~~Note that we made the hypothesis that soil moisture and TWSA observations are independent (whereas in the reality soil moisture can be responsible both for the generation of the quick flow part (mainly) and for the slow flow contribution) given the different temporal (and spatial) scales at which the quick and slow runoff responses act.~~

~~The STREAM v1.3 model runs in a semi-distributed version in which the catchment is divided into s elements, each one representing either a subcatchment with outlet along the main channel or an area draining directly into the main channel. Each element is assumed homogeneous and hence constitutes a lumped system.~~

~~The routing module (controlled by a γ parameter) conveys the Qfu and Qsl response components at each element outlet (subcatchments and directly draining areas, Brocca et al., 2011) and successively at the catchment outlet of the basin. Specifically, the quick component Qfu is routed to the element outlet by the Geomorphological Instantaneous Unit Hydro-graph (GIUH, Gupta et al., 1980) for subcatchments or through a linear reservoir approach (Nash, 1957) for directly draining areas; the Qsl slow component is transferred to the outlet section by a linear reservoir approach. Finally, a diffusive linear approach (controlled by the parameters C and D, i.e., Celerity and Diffusivity, Troutman and Karlinger, 1985) is applied to route the quick and slow runoff components at the outlet section of the catchment (Brocca et al., 2011). In the first case we obtain the *quick-flow* river discharge component, QF [m^3/s], and in the second case the *slow-flow* river discharge component, SF [m^3/s] (see Figure 1).~~

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4.3 STREAM Parameters

~~5.~~ THE ~~STREAM V1.3~~STREAM MODEL USES 8 CALIBRATION PARAMETERS FOR EACH SUB-CATCHMENT ~~*SB*~~ INTO WHICH THE ENTIRE BASIN IS DIVIDED. ~~OF WHICH~~ AMONG THESE PARAMETERS, 5 ~~ARE~~ CONTROL THE ~~USED IN THE SOIL MODULE~~RUNOFF GENERATION PROCESS (α, T~~T [days]~~, β ~~β [mm h^{-1}]~~, mm~~, m~~, C_m~~CM~~) AND 3 ~~IN~~ THE ROUTING ~~MODULE~~ COMPONENT AND THEREFORE THE STREAMFLOW DYNAMICS ~~PART~~ (γ, C ~~[KM H^{-1}]~~ AND D ~~[KM^2 H^{-1}]~~). THE PARAMETER VALUES DETERMINED ~~, DETERMINED~~ WITHIN THE FEASIBLE PARAMETER SPACE (SEE TABLE APPENDIX A FOR MORE DETAILS), ARE CALIBRATED BY MAXIMIZING THE KLING-GUPTA EFFICIENCY INDEX (*KGE*~~KGE~~, GUPTA ET AL., 2009; KLING ET AL., 2012, SEE PARAGRAPH 5.1 FOR MORE DETAILS) BETWEEN OBSERVED AND ~~SIMULATED~~ MODELLED RIVER DISCHARGE. FOR MODEL CALIBRATION, A STANDARD GRADIENT-BASED AUTOMATIC OPTIMISATION METHOD (BOBER 2013) WAS USED.

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~~6.~~5. EXPERIMENTAL DESIGN

5.1 Modelling Setup for Mississippi River Basin

The modelling setup is carried out in three steps (Figure ~~2~~3):

1. *Sub-~~basin~~ catchment delineation.* ~~STREAM v1.3 model is run in the semi-distributed version over the Mississippi River basin.~~ The TopoToolbox (https://topotoolbox.wordpress.com/), a tool developed in Matlab by Schwanghart et al. (2010), and the SHuttle Elevation Derivatives at multiple Scales (HydroSHED, https://www.hydrosheds.org/) DEM of the basin at the 3″ resolution (nearly 90 m at the equator) have been used to derive flow directions, to extract the stream network and to delineate the drainage basins over the Mississippi River basin. In particular, by considering only

rivers with order greater than 3 (according to the Horton-Strahler rules, Horton, 1945; Strahler, 1952), the Mississippi watershed has been divided into 53 ~~sub-basins~~sub-catchments as illustrated in Figure ~~3a~~1a. Blue lines in the figure illustrate the river network pathway connecting the sub-catchments, ~~Red~~ red dots ~~in the figure~~ indicate the location of the 11 river discharge gauging stations selected for the study area.

It has to be specified that the step of sub-basin delineation could be accomplished through tools different from the TopoToolbox. For instance, it could be used the free Qgis software downloadable at https://www.qgis.org/it/site/forusers/download.html, following the instruction to perform the hydrological analysis as in https://docs.qgis.org/3.16/en/docs/training_manual/processing/hydro.html?highlight=hydrological%20analysis.

2. *Extraction of input data.* Precipitation, air temperature~~T_{air}~~, soil moisture and TWSA datasets data have to be extracted for each sub-catchment~~basin~~ of the study area. If characterized by different spatial/temporal resolution, these datasets need to be resampled over a common spatial grid/temporal time step prior to be used as input into the model.

To run the ~~STREAM v1.3~~STREAM model over the Mississippi river basin, input data have been resampled over the precipitation spatial grid at 0.25° resolution through a bilinear interpolation. Concerning the temporal scale, air temperature~~T_{air}~~, soil moisture and precipitation data are available at daily time step, while monthly TWSA data have been linearly interpolated at daily time step. For each of the 53 Mississippi sub-catchment~~subbasins~~, the resampled precipitation, soil moisture, ~~T_{air}~~ air temperature and TWSA data have been extracted (see Figure ~~3~~1b and ~~3c~~1c).

3. *STREAM model calibration.* In situ river discharge data are used as reference data for the calibration of ~~STREAM v1.3~~STREAM model. For Mississippi, the STREAM model has been calibrated at five gauging stations, i.e., the stations 4, 6, 9, 11 and 10. This allowed to identify five sets of STREAM parameters attributed to each catchment according to the river network pathway illustrated in Figure ~~3~~1a. This means that, for example, to the sub-catchments labelled as 1, 2, 5 to

15, 17, 22, 23, and 30 contributing to the ~~station~~gauging station 4 are attributed the parameter set obtained by calibrating the model against river discharge data observed at station 4; to the sub-catchments 31, 37, 38 and 41 contributing to ~~station~~gauging station 6 are attributed the parameter set obtained by calibrating the model with respect to ~~station~~gauging station -6 and so on. Consequently, the sub-catchments highlighted with the same colour in Figure ~~3~~1a are assigned the same model parameters, i.e. the parameters that allow to reproduce the river discharge data observed at the related ~~calibration station~~gage.

~~For Mississippi, the STREAM v1.3 model has been calibrated over five sections as illustrated in Figure 3: the inner sections 4, 6, 9, 11 and the outlet section 10, are used to calibrate the model and all sub-basins contributing to the respective sections are highlighted with the same colour. This means that, for example, the sub-basins labelled as 1, 2, 5 to 15, 17, 22, 23, and 30 contribute to section 4, sub-basins 31, 37, 38 and 41 contribute to section 6 and so on. Consequently, the sub-basins highlighted with the same colour are assigned the same model parameters, i.e. the parameters that allow to reproduce the river discharge data observed at the related outlet section.~~

Once calibrated, the ~~STREAM v1.3~~STREAM model has been run to provide continuous daily ~~Q~~ runoff and ~~R~~ river discharge time series, ~~at the outlet section of each subbasin and~~ over each grid pixel and at the outlet section of each sub-catchment, respectively. By considering the spatial/temporal availability of both in situ and satellite observations, the entire analysis period covers the maximum common observation period, i.e., from ~~01~~ January 2003 to ~~15~~ July 2016 at daily time scale. To establish the goodness-of-fit of the model, the ~~simulated~~ modelled river discharge and runoff timeseries are compared against in situ river discharge and modelled runoff data.

5.2 Model Evaluation Criteria and Performance Metrics

The model has been run over a 13.5-year period split into two sub periods: the first 8 years, from January 2003 to December 2010, ~~have been~~are used to calibrate the model.~~;~~ ~~t~~The model is validated, as described below over ~~successively~~ the ~~validated over the~~ remaining 5.5 years (January 2011 - July 2016).

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In particular, three different validation schemes have been adopted to assess the robustness of the ~~STREAM v1.3~~STREAM model:

1. i~~I~~nternal validation aimed to test the plausibility of both the model structure and the parameter set in providing reliable estimates of the hydrological variables against which the model is calibrated. For this purpose, a comparison between observed and ~~simulated~~ modelled river discharge time series on the ~~sections~~ gauging stations used for model calibration has been carried out for both the calibration and validation sub periods;~~.~~
2. c~~C~~ross-validation testing the goodness of the model structure and the calibrated model parameters to predict hydrological variables at locations not considered in the calibration phase. In this respect, the cross-validation has been carried out by comparing observed and ~~simulated~~ modelled river discharge time series in ~~gauged~~ gauging stations ~~basins~~ not considered during the calibration phase;
3. e~~E~~xternal validation aimed to test the capability of the model "*to get the right answers for the right reasons*" (Kirchner 2006). The rationale behind this concept is that the hydrological models are today highly performing and able to reproduce a lot of hydrological variables. For that, the model performances should not only be evaluated against observed ~~streamflow~~river discharge, but complementary datasets representing internal hydrologic states and fluxes (e.g., soil moisture, evapotranspiration, runoff etc) should be considered. As runoff is a secondary product of the ~~STREAM v1.3~~STREAM model, obtained indirectly from the calibration of the river discharge (basin-integrated runoff), the comparison in terms of runoff can be considered as a further external validation of the model. Runoff, differently from river discharge, cannot be directly measured. It is generally modelled through land surface or hydrological models. Its validation requires a comparison against modelled data that, however, suffer from uncertainties (Beck et al., 2017). Based on that, in this study the GRUN runoff dataset described in the ~~section~~ paragraph 3.3 has been used for a qualitative comparison.

5.3 Performance Metrics

To measure the goodness-of-fit between ~~simulated~~ modelled and observed river discharge data three performance scores have been used:

- the ~~relative~~ root mean square error relative to the mean, $RRMSE$~~RRMSE~~:

$$RRMSE = \frac{\sqrt{\frac{1}{n}\sum_{\cancel{i}j=1}^{n}\left(Q\cancel{sim}mod_{\cancel{i}j} - Q_{obs_{\cancel{i}j}}\right)^2}}{\frac{1}{n}\sum_{\cancel{i}j=1}^{n}\left(Q_{obs_{\cancel{i}j}}\right)}$$

(~~57~~8)

where Q_{obs} and $Q_{\cancel{sim}mod}$ are the observed and ~~simulated~~ modelled river discharge time series of length n. $RRMSE$ ~~RRMSE~~ values range from 0 to +∞, the lower the $RRMSE$ ~~RRMSE~~, the better the agreement between observed and ~~simulated~~ modelled data.

- the Pearson correlation coefficient, ~~R~~rho, measur~~es~~ing the linear relationship between two variables:

$$\cancel{R}rho = \frac{\sum_{\cancel{i}j=1}^{n}\left(Qmod\cancel{sim}_{\cancel{i}j} - \overline{Q_{\cancel{sim}mod}}\,\cancel{\overline{Qsim_i}}\right)\left(Qobs_{\cancel{i}j} - \overline{Q_{obs}}\,\cancel{\overline{Qobs_i}}\right)}{\sqrt{\sum_{\cancel{i}j=1}^{n}\left(Q\cancel{sim}mod_i - \overline{Q_{\cancel{sim}mod}}\,\cancel{\overline{Qsim_i}}\right)^2\left(Qobs_{\cancel{i}j} - \overline{Q_{obs}}\,\cancel{\overline{Qobs_i}}\right)^2}}$$

(~~68~~9)

where $\overline{Q_{obs}}$ and $\overline{Q_{\cancel{sim}mod}}$ represent the mean values of Q_{obs} and $Q_{\cancel{sim}mod}$, respectively. The values of rho~~R~~ range between −1 and 1; higher values of R indicate a better agreement between observed and ~~simulated~~ modelled data.

- the Kling-Gupta efficiency index (KGE~~KGE~~, Gupta et al., 2009), which provides direct assessment of four aspects of river discharge time series, namely shape, timing, water balance and variability. It is defined as follows:

$$KGE = 1 - \sqrt{(\cancel{R}rho - 1)^2 + (\delta - 1)^2 + (\varepsilon - 1)^2} \quad (\cancel{79}10)$$

where ~~R is the correlation coefficient,~~ δ is the relative variability and ε the bias normalized by the standard deviation between observed and ~~simulated~~ modelled river discharge. The KGE ~~KGE~~ values range between -∞ and 1; the higher the KGE ~~KGE,~~ the better is the agreement between observed and

~~simulated~~ modelled data. Simulations characterized by values of KGE ~~KGE~~ in the range -0.41 and 1 can be assumed as reliable; values of KGE ~~KGE~~ greater than 0.5 have been assumed good with respect to their ability to reproduce observed time series (Thiemig et al., 2013).

5.4 STREAM sensitivity analysis

To investigate how the variation of the STREAM parameters influences the variation of the STREAM model outputs, a global sensitivity analysis has been carried out. Specifically, the Variance-Based sensitivity analysis (VBSA, Sobol 1993) implemented into the Sensitivity Analysis For Everybody toolbox (SAFE, Pianosi et al., 2015, https://www.safetoolbox.info/) has been applied. VBSA relies on the variance decomposition and consists of assessing the contributions to the variance of the model output from variations in the parameters. In this study, we use as sensitivity index the first-order (main effect) index, which measures the variance contribution from variations in an individual input factor alone (i.e., excluding interactions with other factors) and the total sensitivity indices, which measure the total contribution of a single input factor or a group of inputs including interactions with all other inputs. The following steps were carried out to execute the VBSA. Firstly, the locality-sensitive hashing (LSH) technique was used to generate 15000 samples from the model parameter space (see Table 1A). Previous hydrological studies (e.g., Tang et al., 2007) recommend the LHS sampling method for its sampling efficiency. Secondly, 15000 STREAM model runs were executed and the corresponding KGE ~~KGE~~ values ~~(11 values, each one for each gauging section) f or each run~~(11x15~~,~~000 values, one for each gauging ~~section~~station for each run) were retained. Thirdly, the parameters and the 15000 KGE ~~KGE~~ samples were used in the SAFE toolbox to compute the sensitivity indices.

For major details on the workflow needed to implement the VBSA the reader is referred to Noacco et al. (2020).

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~~8.~~6. RESULTS

The testing and validation of the ~~STREAM v1.3~~STREAM model is presented and discussed in this ~~section~~ paragraph according to the scheme illustrated in ~~section~~ paragraph 5.2.

6.1 Internal Validation

The performance of the ~~STREAM v1.3~~STREAM model over the ~~the calibrated river~~ gauging ~~sections~~ stations used for calibration is illustrated in Figure 4 and summarized in Table 2. Figure 4 shows observed and ~~simulated~~ modelled river discharge time series over the whole study period (2003-2016); in Table 2 the performance scores are evaluated separately for the calibration and validation sub periods. It is worth noting that the model accurately ~~simulates~~ predicts the observed river discharge data and is able to give the "right answer" with good modelling performances. Score values of KGE ~~KGE~~ and ~~R~~ rho over the calibration ~~(validation)~~ period are higher than 0.~~62~~ 78~~(0.67) and 0.75 (0.75) (resp.)~~ for all the calibrated gauging ~~sections~~stations; $RRMSE$ ~~RRMSE~~ is lower than ~~46~~45% ~~(51%)~~ for all the calibrated gauging ~~sections~~ stations except for station ~~section~~ 9, where it rises up to ~~71~~66%. ~~(77%).~~ The performances remain good even if they are evaluated over the validation period or the entire study period as indicated by the scores on the top of each plot of Figure 4.

6.2 Cross-validation

The cross-validation has been carried out over the six ~~river sections~~gauging stations illustrated in Figure 5 not used in the calibration step. The performance scores on the top of each plot refer to the entire study periods; the scores split for calibration and validation periods are reported in Table 2. For some river discharge gauging ~~sections~~ stations the performance is quite low (see, e.g., gauging station ~~river section~~ 1, 2 and 5) whereas for others the model is able to ~~simulate~~ estimate ~~the observed~~ river discharge data quite accurately (e.g., 7 and 8). In particular, for the gauging stations ~~river sections~~ 1 and 2 even if KGE ~~KGE~~ reaches values equal to 0.~~35~~ 39 and 0.~~40~~ 46 ~~-(~~for the whole period~~)~~, respectively, there is not a good agreement between observed and ~~simulated~~ modelled river discharge and the rho~~R~~ score is lower than 0.~~55~~ 56 for both ~~river~~ the ~~sections~~stations. The worst performance is obtained over the gauging ~~section~~ station 5, with negative KGE ~~KGE~~ and low ~~R~~ rho values~~(high RRSME)~~. These results are certainly influenced by the presence of large dams located upstream to these ~~river sections~~stations (i.e., Garrison, Gavins Point and Kanopolis dams, see Table 1) which have a strong impact on river discharge: the model, not having a specific module for modelling reservoirs, is not able to accurately reproduce the dynamics of river discharge over regulated river ~~sections~~stations. Positive KGE ~~KGE~~ values are obtained over ~~river sections~~the gauging stations 3, 7 and 8. In particular, over ~~section~~ the gauging station 3 the ~~STREAM v1.3~~STREAM model overestimates the observed river discharge due the presence of large dams along the Missouri river, over the Great Plains region. This area is well known from other large-scale hydrological models (e. g., ParFlow-CLM and WRF-Hydro) to be an area with very low performances in terms of river discharge modelling (O'Neill et al., 2020, Tijerina et al., 2021).

Over ~~section~~ the gauging station 7, located over the Rock river, a relatively small tributary of the Mississippi river (see Table 1), the ~~STREAM v1.3~~STREAM model overestimation has to be attributed to: 1) the different characteristics of the Rock river basin with respect to the entire basin closed to ~~section~~ station 6 where the model has been calibrated (see Figure ~~3~~1a); 2) the small size of the Rock river basin (23'000 km^2 , if compared with GRACE resolution, 160'000 km^2) for which the model accuracy is expect to be lower. Conversely, the performances over ~~river section~~the gauging station 8, whose parameters have been set equal to the ones of ~~river section~~gauging station 10, are quite high (KGE ~~KGE~~ equal to 0.71, 0.~~80~~ 81 and 0.~~77~~ 78 for the entire, the calibration and the validation period, respectively; rho ~~R~~ equal to 0.~~83~~82, 0.84 and 0.~~84~~ 83 for the entire, calibration and validation periods, respectively). This outcome demonstrates that under some circumstances, the ~~STREAM v1.3~~STREAM model can be used to estimate river discharge in basins not calibrated over, especially those without upstream dams and with comparable size and land cover.

On overall, the cross-validation results suggest that the performances of STREAM model, as any hydrological model calibrated against observed data, decrease over the gauging stations not used for

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the calibration raising doubts about the robustness of model parameters and whether it is actually possible to transfer model parameters from one river section to another with different inter-basin characteristics. A more in-depth investigation about the model calibration procedure, with special focus on the regionalization of the model parameters, should be carried out but this topic is beyond the scope of the manuscript~~Although it is expected that the performances of STREAM v1.3~~STREAM ~~model, as any hydrological model calibrated against observed data, can decrease over the gauging sections not used for the calibration, the findings obtained above raises doubts about the robustness of model parameters and whether it is actually possible to transfer model parameters from one river section to another with different interbasin characteristics. A more in-depth investigation about the model calibration procedure, with special focus on the regionalization of the model parameters, should be carried out but this topic is beyond the scope of the manuscript~~.

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6.3 External Validation

For the external validation, the monthly runoff time series provided by the GRUN datasets have been compared against the ones computed by the ~~STREAM v1.3~~STREAM model. For that, STREAM daily runoff time series have been aggregated at monthly scale and re-gridded at the same spatial resolution of the GRUN dataset (0.5°). The comparison is illustrated in Figure 6 for the common period 2003–2014. Although the two datasets consider different precipitation inputs, the two models agree in identifying two distinct zones in terms of runoff, i.e., the western dry and the eastern wet area. ~~This two distinct zones~~These two distinct zones can be clearly identified also in the GSWP3 and TMPA 3B42 V7 precipitation maps (see Figure S1) used as input in GRUN and ~~STREAM v1.3~~STREAM, respectively, stressing that STREAM runoff output is correctly driven by the input data. However, likely due to the calibration procedure, the STREAM runoff map appears patchier with respect to GRUN and discontinuities along the sub-basin boundaries (identified in Figure ~~3~~1a) can be noted. This should be ascribed to the automatic calibration procedure of the model that, differently from other calibration techniques (e. g., regionalization procedures), does not consider the basin physical attributes like soil, vegetation, and geological properties that govern spatial dynamics of hydrological processes. This calibration procedure can generate sharp discontinuities even for neighbouring sub-catchments individually calibrated. It leads to discontinuities in model parameter values and consequently in the ~~simulated~~ modelled hydrological variable (runoff).

6.4 Sensitivity analysis results

The results of the VBSA, are illustrated in Figure 7a in terms of main effect indices and in Figure 7b in terms of total effect. Specifically, the figure refers to Vicksburg station but similar results have been obtained for all the 11 gauging stations in the Mississippi basin. By looking at Figure 7, we observe that the model parameters most influencing the model response are β ~~β~~ ~~βετα~~ and m, i.e., the two parameters controlling the *slow-flow* runoff response of the lower soil storage. In particular, the total effect sensitivity index of these two parameters is higher than the main effect sensitivity index. This means that these two parameters have an effect on the model output not only through their individual variations but also through interactions with other parameters. Instead, the other five parameters (α ~~αalpha~~, T, γ~~gamma~~, C, D and C_m) have low main and total effect indices, and consequently, these parameters have a small effect, both direct and through interactions, on model response. Among these, only the α ~~alpha~~ parameter shows a slightly high main and total effect sensitivity indices.

This outcome is very important as it allows to clearly distinguish model parameters which values should be carefully determined when calibrating the model (β ~~β~~ and m~~m~~ and partially α ~~α~~) from the least sensitive (T, γ, C, D and C_m ~~D and Cm~~) which values could be set values within the model parameters' range of variability and then excluded during the calibration phase.

~~10.~~7. DISCUSSION

In the previous sections, the ability of the ~~STREAM v1.3~~STREAM model to ~~accurately simulate~~ estimate river discharge and runoff time series has been presented. In particular, Figures 4, 5 and 6

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demonstrate that satellite observations of precipitation, soil moisture and ~~terrestrial~~ total water storage anomalies can provide accurate daily river discharge estimates for near-natural large basins (absence of upstream dams), and for basins with draining area ~~lower~~ greater than 160'000 km^2 (see ~~section~~ paragraph ~~7~~6.2), i.e., at spatial/temporal resolution ~~lower~~ greater than the ones of the TWSA input data (monthly, 160'000 km^2). This is an important result of the study as it demonstrates, on one hand, that the model structure is appropriate with respect to the data used as input and, on the other hand, the great value of information contained into TWSA data that, even if characterized by limited spatial/temporal resolution, can be used to ~~simulate~~ estimate runoff and river discharge at basin scale. This finding has been also confirmed by a preliminary sensitivity analysis in which the ~~STREAM v1.3~~STREAM model has been run with different hydrological inputs of precipitation, soil moisture and total water storage anomaly (not shown here for brevity). In particular, by running the ~~STREAM v1.3~~STREAM model with different input configurations (e.g., by using TMPA 3B42 V7 or ~~Climate Prediction Center (~~CPC ~~)~~ data for precipitation, ESA CCI or Advanced SCATterometer (ASCAT) data for soil moisture, TWSA or ESA CCI soil moisture data to ~~simulate~~ model the slow-flow river discharge component), we found that STREAM results are more sensitive to soil moisture data rather than to precipitation input. In addition, by running ~~STREAM v1.3~~STREAM model with soil moisture data as input to ~~simulate~~ model the slow-flow river discharge component (i.e. without using TWSA data) we found a deterioration of the model results. This outcome along with the one obtained in the paragraph 6.3, demonstrating the high sensitivity of the model parameters related to *slow-flow* river discharge component, confirm the paramount role of TWSA in estimating river discharge. In this respect, the availability of GRACE data up to July 2016 could represent an issue for the model application beyond that date. However, the GRACE-FO along with the numerous literature studies devoted to fill the GRACE data gap between GRACE and GRACE-FO (see e.g., Landerer et al., 2020 or Yi and Sneeuw, 2021), can provide the needed data to extend the STREAM model application up to present. Further developments in this direction are expected with the ESA's Next Generation Gravity Mission (NGGM), a candidate Mission of Opportunity for ESA–NASA cooperation in the

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frame of the Mass Change and Geosciences International Constellation (MAGIC), that will enable long-term monitoring of the temporal variations of Earth's gravity field at relatively high temporal (down to 3 days) and increased spatial resolutions (up to 100 km). This implies also that time series of GRACE and GRACE-FO can be extended towards a climate series (Massotti et al., 2021).

By looking at technical reviews of large-scale hydrological models (e.g., Sood and Smakhtin, 2015, Kauffeldt et al., 2016), it can be noted there are many established models, similar in objective and limitations to STREAM model, already existing with support and user base (e.g., among others, Community Land Model, CLM, Oleson et al., 2013; European Hydrological Predictions for the Environment, E-HYPE, Lindström et al., 2010; H08, Hanasaki et al., 2008, PCR-GLOBWB, van Beek and Bierkens, 2008; Water – a Global Assessment and Prognosis WaterGAP, Alcamo et al., 2003; ParFlow–CLM, Maxwell et al., 2015; WRF-Hydro, Gochis et al., 2018; Precipitation-Runoff Modeling System, PRMS; Markstrom et al., 2015). Some of them, e.g., ParFlow-CLM, WRF-Hydro or PRMS have been specifically configured across the continental United States and showed good capability to reproduce observed streamflow data over the Mississippi river basin with performances decreased throughout the Great Plains (O'Neill et al., 2020, Tijerina et al., 2021) which is consistent with the results we obtained with the STREAM model. However, with respect to classical hydrological and land surface models, STREAM is based on a new concept for estimating runoff and river discharge which relies on ~~: (a)~~ the almost exclusive use of satellite observations, and, ~~(b)~~ a simplification of the processes being modelled.

This approach brings several advantages: 1) satellite data implicitly consider the human impact on the water cycle observing some processes, such as irrigation application or groundwater withdrawals, that are affected by large uncertainty in classical hydrological models, 2) the satellite technology grows quickly and hence it is expected that the spatial/temporal resolution and accuracy of satellite products will be improved in the near future (e.g., 1 km resolution from new satellite soil moisture products and the next generation gravity mission); the STREAM model is able to fully exploit such

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7.1 Strengths and limitations of STREAM model

Hereinafter, the strengths and the main limitations of the ~~STREAM v1.3~~STREAM model are discussed.

Among the strengths of the ~~STREAM v1.3~~STREAM model it is worth highlighting:

~~1.~~ **Simplicity**. The ~~STREAM v1.3~~STREAM model structure: 1) limits the input data required~~.~~. ~~(o~~Only precipitation, air temperature, soil moisture and TWSA data are needed as input whereas~~;~~ LSM/GHMs require many additional inputs such as wind speed, shortwave and longwave radiation, pressure and relative humidity~~)~~; 2) limits and simplifies the processes to be modelled for runoff and river ~~/~~discharge simulation. Processes like evapotranspiration or~~, infiltration or~~ percolation, are not modelled therefore avoiding the need of using sophisticated and highly parameterized equations (e.g., Penman-Monteith for evapotranspiration, Allen et al.,1998~~, Richard equation for infiltration, Richard, 1931~~); 3) limits the number of parameters (only 8 parameters have to be calibrated) thus simplifying the calibration procedure and potentially reduces the model uncertainties related to the estimation of parameter values.

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In particular, the STREAM model is even simpler than the classical semi-distributed conceptual hydrological models available in literature. As an example, for the comparison we could refer to the Hydrologiska Byråns Vattenbalansavdelning model (HBV, Bergström 1995) or to the Hydrologic Engineering Center – Hydrologic Modeling System (HEC-HMS, Feldman, 2000). HBV model counts

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14 parameters to be calibrated and needs precipitation, air temperature and potential evapotranspiration as input data. Similar input data are required for HEC-HMS which counts 23 parameters. Both the models, uses conceptual equations to estimate the soil losses and to model the soil water storage.

~~2.~~ **Versatility**. The ~~STREAM v1.3~~STREAM model is a versatile model suitable for daily runoff and river discharge estimation over sub-basins characterized by ~~with~~ different physiographic/climatic characteristics (see e.g., ~~,~~the outcomes obtained for the gages 9 and 11 located in the driest and wetter part of the Mississippi basin). This aspect is paramount as it ~~The results obtained in this study clearly~~ gives an insight about ~~indicate~~ the ~~potential~~potential ~~of~~ of ~~this~~ the ~~approach~~ model to be extended at the global scale. Moreover, the model can be easily adapted to ingest input data with spatial/temporal resolution different from the one tested in this study (0.25°/daily). For instance, satellite missions with higher space/time resolution (e.g., GPM Final Run, ASCAT and NGGM-MAGIC) or near-real time products (e.g., GPM Early Run, EUMETSAT H16, GRACE European Gravity Service for Improved Emergency Management, EGSIEM GRACE data Jäggi et al., 2019) ~~, or near real-time satellite products~~ could be considered. ~~As an example, the Next Generation Gravity Mission (Massotti et al., 2021) design studies all encompass double-pair scenarios, which would greatly improve upon the current spatial resolution of single-pair missions like GRACE and GRACE-FO (> 100'000 km²).~~ Additionally, the STREAM model ~~is~~shows, highly flexibility as: 1) it can accommodate application domains comprising single or multiple basins of any size; and 2) the sub-catchment delineation procedure can be easily adapted to introduce intermediate outlets along the river in correspondence of gages with available observed river discharge data, useful for model calibration.~~The STREAM v1.3STREAM model shows high flexibility also in the possibility to modify the subbasin delineation and to introduce additional observational river discharge data to be used for the model calibration.~~

~~3.~~ **Low ~~C~~computational~~ly~~ ~~inexpensive~~cost**. Due to its simplicity and the limited number of parameters to be calibrated, the computational effort for the ~~STREAM v1.3~~STREAM model is very

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However, some limitations have to be acknowledged for the current version of the ~~STREAM v1.3~~STREAM model:

1. ~~1.~~ **Presence of reservoir, diversion, dams or flood plain**. As the ~~STREAM v1.3~~STREAM model does not explicitly consider the presence of discontinuity elements along the river network (e. g, reservoir, dam or floodplain), river discharge estimates obtained for gauging ~~sections~~ stations located downstream of such elements might be inaccurate (see, e.g., ~~river sections~~gauging stations 1 and 2 in Figure 5).

~~2.~~ **Snow modelling**. A potential limitation of the current version of the STREAM model is related to the rain/snow differentiation, based on the degree-day coefficient. A different scheme based e.g., on the wet bulb temperature like in IMERG (Wang et al., 2019; Arabzadeh and Behrangi, 2021), could be investigated in future developments.

~~We have to acknowledge that, even though this rain/snow differentiation method works quite efficiently at a large grid size like the one used in the study (25 x 25 km), the topographic complexity of higher elevations can be lost. A different differentiation scheme based e.g., on the wet bulb temperature like in IMERG (Wang et al., 2019; Arabzadeh and Behrangi, 2021), is another possibility.~~

~~2~~3. **Need of in situ data for model calibration and robustness of model parameters**. As discussed in the results ~~section~~paragraph, the parameter values of the ~~STREAM v1.3~~STREAM model are set through an automatic calibration procedure aimed at minimizing the differences between ~~simulated~~ modelled and observed river discharge. The main drawbacks of this parameterization technique ~~is that the models parameterized with this technique may exhibit~~are~~:~~ ~~(1)~~a poor predictability of state variables and fluxes at locations and periods not considered in the calibration, and ~~(2)~~the presence of sharp discontinuities along sub-basin boundaries in state flux~~,~~ and parameter fields (e.g., Merz and

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Blöschl, 2004). To overcome these issues, several regionalization procedures, as for instance summarized in Cislaghi et al. (2020), could be conveniently applied to transfer model parameters from hydrologically similar catchments to a catchment of interest. In particular, the regionalization of model parameters could allow to,~~: i)~~ firstly, estimate river discharge and runoff time series over ungauged basins overcoming the need of river discharge data recorded from in–situ networks,~~;~~ secondly,~~ii)~~ estimate the model parameter values through a physically consistent approach, linking them to the characteristics of the basins and, thirdly,~~; iii)~~ solve the problem of discontinuities in the model parameters, avoiding to obtain patchy unrealistic runoff maps. As this aspect requires additional investigations and it is beyond the paper purpose, it will not be tackled here.

~~By looking at technical reviews of large-scale hydrological models (e.g., Sood and Smakhtin, 2015, Kauffeldt et al., 2016), it can be noted there are many established models, similar in objective and limitations to STREAM v1.3 model, already existing with support and user base (e.g., among others, Community Land Model, CLM, Oleson et al., 2013; European Hydrological Predictions for the Environment, E-HYPE, Lindström et al., 2010; H08, Hanasaki et al., 2008, PCR-GLOBWB, van Beek and Bierkens, 2008; Water – a Global Assessment and Prognosis WaterGAP, Alcamo et al., 2003; ParFlow–CLM, Maxwell et al., 2015; WRF-Hydro, Gochis et al., 2018; Precipitation-Runoff Modeling System, PRMS; Markstrom et al., 2015). Some of them, e.g., ParFlow-CLM, or WRF-Hydro or PRMS have been specifically configured across the continental United States and showed good capability to reproduce observed streamflow data over the Mississippi river basin with performances decreased throughout the Great Plains (O'Neill et al., 2020, Tijerina et al., 2021) which is consistent with the results we obtained with STREAM v1.3 model. However, with respect to classical hydrological and land surface models, STREAM v1.3 is based on a new concept for estimating runoff and river discharge which relies on: (a) the almost exclusive use of satellite observations, and, (b) a simplification of the processes being modelled.~~

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~~This approach brings several advantages: 1) satellite data implicitly consider the human impact on the water cycle observing some processes, such as irrigation application or groundwater withdrawals, that are affected by large uncertainty in classical hydrological models, 2) the satellite technology grows quickly and hence it is expected that the spatial/temporal resolution and accuracy of satellite products will be improved in the near future (e.g., 1 km resolution from new satellite soil moisture products and the next generation gravity mission); the STREAM v1.3 model is able to fully exploit such improvements; 3) STREAM v1.3 model simulates only the most important processes affecting the generation of runoff, and considers only the most important variables as input (precipitation, surface soil moisture and groundwater storage). In other words, the model does not need to simulate processes, such as evapotranspiration and infiltration and therefore it is an independent modelling approach for simulating runoff and river discharge that can be also exploited for benchmarking and improving classical land surface and hydrological models.~~

~~14.~~8. CONCLUSIONS

This study presents a new conceptual hydrological model, ~~STREAM v1.3~~STREAM, for runoff and river discharge estimation. By using as input satellite data of precipitation, soil moisture and ~~terrestrial~~ total water storage anomalies, the model has been able to provide accurate daily river discharge and runoff estimates at the outlet river section and the inner river sections and over a 0.25°×0.25° spatial grid of the Mississippi river basin. In particular, the model is suitable to reproduce:

1. river discharge time series over the calibrated river section with good performances both in calibration and validation periods;
2. river discharge time series over river sections not used for calibration and not located downstream dams or reservoirs;
3. runoff time series with a quite good agreement with respect to the well-established GRUN observational-based dataset used for comparison.

The integration of observations of soil moisture, precipitation and ~~terrestrial~~ total water storage anomalies is a first alternative method for river discharge and runoff estimation with respect to classical methods based on the use of TWSA-only (suitable for river basins larger than 160’000 km², monthly time scale) or on classical LSMs (Cai et al., 2014).

Moreover, although simple, the model has demonstrated a great potential to be easily applied over sub-basins with different climatic and topographic characteristics, suggesting also the possibility to extend its application to other basins. In particular, the analysis over basins with high human impact, where the knowledge of the hydrological cycle and the river discharge monitoring is very important, deserves special attention. Indeed, as the ~~STREAM v1.3~~STREAM model is directly ingesting observations of soil moisture and ~~terrestrial~~ total water storage data, it allows the modeller to neglect processes that are implicitly accounted for in the input data. Therefore, human-driven processes (e.g., irrigation, land use change), that are typically very difficult to ~~simulate~~ model due to missing information and might have a large impact on the hydrological cycle, hence on ~~total~~ runoff, could be implicitly modelled. The application of the ~~STREAM v1.3~~STREAM model on a larger number of basins with different climatic- physiographic characteristics (e.g., including more arid basins, snow-dominated, lots of topography, heavily managed) along with the results about the sensitivity analysis of the model parameters, -will allow to investigate the possibility to regionalize the model parameters and overcome the limitations of the automatic calibration procedure highlighted in the discussion ~~section~~paragraph.

AUTHOR CONTRIBUTION

S.C. performed the analysis and wrote the manuscript. G.G. collected the data and helped in performing the analysis; C.M, L.B., A.T., N.S., H.H.F., C.M., M.R. and J.B. contributed to the supervision of the work. All authors discussed the results and contributed to the final manuscript.

CODE AVAILABILITY

The STREAM model version 1.3, with a short user manual, is freely downloadable in Zenodo (https://zenodo.org/record/4744984, doi: 10.5281/zenodo.4744984). The ~~STREAM v1.3~~STREAM model code is distributed through M language files, but it could be run with different interpreters of M language, like the GNU Octave (freely downloadable here https://www.gnu.org/software/octave/download).

DATA AVAILABILITY

All data and codes used in the study are freely available online. Air temperature data are available at https://psl.noaa.gov/data/gridded/data.cpc.globaltemp.html (last access 25/11/202). In situ river discharge data have been taken from the Global Runoff Data Center (GRDC, https://www.bafg.de/GRDC/EN/Home/homepage_node.html (last access 25/11/202). Precipitation and soil moisture data are available from http://pmm.nasa.gov/data-access/downloads/trmm and https://esa-soilmoisture-cci.org/, respectively.

COMPETING INTERESTS

The authors declare that they have no conflict of interest.

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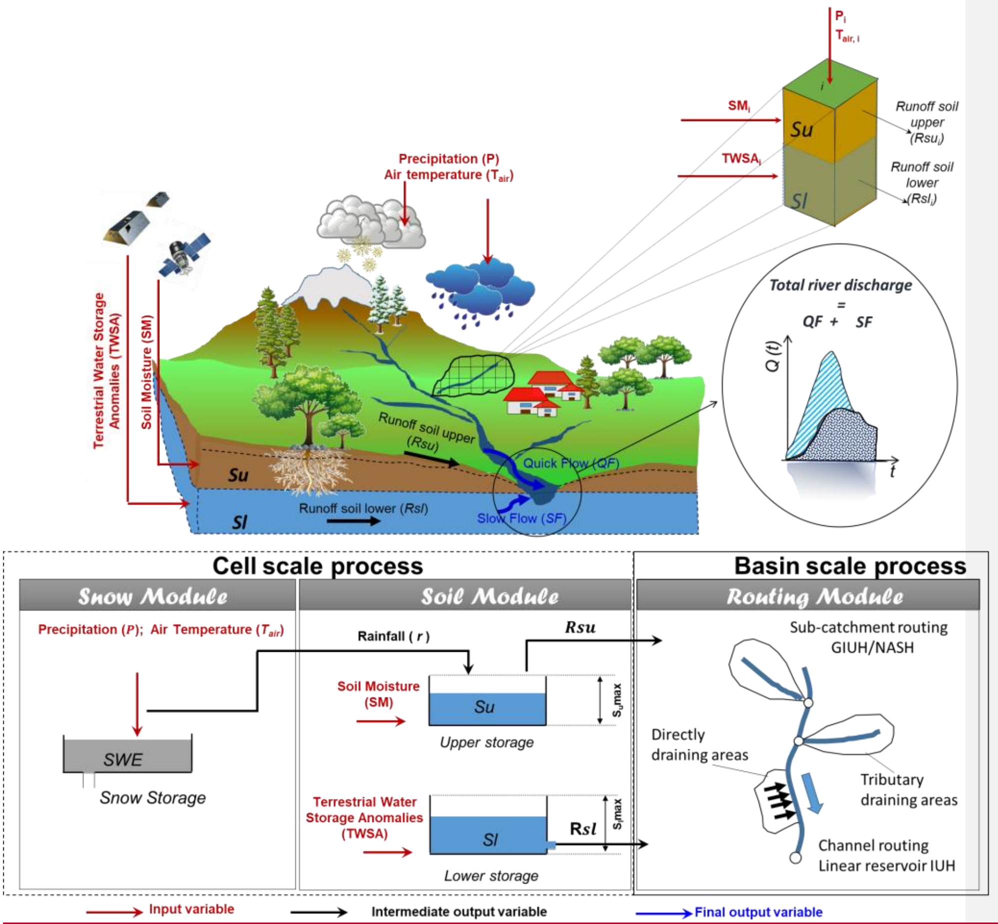
Table 1. Location of river discharge gauging stations over the Mississippi basins and upstream contributing area. Bold text is used to indicate ~~stations~~ gages where the ~~STREAM v1.3~~STREAM model has been calibrated.

#	**River**	**~~Station~~ Gage name**	**Latitude (°)**	**Longitude (°)**	**Upstream area (km^2)**	**Mean annual river discharge (m^3/s)**	**Presence of dam**
1	Missouri	Bismarck, ND	-100.82	46.81	481 232	633	Garrison dam
2	Missouri	Omaha, NE	-95.92	41.26	814 371	914	Gavins Point Dam
3	Missouri	Kansas City, MO	-94.59	39.11	1 229 427	1499	---
4	**Missouri**	**Hermann, MO**	**-91.44**	**38.71**	**1 330 000**	**2326**	---
5	Kansas	Wamego, KS	-96.30	39.20	143 054	141	Kanopolis
6	**Mississippi**	**Keokuk, IA**	**-91.37**	**40.39**	**282 559**	**1948**	---
7	Rock	Near Joslin, IL	-90.18	41.56	23 835	199	---
8	Mississippi	Chester, IL	-89.84	37.90	1 776 221	6018	---
9	**Arkansas**	**Murray Dam Near Little Rock, AR**	**-92.36**	**34.79**	**408 068**	**1249**	---
10	**Mississippi**	**Vicksburg, MS**	**-90.91**	**32.32**	**2 866 590**	**17487**	---
11	**Ohio**	**Metropolis, ILL.**	**-88.74**	**37.15**	**496 134**	**7931**	---

Table 2. Performance scores obtained over the Mississippi river ~~sections~~ gauging stations during the calibration and validation periods.

#	CALIBRATION PERIOD			VALIDATION PERIOD		
SCORE	KGE (-)	rho (-)	$RRMSE$ (%)	KGE (-)	rho (-)	$RRMSE$ (%)
GAUGING STATIONS USED FOR CALIBRATION						
10	0.78	0.78	30	0.71	0.80	40
9	0.79	0.80	66	0.21	0.90	112
6	0.80	0.80	42	0.74	0.81	48
4	0.78	0.78	45	0.73	0.76	49
11	0.80	0.81	45	0.72	0.85	51
GAUGING STATIONS NOT USED FOR CALIBRATION						
1	-3.07	0.09	131	0.43	0.45	93
2	-0.46	0.50	110	0.44	0.54	86
3	0.23	0.73	78	0.42	0.72	69
5	-1.43	0.24	361	-1.23	0.31	355
7	0.55	0.62	72	0.34	0.64	76
8	0.81	0.84	35	0.78	0.83	39



P_i
$T_{air,i}$
SM_i
$TWSA_i$
Su
Sl
Runoff soil upper (Rsu_i)
Runoff soil lower (Rsl_i)
Precipitation (P)
Air temperature (T_{air})
Terrestrial Water Storage Anomalies (TWSA)
Soil Moisture (SM)
Runoff soil upper (Rsu)
Quick Flow (QF)
Runoff soil lower (Rsl)
Slow Flow (SF)
Total river discharge = QF + SF
Q (t)
t
Cell scale process
Basin scale process
Snow Module
Soil Module
Routing Module
Precipitation (P); Air Temperature (T_{air})
SWE
Snow Storage
Rainfall (r)
Rsu
Soil Moisture (SM)
Upper storage
$S_u$max
Terrestrial Water Storage Anomalies (TWSA)
Rsl
$S_l$max
Lower storage
Sub-catchment routing GIUH/NASH
Directly draining areas
Tributary draining areas
Channel routing Linear reservoir IUH
Input variable
Intermediate output variable
Final output variable

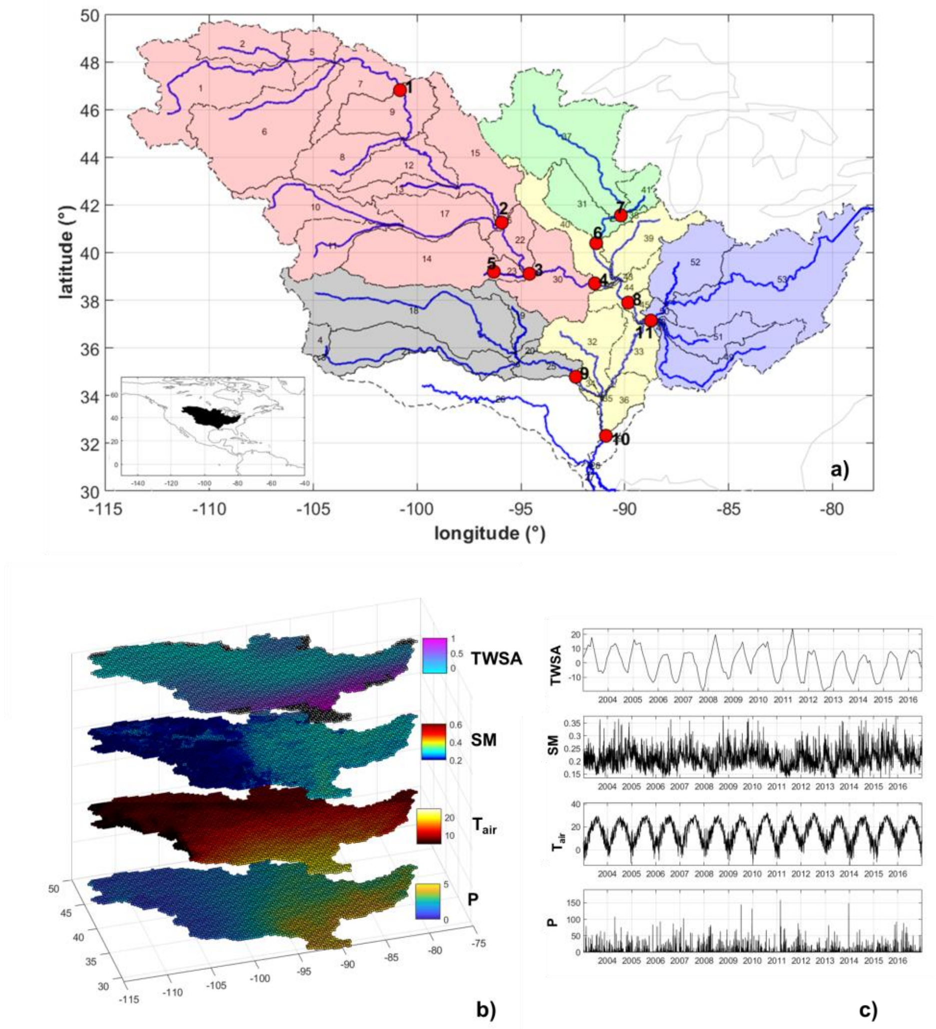
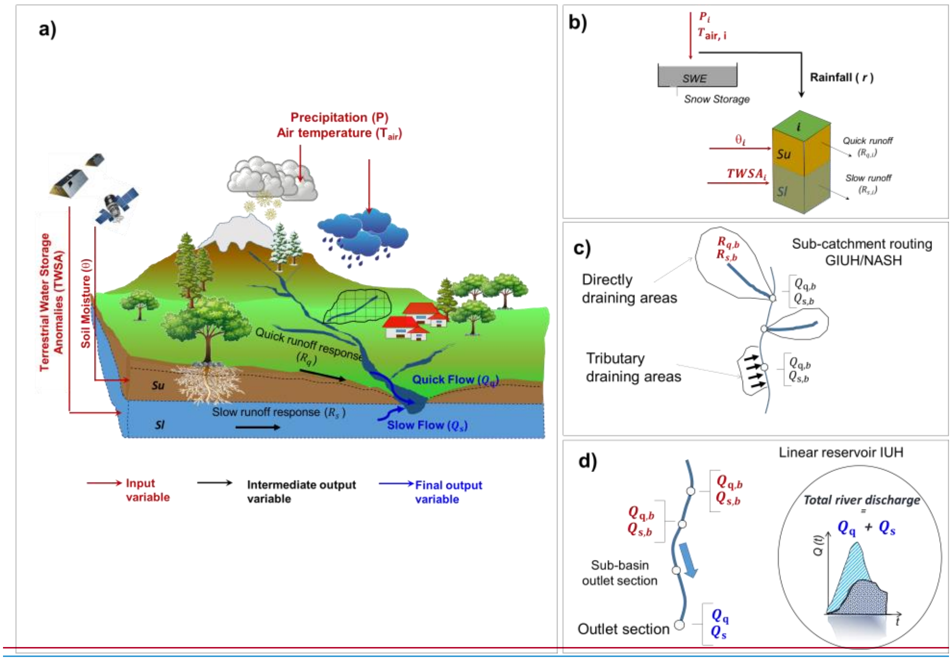


Figure 1. Mississippi river basin. Figure 1a) illustrates the sub-catchments delineation. The black dashed lines and the numbers in the map identify the 53 sub-catchments (tributary and directly draining areas) in the Mississippi basin, blue lines represent the mainstem of each sub-catchment. Red dots indicate the location of the river discharge gauging stations; different colours identify different inner cross-sections (and the related contributing sub- catchments) used for the model calibration. Figure 1b) shows the gridded mean daily values of the input data for the period 2003-2016. Figure 1c) illustrates the input time series over a point located inside the basin.



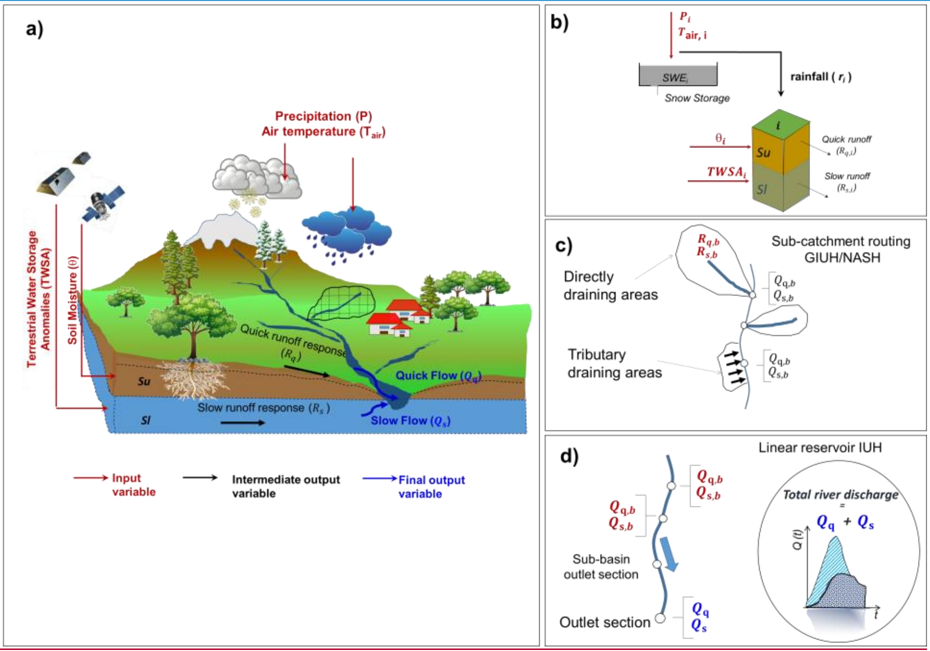


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Figure ~~1~~2. Configuration of the STREAM model adopted for runoff and river discharge estimation. Figure ~~1~~2a) gives an overview of the needed input data and the variables can be obtained as model output. Figure ~~1~~2b) illustrates the runoff generation at cell scale.~~,~~ Figure ~~1~~2c) refers to the sub-catchment river discharge calculation and Figure ~~1~~2d) illustrates the river discharge routing through river networks. Red arrows indicate input variables; black arrows indicate intermediate output variables; blue arrows indicate final output variables. Please refer to text for symbols. ~~Figure 1. Configuration of the STREAM v1.3 model adopted for total runoff estimation. The model includes three modules, the snow module allowing to separate snowfall from precipitation, the soil module that simulates the slow and quick runoff components (*Qsu* and Qfu, respectively) and the routing module for flood simulation. Red arrows indicate input variables; black arrows indicate intermediate output variables; blue arrows indicate final output variables. The components *Qfu* and *Qsu* are computed by using satellite *P*, soil moisture and TWSA data as input to the soil module. Please refer to text for symbols.~~

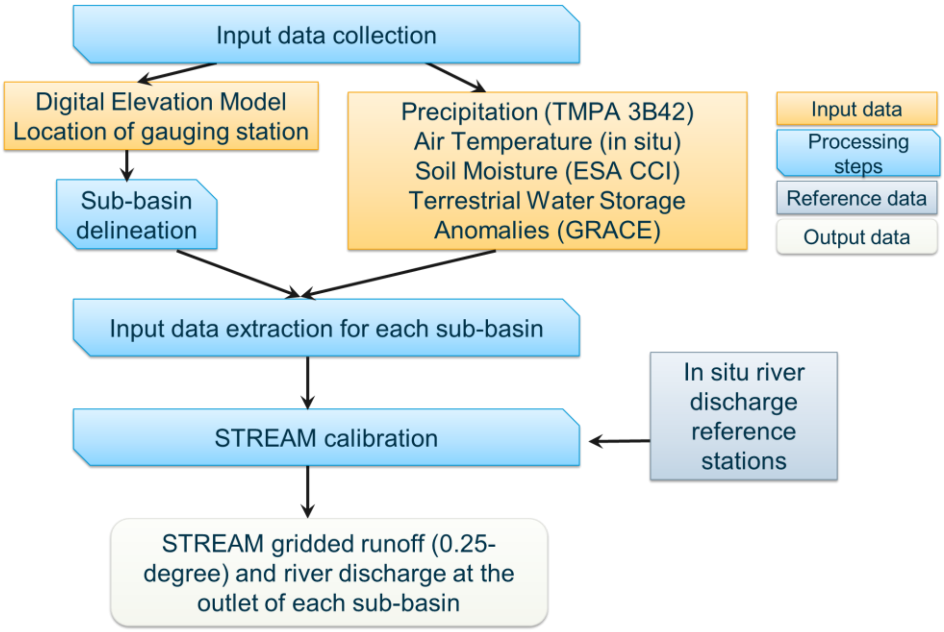

Figure ~~2~~3. Processing steps of the ~~STREAM v1.3~~STREAM model.

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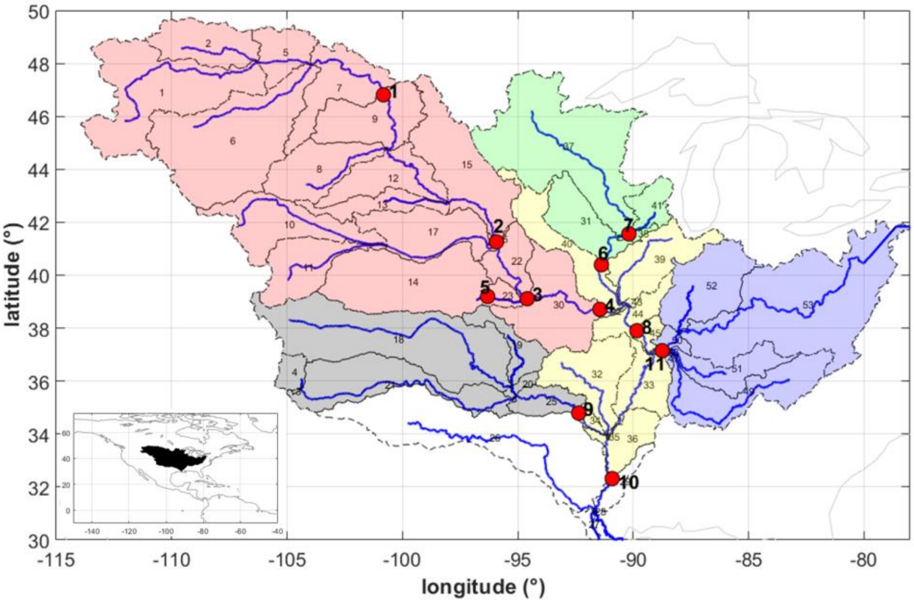
latitude (°)
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50
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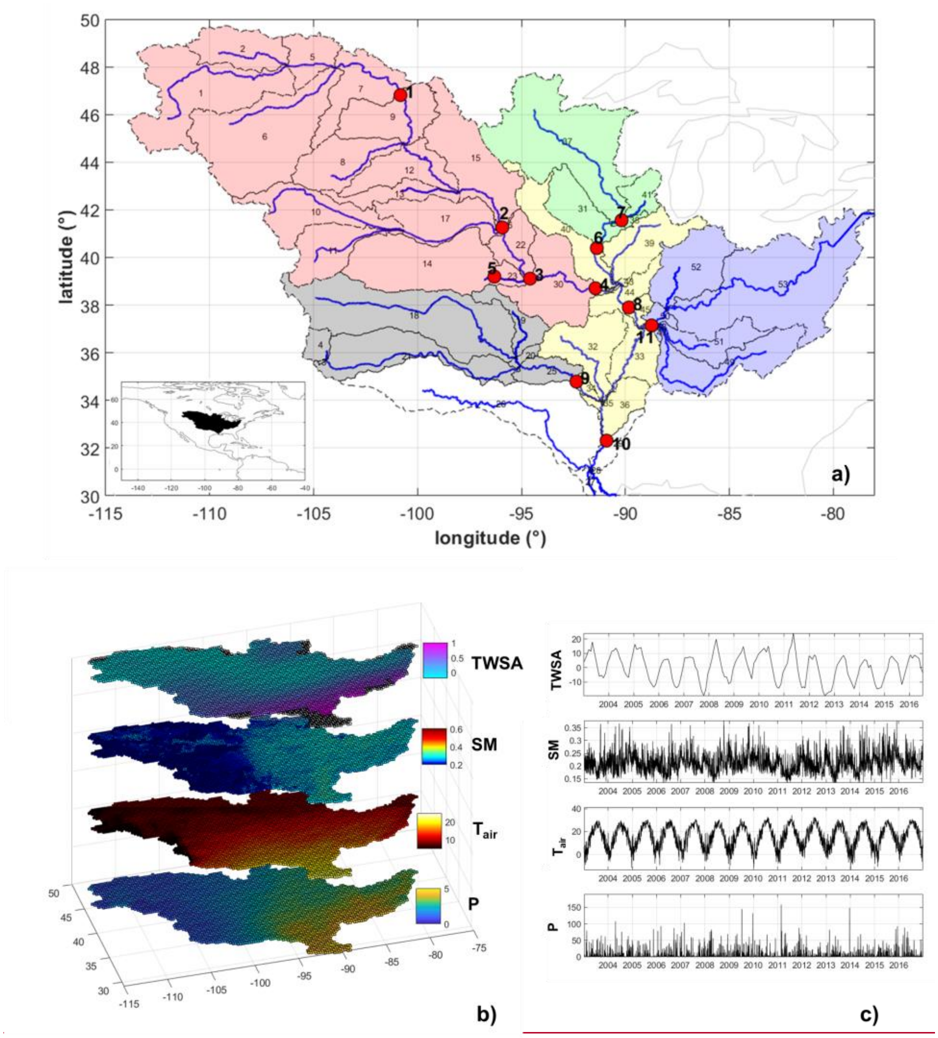

~~Figure 3. Mississippi river basin. a) Sub-catchment sub-basin delineation; gridded mean daily values of the input data for the period 2003-2016 b) and input time series over a point located inside the basin c). Black dashed lines in the plot a) delineate the 53 sub-catchments (tributary and directly draining areas) identified in the Mississippi basin, blue lines represent the mainstem of each sub-catchment. Red dots indicate the location of the river discharge gauging stations; different colours identify different inner cross-sections (and the related contributing sub- catchments basins) used for the model calibration.~~

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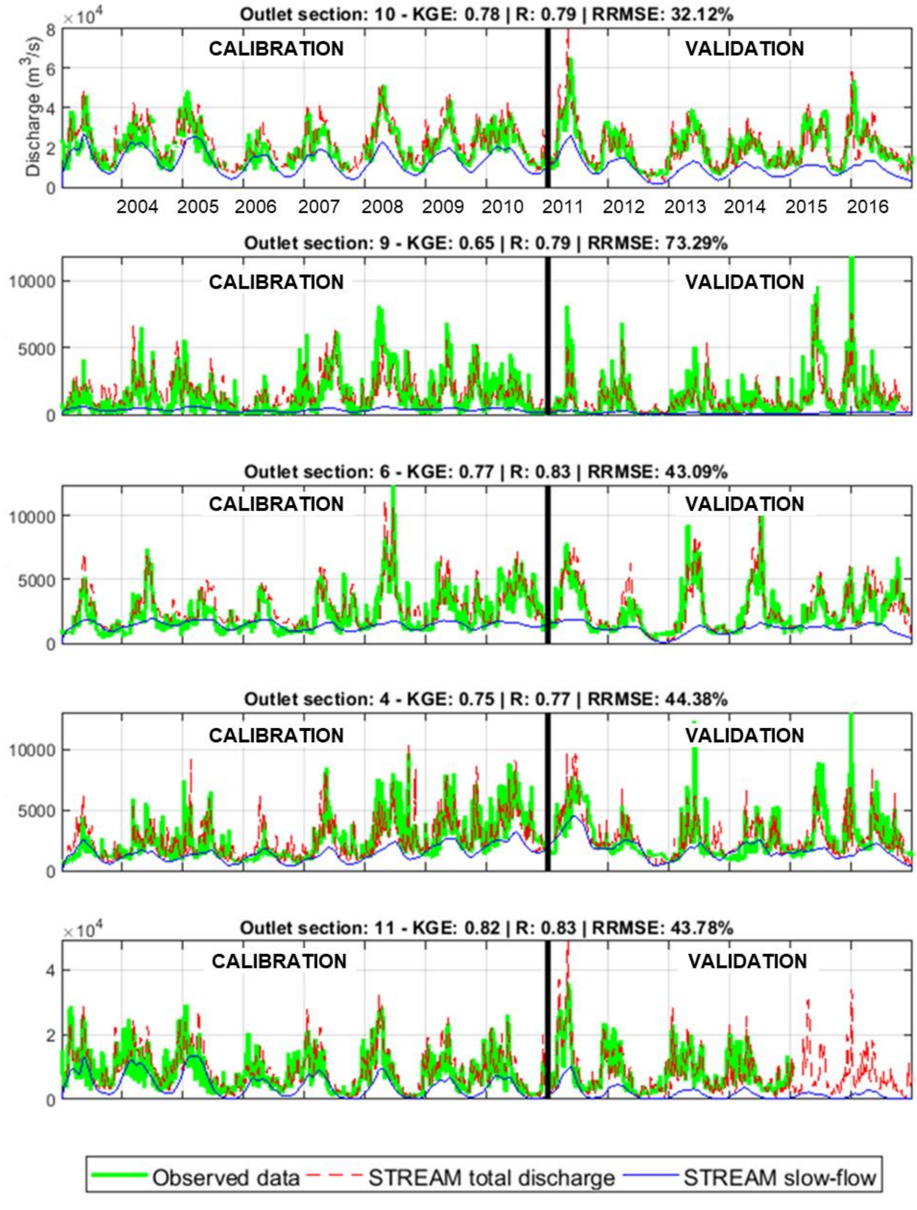
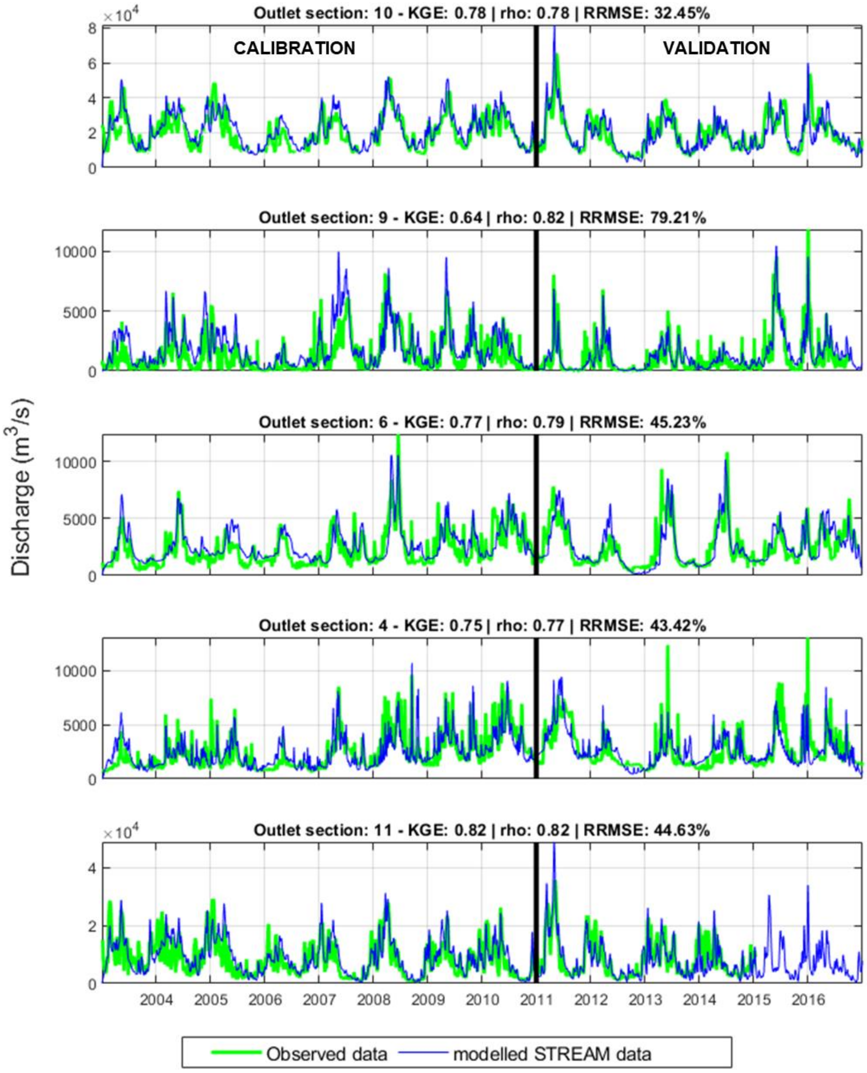
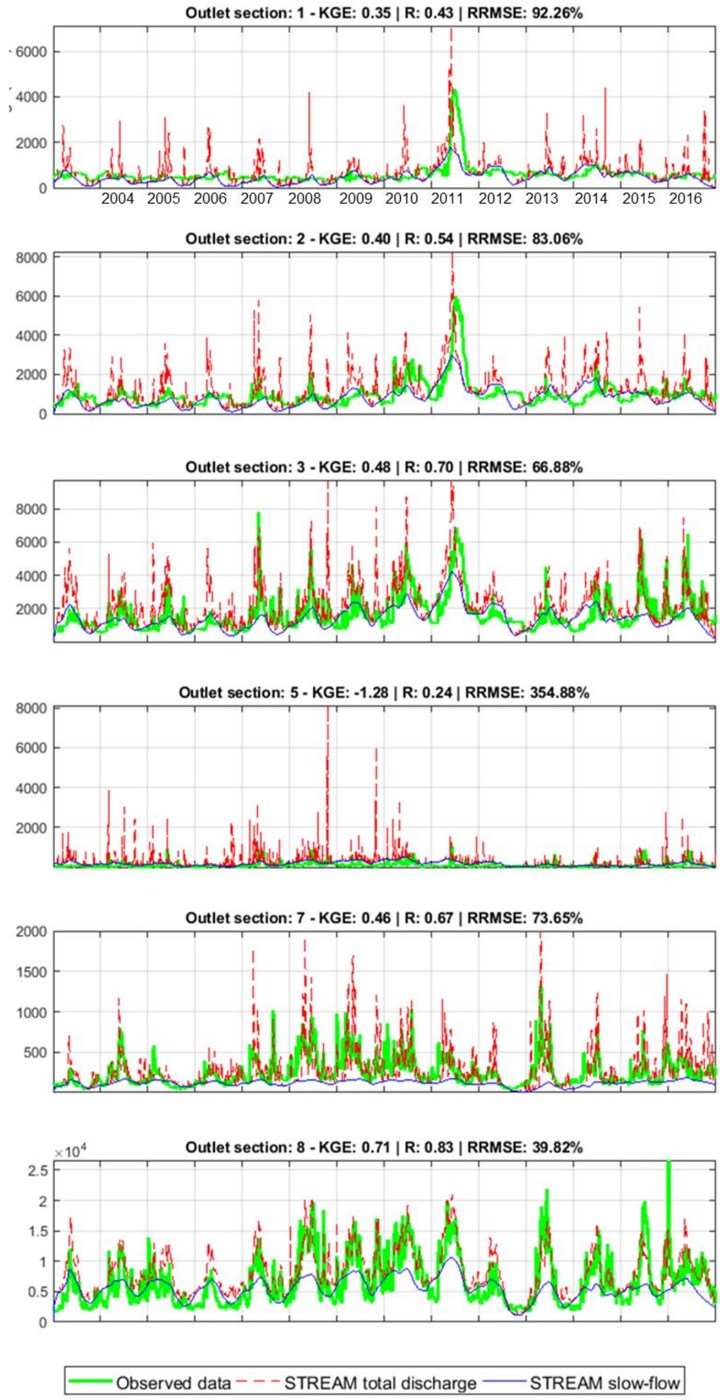


Outlet section: 10 - KGE: 0.78 | R: 0.79 | RRMSE: 32.12%
×10^4
Discharge (m^3/s)
CALIBRATION
VALIDATION
2004 2005 2006 2007 2008 2009 2010 2011 2012 2013 2014 2015 2016
Outlet section: 9 - KGE: 0.65 | R: 0.79 | RRMSE: 73.29%
Outlet section: 6 - KGE: 0.77 | R: 0.83 | RRMSE: 43.09%
Outlet section: 4 - KGE: 0.75 | R: 0.77 | RRMSE: 44.38%
Outlet section: 11 - KGE: 0.82 | R: 0.83 | RRMSE: 43.78%
Observed data
STREAM total discharge
STREAM slow-flow



lischarge time series over the five calibrated sections ~~over~~ in the Mississippi river basin. Performance scores at the top of each plot refer to the entire study period (2003–2016).

1867



Outlet section: 1 - KGE: 0.35 | R: 0.43 | RRMSE: 92.26%
6000
4000
2000
0
2004 2005 2006 2007 2008 2009 2010 2011 2012 2013 2014 2015 2016
Outlet section: 2 - KGE: 0.40 | R: 0.54 | RRMSE: 83.06%
8000
6000
4000
2000
0
Outlet section: 3 - KGE: 0.48 | R: 0.70 | RRMSE: 66.88%
8000
6000
4000
2000
Outlet section: 5 - KGE: -1.28 | R: 0.24 | RRMSE: 354.88%
8000
6000
4000
2000
Outlet section: 7 - KGE: 0.46 | R: 0.67 | RRMSE: 73.65%
2000
1500
1000
500
Outlet section: 8 - KGE: 0.71 | R: 0.83 | RRMSE: 39.82%
$\times 10^4$
2.5
2
1.5
1
0.5
0
Observed data
STREAM total discharge
STREAM slow-flow

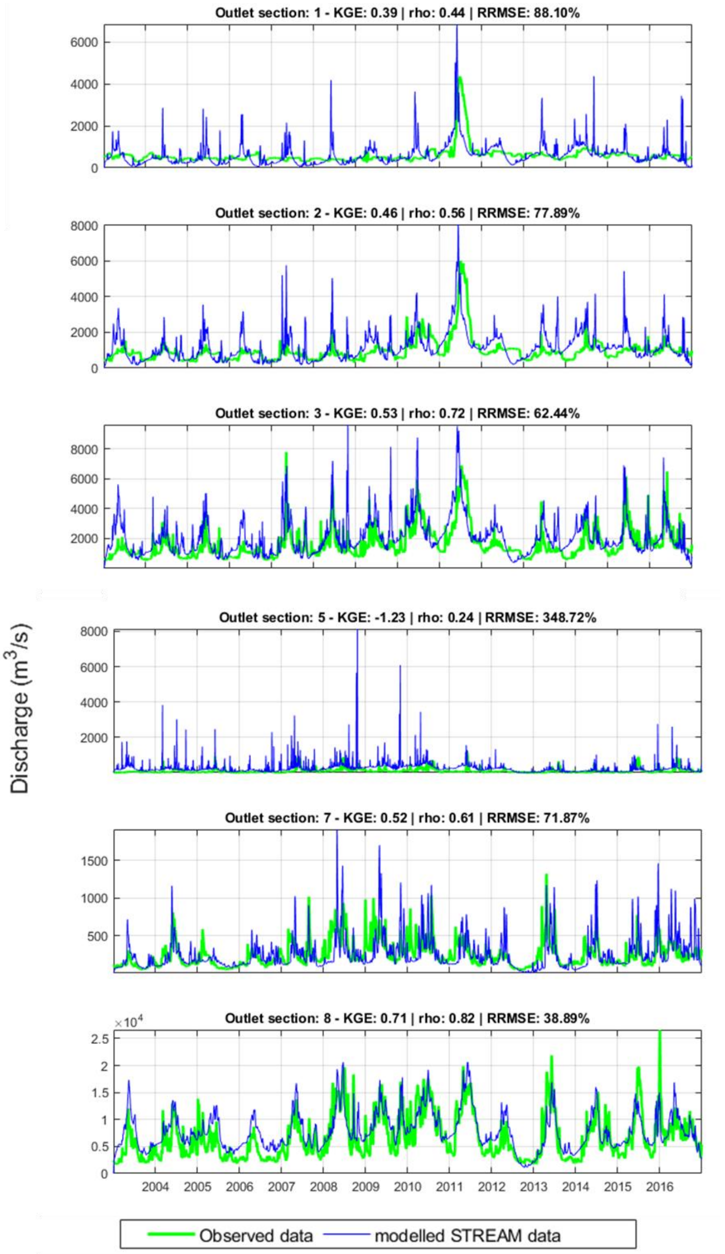


Figure 5. Comparison between observed and ~~simulated~~ modelled river discharge time series over the gauged sections not used in the calibration phase. Performance scores at the top of each plot refer to the entire study period (2003–2016).

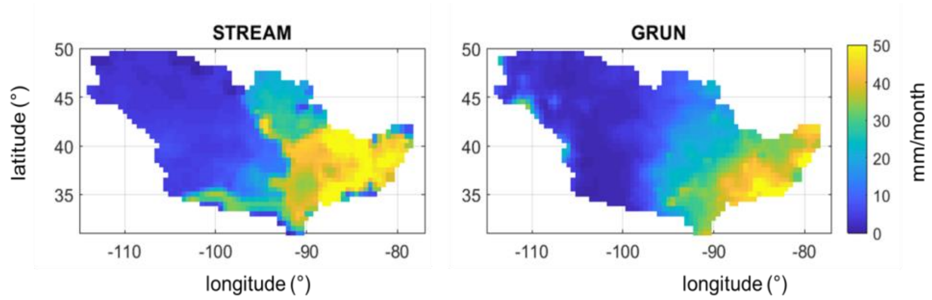


Figure 6. Mississippi river basin: mean monthly runoff for the period 2003–2014 obtained by ~~STREAM v1.3~~STREAM and GRUN models.

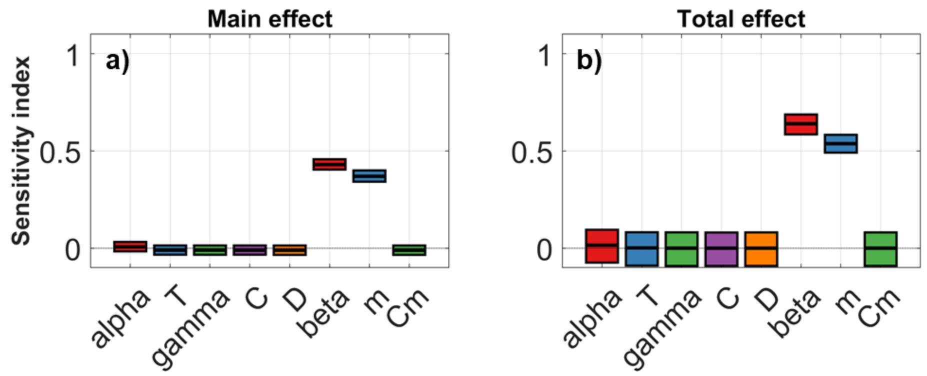


Figure 7. Main effect a) and total effect b) sensitivity indices calculated using the VBSA method for Vicksburg gauging station. The boxes represent the 95% bootstrap confidence intervals and the central black lines indicate the bootstrap mean.

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APPENDIX

Table 1A. Description of ~~STREAM v1.3~~STREAM parameters, belonging module, variability range and unit.

Parameter	**Description**	**Module**	**Range Variability**	**Unit**
Cm	degree-day coefficient	Snow	0.1/24-3	[-]
α	exponent of infiltration	Soil	1-30	[-]
T	characteristic time length	Soil	0.01-80	[days]
β	coefficient relationship *slow-flow* runoff component and TWSA	Soil	0.1-20	[mm h^{-1}]
m	exponent in the relationship between *slow-flow* runoff component and TWSA	Soil	1-15	[-]
γ	parameter of GIUH	Routing	0.5-5.5	[-]
C	Celerity	Routing	1-60	[km h^{-1}]
D	Diffusivity	Routing	1-30	[km^2 h^{-1}]

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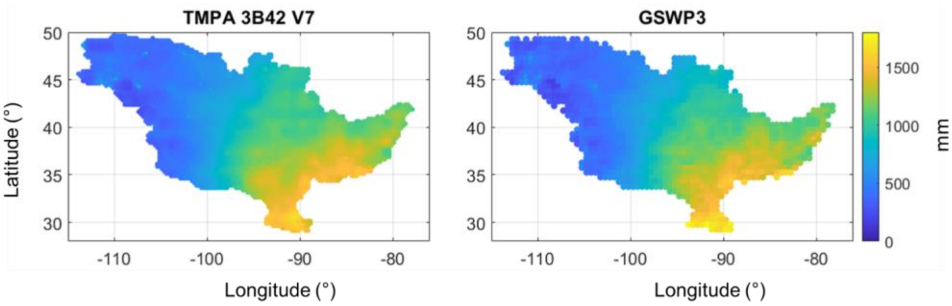

Figure S1. Mean annual precipitation data over the period 2003-2014 obtained by TMPA 3B42 V7 and GSWP3 datasets over the Mississippi river basin.