

Porosity and Permeability Prediction through Forward Stratigraphic Simulations Using GPMTM and PetrelTM: Application in Shallow Marine Depositional Settings.

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Abstract

The forward stratigraphic simulation approach ~~was used~~ is applied to ~~model~~ forecast porosity and permeability ~~attributes~~ trends in the Volve field, ~~Norway. This was achieved by applying spatial data subsurface model. Variograms and synthetic well logs from the forward stratigraphic simulation to control property distribution in the reservoir model.~~ were combined with known data to guide porosity and permeability distribution. Building a reservoir model that fits data at different locations ~~is a task associated~~ comes with high levels of uncertainty. ~~To minimise property representation uncertainties in a reservoir model, geologically realistic sediment distribution patterns must be developed~~ Therefore, it is critical to predict generate an appropriate stratigraphic framework to guide lithofacies ~~units~~ and associated petrophysical ~~properties~~ distribution in a subsurface model. The workflow adopted is in three parts; first, ~~the simulation of twenty scenarios of sediment transportation and deposition using the~~ geological process modeling (GPMTM) software developed by Schlumberger ~~was used to simulate scenarios of sediment transportation and deposition in the model area.~~ Secondly, an estimation of the extent and proportion of lithofacies proportions in the stratigraphic model ~~was done~~ using the property calculator tool in ~~the~~ PetrelTM ~~software~~. Finally, porosity and permeability values were assigned to corresponding lithofacies-associations in the forward stratigraphic model to produce a forward stratigraphic-based ~~petrophysical model~~ porosity and permeability models. Results show a lithofacies distribution ~~that is controlled by model,~~ which depends on sediment diffusion rate, sea level variation, flow rate, wave processes, and tectonic events. This observation is consistent with ~~real-world events, were~~ the natural occurrence, where variation

in sea level, ~~volume of~~ sediment ~~input~~supply, and accommodation control ~~the build-up of~~ stratigraphic ~~sequences~~sequences. Validation wells, VP1 and VP2 located in the original Volve field ~~petrophysical~~ model and the forward stratigraphic-based models show a ~~good match in porosity and permeability attributes at 5 m vertical sample intervals. The resultant forward stratigraphic-based porosity and permeability models suggest~~significant similarity, especially in the porosity models. These results suggest that forward stratigraphic simulation outputs can be ~~integrated into classical~~used together with geostatistical modeling workflows to improve subsurface property representation, ~~and well planning strategies. in reservoir models.~~

Introduction

- The distribution of reservoir properties such as porosity and permeability is a direct function of a complex combination of sedimentary, geochemical, and mechanical processes (Skalinski & Kenter, 2014). The impact of reservoir petrophysics on well planning and ~~extraction~~production strategies makes it imperative to use reservoir modeling techniques that present realistic property variations ~~in~~via 3-D models (Deutsch and Journel, 1999; Caers and Zhang, 2004; Hu & Chugunova, 2008). Typically, reservoir modeling ~~require~~ requires continued property modification until an ~~a~~ appropriate match to ~~known~~ subsurface data ~~is obtained~~. However, ~~acquisition of~~ Meanwhile, subsurface ~~datasets~~data acquisition is ~~costly, expensive~~, thus restricts ~~data~~ collection and accurate subsurface property modeling ~~conditions~~. Several ~~studies~~, ~~e.g.~~ Hodgetts et al. (2004) and Orellana et al. (2014) have demonstrated ~~that~~how stratigraphic patterns, and therefore petrophysical attributes ~~can be extrapolated from~~ in seismic, ~~outcrop data, outcrops~~, and well logs ~~are applicable in subsurface modeling~~. However, ~~this notion is limited by~~ the absence of ~~accurate and reliable~~ detailed 3-Dimensional depositional ~~models~~frameworks to guide property modeling ~~in reservoir units~~ inhibits this strategy (Burgess et al. 2008). Reservoir modeling techniques with the capacity to integrate forward stratigraphic simulation outputs with stochastic modeling techniques for subsurface property modeling will improve reservoir heterogeneity characterization, because they more accurately produce geological realism than the other modeling methods (Singh et al. 2013). The use of geostatistical-based methods to represent ~~the~~ spatial variability of reservoir properties ~~have~~has been ~~widely accepted~~ in many exploration and production projects (~~e.g.~~ Kelkar and Godofredo, 2002). In the geostatistical modeling ~~methods~~method, an alternate numerical 3-D model (~~i.e.~~ realizations) ~~is derived to demonstrate~~shows different ~~scenarios of~~ property distribution scenarios that ~~can be conditioned~~

20—~~are most likely to match~~ well data (Ringrose & Bentley, 2015). ~~Reservoir modeling practioners are normally faced with~~ However, due to cost reservoir modeling practitioners continue to encounter the

21—~~challenge of getting a lot of obtaining adequate~~ subsurface data to deduce reliable ~~variogram models as a result of cost,~~

22—~~variograms for subsurface modeling,~~ therefore introducing a significant level of uncertainty in ~~a~~-reservoir ~~model~~models (Orellena et al. 2014). The

23—~~advantages of applying geostatistical modeling approaches in populating propoertiesto represent reservoir properties in models are discussed~~ in ~~reservoir models is well~~

24—~~established (e.g. studies by~~ Deutsch and Journel, ~~(1999);~~ Dubrule, ~~(1998), but~~). A notable disadvantage is that the geostatistical-~~based~~ modeling method tends to

25—~~confine -reservoir -property -models-distribution to -known-subsurface data -and -rarely -realize-produces geological -realism -to capture~~

26—~~sedimentary events~~ that ~~have~~ led to reservoir formation (Hassanpour et al. 2013). In effect, the geostatistical

27— modeling technique ~~is unable to~~does not reproduce a long-range continuous reservoir properties ~~that,~~
which are essential

28— for generating realistic reservoir connectivity models (Strebelle & Levy, 2008). ~~Based-~~The forward
stratigraphic simulation approach was applied in this contribution to forecast lithofacies, porosity, and
permeability in a reservoir model, based on lessons from a

29— ~~previous work (e.g. Otoo and Hodgetts, (2019), the forward stratigraphic simulation approach was~~
~~applied~~

30— ~~in this contribution to predict lithofacies units, porosity, and permeability properties in a 3-D model. An~~
~~important).~~ A significant aspect of this work is ~~the use of~~using variogram parameters from forward
stratigraphic-based

32— synthetic wells to ~~populate petrophysical properties~~simulate porosity and permeability trends in the
reservoir model ~~grid~~. Forward stratigraphic

33— modeling involves ~~the uses~~ morphodynamic rules to ~~derive sedimentary~~replicate 3-dimensional
stratigraphic depositional trends ~~to reflect~~

34— ~~observed in data (e.g. seismic). Forward~~ stratigraphic ~~patterns in known data. The approach is driven~~
~~by modeling operates on~~ the guiding principle that multiple sedimentary

35— process-based simulations in a 3-D framework will improve facies, and therefore petrophysical
property

36— distribution in a geological model.

37— ~~The geological process modeling GPM™ software (Schlumberger, 2017), which operates on forward~~
stratigraphic simulation principles, replicates a depositional sequence to provide a 3-dimensional
framework to predict porosity, permeability in the study area. The reservoir interval under study is
~~located~~ within the Hugin formation. Studies by Varadi et al. (1998);

38— Kieft et al. (2011), ~~suggest~~ indicate that the Hugin formation ~~consist~~consists of a complex depositional
architecture of waves,

39— tidal, and fluvial processes. This ~~indicates~~knowledge suggests that a single depositional model will not
be adequate to produce

40— a ~~realisit~~realistic lithofacies or petrophysical distributions model of the area. Furthermore, the
complicated Syn-depositional rift-

41— related faulting system, significantly ~~influence~~influences the stratigraphic architecture (Milner and Olsen,
1998).

42— ~~The~~ Therefore, the focus ~~of this work~~here is to produce a depositional sequence ~~in the shallow marine~~
environment by using

43 a forward stratigraphic modeling approach, which captures subsurface attributes observed in the GPM™
(Schlumberger, 2017), seismic and use variogram well data to guide property modeling.

44 parameters from the forward model to control porosity and permeability property representation in
the
45 Volve field model grid.

46 **Study Area**

47 The Volve field (Figure 1), located in Block 15/9 south of the Norwegian North Sea ~~is Jurassic in age~~
48 ~~(i.e. late Bajocian to Oxfordian) with,~~ has the Hugin Formation as the ~~main~~-reservoir ~~unit~~interval from
which
49 hydrocarbons are produced (Vollset and Dore, 1984). The Hugin formation, which is Jurassic in age
(late Bajocian to Oxfordian), is made up of shallow marine
50 to marginal marine sandstone deposits, coals, and a significant influence of wave events that tend to
51 control lithofacies distribution in the formation (Varadi et al. 1998; and Kieft et al. 2011). ~~Several~~
~~studies,~~
52 ~~e.g. Studies by~~ Sneider et al. (1995~~7~~) and Husmo et al. (2003) associate sediment deposition ~~in~~into the
~~Hugin system study area~~ to

a rift-related subsidence and successive flooding during a large transgression of the Viking Graben within the Middle to Late Jurassic period. Also, Cockings et al. (1992), Milner and Olsen (1998) indicate that the Hugin formation comprises of marine shoreface, lagoonal and associated coastal plain, back-stepping delta-plain, and delta front. However, recent studies by Folkestad and Satur (2006) also provide evidence of a high tidal event, which introduces another dimension that requires attention in any subsurface modeling task in the study area. The thickness of the Hugin formation is estimated between 5 m and 200 m, but can be thicker off-structure and non-existent on structurally high segments due to post-depositional erosion (Folkestad and Satur, 2006).

~~the Middle to Late Jurassic period. Previously it was interpreted to comprise of marine shoreface, lagoonal and associated coastal plain, back stepping delta plain and delta front deposits (e.g. Cockings et al. 1992; Milner and Olsen, 1998), but recent studies, e.g. Folkestad and Satur, (2006) suggest the influence of a strong tidal event, which introduces another dimension in property modeling of the reservoir. The thickness of the Hugin formation is estimated to range between 5 m and 200 m but can be thicker off-structure and non-existent on structurally high segments as a result of post-depositional erosion (Folkestad and Satur, 2006).~~

Based on studies by Kieft et al. (2011), a summarised sedimentological delineation within the Hugin formation is presented in derived based on studies by Kieft et al. (2011). In Table -1- Lithofacies, lithofacies-association codes -A, -B, -C, -D, and -E used in the classification represents bay fill units, shoreface sandstone facies, mouth bar units, fluvio-tidal channel fill sediments, and coastal plain facies units, respectively. In addition Additionally, a lithofacies association prefixed code F was interpreted to consist, which consists of open marine shale units, mudstone-with. Within it are occasional siltstone beds, parallel laminated soft sediment deformation that locally develop at bed tops. The lateral extent of the code F lithofacies package in the Hugin formation is estimated to be 1.7 km to 37.6 km, but the total thickness of code F lithofacies is not known (Folkestad & Satur, 2006).

Data and Software

This work is based on the description, and interpretation of petrophysical datasets in the Volve field by Statoil, now Equinor. Datasets include 3-D seismic sections, and a suite of 24 wells that consist of formation pressure data, core data, petrophysical and sedimentological logs. Previous ~~works such as~~ studies by Folkestad & Satur (2006) and Kieft et al. (2011) in this reservoir interval show varying grain size, sorting, sedimentary structures, bounding contacts of sediment matrix ~~that play a significant part of the reservoir petrophysics.~~ Grain size, sediment matrix, and the degree of sorting will typically drive the volume of the void created, and therefore the porosity and permeability attributes. Wireline-log attributes such as gamma-ray (GR), sonic (DT), density (RHOB), and neutron-porosity (NPHI) ~~were used to~~ distinguish lithofacies units, stratigraphic horizons, and zones that are required to build ~~essential for building~~ the 3-D property model. ~~Porosity, and permeability models, of the Volve field,~~

~~were generated~~ in Schlumberger's PetrelTM software. ~~Importantly, Besides,~~ this ~~workstudy~~ also seeks to produce

~~geologically a~~ realistic depositional ~~architecture that is comparable to a real world model like the natural~~ stratigraphic framework

~~in a shallow marine environment. Deriving a representative depositional setting.~~ Therefore, obtaining a

~~D stratigraphic model of the reservoir~~ dimensional stratigraphic model that shows a similar stratigraphic

~~sequence observed in the seismic data allows us to deduce variogram parameters to serve as input in actual~~

~~subsurface property modeling.~~

~~allows us to deduce geometrical and variogram parameters as input datasets in actual subsurface~~ property

~~modeling.~~

~~Schlumberger's Twenty~~ forward stratigraphic simulations were produced in the geological process modeling (GPMTM) software ~~was used to undertake twenty forward~~

~~stratigraphic simulation in an attempt to replicate to illustrate~~ depositional processes that resulted in the build-up of

~~the reservoir interval under study. Simulations were constrained to twenty scenarios because the~~ desired

~~stratigraphic sequence and associated sediment patterns were achieved at~~ By the fourth simulation. ~~The main~~

~~criteria for evaluating the realistic nature, there was a development of a stratigraphic model was to~~ compare it to patterns that shows similar sequences as those observed in seismic, hence the depositional

~~sequence observed in the seismic section in Figure 3b. Several process modeling software packages exist~~

~~and have been applied in similar studies; e.g. decision to constrain the simulation to twenty scenarios.~~ Delft3D-FlowTM; Rijn & Walstra, (2003); DIONISOSTM;

~~Burges et al. (2008). The geological) are examples of subsurface process modeling (GPMTM) software~~ was preferred because of the

~~used in similar studies. The~~ availability of the GPMTM software license, and also the ease in integrating of its capacity to integrate stratigraphic simulation outputs into the property modeling

~~workflow in PetrelTM is the reason for using the geological process modeling software in this study.~~

Methodology

The workflow (Figure 2a) combines the stratigraphic simulation capacity of the GPMTM software in different ~~depositional settings, sedimentary processes~~ and the property modeling tools in PetrelTM to predict the distribution of porosity and permeability properties away from ~~wellknown~~ data. ~~Three~~ This involves three broad ~~steps have been used here to~~ achieve this goal: (i) forward stratigraphic simulation ~~(FSS)~~ in GPMTM ~~software~~ (2019.1 version), (ii) lithofacies ~~classification using the calculator tool in PetrelTM, and~~ (iii) ~~lithofacies,~~ porosity, and permeability modeling in PetrelTM (2019.1 version).

~~Process Modeling~~ Forward Stratigraphic Simulation in GPMTM

The GPMTM software ~~consist~~ consists of different geological processes ~~that are designed~~ to replicate sediment deposition in clastic and carbonate environments. ~~For example, previous studies, e.g.~~ Kieft et al., (2011)

in their work in this area, identified the influence of riverine (fluvial), and wave processes in the genetic structure of sediments in

the Hugin formation. These geological processes could be very rapid, depending on accommodation generated as a result of by sea-level variation, and or sediment composition and flow intensity.

The deposition of sediments into a geological basin and its response to post-depositional sedimentary and tectonic processes are significant in the

ultimate distribution of subsurface lithofacies units. To attain stratigraphic outputs that fall within the depositional architecture captured in the seismic section (Figure 3b), the and petrophysics. Therefore, different input parameters were varied as

illustrated by different scenarios in Table 2. The for the forward simulation generated geologically realistic stratigraphic

trends, but to attain a stratigraphic output that fits existing knowledge of paleo-sediment transportation and deposition into the study area (see Table 2). The forward simulation at all stages portrayed geological realism concerning stratigraphic sequence, but it also revealed some limitations, such as instability in the simulator when more than three

geological processes and sub-operations run at a time. In view of concurrently. Given this, the diffusion and tectonic processes

were combined with other processes such as remained constant, whiles varying the steady flow, unsteady flow, and sediment accumulation to processes at each run.

replicate the Volve field stratigraphic depositional scenarios.

Steady & Unsteady Flow Process

The steady flow process in GPM simulates flows that changes slowly over a period, or sediment transport

scenarios where flow velocity and channel depth do not vary abruptly; e.g., rivers at a normal stage, deltas,

and sea currents. The steady flow process can be specified to the desired setting in the “run sedimentary

simulation” dialog box in the Petrel™ software (version 2017.1 and above). Considering the influence of

fluvial activities during sedimentation in the build-up of the Hugin formation, it was important is significant to capture its impact on the

resultant simulated output. To attain stability in the simulator, it is advisable to undertake preliminary

122 runs to ascertain the appropriateness of input parameters that will be used in the simulation. For steady

123 flow process, a boundary condition ~~must be~~ specified at the edges of the model. structure to guide sediment and fluid movement in the model. For example ~~in~~, where the boundary condition is an open

124 flow system, negative integers (~~i.e.~~ values below zero) must be assigned to the edges of the hypothetical

125 paleo-surface to allow water to enter and leave the ~~simulation area~~. of interest.

126 Unsteady Flow Process

127 The unsteady flow process can ~~model flows that are simulate~~ periodic, flows and run for a limited time; for example, in

128 turbidites where the velocity of flow and depth changes abruptly over time. The unsteady flow process

129 algorithm ~~is set up to apply a number of~~ applies several fluid elements, ~~that are affected~~ driven by gravity, and ~~by~~ friction against

the hypothetical topographic surface. A contribution on the application of the unsteady in stratigraphic simulation, and how its settings can be configured to attain geological realistic outcomes is discussed in In Otoo and Hodgetts, (2019), is an account of how the unsteady process in GPM™ attains realistic distribution of lithofacies units in a turbidite fan system. The steady and unsteady flow processes are based on simplified Navier-Stokes equations to represent flows in channels and pathways that have irregular cross-sections and or channels that converge as tributaries or diverge as distributaries such as turbidite flow. The simplified Navier-Stokes comprises of two key parameters that partly rely on channel geometry and flow velocity. The Navier-Stokes equation combines the continuity equation (2) and the momentum equation (3) to generate the equation on which the steady and unsteady flow processes evolve.

The continuity equation integrates the conservation of mass:

$$\frac{\partial \rho}{\partial t} + \nabla \cdot \rho \mathbf{q} = 0 \quad (1)$$

Where ρ is fluid density, t is time, and \mathbf{q} the flow velocity vector.

The equation that shows the changes in momentum by the fluid:

$$\rho \left(\frac{\partial \mathbf{q}}{\partial t} + (\mathbf{q} \cdot \nabla) \mathbf{q} \right) = -\nabla P + \nabla \cdot \mu \mathbf{U} + \rho(\mathbf{g} + \Omega \mathbf{q}) \quad (2)$$

Where P is pressure, t is time, μ is fluid viscosity, and \mathbf{U} is the Navier Stokes tensor.

Keeping density (ρ) and viscosity (μ) as constant, a simple flow equation is obtained:

$$\frac{\partial \mathbf{q}}{\partial t} + (\mathbf{q} \cdot \nabla) \mathbf{q} = -\nabla \Phi + \nu \nabla^2 \mathbf{q} + \mathbf{g} \quad (3)$$

Where, Φ is the ratio of pressure to constant density (i.e. P/ρ), and ν is the kinematic viscosity (i.e. μ/ρ)

The solution of the framework formed in (3) is completely obtained by specifying various boundary conditions that are used in the steady and or unsteady flow processes.

A full description of equations that form the building block for sediment movement under steady and unsteady flow processes in the simulator is available in Tetzlaff & Harbaugh (1989).

133 **Sediment Diffusion Process**

134 The diffusion process can effectively replicate sediment ~~erosion~~movement from ~~areas of a~~ higher slope
(~~i.e.~~ source
135 location) and ~~their~~its deposition ~~to into a~~ lower elevation of the model area. Sediment
~~dispersion~~movement in the diffusion
136 process is ~~carried out~~ through erosion and transportation processes that are driven by gravity ~~in the~~
137 ~~simulator. The~~ Sediment diffusion ~~process is based~~runs on the assumption that sediments are
transported downslope at
138 a proportional rate to the topographic gradient; ~~therefore~~, making fine-grained sediments
easily
139 transportable than coarse-grained sediments. ~~Diffusion is controlled by two~~ Sediment diffusion
depends on three parameters; (i) ~~diffusion~~
140 ~~coefficient, which controls the strength of the diffusion, and~~ sediment grain size and turbulence in the
flow (ii) diffusion coefficient, and (iii) diffusion curve that serves as a unitless
141 multiplier in the algorithm. ~~The governing equation for the~~ Based on Dade & Friend (1998); and Zhong
(2011), a mathematical summary of the influence these factors have on the resultant ~~diffusion~~ process is profile is
derived. Considering that the grain size for each sediment component (coarse sand, fine sand, silt, and clay) are
known, the assumption is that these particles have a uniform diameter (D) in the flow mix. In that case, external
fore (F_e), which consist of drag, lift, virtual mass, and Basset history force is given as:

142
$$\frac{\partial z}{\partial t} = -k \nabla^2 z, F_e = \alpha_e M_e + \alpha_e \Phi_D \frac{U_{fi} - U_{ei}}{T_p} \quad (4)$$

M_e is the resultant force of other forces with the exception of drag force, T_p stokes relation time,
expressed as: T_p = ρ_fD²/(18ρ_fV_f), with ρ_f and V_f as density and viscosity of fluid respectively. Φ_D is a
coefficient that accounts for the non-linear dependence of drag force on grain slip Reynolds number
(R_p).

$$\Phi_D = \frac{R_p}{24} C_D \quad (5), \text{ with } C_D \text{ sediment grain coefficient.}$$

With Einstein equation. Using an assumption that the diffusion coefficient decreases with increasing grain size the ent and rise in temperature, and that the coefficient f is known, the expression for D_i is:

flow $(D_i$
com) is

$$D_i = \frac{K_B.T}{f} \text{ (6)}$$

pone de Meanwhile, f is a function of the dimension of the spherical particle involved at a particular time (t). In nt in du accounting for f, the equation for D_i changes into:

plac ce
e, d

$$D_i = \frac{K_B.T}{6.\pi.\eta_0.r} \text{ (7)}$$

the fro The rate diffusion of diffusion relative to topography in the simulator is achieved through;

diffu m
sion the

$$\frac{\partial z}{\partial t} = D_i \nabla^2 z \text{ (8)}$$

coeff Ei where z is topographic elevation, k the diffusion coefficient, t for time, and $\nabla^2 z$ is the
143 _laplacian.

144 **Sediment Accumulation**

145 In the GPM™-software, sediment source can be set to a point location or considered to emanate from a
146 _whole area. Sediment accumulation ~~deals with~~represents sediment deposition ~~via~~through an areal
source. For example,

147 _where a lithology is ~~interpreted to be uniformly distributed~~distribution is invariable, the sediment
accumulation process can be

148 ~~used to~~replicate such a depositional scenario. The areal input rates for each sediment type (~~e.g.~~ coarse
149 _grained, fine grained sediments) ~~used in the accumulation process must be specified in the settings.~~

150 ~~Specifying the areal rates for each sediment is important because the software is configured to use~~
the

151 _value of the surface at each cell in the model grid and ~~multiplies~~multiply it by -a value (~~i.e. value~~ from a
unitless

152 _curve) at each time step in the simulation to estimate the thickness of sediments accumulated or eroded

153 _from a cell in the model. Based on Tetzlaff & Harbaugh (1989), the equation for estimating sediment accumulation is given:

$$\frac{d(H-Z)}{dt} = f(Q, \nabla H, \nabla Z, L, F, K_s, k(Z)) \quad (9)$$

Where:

H is the free surface elevation to sea level, Z is the topographic elevation for sea level, K_s is the sediment type, l_{ks} is the volumetric sediment concentration of a specific type (k), L is the vector that defines sediment concentration of each type, F is the matrix of coefficients that define each sediment type, and t is the time.

Sediment accumulation relies on (i) basin geometry and tectonics (Bajpai et al. 2001) (ii) erosion and volume of sediment transported (Cheng, et al. 2018), (iii) prevailing accommodation.

Based on Cheng et al. (2018), sediment accumulation over a period (A_r) is:

$$A_r = V_{er} - V_{es} \quad (10)$$

V_{es} is the total volume of sediments that may escapes from the basin. V_{er} is the total volume of sediments eroded into the basin. $V_{er} = A_{er} \times R_{er} \times t$; where A_{er} is the average erosion area, R_{er} is the average erosion rate, and t, time.

Because source position for the sediment accumulation process is areal, the volume of sediments accumulated in a specific layer (k) in the basin; excluding porosity, is expressed as:

$$A_r = \sum_{k=1}^n A_{rk} \quad (11)$$

Taking into account the impact of porosity (ϕ) in this process, the equation for the sediment accumulation is:

$$A_r = \sum_{k=1}^n [(1 - \phi_0 * e^{-c*Z_k}) \times V_{observed_k}] \quad (12)$$

Where; $V_{observedk}$ is the volume of sediment and porosity observed in a specific layer (k), ϕ_0 is the surface porosity, c is the porosity-depth coefficient (after Sclater & Christie, 1980), and Z_k is the average depth of the layer k.

154 Boundary Conditions for Forward Stratigraphic Simulation

155 ~~A realistic~~Realistic reproduction of stratigraphic patterns in the ~~study model~~ area ~~will require~~requires input parameters ~~or~~(initial
156 ~~_conditions_)~~, such ~~-as:-~~hypothetical paleo-topography, ~~-sea-level -curves, -sediment -source -location,~~

and

157 — distribution curve, tectonic event maps (~~i.e.~~ subsidence and uplift), and sediment mix velocity. The
158 — application of these input parameters in GPMTM, and their ~~influence~~ impact on the resultant
stratigraphic
159 — framework ~~are discussed~~ is below.

160 — **Hypothetical Paleo-Surface:** The hypothetical paleo-topographic ~~surface, on which~~ for the stratigraphic
simulation ~~evolves was~~
161 — ~~inferred~~ is from the seismic ~~section. This is done with~~ data (Figure 3), using the assumption that the present day
stratigraphic surface (~~i.e.~~
162 — paleo shoreline in Figure ~~3a~~ 4a) occurred as a result of basin filling ~~through different~~ over geological ~~periods~~ time.
Since the
163 — ~~hypothetical topography generated~~ surface obtained from the seismic section have undergone various phases of
subsidence and
164 — uplifts, ~~it is significant to note that~~ the paleo topographic surface used in this work does not ~~present~~ represent an
accurate description of the basin at the
165 — period of sediment deposition. ~~To obtain~~ ; thus ~~presenting another level of uncertainty in the simulation. To~~
derive an appropriate paleo-topographic for this task, ~~five~~ paleo
166 — topographic surfaces (TPr) were generated, by adding or subtracting elevations from the inferred paleo
topographic surface (see Figure 4g) using the equation:

$$\text{TPr} = \text{Sbs} + \text{EM}, \text{---} (13)$$

167 — where, Sbs is the base surface
168 — scenario (in this instance, scenario 6), and -EM an elevation below -and above the base -surface. ~~Paleo-~~
169 — ~~The~~ paleo-topographic surface in scenario 3 (figure 4d) ~~was~~ is selected, because it ~~controlled the~~
~~development of~~
170 — ~~produced a~~ stratigraphic sequences that fit the ~~conceptual knowledge of~~ depositional ~~framework as~~
~~observed in~~ patterns interpreted from the
171 — seismic section (Figure 5d).

172 — **Sediment Source Location:** Based on regional well correlations in ~~previous studies (e.g.~~ Kieft et al.

173 — 2011), and seismic interpretation of the basin structure, the sediment entry point ~~was~~is placed in the
north-
174 — eastern section of the hypothetical paleo-topography. ~~Since the~~ surface. The exact sediment entry point ~~is~~
~~not known,~~
175 — ~~multiple~~into this basin is unknown, so three entry points were placed at a 4 km radius around the primary
location ~~in~~ (Figure 3c), ~~in order~~ to
176 — capture possible sediment source locations. in the model area. The source position is ~~characterised by a~~
positive ~~integers (i.e.~~
177 integer (values greater than zero) to enable ~~fluid flow~~sediment movement to other parts of the
~~simulation~~topographic surface.

178 **Sea Level:** ~~Sea-~~The sea-level ~~variation was inferred~~ curve is deduced from -published studies and facies
description in -shallow

179 -marine depositional environments (e.g. Winterer and Bosellini, 1981). To ~~attain stability in the simulator,~~

180 ~~we assumed a~~ sea level ~~that range between 15 m to 45 m; averaging was constrained~~ 30 m for short
simulation ~~-runs, e.g.~~

181 ~~(5000 to 20000 years. The sea level was -), but~~ varied with the increasing duration of the simulation (~~illustrated~~
~~in~~

182 ~~see~~ Table 2). The peak sea-level in the simulation ~~represents~~depicts the maximum flooding surface (Figure 5d),
and

183 ~~therefore the inferred sequence boundary in the geological process model.~~

184 **Diffusion and Tectonic Event Rates:** The sediment mix proportion, diffusion rate, and tectonic event
185 functions ~~were inferred~~are from ~~previous~~ studies ~~(e.g. such as~~ Walter, (1978;), Winterer and Bosellini,
(1981), and

186 Burges et al., (2008). The diffusion and tectonic event rates ~~are were~~ increased or reduced to produce a
187 stratigraphic model that fit our knowledge of ~~the~~ basin evolution. ~~A key criteria for selecting parameters~~
188 ~~is their capacity to produce stratigraphic outputs that depict depositional scenarios~~ in the study area.
For

189 ~~example, in scenario 1 (Figure 6a), the early stages of clinoform development show resemblance to~~
190 ~~interpreted trends in the seismic section (Figure 3b). As a result, input figures that were higher and~~
~~lesser~~

191 ~~than those used in generating scenario 1 were generated to serve as the simulation parameters for~~
~~the~~

192 ~~twenty scenarios. In scenario 1, The process commenced with~~ a diffusion coefficient of 8 m²/a ~~was used~~
~~to produce a realistic clinoform~~

193 ~~build up, so the figure was, but it~~ varied ~~with +/- 5~~ at each scenario to obtain ~~figures that could~~ diffusion
coefficients to improve the model ~~derived in~~

194 ~~scenario 1. The, Excluding the~~ initial topography (TP,) ~~was kept constant throughout a simulation,~~
~~but~~ Figure 4d), input parameters in geological processes such as wave events,

195 ~~steady/unsteady flow, diffusion, and tectonic events~~ used curve functions to provide variations ~~within in~~
the simulation.

196 simulation. A sudden change in subsidence rate tends to constrain coarse to medium sediments
at

197 proximal distance to source location than in scenarios where the rate of subsidence was made gradual.

198 The ~~influence~~sensitivity of input parameters in the forward stratigraphic simulation is evident
~~whenever~~notable when there is a ~~slight~~ change of value

199 in sediment diffusion, and tectonic ~~rates or dimension~~ of the ~~hypothetical topographic surfaces.~~
topography. For

200 example, a change in sediment source position ~~has a strong impact on~~affects the extent and depth ~~to~~
~~which~~of sediments ~~are~~

201 ~~deposited~~deposition in the ~~basin~~simulation. Shifting the source point to the mid-section of the
topography (~~i.e.~~ the mid-point

202 of the topography in a basin-ward direction) resulted in the accumulation of distal elements ~~that are~~

203 identical to turbidite lobe systems. This output is consistent with morphodynamic experiments by de
Leeuw et

204 al., (2016), where sediment discharge from the basin slope leads to the build-up of basin floor fan units.

205 Property Classification in Stratigraphic Model

206 In our opinion, the most appropriate ~~model in this work~~output is the stratigraphic model in Figure 5d. This
207 point of view is because, ~~when~~-compared to
208 the depositional description in studies such as Folkestad and Satur (2006); ~~kieft~~Kieft et al., (2011), ~~it~~
209 produced and the seismic interpretation presents a
210 similar stratigraphic sequence ~~that mimics the depositional sequence in the study area. The stratigraphic~~
211 ~~model~~
212 ~~was converted into a 3-D format, 20 m x 20 m x 2 m grid cells in order to be used in the property modeling~~
213 ~~tool in Petrel™. Lithofacies, porosity, and permeability properties are characterized in the stratigraphic~~
214 ~~using a rule based approach (Table 3).~~ Sediment distribution in each time step of the simulation ~~were~~
215 was stacked into a single zone framework to attain a simplified model. This ~~was done with the assumption~~
216 strategy assumes that sedimentary processes that lead to the final build-up of genetic related units within zones
217 of the model
218 will not vary significantly over the simulation period. ~~Property classification in the model was achieved~~The
219 stratigraphic model (Figure 5d) was converted into a 3-D format (20 m x 20 m x 2 m grid cells) for the property
220 modeling in Petrel™.
221 ~~with Facies, porosity, and permeability representation in the property calculator tool~~stratigraphic model was
222 done via a rule based approach in Petrel™. (see Table 3). The classification ~~was~~is driven by depositional depth,
223 geologic
224 flow velocity, and sediment distribution patterns as indicated in **Figure 7**. Lithofacies representation in
225 the stratigraphic model ~~was based~~relied on the sediment grain size pattern, and proximity to sediment source.
226 For example, shoreface lithofacies units ~~were characterized using~~are medium-to-coarse grained sediments,
227 which accumulate at a proximal distance to the sediment source. In contrast, mudstone units ~~were restricted~~
228 are confined to fine-grained sediments ~~that accumulate at in the~~ distal section of the simulation domain.

229 Using knowledge from published studies by Kieft et al., (2011), ~~porosity and permeability variations in~~
230 ~~the stratigraphic~~
231 ~~model were estimated from) and~~ wireline-log attributes such as gamma ray, neutron, sonic, and density
232 logs

223 ~~outlined in~~, porosity and permeability variations in the stratigraphic model are estimated (Table 1-). In
previous studies on the Sleipner Øst, and Volve field (~~e.g.~~ Equinor, 2006; Kieft et
224 ~~al.~~, 2011), ~~Shoreface~~ shoreface deposits ~~were identified to~~ make up the best reservoir units, ~~whilst~~ whiles
lagoonal deposits
225 ~~formed~~ the worst reservoir units. ~~Using~~ With this ~~as~~ guide, shoreface sandstone units and mudstone/shale
units
226 ~~in~~ the forward stratigraphic model ~~were characterized as~~ are best and worst reservoir units respectively.
The
227 porosity and permeability values in Table 4 ~~were derived~~ are from equations in Statoil's petrophysical
report
228 of the Volve field (Equinor, 2016):

$$\varnothing_{er} = \varnothing_D + \alpha \cdot (NPHI - \varnothing_D) + \beta \div \text{---} (14)$$

229 where \varnothing_{er} is the estimated porosity range, \varnothing_D is density porosity, α and
230 β are regression constants; ranging between -0.02 – 0.01 and 0.28 – 0.4 respectively, $NPHI$ is neutron
porosity. In instances where $NPHI$ values for lithofacies units is not available from the published references, an
average of 0.25 was used.

porosity. In instances where NPHI values for lithofacies units is not available from the published references, an average of 0.25 was used.

$$KLOGH_{er} = 10^{(2 + 8 * PHIF - 5 * VSH_{er})} \quad (15)$$

where $KLOGH_{er}$ is the estimated permeability range, VSH is the volume of clay/shale in the lithofacies unit, and $PHIF$, the fractured porosity. The VSH range between 0.01 – 0.12 for the shoreface units, and 0.78 – 0.88 for lagoonal deposits.

for the shoreface units, and 0.78 – 0.88 for lagoonal deposits.

Property Modeling in Petrel™

The workflow (Figure 2b) used for subsurface property (e.g. lithofacies, and petrophysical) modeling in Petrel™ is extended applied to represent lithofacies, porosity, and permeability properties in the forward stratigraphic model. These processes include involve:

1. Structure modelling: identified faults within the study area are modelled modeled together with

interpreted surfaces from seismic and well data correlation to generate the main structural framework,

within which the entire property model will be built. The procedures involve modification of

Here, fault pillars and connecting fault bodies are linked to one another to attain obtain the kind of fault framework

(1) interpreted from the seismic and core data.

(2) Pillar gridding: building a “grid skeleton” that is made up of a top, middle and base architectures. Typically,

(2) pillars join corresponding corners of every grid cell of the adjacent grid to form the foundation for each cell within the model. The prominent orientation of faults (I-direction) within the model area was in

an N-S and NE-SW direction, so the “I-direction” was set to NNE-SSW to capture the general structural description of the area.

each cell within the model. The prominent orientation of faults (i.e. I direction) within the model area generally trends in a N-S and NE-SW direction, so the “I-direction” was set to the NNE-SSW direction to capture the structural description.

(3) Horizons, Zones, and Vertical Layering: stratigraphic horizons and subdivisions (zones) delineates

delineate the geological formation’s boundaries. As stratigraphic horizons are inserted introduced into the model grid,

the surfaces are trimmed iteratively and modified along faults to correspond with displacements

across multiple faults. Vertical layering on the other hand defines shows the thicknesses and orientation

between the layers of the model. Layers in this context describes refers to significant changes in particle

size or sediment composition in a geological formation. Using a vertical layering scheme makes

it possible to honour honor the fault framework, pillar grid, and horizons that have been derived. A

257 ~~constant cell thickness~~ thickness of 1 m ~~across is used in~~ the model ~~was defined~~ to control the vertical scale, ~~in~~

258 (3) ~~which subsurface properties such as~~ of lithofacies, porosity, and permeability ~~attributes are modelled~~ modeling.

259 ~~(4)~~ Upscaling: involves the ~~substitution~~ substitution of ~~fine~~ smaller grid cells with coarser grid cells. ~~This~~ Here, log data is ~~done~~ transformed from 1-dimensional to ~~assign~~

260 ~~property values~~ a 3-dimensional framework to ~~cells in order to~~ evaluate which discrete value suits ~~each a~~ selected data point.

261 (4) in the model. One advantage of the upscaling procedure is to make the modeling process faster.

262 Porosity and Permeability Modeling

263 The Volve field porosity and permeability model ~~that was built by from~~ Equinor ~~for their operations in the Volve field was~~

264 are adopted as the base (reference) model. ~~The model~~, which ~~cover an area of~~ covers 17.9 km² was generated with the reservoir

265 management software (RMS), developed by Irap and Roxar (Emerson™). The petrophysical ~~model~~ has

266 a grid dimension of 108 m x 100 m x 63 m, and was compressed by 75.27% of cell size from an

267 approximated cell size of 143 m x 133 m x 84 m. To achieve a comparable model resolution as the Volve

268 field porosity and permeability model, the forward stratigraphic output, which had an initial resolution of

269 90 m x 78 m x 45 m ~~was~~, is upscaled to a grid of 107 m x 99 m x 63 m. ~~Two Variograms being a critical aspect of this work, we submit two options were explored with~~

270 respect to the use of extrapolate variogram parameters ~~derived from the~~ forward ~~model~~ stratigraphic-based synthetic wells, porosity and permeability models. In Option -1

271 ~~was to assign, the~~ porosity and permeability values were assigned to the synthetic lithofacies wells that ~~correspond to~~ correlate with known

272 facies ~~associations as indicated in~~ association in the study area (see Table 4.). The ~~synthetic~~ pseudo wells ~~with~~ comprising porosity and permeability ~~data~~ are

273 placed situated in-between ~~known data~~ well locations to guide porosity and permeability ~~property distributions~~ simulation in the

274 model. For ~~option -2, the~~ best-fit ~~forward~~ stratigraphic ~~model~~ ~~was populated with~~ changes by

assigning porosity, and

275 — permeability ~~attributes~~attribute using the ~~major~~general stratigraphic orientation captured in the seismic data (~~i.e.~~ NE-SW;

276 — ~~240°) to control property distribution trends.~~⁰). Porosity and permeability ~~were populated into the model by~~

277 — ~~using the property modeling process in Petrel™. Porosity and permeability synthetic pseudo~~
(synthetic) logs ~~are~~were then

278 — extracted from the forward stratigraphic output to build the porosity and permeability models (**Figure 8**).

Porosity modeling is through normal distribution, whiles the permeability models were produced using a log-normal distribution and the corresponding porosity property for collocated co-kriging.

279 — ~~Taking into account the possibility~~Considering that vertical trends in options -1 and -2 -will -be similar ~~in~~within a sampled

280 — interval, ~~it is our opinion that~~ option 2 ~~will provide~~presented a viable 3-D representation of property variations in

281 — the major and minor directions of the forward stratigraphic model. Ten synthetic wells (SW), ranging

282 — between 80 m and ~~a~~ 120 m in total depth (TD) ~~were~~), are positioned in the forward model to capture the vertical

283 — distribution of porosity-permeability at different sections of the forward stratigraphic ~~model~~-based models.

The ~~forward-based~~ synthetic wells (**Figure 9 c**) with porosity and permeability ~~logs data~~ were upscaled ~~to~~
~~populate, and distributed into~~ the ~~original structural model using the sequential Gaussian simulation~~
~~method. Here, the~~
 The synthetic wells derived from the stratigraphic model ~~is to provide~~ served as an additional ~~well data control~~
~~for use in a~~
~~traditional porosity and permeability modeling workflow as was in~~ the ~~case in the building of original Volve~~
~~model. Considering field. Because~~ the
~~advantages of~~ variogram-based modeling ~~in relation to~~ approach is efficient in subsurface data conditioning,
~~the this idea was~~ presents an opportunity to get more wells
~~into the model grid at no additional cost~~ to control porosity and permeability distribution. Upscaling the
~~synthetic well data in~~
~~this context is to "transform" the data from 1-D into a 3-D framework to build the property model. Using~~
~~the same structural model was to attain a comparable framework for evaluating the modeling outputs.~~
 The variogram model (**Figure 10**) of dominant lithofacies units in the ~~formation~~ stratigraphic model served as a
 guide in ~~the~~
~~estimation of~~ estimating variogram parameters ~~from the forward model. A~~ for porosity and permeability
modeling. The variogram has major and minor range of 1400 m and
 400 m respectively, and an average sill value of 0.75 ~~derived from forward stratigraphic-based synthetic~~
~~wells were used to populate porosity and permeability properties in the model. Porosity models~~
~~were~~
~~derived with a normal distribution, whilst the permeability models were produced using a log-~~
~~normal~~
~~distribution and the corresponding porosity property for collocated co-kriging. Out of~~ Six out of
~~fifty model~~
~~realizations, six realizations~~ that ~~showed~~ show some similarity to the original ~~petrophysical~~ porosity and
permeability model ~~are presented~~
~~formed the basis of our analysis (Figure 11). This~~ The selection of six realizations was ~~accomplished through~~ on
a visual and statistical comparison of zones in the original
~~Volve field model, Volve field model and the stratigraphic-based porosity/permeability model. The statistical~~
~~approach involved summary statistics from the reference model and the stratigraphic-based~~
~~porosity/permeability models. The statistical approach~~
~~involved a comparison of summary statistics from the original Volve model, and the porosity/permeability~~
~~model generated through forward stratigraphic modeling. The model. In contrast, the visual comparison on~~

~~the other hand looked~~

~~at how evaluation compared the geological realistic the output is, and if it conforms with our conceptual~~
~~idea of the Volve field realism of forward stratigraphic-based realizations to the base model.~~

~~model.~~

Results

The stratigraphic model in stage 4 (**Figure 5d iv**) shows the final geometry after 700,000 years of

simulation time. ~~initial~~ The initial stratigraphic simulation produced a progradation sequence with
foreset-like features (**Figure**

~~5d i).~~ A) and a sequence boundary, which ~~indicates the highest sea level in the model~~ separates the
initial

simulated output from the next prograding phase (**Figure 5d ii**). ~~Initiation of an aggradation~~ An
aggradational stacking

310 pattern ~~starts, commences~~ and becomes prominent in stage 3 (**Figure 5d iii**). These aggradational
sequences observed in the forward stratigraphic model are consistent with ~~real-~~

311 ~~world scenario-natural events~~ where sediment supply matchup with accommodation ~~created as a result~~
~~of the relative~~

312 ~~due to~~ sea-level rise within a geological period (~~e.g.~~ Muto and Steel, 2000; Neal and Abreu, 2009). ~~The~~
~~diffusion process~~

313 ~~in GPM™ was used to define the stratigraphic architecture before introducing additional geological~~

314 ~~processes such as steady flow, unsteady flow, wave events to capture the range of possible~~
~~depositional~~

315 ~~styles that have been discussed in published literature (e.g. Folkestad & Satur, 2006; Kieft et al., 2011).~~

316 ~~The impact of the~~ Impact of the forward stratigraphic simulation on porosity and permeability
representation in the reservoir model ~~was~~

317 ~~evaluated~~ is evident by comparing its outcomes to the Volve field porosity and permeability models by
using two

318 ~~synthetic well, (VP1 and VP2, which were);~~ sampled ~~vertically~~ at a 5 m ~~intervals. Considering vertical~~
~~interval. Taking into account the fact~~ that the

319 ~~Volve field petrophysical model (Figure 11a) have undergone~~ went through various phases of history
matching to enhance

320 ~~obtain a model to improve~~ well planning; and production strategies ~~in the Volve field~~, it is reasonable to
assume that porosity and

321 ~~permeability distribution in the petrophysical model will be geologically realistic and less uncertain. A~~

322 ~~This view formed the basis for using the porosity and permeability models developed by Equinor as a~~
~~reference for comparing outputs in the stratigraphic model. Table 5a shows an almost good match in~~
porosity ~~was observed in validation wells that penetrate the model realizations; at different intervals in~~
~~the forward stratigraphic-based models (i.e. R14, R20,~~

323 ~~R26, R36, R45, and R49 (Table 5a)).~~ An analysis of the well logs in the model area shows that a large

proportion of reservoir porosity is between 0.18 – 0.24. Also, the analysis of the forward stratigraphic-based

porosity model is consistent with the porosity range in the Volve field model (see Figure 12 ~~shows the porosity~~
~~variation (0.18 – 0.24) in some selected).~~

324 ~~realizations. This value (i.e. 0.18 – 0.24) is within the range of porosity estimates in the Volve field~~

(Equinor, 2016). In view of the A notable limitation in making variations within a simulation run in GPM™, the forward stratigraphic based model (FSM) ~~was derived with an~~ with this approach is the assumption that variogram parameters, and stratigraphic inclination within zones ~~will remain constant. As a result, remained constant throughout the simulation. The difference in permeability attributes between~~ the original ~~petrophysical model,~~ which involve permeability model and the forward stratigraphic-based type is the application of other measured ~~attributes within the stratigraphic zone was not considered~~ parameters in the forward stratigraphic modeling based permeability original model, hence the major variations noted in (Table 5b).

). Typically, a petrophysical model like the Sleipner Øst and Volve field model will ~~take into account~~ factor in other sources of data. For example, data from a datasets such as special core analysis (SCAL) ~~will improve the~~ and level of cementation, which enhances reservoir petrophysics assessment. ~~Considering~~ Bearing in mind that the ~~FSM approach~~ forward stratigraphic model did not involve ~~these~~ some of this additional information from the ~~formation, reservoir,~~ it is ~~reasonable-practicable~~ to suggest that results obtained in the forward stratigraphic-based porosity and permeability models have ~~been~~ adequately conditioned to known subsurface data.

Discussion

Results show the influence of sediment transport rate, (or diffusion rate), initial basin topography, and sediment source location on the stratigraphic simulation in the GPM™ software. Similar. Compared to other studies (e.g. such as Muto & Steel, (2000); and Neal & Abreu, (2009), we observed that a variationsvariation in sea-level controls the volume of sediment that could be is retained or transported further into the basin; therefore controlling the kind-ofresultant stratigraphic sequences that are generated. In a related work by Burges et al. (2008), it was established) suggest that a sediment-wedge topset width wasconnects directly linked to the initial bathymetry, in which the sediment-wedge structure was formed, as well as develops, and the correlation between sediment supply and accommodation rate. This opinion is in line with observations in this study, where the initial sediment deposit controlcontrols the geometry of subsequent phase phases of depositions. in the hypothetical basin. The uncertainty of initial conditions used in this work led to the generation of multiple forward stratigraphic scenarios to account for the range of bathymetries that may have influenced sediment transportation to form the present-day Hugin formation. reservoir units in the Volve field.

The simulation produced well-defined sloping depositional surfaces in a stratigraphic architecture (i.e. clinoforms) and sequence boundaries that depict the pattern observed patterns seen in the seismic data. Indicated in previous studies, (e.g. In their work, Allen and Posamentier, (1993); Ghandour and Haredy, (2019) explained the importance of sequence stratigraphy is vital in the lithofacies characterization of lithofacies in , and therefore petrophysical property distribution in sedimentary systems. Therefore, a reproduction of stratigraphic sequence-Also, sediment deposition into a geological basin in the natural order is controlled by mechanical and geochemical processes that modify petrophysical attributes (Warrlich et al. 2010); therefore, using different geological processes and initial conditions to generate depositional scenarios in 3-D, using the forward

351 ~~stratigraphic modeling approach in GPM™ provide a good~~ dimension provides a framework to analyse
property variations in

352 ~~a hydrocarbon reservoir. A~~ The approach produces a porosity-permeability model ~~matching comparable to~~ the
original petrophysical model ~~was produced~~ using

353 ~~synthetic porosity and permeability logs from the forward stratigraphic model as input datasets in the~~
~~sequential Gaussian simulation algorithm.~~ As mentioned ~~previously~~, this exercisework did not ~~take into~~
354 ~~account~~ include variations in the layering scheme that develops in different zones of the stratigraphic model.

355 Under this circumstance, ~~we concede that~~ there is a possibility to overestimate and or underestimate
356 ~~porosity and permeability properties as observed~~ property in some sampled intervals ~~of in~~ the validation wells.
~~In~~

357 ~~view of this, it is our suggestion. Therefore, we suggest~~ that the forward stratigraphic simulation outputs
~~should be applied as~~

358 ~~such as the example presented in this contribution serve as~~ additional ~~data to understand sediment~~
distribution ~~patterns,~~ and ~~associated vertical and horizontal~~

359 ~~petrophysical trends in the depositional environment than using its outputs, and not~~ as ~~an~~ absolute
conditioning

360 ~~data in subsurface property modeling.~~

362 ~~Assumptions~~The assumptions made ~~with respect to~~concerning the type of geological processes, and input
 parameters ~~to use~~ in the
 363 stratigraphic simulation certainly differ from what existed during ~~the period of~~sediment deposition. So,
 applying stratigraphic
 364 ~~models that fit a basin-scale description to a~~ relatively smaller scale reservoir ~~context~~ presents another
~~degree~~level of
 365 ~~uncertainty in the approach~~used here. For example, in their study, This finding agrees with Burges et al.,
 (2008) ~~shows~~, where they indicate that the
 366 ~~diffusion geological process~~ simulation fits the description of large-scale sediment transportation; ~~suggesting.~~
This view further buttresses the point that ~~an~~
 367 ~~extrapolation of its outputs~~integrating forward stratigraphic simulation into a well-scale framework ~~could~~
~~produce results~~has a high chance of producing outcomes that deviate from the real
 368 ~~world distribution.~~subsurface description. In ~~reality, sediment deposition into a geological basin is also~~
~~controlled by mechanical~~
 369 ~~and geochemical processes that tend to modify a formations petrophysical attributes (Warrlich et~~
~~al.~~
 370 ~~2010). Therefore, using different geological processes and initial conditions to generate depositional~~
 371 ~~scenarios is a reasonable approach. However, based on the approach limitation, which are also~~
~~discussed~~
 372 ~~line with observations in similar works (e.g. Bertoncello et al. (2013); Aas et al. (2014); and Huang et al.~~
 (2015) ~~caution must be~~
 373 ~~taken in using its relations to limitations in the forward stratigraphic simulation method, it is advisable to use~~
~~its outputs~~ cautiously in ~~real~~ reservoir modeling; ~~as it~~ such outputs from forward stratigraphic models could
 lead ~~to an~~ increase in property
 374 ~~representation bias.~~ in a model.

375 The correlation between reservoir lithofacies and petrophysics, and its prediction through reservoir
models, have been extensively examined in ~~previous~~several studies,
 376 ~~e.g. (Falivene et al. (2006); Hu and Chugunova, (2008), but).~~ Meanwhile, the ~~difference in~~ predicted
~~and outputs most often do not depict the~~ actual reservoir
 377 ~~character is less understood. This in large part is~~ due to the absence of a realistic 3-D stratigraphic
 378 ~~framework to guide reservoir property representation in~~ geocellular geological models. ~~It is our opinion~~
~~that~~The forward

379 _stratigraphic modeling ~~methods provide~~method, notwithstanding its limitations, provides reservoir
modeling practitioners ~~a better~~an platform to generate subsurface models that reflect the natural variation of
reservoir properties.

380 ~~appropriate 3-D lithofacies models to improve petrophysical property prediction in a reservoir, but its~~
381 ~~outputs should be used cautiously and together with verifiable subsurface patterns from seismic and~~
~~well~~
382 ~~datasets.~~

383 Conclusion

384 In this paper, ~~spatial data~~variogram parameters from a forward stratigraphic simulation ~~is~~are combined
with subsurface data ~~from~~
385 ~~the Volve field, Norway~~ to constrain porosity and permeability distribution in ~~inter-well regions of~~ the
386 Volve field model ~~area. As. The~~ caution, for subsurface modeling practitioners is that the ~~forward~~
stratigraphic simulation scenarios presented in this contribution do
387 ~~not ultimately~~ prove that spatial and geometrical data derived from forward stratigraphic ~~modeling can~~
~~be used as~~

388 ~~models are~~ absolute input parameters for a real-world reservoir modeling task. Uncertainties in the choice
of ~~initial~~

389 ~~condition~~boundary conditions and processes for the stratigraphic simulation led the variation of input
parameters ~~in order to~~

390 ~~attain a depositional architecture that is geologically realistic and comparable to the stratigraphic~~

391 ~~correlation suggested in some published studies of the study area. The good match~~ in porosity
~~obtained from~~

392 ~~by comparing~~ validation wells in the original and stratigraphic-based petrophysical model, ~~leads us to~~
~~the suggestion~~

393 ~~indicates~~ that ~~an integration of~~combining variogram parameters from well data and forward stratigraphic
simulation ~~outputs~~

394 ~~will improve property prediction in inter-well zones. This suggestion is supported by~~supports the idea
that more

395 ~~conditioning data (well data) will increase the chance of producing realistic property distribution in the~~

396 ~~model area. In addition, this~~This work also made some key findings:

397 ~~1. For a specific application of forward stratigraphic modeling~~simulation in GPMTM and a range of
model

398 ~~parameters, the process of~~ sediment transportation and deposition is ~~influenced by~~based on
diffusion rate, and proximity to

399 ~~sediment source. This opinion is consistent with several published works on sequence~~
~~stacking~~stratigraphy and or

400 ~~system tracts in shallow marine settings, but. However,~~ further work with different stratigraphic
modeling

401 ~~1. simulators could be useful in mitigating~~mitigate some of the challenges faced in this work.

402 ~~2. A geologically viable 3-D A lithofacies distribution that is consistent with previous studies was~~
~~produced in the shallow marine Hugin formation was~~

403 ~~achieved, which is stratigraphic model. This position is~~ evident ~~in scenarios where sediment~~
distribution ~~vertically matches with~~

404 ~~2. lithofacies variation in a sampled interval in an actual well log.~~

405 ~~Geologically feasible stratigraphic patterns generated in the forward stratigraphic model provide~~

406—_additional confidence in the representation of lithofacies, and therefore porosity and permeability
property

407—_variations in the depositional setting under study. The resultant forward stratigraphic-based porosity and
408_permeability model suggests that forward stratigraphic simulation outputs can be integrated into classical
modeling workflows to improve subsurface property modeling and well planning strategies.

409 — modeling workflows to improve subsurface property modeling , and well planning strategies.

410 **Data and Code Availability**

411 The datasets ~~used in for~~ this work ~~was obtained~~are from Equinor on their operations in Volve field
412 operations, Norway. ~~This~~
413 ~~The data~~ include: 24 suits of well logs, and 3-D reservoir models in Eclipse and RMS formats. The data,
models
414 (eclipse and RMS formats), and the rule-based calculation script to generate lithofacies and porosity/permeability
proportions are archived on Zenodo as Otoo & Hodgetts, (2020).

414 ~~proportions are archived on Zenodo as Otoo & Hodgetts, (2020).~~

415 **GPM™ Software**

416 The ~~version~~ (2019.1) version of GPM™ software was used in completing this work after an initial 2018.1 version.
Available
417 on: ~~<https://www.software.slb.com/products/gpm>~~ <https://www.software.slb.com/products/gpm>. The
software license and code used in the GPM™ cannot be
418 provided, because Schlumberger does not allow the code for its software to be shared in publications.

419 **Model Availability in Petrel™**

420 ~~The work started in~~ Petrel™ software (2017.1), ~~but it~~ was ~~initially used for the task, but~~ completed with
Petrel™ software (2019.1);
421 ~~). The software is~~ available on:
~~<https://www.software.slb.com/products/petrel>~~ <https://www.software.slb.com/products/petrel>. The software
~~run~~runs on a ~~windows~~Windows PC with the
422 following specifications: Processor; Intel Xeon CPU E5-1620 v3 @3.5GHz 4 cores-8 threads, Memory;
423 64 GB RAM. The computer should be high end, because a lot of processing time is required ~~to execute~~
424 for the task. The forward stratigraphic models are ~~achieved~~ in Zenodo as Otoo & Hodgetts, (2020).

425 **Author Contribution**

426 Daniel Otoo designed the model workflow, conducted the simulation using the GPM™ software, and
427 evaluated the results. David Hodgetts converted the Volve field data into Petrel compactible format for
easy integration with outputs from the forward stratigraphic simulation.

428 ~~easy integration with outputs from the stratigraphic simulation.~~

429 **Acknowledgement**

430 Thanks to Equinor for making available the Volve field dataset. Also, thanks to Schlumberger for
431 providing us with the GPM™ software license. A special thanks to ~~Schlumberger for providing the~~
432 ~~software, and~~ Mostfa Legri (Schlumberger) for his technical support in the use of GPM™. Finally, to the
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~~436 marine sands: an example from the Peira Cava sub-basin. The geologic society, 387(1), 247-269,~~
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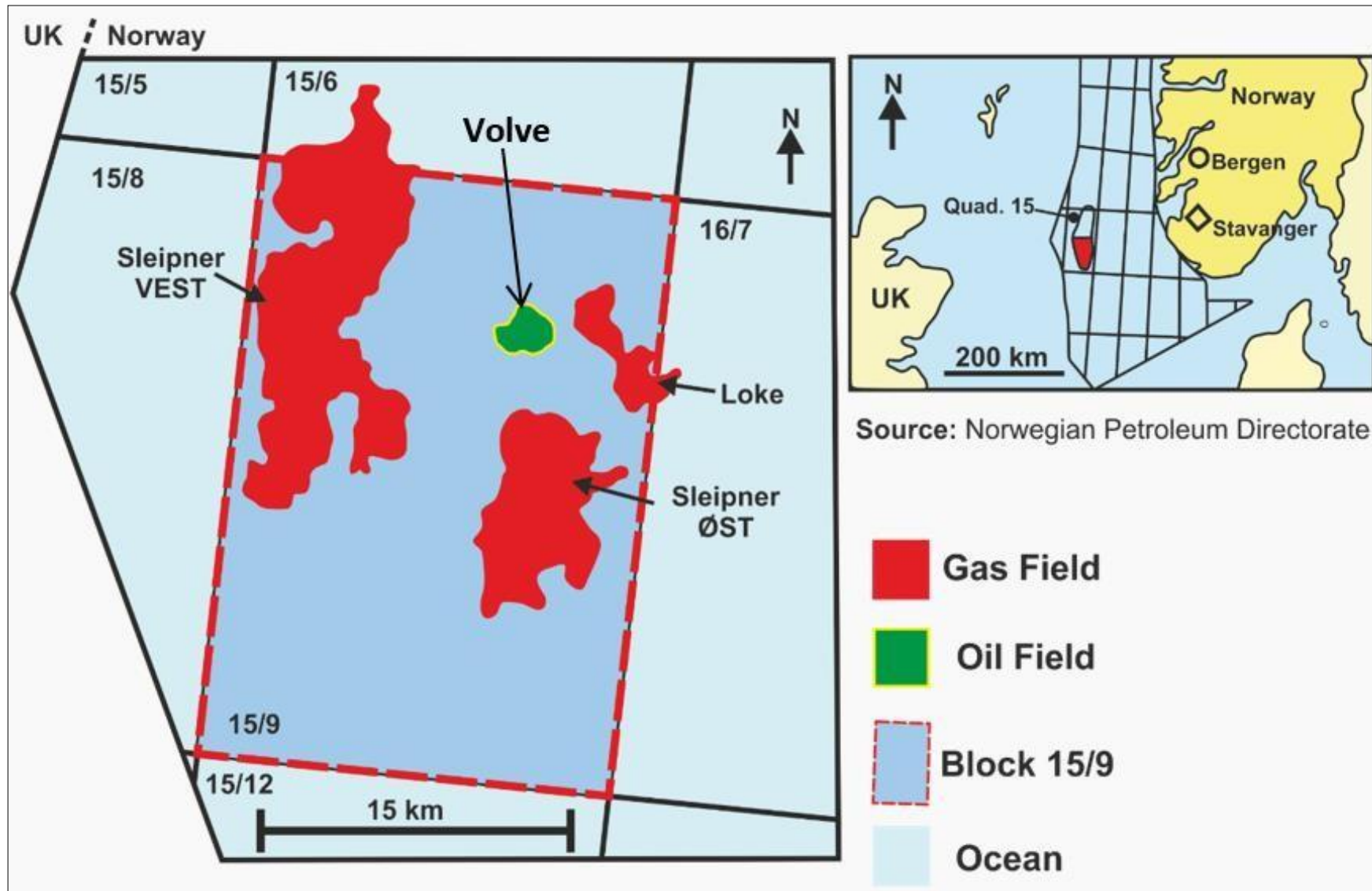
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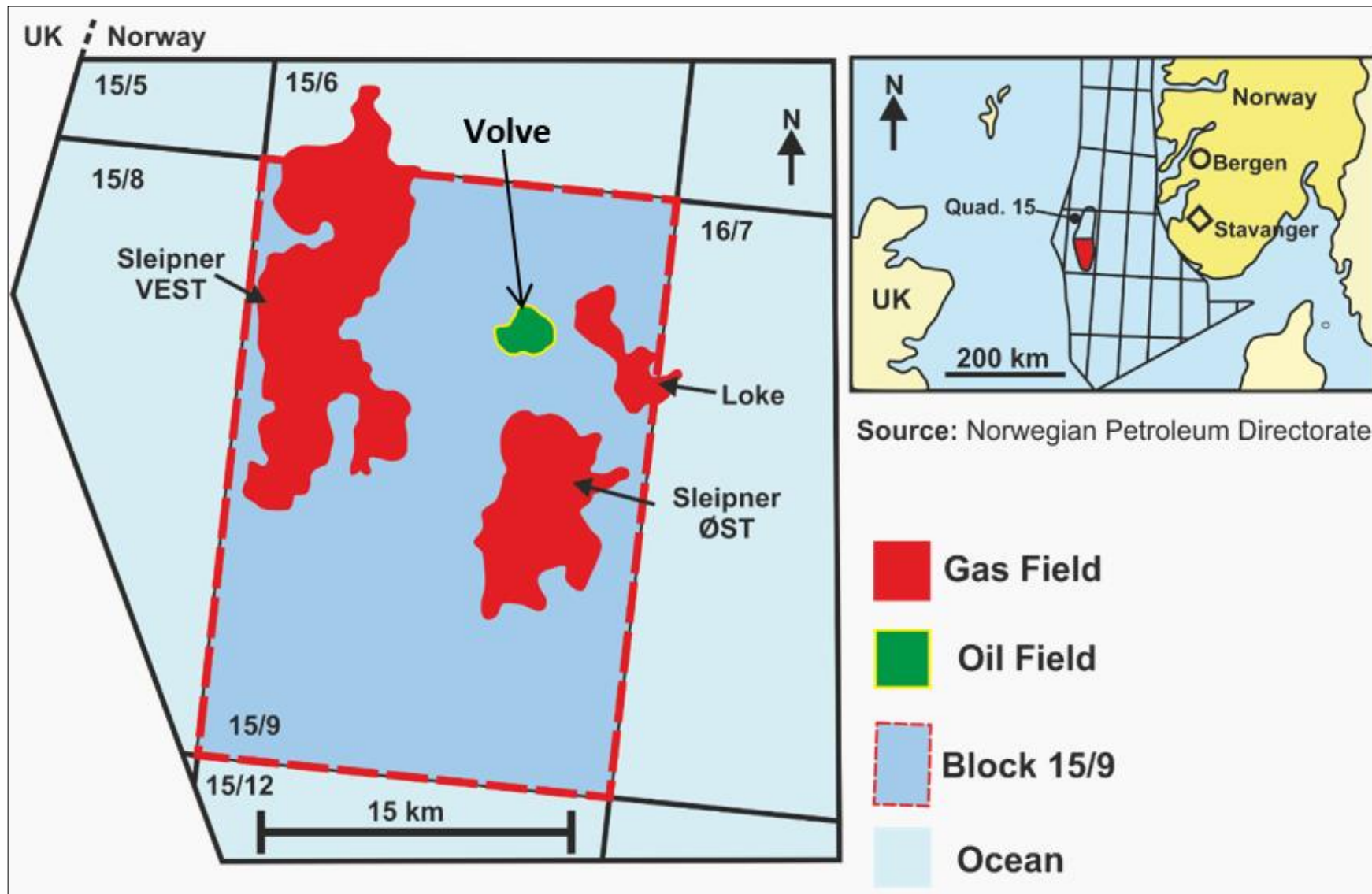
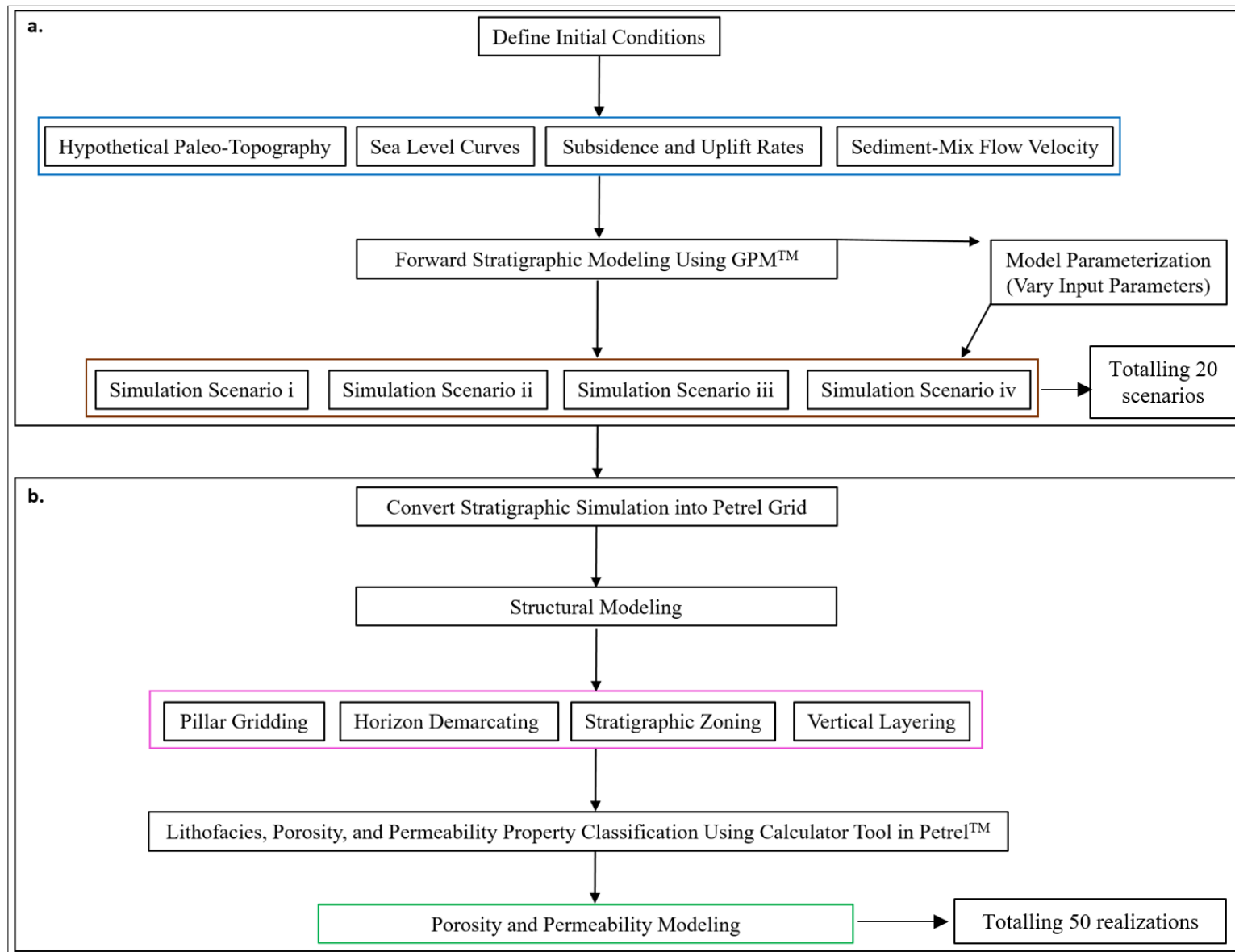


Fig 1. Location map of the Volve field, showing gas and oil fields in quadrant 15/9, Norwegian North Sea (Adapted from Ravasi et al., 2015).



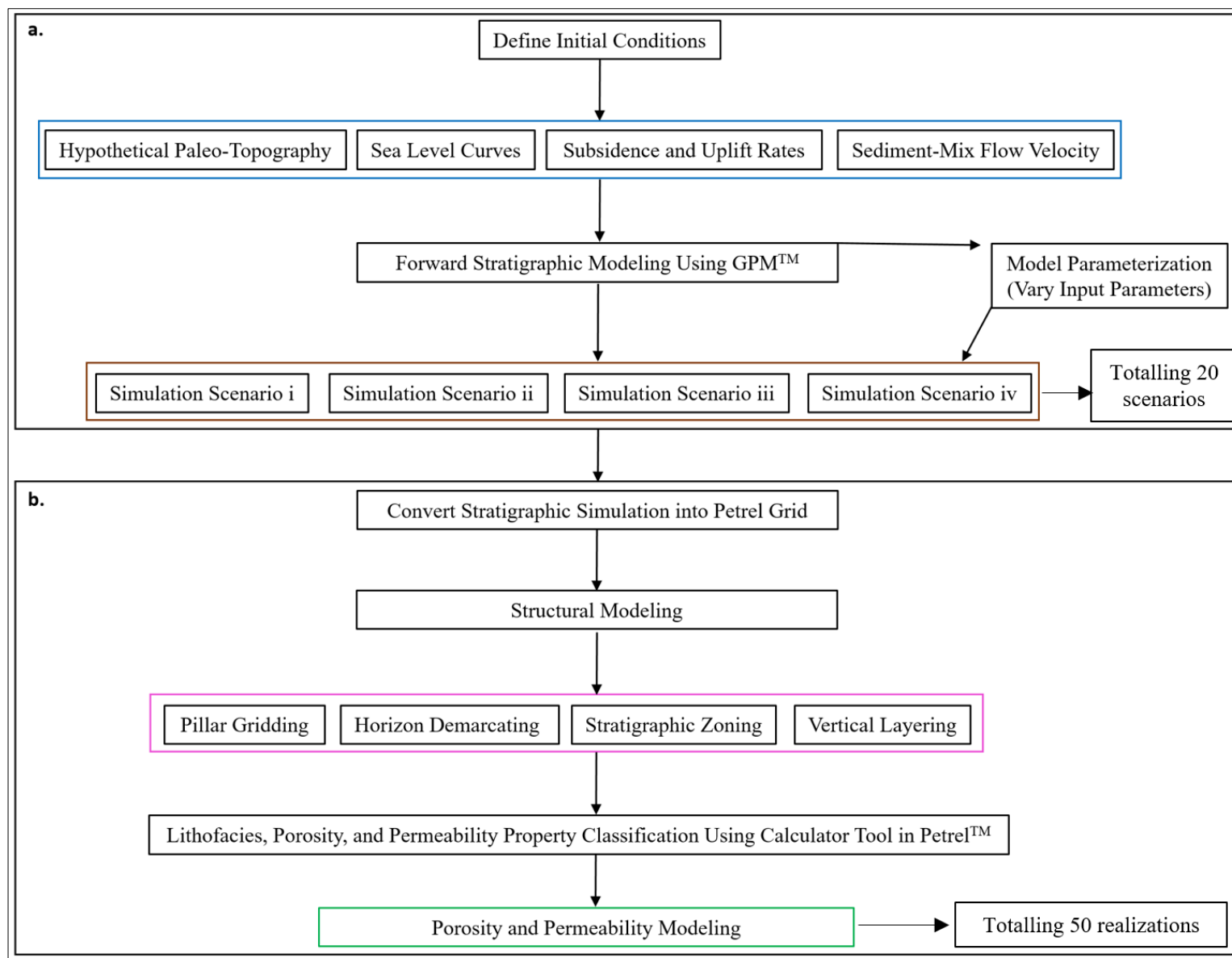
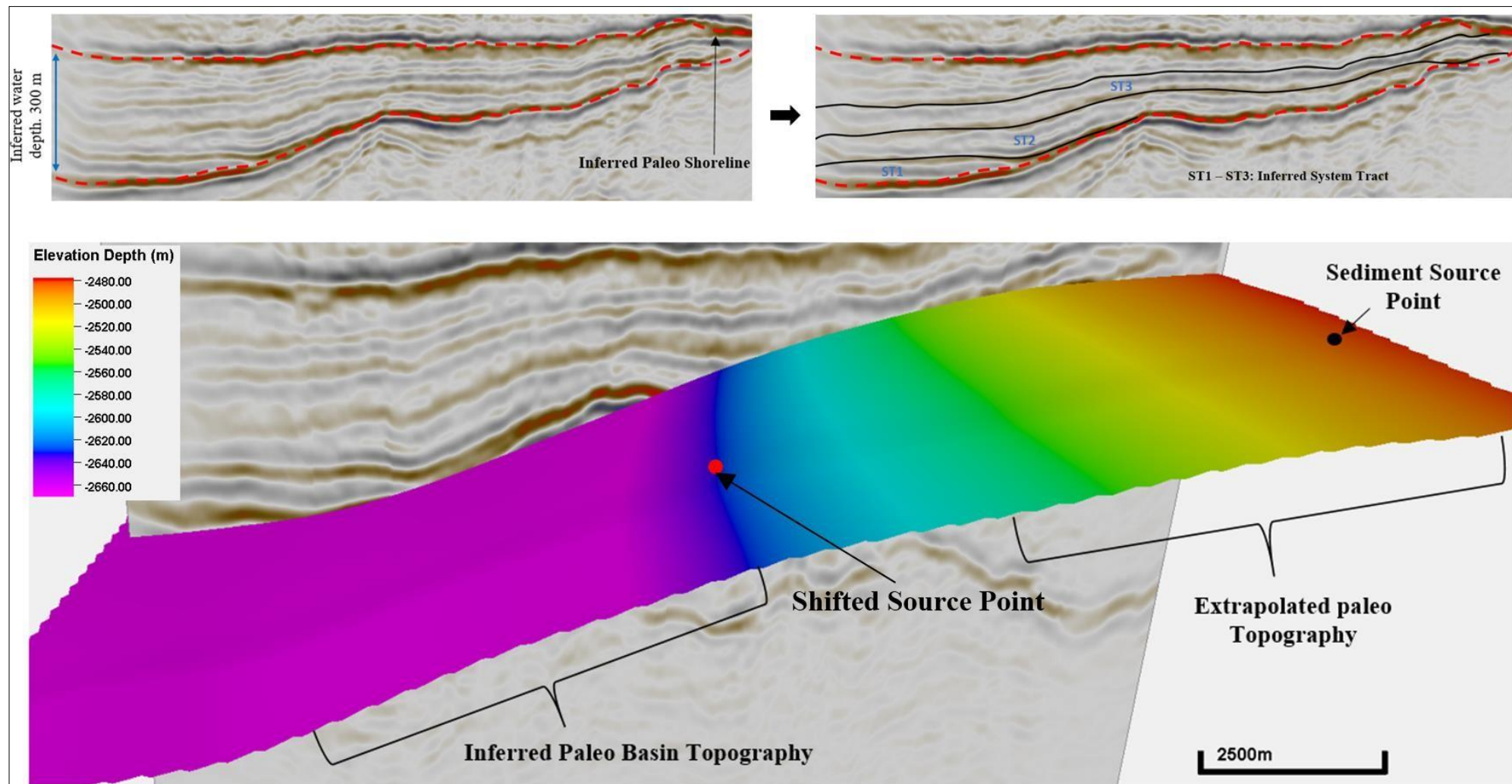


Fig 2. Schematic workflow of processes involved in this work. a. providing information of initial boundary conditions (~~or~~ input parameters) ~~that were~~ used in the forward stratigraphic simulation in GPMTM; b. ~~demonstrating~~demonstrate how the forward stratigraphic ~~were~~model are converted into a grid that is usable in PetrelTM for porosity and permeability modeling.



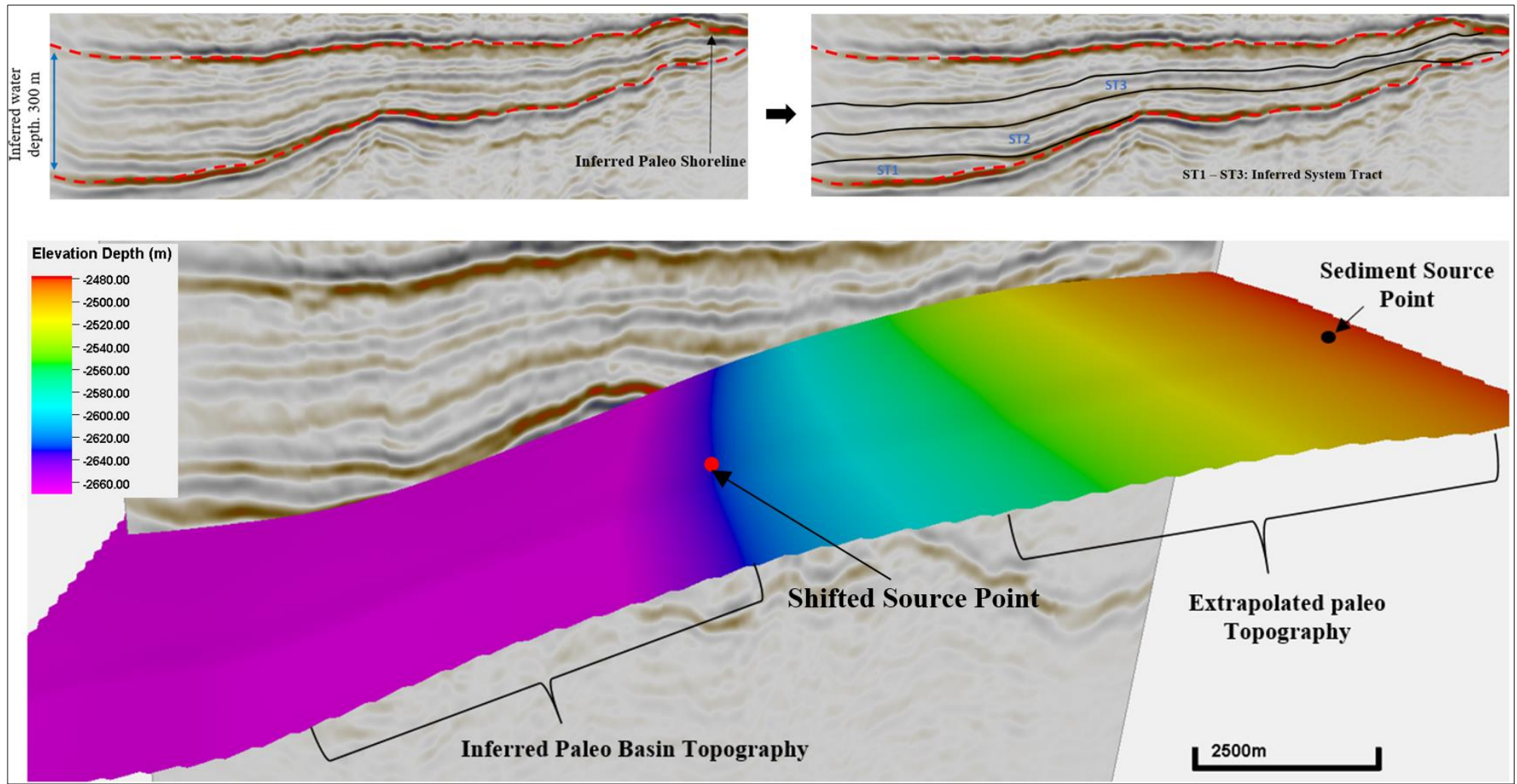
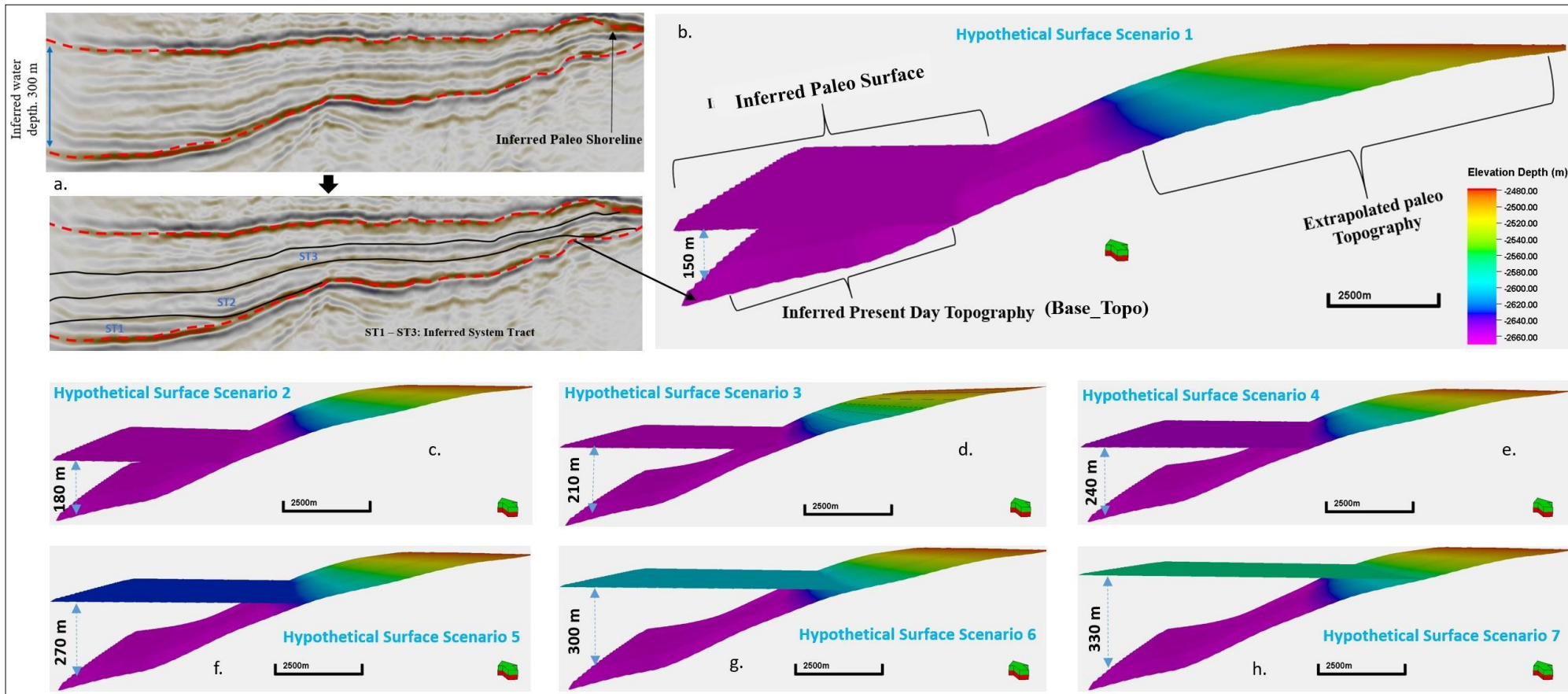


Fig 3. 3-D seismic section of the study area, from which the hypothetical topographic surface was derived for the simulation. The sedimentary entry point into the basin is located in the North Eastern section, (based on previous study in the model area (e.g. Kieft et al. 2011).



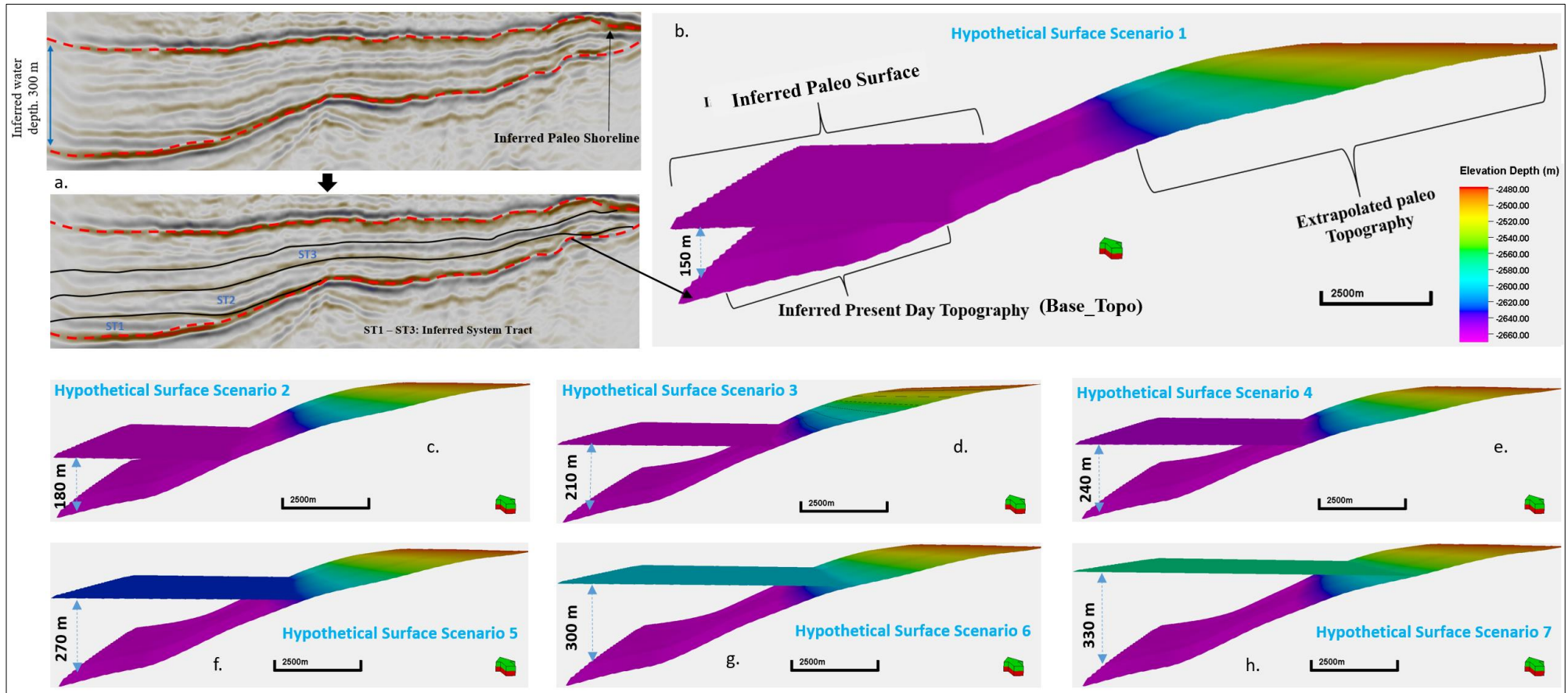
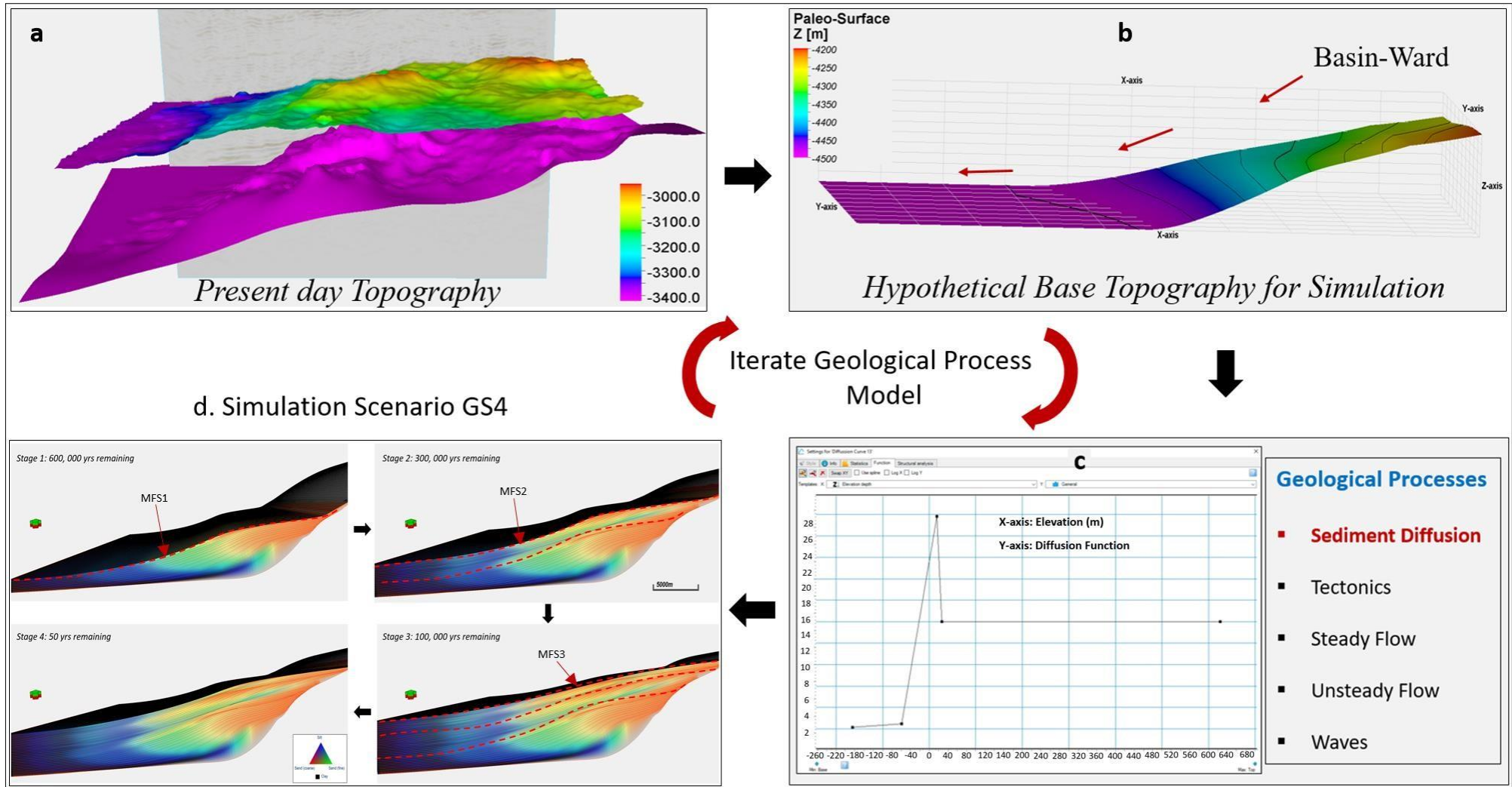


Fig 4. ~~Inferred paleoPaleo~~ topographic surface from seismic, ~~also. Also,~~ illustrating different topographic surface scenarios ~~used in~~ that are produced for the simulation.



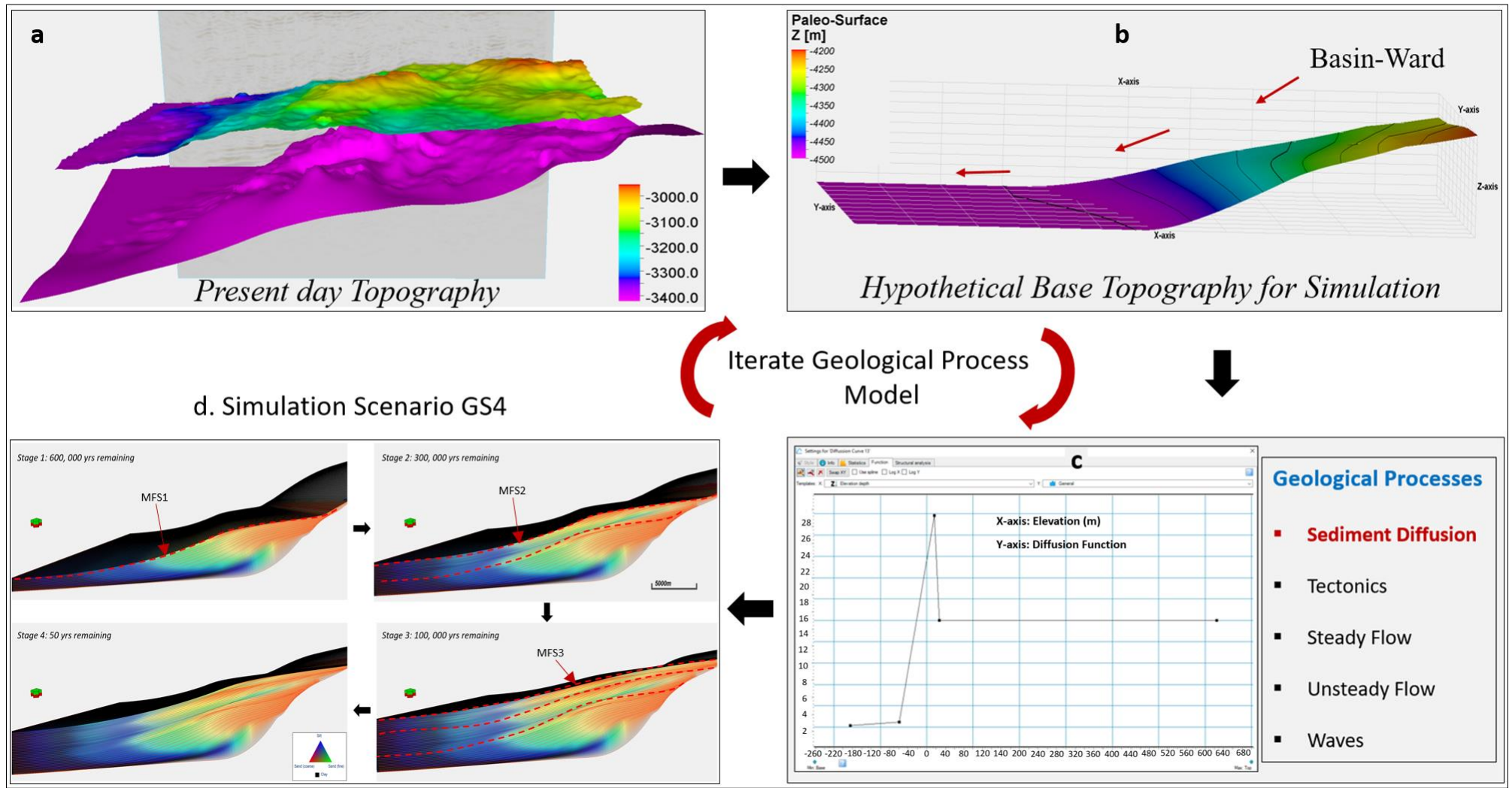
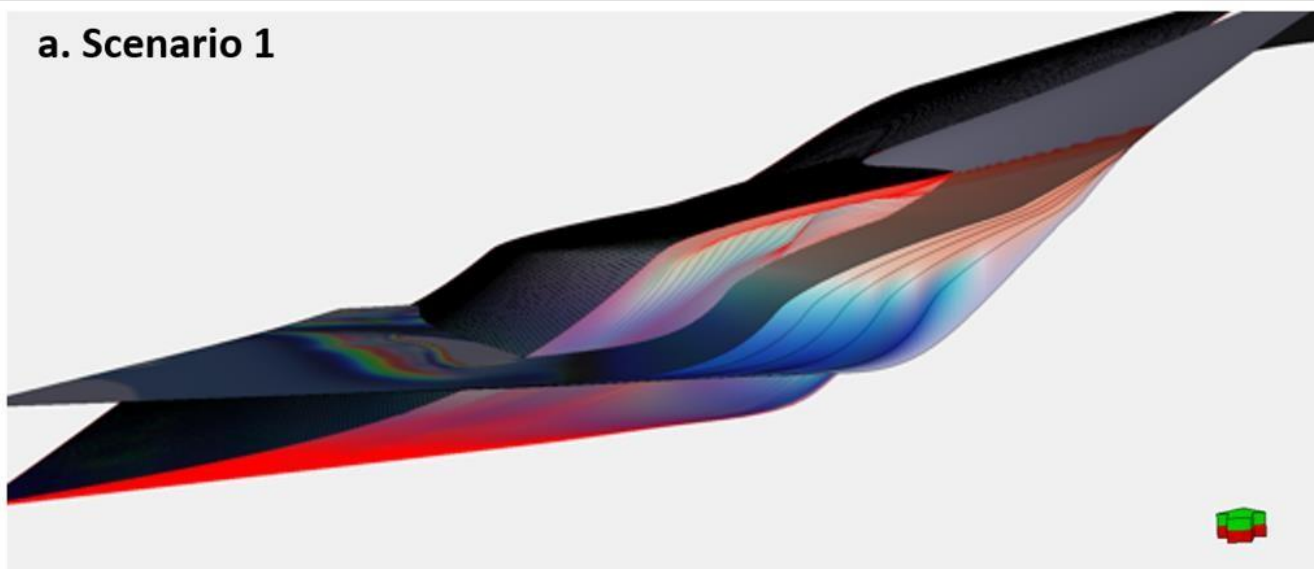
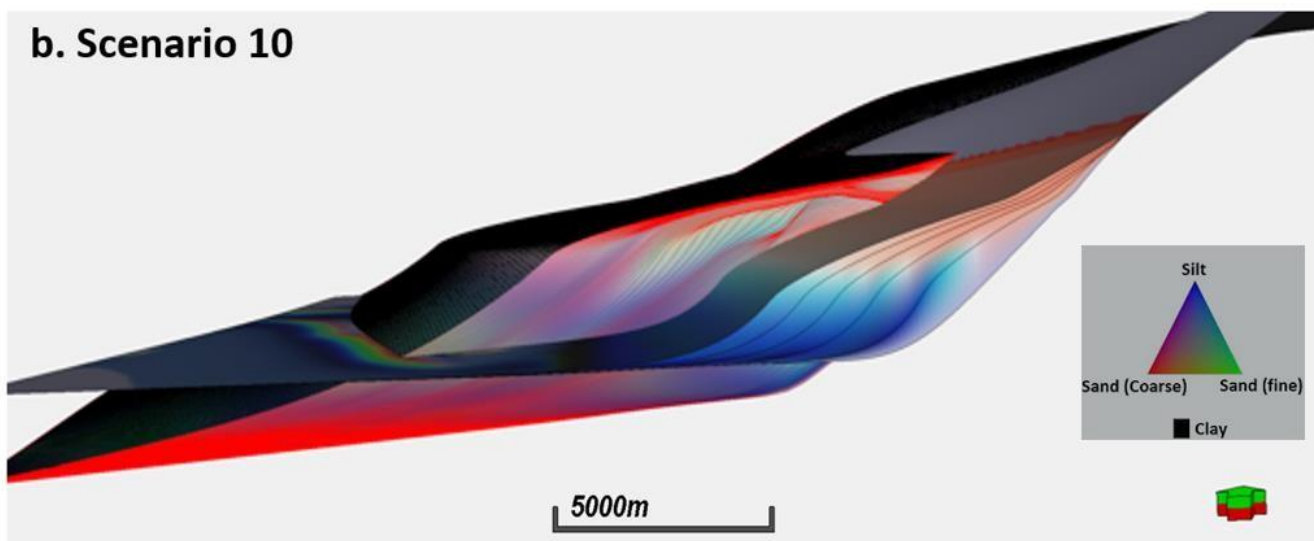


Fig 5. a. present-day top and bottom topographic surfaces of the Hugin formation; b. hypothetical topographic surface *derived* from seismic data; c. geological processes involved in the forward stratigraphic simulation; d. forward stratigraphic models at different simulation time-intervals.

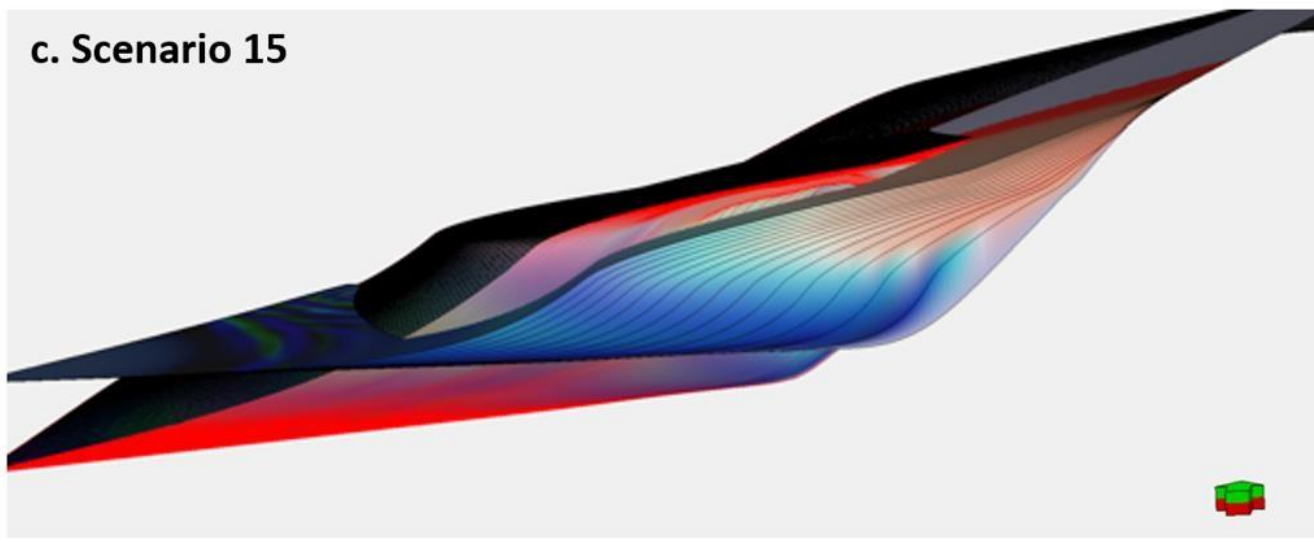
a. Scenario 1



b. Scenario 10



c. Scenario 15



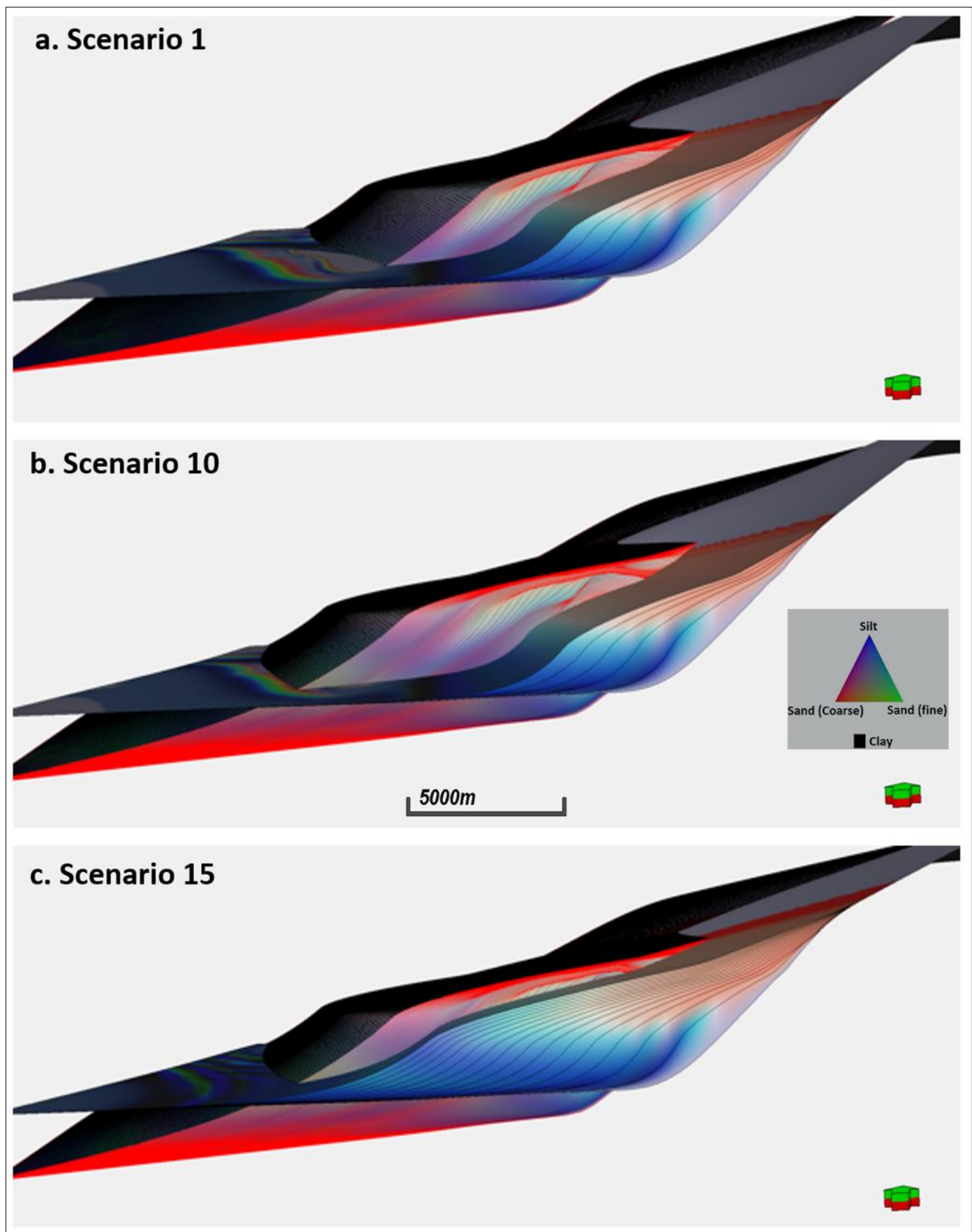
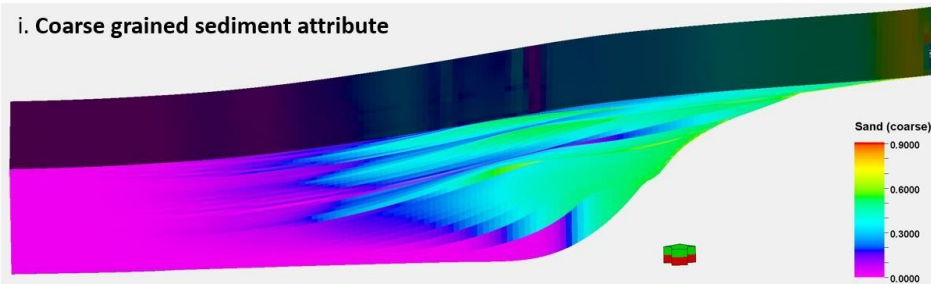


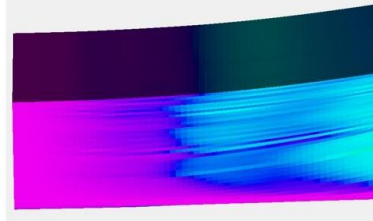
Fig 6. Stratigraphic simulation scenarios depicting sediment deposition in a shallow marine framework. **a.** scenario 1 involves equal proportions of sediment input, a relatively low subsidence rate and low water depth, **b.** scenario 10 uses high proportions of fine sand and silt (*i.e.* 70%) in the sediment mix, abrupt changes in subsidence rate, and a relatively high water depth, **c.** scenario 15 involves very high proportions of fine sand and silt (*i.e.* 80%), steady rate of subsidence and uplift in the sediment source area, and a relatively low water depth.

a. Sediment Distribution

i. Coarse grained sediment attribute

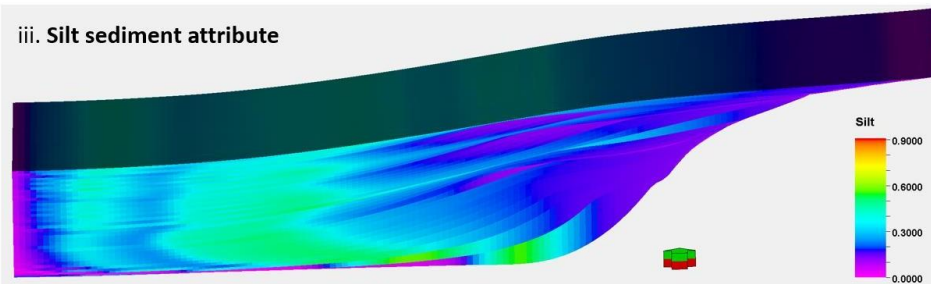


ii. fine grained sediment attribute



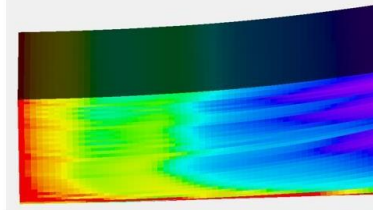
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iii. Silt sediment attribute

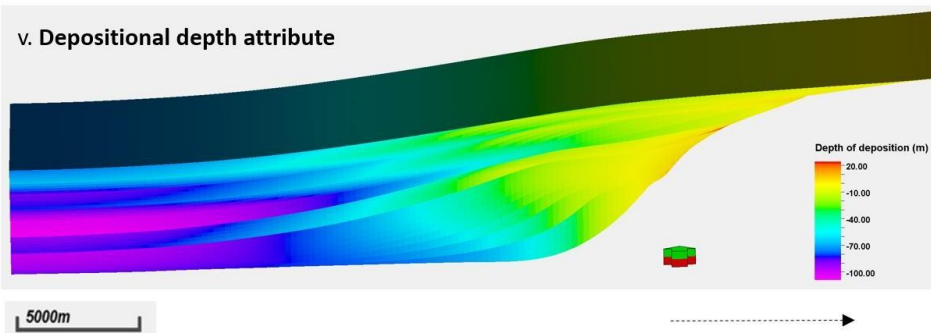


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iv. Clay sediment attribute

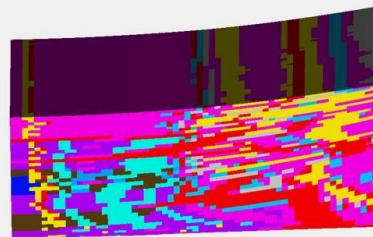


v. Depositional depth attribute



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b. Lithofacies Classification



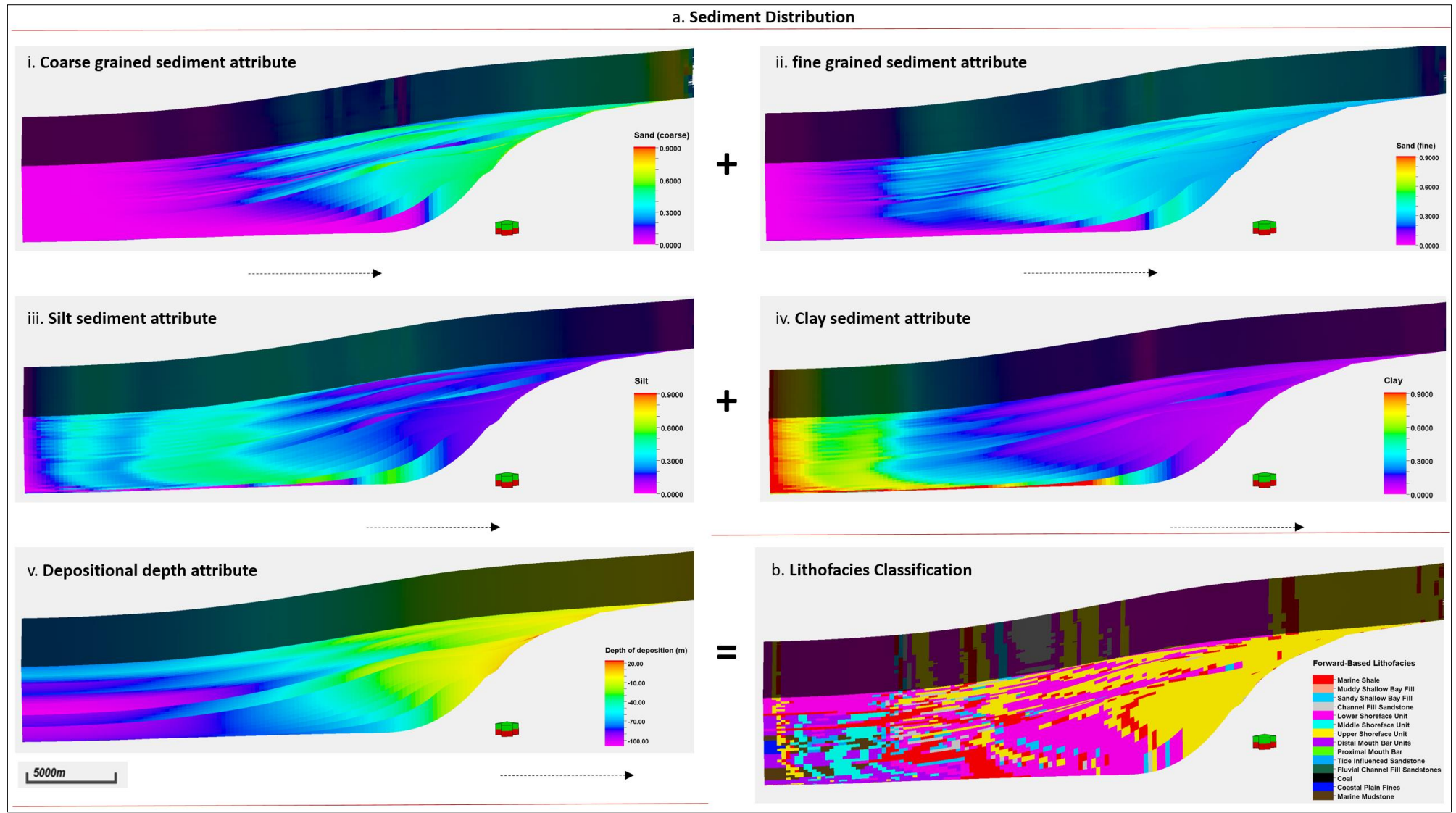
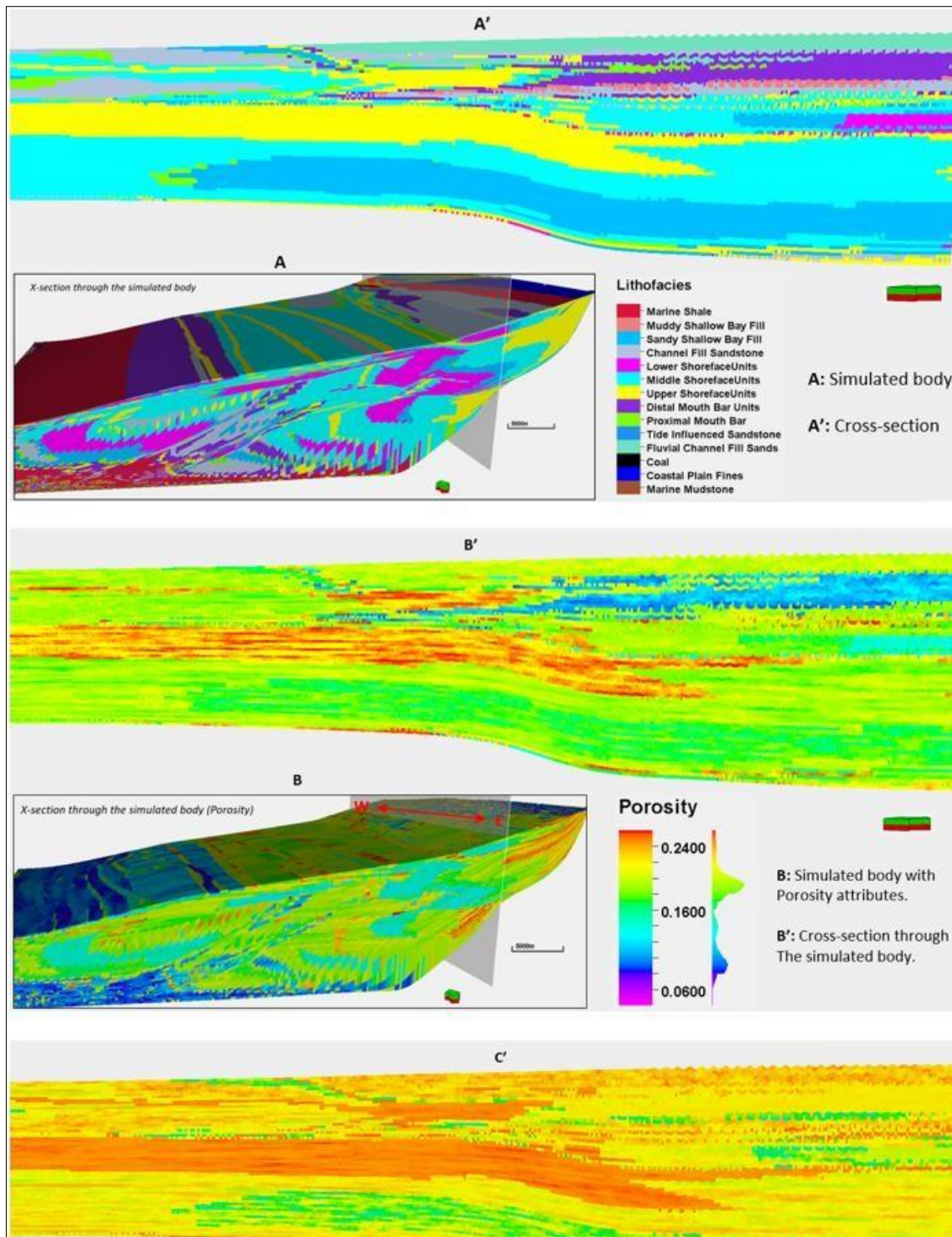


Fig 7 a. Sediment distribution patterns in the geological process modeling software. **b.** lithofacies classification using the property calculator tool in Petrel™.



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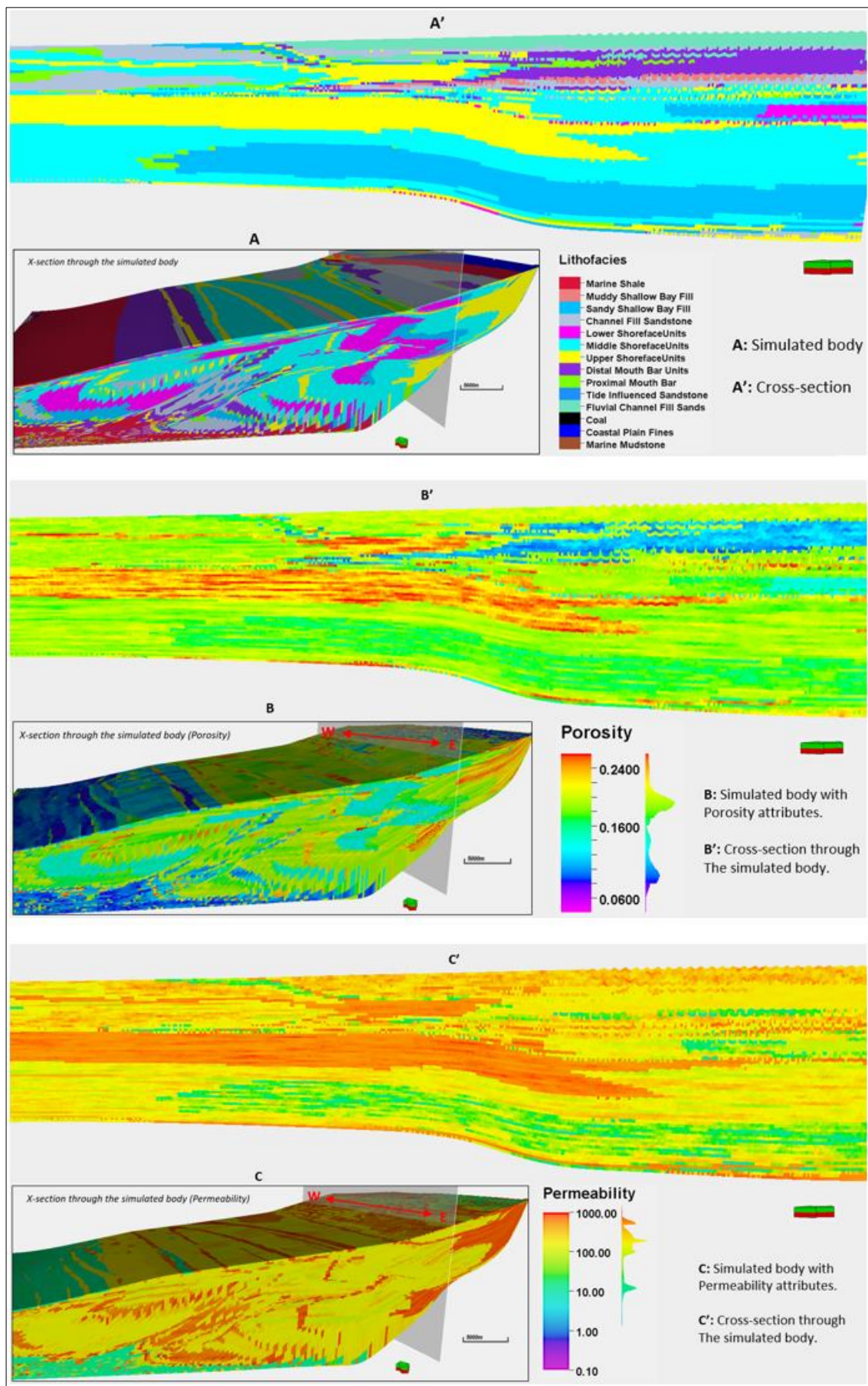
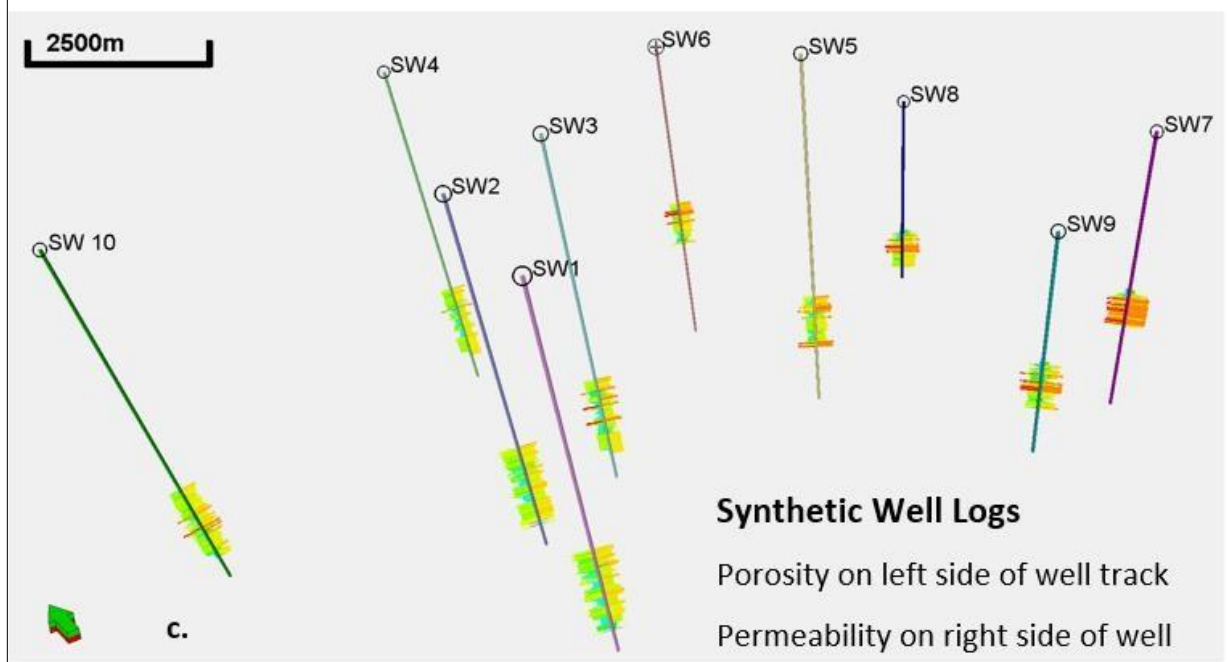
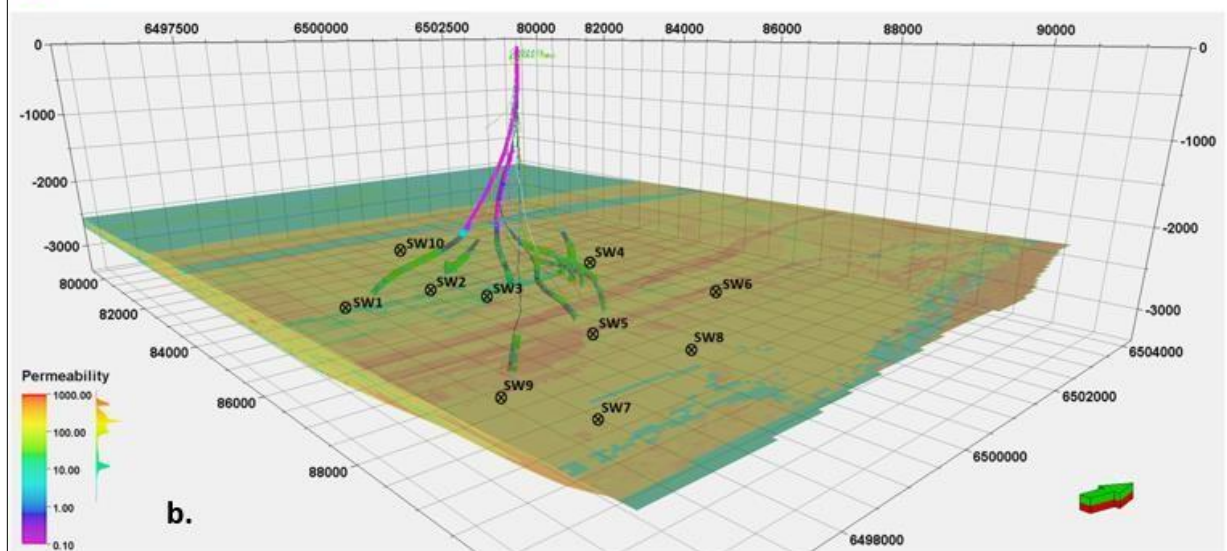
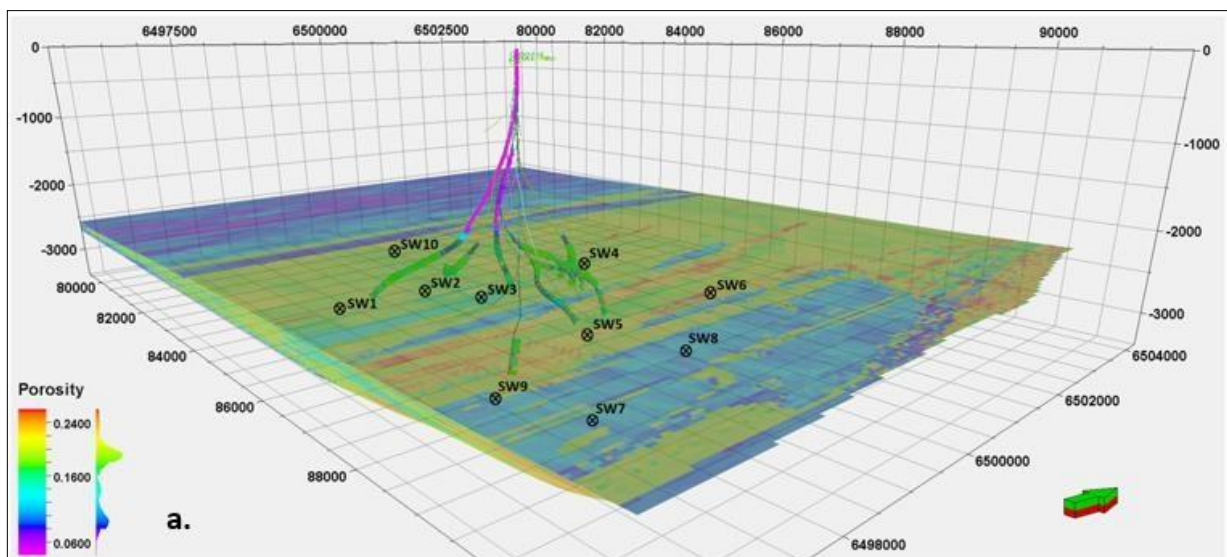


Fig 8. ~~Property~~ Lithofacies, porosity and permeability characterization in the stratigraphic ~~using~~ model through the property calculator tool in ~~Petrel~~ Petrel™. Also ~~showing, is~~ a cross-sectional view ~~through~~ of the ~~model~~ 3-D models.



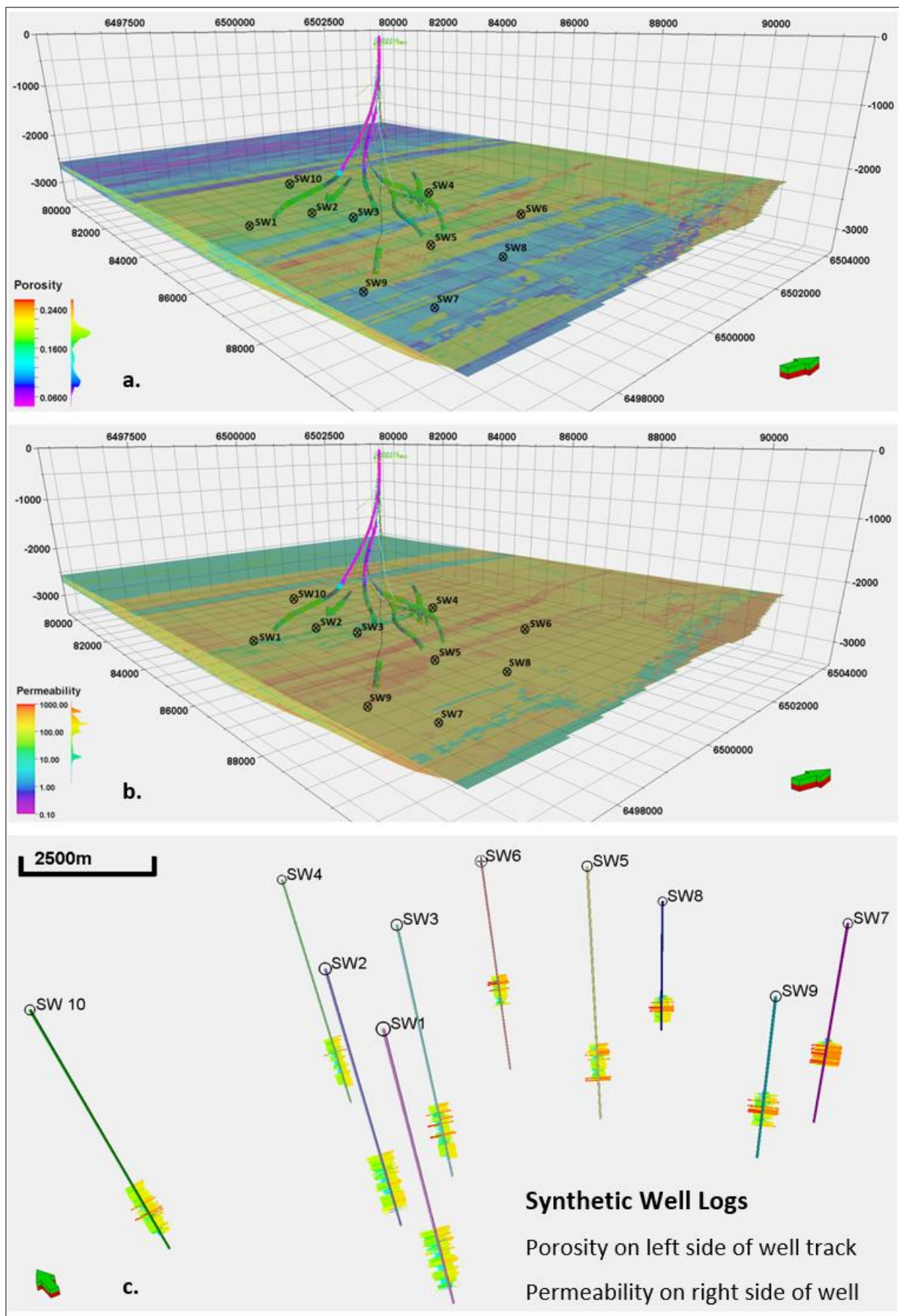
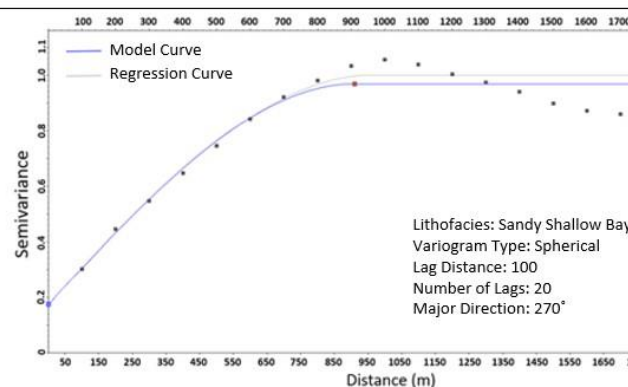
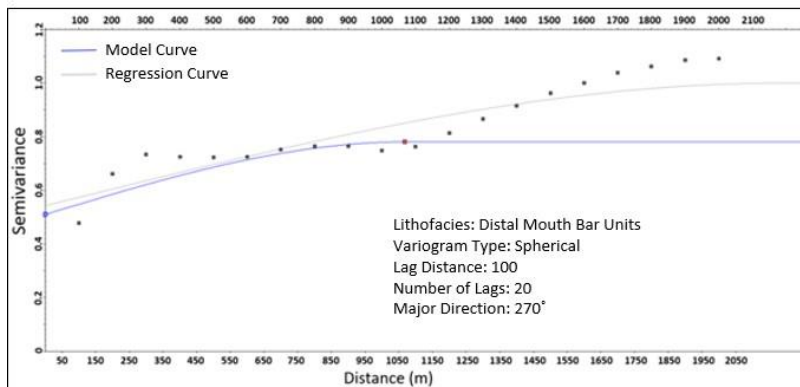
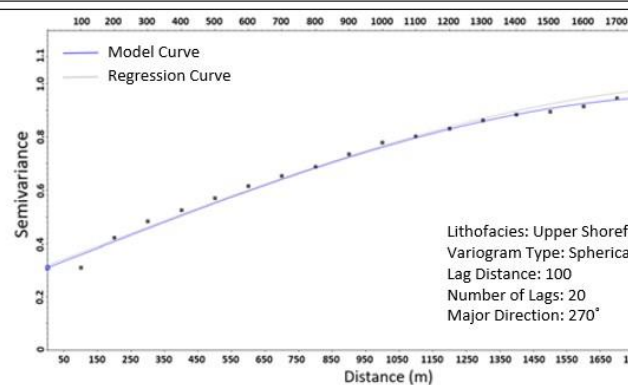
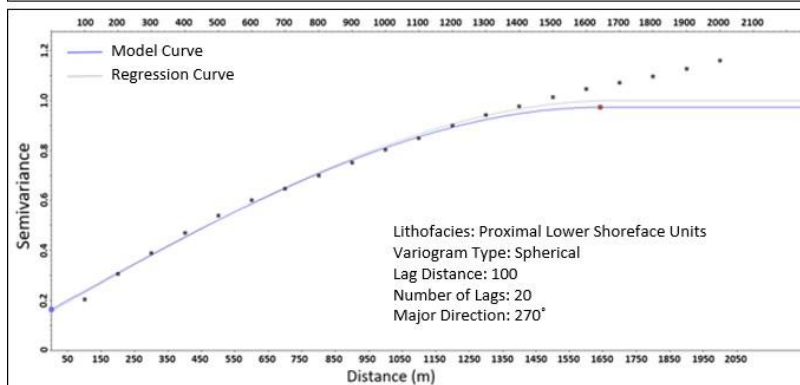
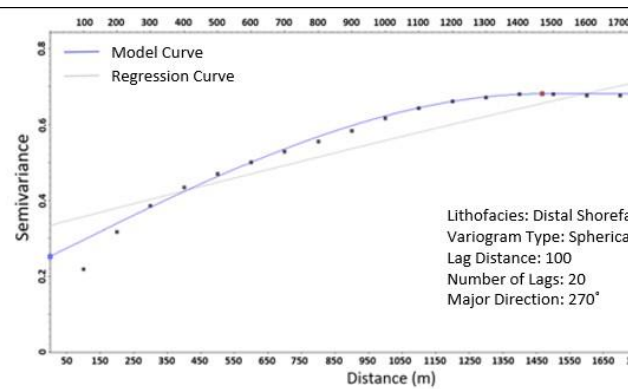
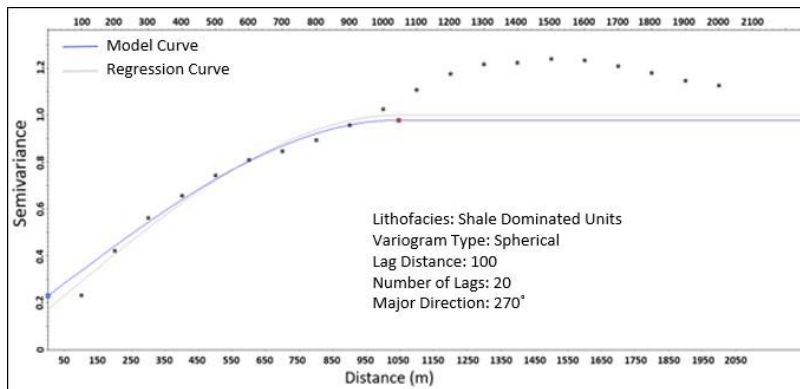


Fig 9. Synthetic wells ~~derived~~ from a forward stratigraphic-driven porosity and permeability ~~models.model~~. The average separation distance between the synthetic wells shown in Figure 9c is about 0.9 km apart (maximum and minimum separation distance of 1.3 km and 0.65 km, respectively).



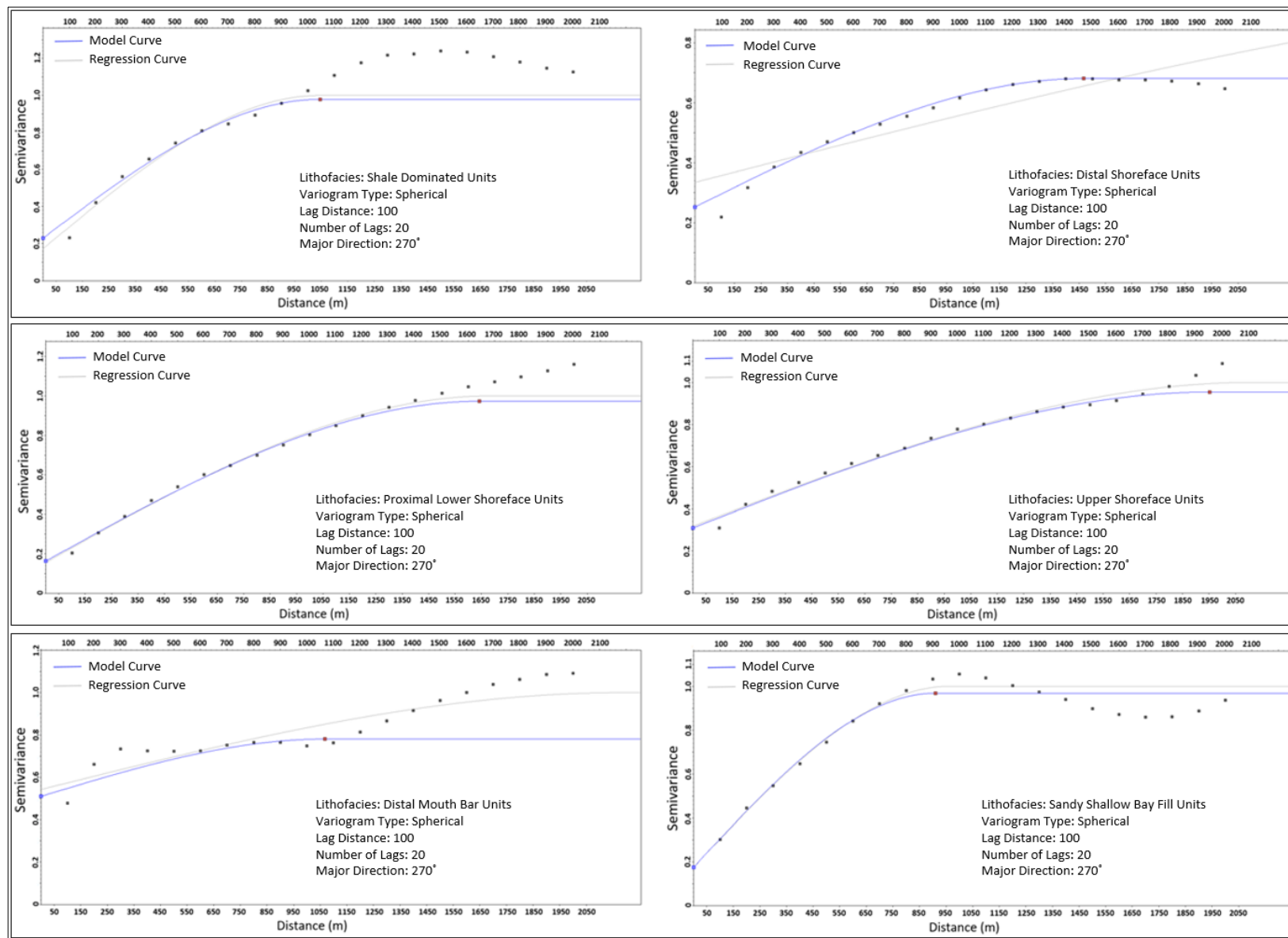
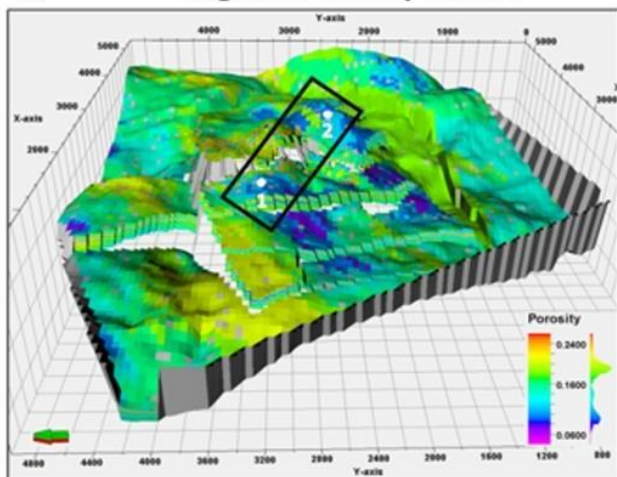
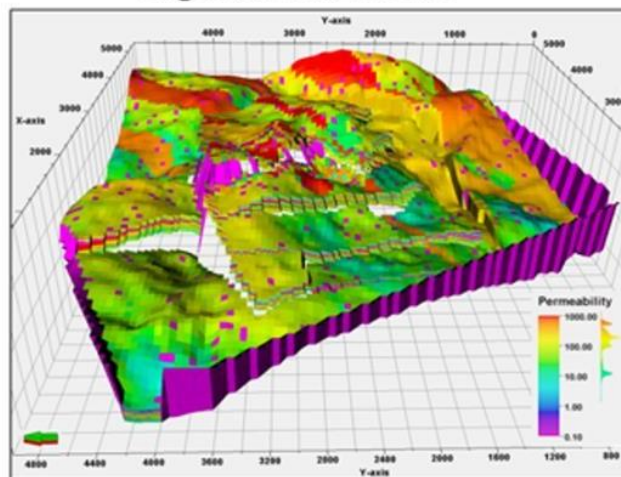


Fig 10. Variogram model of dominant lithofacies units ~~extracted~~ from the ~~FSM~~forward stratigraphic model. The points indicate the number of lags in the variogram. The distance between these lags is about 100 m. This figure shows the lags between sample pairs for calculating the variogram in the major direction (NE-SW) of the stratigraphic model.

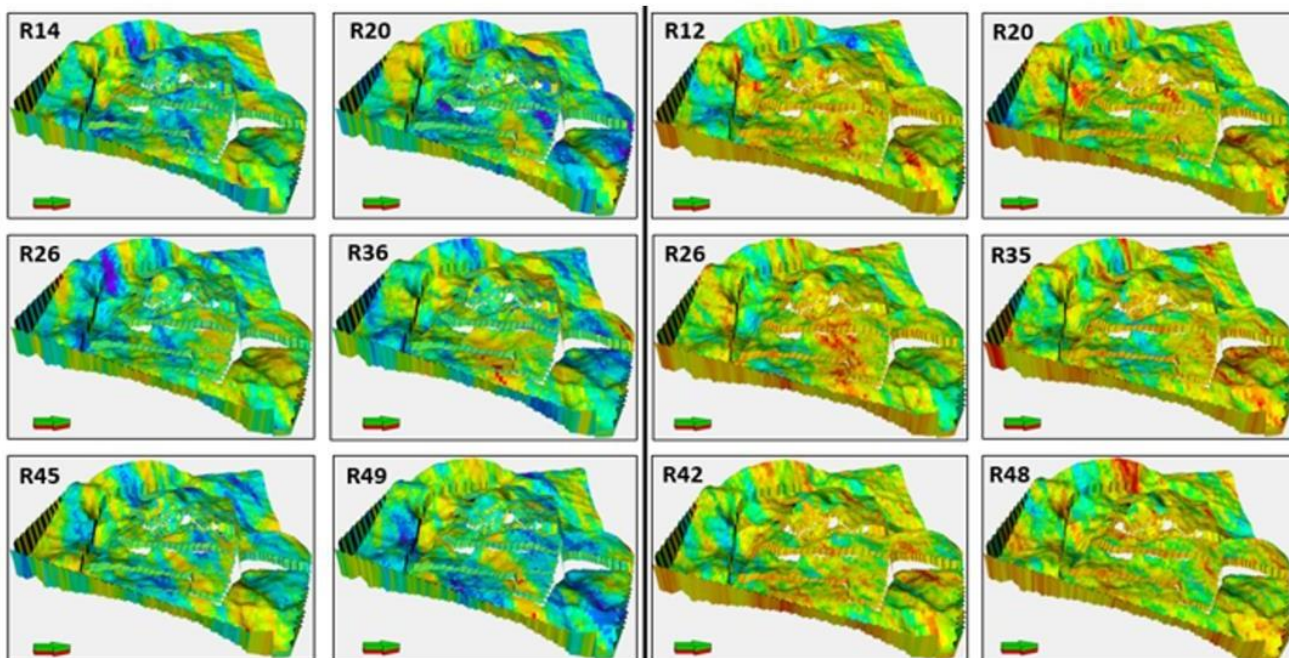
a. Original Porosity Model



Original PermZ Model

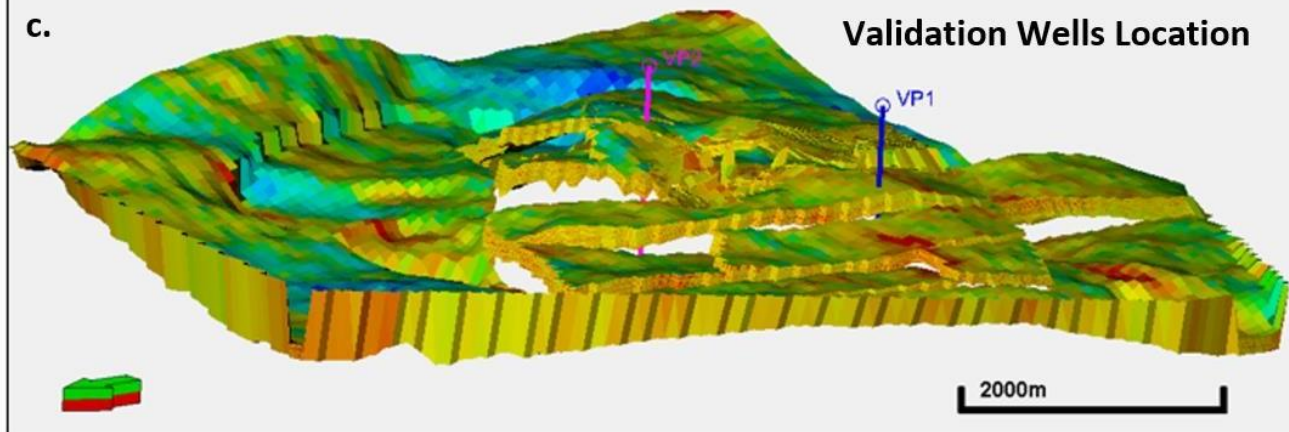


b. Forward Modeling-Based Porosity and Permeability Model Realizations



c.

Validation Wells Location



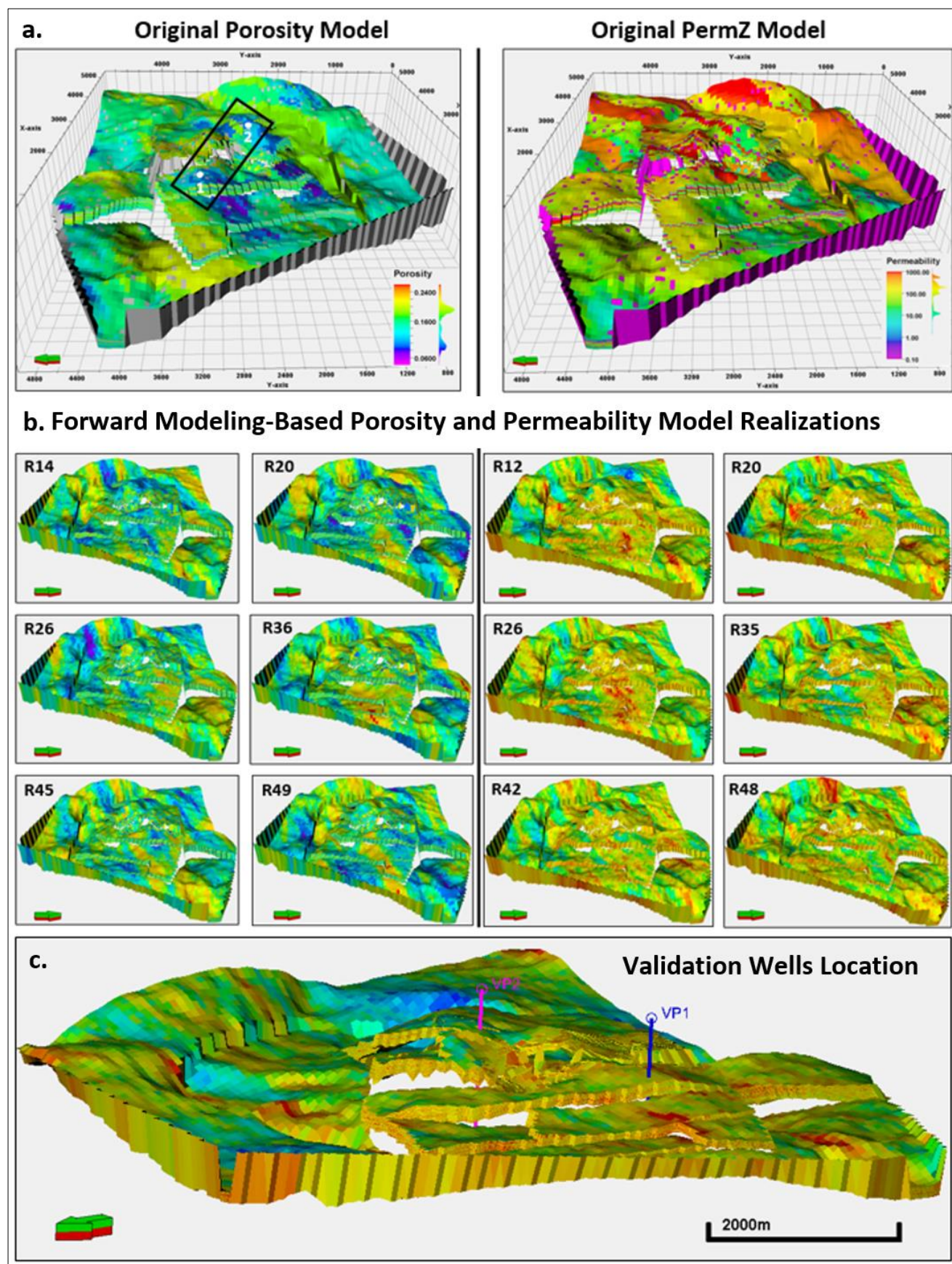
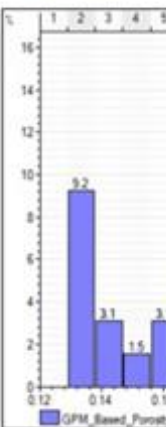
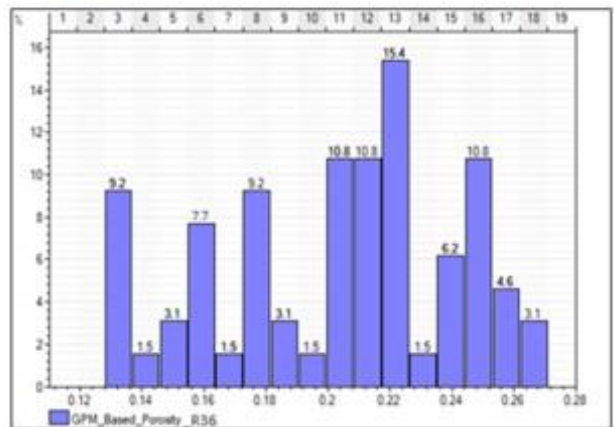
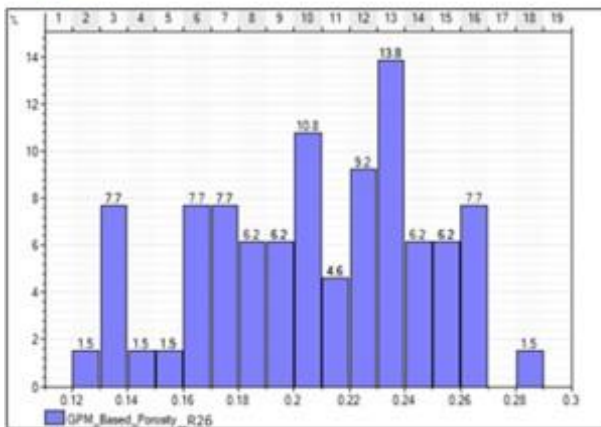
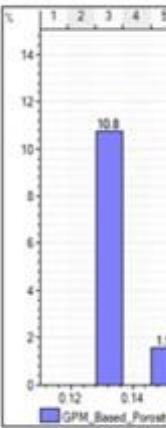
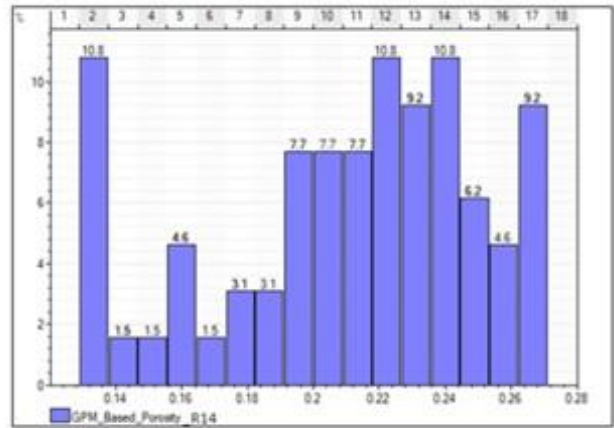
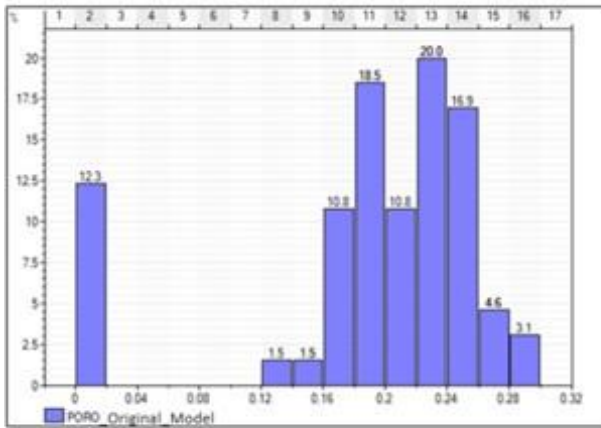


Fig 11. Comparing original Volve field model to the forward modeling-based models. Realizations 16, 20, 26, 36, 45, and 49 on the left half are porosity models, while realizations 12, 20, 26, 35, 42, and 48 on the right half show permeability models.

a. Validation Well 1



a. Validation Well 1

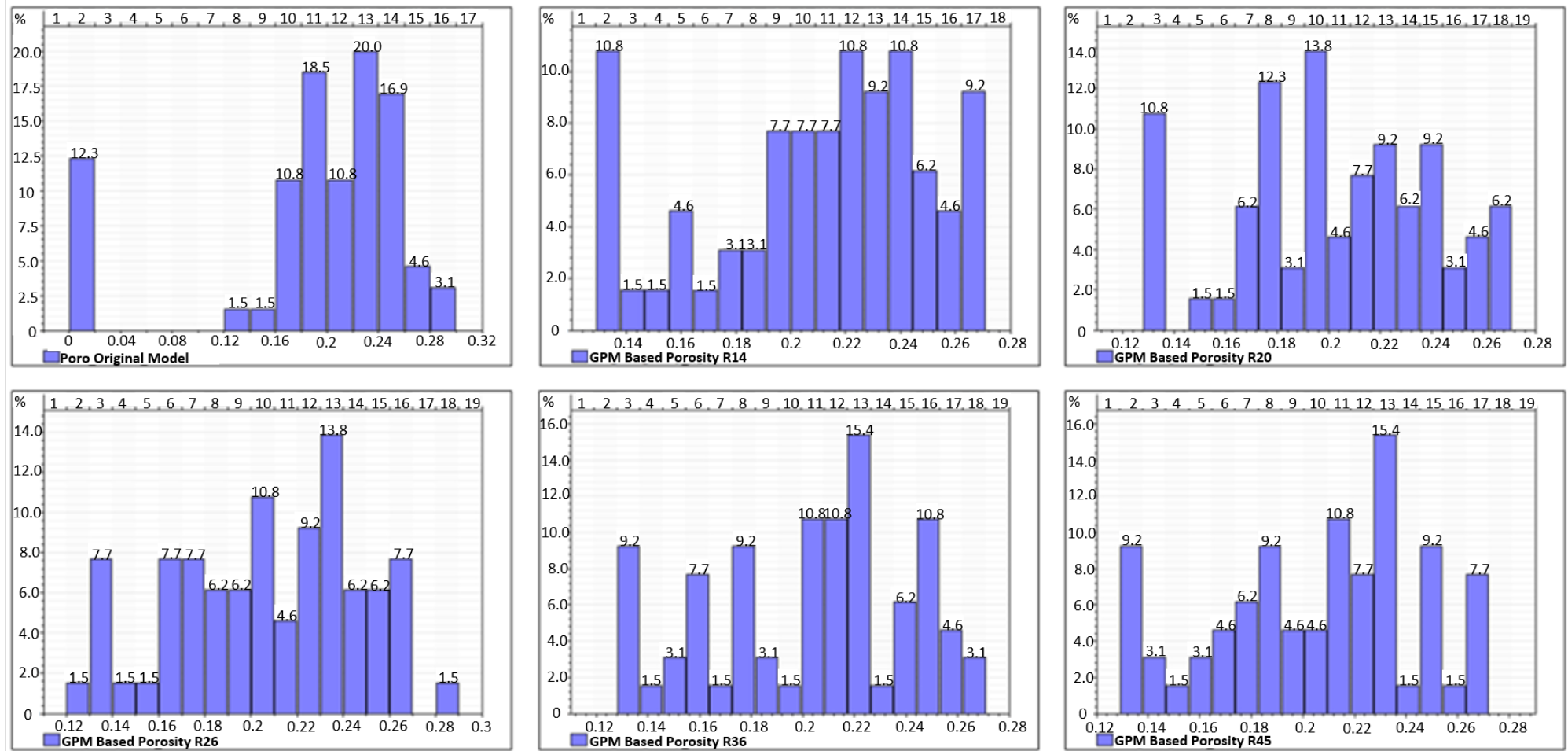
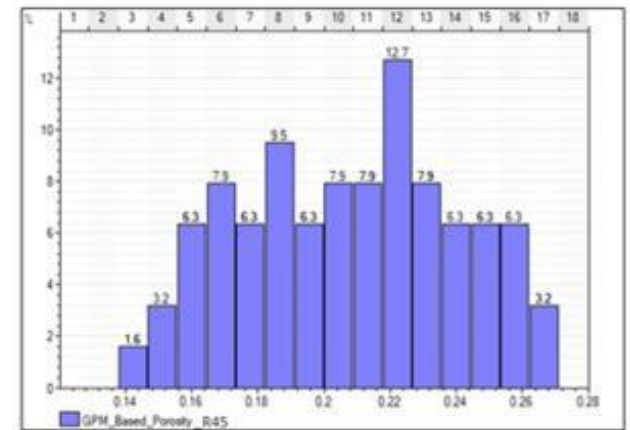
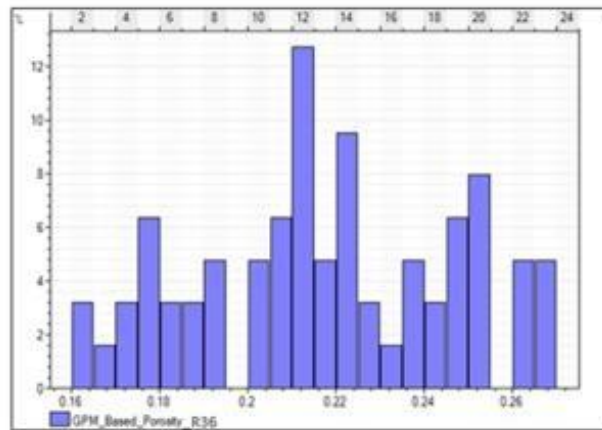
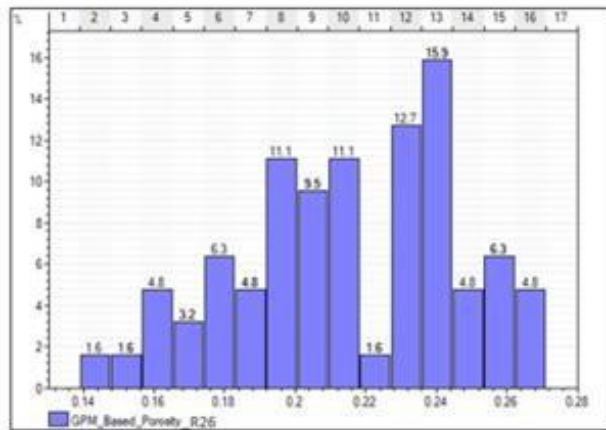
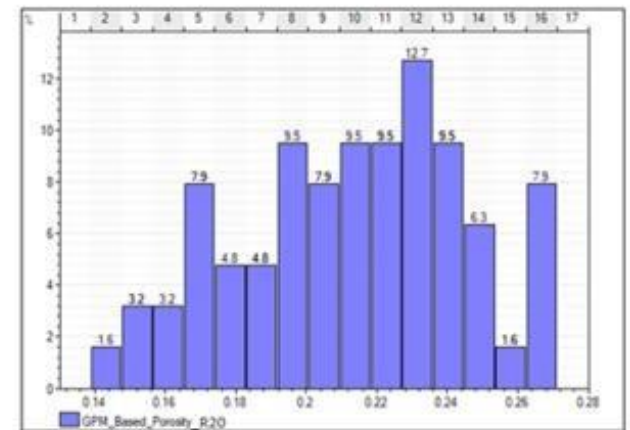
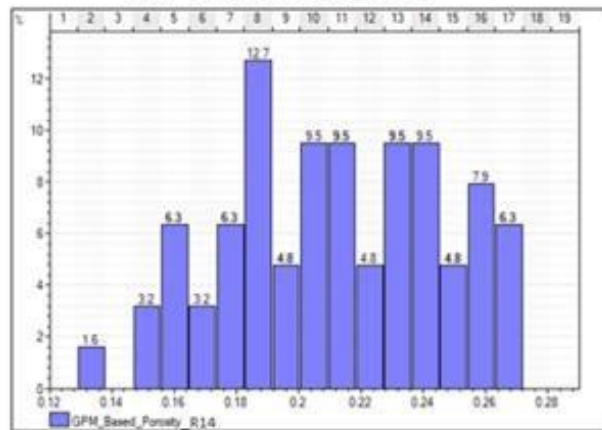
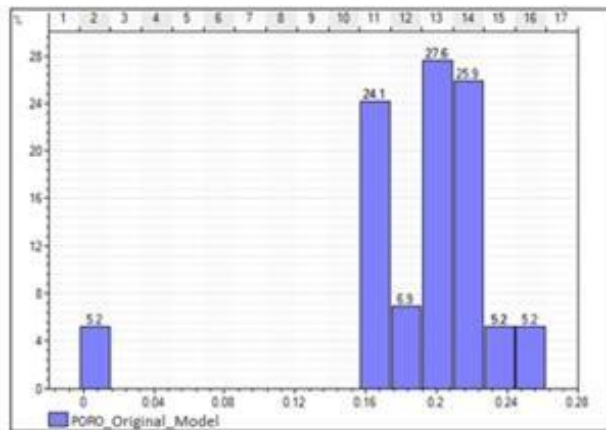


Figure 12a. Samples of Comparing porosity in validation Well 1 in five selected realizations , and how it compares to the samples original model at similar vertical interval in the original porosity and permeability models.

b. Validation Well 2



intervals.

b. Validation Well 2

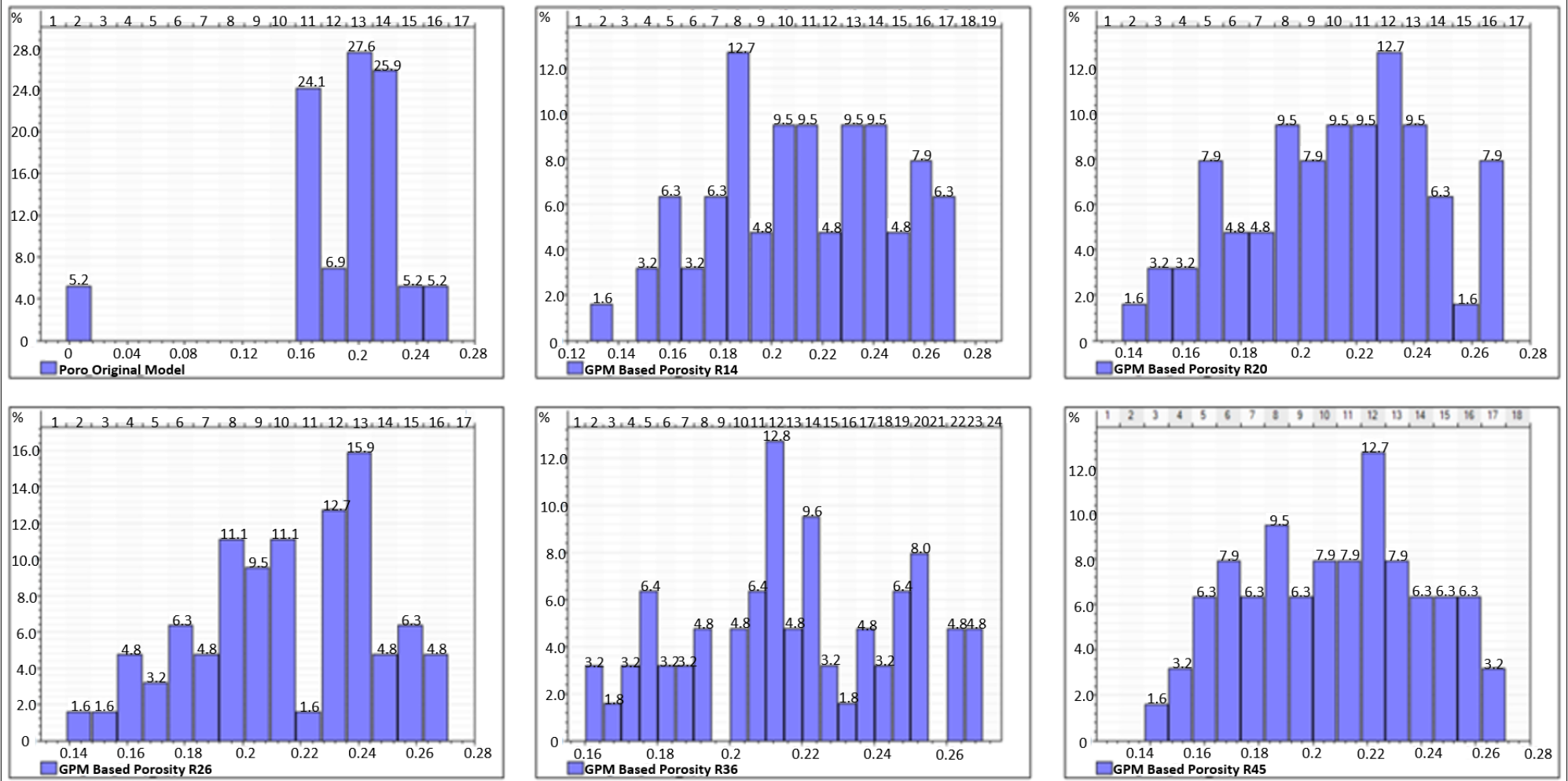


Figure 12b. Samples of Comparing porosity in validation Well 2 -in- five selected realizations , and how it compares to the samples original model at similar vertical interval in the original porosity and permeability models.

intervals.

Code	Facies	Description	Thickness (t); extent (l)	Wireline-log Attribute	Interpretation
A	A1	Parallel-laminated mudstone with occasional siltstone inputs. Monospecific pattern of disorder bivalves parallel to bedding.	t= 30-425 cm l= 6 to 29 km	GR= 41-308 API DT= 225-355 μsm^{-1} NPHI= 0.17-0.45 v/v RHOB= 2280-2820 gcm^{-3}	Restricted marine shale
	A2	Interbedded claystone and very fine-grained sandstone; non-parallel and wavy lamination. Scarcely bivalve shells oriented parallel to bedding.	t= 10-725 cm l= 8 km to 13 km	GR= 71-65 API DT= 189-268 μsm^{-1} NPHI=? RHOB= 2280-2820 gcm^{-3}	Muddy Shallow bay-fill
	A3	Fine to medium grained sandstone; moderately to well sorted grains. Wavy bedding, cross bedding, rare wave ripples	t= 60-370 cm l= <8 km	GR= 18-46 API DT= 199-314 μsm^{-1} NPHI= 0.07-0.52 v/v RHOB= 1690-2745 gcm^{-3}	Sandy shallow bay-fill
	A4	Coarse to fine-grained sandstones with alternating upward fining to coarsening trend. Moderately sorted grains. Sparse sedimentary structures.	t= 250-500 cm l= 1.8 km to 4.2 km	GR= 7-35 API DT= 175-230 μsm^{-1} NPHI= 0.038-0.146 v/v RHOB= 2280-2820 gcm^{-3}	Marine channel-fill sandstones
B	B1	Upward-coarsening siltstone to fine-grained moderate sorted sandstones, with shell debris, and quartz granules.	t= 30-480 cm l= <2 km	GR= 18-80 API DT= 168-291 μsm^{-1} NPHI= 0.038-0.191 v/v RHOB= 2322-2723 gcm^{-3}	Distal lower shoreface
	B2	Very fine-fine grained, moderate to well sorted sandstone. Fine grained carbonaceous laminae, typically low angle cross beds.	t= 130-440 cm l= 1.7 km – 8 km	GR= 20-56 API DT= 179-277 μsm^{-1} NPHI= 0.048-0.168 v/v RHOB= 2314-2696 gcm^{-3}	Proximal lower shoreface
	B3	Coarsening upward, cross laminated, fine to medium grained, well sorted sandstone; consist carbonaceous fragments	t= 425-800 cm l= 1.7 km – 8 km	GR= 15-25 API DT= 250-275 μsm^{-1} NPHI= 0.09-0.113 v/v RHOB= 2271-2342 gcm^{-3}	Upper Shoreface
C	C1	Highly bioturbated siltstone to very fine sandstones, which has beds of rounded granules	t= 175-1010 cm l= 7.2 km – 19.6 km	GR= 20-80 API DT= 230-260 μsm^{-1} NPHI= 0.08-0.169 v/v RHOB= 2327-2521 gcm^{-3}	Distal mouth bar
	C2	Very fine to fine grained sandstones; low angle cross-bedding.	t= 290-775 cm l= < 5 km	GR= 12-58 API DT= 167-397 μsm^{-1} NPHI= 0.05-0.595 v/v RHOB= 1612-2705 gcm^{-3}	Proximal mouth bar

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Table 1 Lithofacies-associations in the Hugin formation, Volve Field (after Kieft et al. 2011).

Code	Facies	Description	Thickness (t); Extent (l)	Wireline-log Attribute	Interpretation
A	A1	Parallel-laminated mudstone with occasional siltstone inputs. Monospecific pattern of disorder bivalves parallel to bedding.	t = 30 - 425 cm l = 6 - 29 km	GR = 41 - 308 API DT = 225 - 355 μsm^{-1} NPHI = 0.17 - 0.45 v/v RHOB = 2280 - 2820 gcm^{-1}	Restricted marine shale
	A2	Inter-bedded claystone and very fine-grained sandstone; non-parallel and wavy lamination. Scarcely bivalve shells oriented parallel to bedding.	t = 10 - 725 cm l = 8 - 13 km	GR = 17 - 65 API DT = 189 - 268 μsm^{-1} NPHI = ? RHOB = 2280 - 2820 gcm^{-1}	Muddy hallow bay fill
	A3	Fine to medium grained sandstone; moderately to well sorted grain. Wavy bedding, cross bedding, rare wave ripples.	t = 60 - 370 cm l = 1 - 8 km	GR = 18 - 46 API DT = 199 - 268 μsm^{-1} NPHI = 0.07 - 0.52 v/v RHOB = 1690 - 2745 gcm^{-1}	Sandy shallow bay fill
	A4	Parallel-laminated mudstone with occasional siltstone inputs. Monospecific pattern of disorder bivalves parallel to bedding.	t = 30 - 425 cm l = 6 - 29 km	GR = 7 - 35 API DT = 175 - 230 μsm^{-1} NPHI = 0.04 - 0.15 v/v RHOB = 2280 - 2820 gcm^{-1}	Marine channel fill sandstone
B	B1	Upward coarsening siltstone to fine-grained; moderately sorted sandstone. Shell debris and quartz granules.	t = 30 - 480 cm l = 1 - 2 km	GR = 18 - 80 API DT = 168 - 291 μsm^{-1} NPHI = 0.04 - 0.191 v/v RHOB = 2322 - 2723 gcm^{-1}	Distal lower shoreface
	B2	Very fine-fine grained sandstone. Moderate to well sorted; fine grained carbonaceous laminae, typically low angle cross beds.	t = 130 - 440 cm l = 1.7 - 12 km	GR = 20 - 56 API DT = 179 - 277 μsm^{-1} NPHI = 0.05 - 0.168 v/v RHOB = 2314 - 2696 gcm^{-1}	Proximal lower shoreface
	B3	Coarsening upward, cross laminated, fine to medium grained sandstone; consist of carbonaceous fragments.	t = 425 - 800 cm l = 1.7 - 8 km	GR = 15 - 25 API DT = 250 - 275 μsm^{-1} NPHI = 0.09 - 0.113 v/v RHOB = 2271 - 2342 gcm^{-1}	Upper shoreface
C	C1	Highly bioturbated siltstone to very fine sandstone, with beds of rounded granules.	t = 175 - 1010 cm l = 7.2 - 19.6 km	GR = 20 - 80 API DT = 230 - 260 μsm^{-1} NPHI = 0.08 - 0.169 v/v RHOB = 2327 - 2521 gcm^{-1}	Distal mouth bar
	C2	Very fine to fine grained sandstone, low angle cross bedding.	t = 290 - 775 cm l = 1 - 5 km	GR = 12 - 58 API DT = 167 - 397 μsm^{-1} NPHI = 0.05 - 0.595 v/v RHOB = 1612 - 2705 gcm^{-1}	Proximal mouth bar
D	D1	Fining upward coarse to fine grained sandstone. Stacked fining upward beds with rare coarse grained stringers.	t = 740 - 820 cm l = 1 - 2 km	GR = 8 - 134 API DT = 235 - 335 μsm^{-1} NPHI = 0.14 - 0.46 v/v RHOB = 2284 - 2570 gcm^{-1}	Tidal influenced fluvial channel fill sandstone
	D2	Fining upward coarse to medium grained sandstone. Carbonaceous laminae and fragments. Sharp and cohesive contact at base of bed.	t = 580 cm l = < 2 km	GR = 9 - 34 API DT = 241 - 297 μsm^{-1} NPHI = 0.14 - 0.289 v/v RHOB = 2168 - 2447 gcm^{-1}	fluvial channel fill sandstone
E	E1	Coal and carbonaceous shale. Basal contact typically parallel, although maybe undulose.	t = 30 - 520 cm l = 6 - 19.6 km	GR = 8 - 56 API DT = 313 - 427 μsm^{-1} NPHI = 0.24 - 0.529 v/v RHOB = 1930 - 2225 gcm^{-1}	Coal
	E2	Alternating dark grey mudstone/claystone and siltstone to very fine grained sandstone. Wavy to non-parallel lamination.	t = 60 cm l = < 2 km	GR = 32 - 60 API DT = 358 - 415 μsm^{-1} NPHI = 0.43 - 0.49 v/v RHOB = 1994 - 2148 gcm^{-1}	Coastal plain fines
F	F	Mudstone with rare siltstone beds. Parallel lamination, soft sediment deformation developed locally on top of beds.	t = section tot completely penetrated l = 1.7 - 36.7 km	GR = 4 - 134 API DT = 187 - 450 μsm^{-1} NPHI = 0.114 - 0.618 v/v RHOB = 1730 - 2925 gcm^{-1}	Open marine shale

Table 2. Input parameters ~~applied in running the~~ for forward stratigraphic simulations in GPM™

		Initial Conditions- GPM Input Parameters												
		Simulation Duration	Sediment Type Proportion (%)				Avg. Water Velocity	Avg. Sediment Velocity	Erodibility	Diffusion Coefficient	Avg. Sea Level	Turbidite Event Interval	Steady Flow Iteration	Sediment Movement
GPM Scenarios (GS)		(Ma– 0a) Years	Sand (Coarse)	Sand (Fine)	Silt	Clay	(m/a)	(m/a)			Interval (m)	(/years)	(/hrs)	Coefficient
	S1	0.02 – 0	25	25	25	25	0.11	0.03	0.35	0.11	30	2500	10	0.001
	S2	0.25 – 0	25	25	25	25	0.15	0.03	0.45	0.15	70	1000	15	0.012
	S3	0.5 – 0	25	25	25	25	0.11	0.02	0.55	0.11	120	1000	20	0.012
	S4	0.7 – 0.05	25	25	25	25	0.08	0.02	0.35	0.08	100	500	25	0.0011
	S5	1.5 – 0	15	35	30	20	0.15	0.04	0.50	0.15	80	5000	20	0.001
	S6	3.0 – 0	50	25	15	10	0.13	0.04	0.50	0.13	70	5000	30	0.0012
	S7	3.5 – 0	50	25	15	10	0.11	0.04	0.50	0.11	70	10000	15	0.001
	S8	4.0 – 0	50	25	15	10	0.13	0.04	0.50	0.13	90	5000	20	0.0015
	S9	4.5 – 0	15	45	25	15	0.1	0.02	0.45	0.1	50	10000	30	0.0012
	S10	5.0 – 0	15	45	25	15	0.12	0.02	0.45	0.12	55	10000	35	0.0013
	S11	5.5 - 0	15	45	25	15	0.12	0.02	0.45	0.12	40	5000	40	0.0013
	S12	6.0 – 0	15	45	25	15	0.1	0.02	0.45	0.1	60	10000	35	0.0011
	S13	6.5 – 0	10	25	55	10	0.13	0.03	0.48	0.13	100	20000	50	0.0010
	S14	7.0 – 0	10	25	55	10	0.16	0.03	0.48	0.16	40	20000	45	0.0011
	S15	7.5 – 0	10	25	55	10	0.13	0.03	0.48	0.13	40	20000	40	0.0012
	S16	8.0 – 0	10	25	55	10	0.15	0.03	0.48	0.15	30	10000	30	0.0010
	S17	8.5 – 0	10	25	45	20	0.14	0.02	0.45	0.14	50	50000	50	0.0010
	S18	9.0 – 0	30	30	18	22	0.13	0.02	0.52	0.13	60	25000	35	0.0012
	S19	9.5 – 0	30	40	12	18	0.12	0.02	0.55	0.12	55	25000	20	0.0013
	S20	10.0 - 0	30	42	18	10	0.11	0.01	0.40	0.11	50	5000	15	0.0011
Sediment Property														
	Sediment Type	Diameter	Density	Initial Porosity	Initial Permeability	Compacted Porosity	Compaction	Compacted Permeability	Erodibility					
	Coarse Grained Sand	1.0 mm	2.70 g/cm ³	0.21 m ³ /m ³	500 mD	0.25 m ³ /m ³	5000 KPa	50 mD	0.6					
	Fine Grained Sand	0.1 mm	2.70 g/cm ³	0.3 m ³ /m ³	100 mD	0.15 m ³ /m ³	2500 KPa	5 mD	0.45					
	Silt	0.01 mm	2.65 g/cm ³	0.38 m ³ /m ³	50 mD	0.12 m ³ /m ³	1200 KPa	2 mD	0.3					
	Clay	0.001 mm	2.65 g/cm ³	0.48 m ³ /m ³	5 mD	0.05 m ³ /m ³	500 KPa	0.1 mD	0.15					

		Initial Conditions- GPM Input Parameters												
		Simulation Duration	Sediment Type Proportion (%)				Avg. Water Velocity	Avg. Sediment Velocity	Erodibility	Diffusion Coefficient	Avg. Sea Level	Turbidite Event Interval	Steady Flow Iteration	Sediment Movement
GPM Scenarios (GS)		(Ma– 0a) Years	Sand (Coarse)	Sand (Fine)	Silt	Clay	(m/a)	(m/a)			Interval (m)	(/years)	(/hrs)	Coefficient
	S1	0.02 – 0	25	25	25	25	0.11	0.03	0.35	0.11	30	2500	10	0.001
	S2	0.25 – 0	25	25	25	25	0.15	0.03	0.45	0.15	70	1000	15	0.012
	S3	0.5 – 0	25	25	25	25	0.11	0.02	0.55	0.11	120	1000	20	0.012
	S4	0.7 – 0.05	25	25	25	25	0.08	0.02	0.35	0.08	100	500	25	0.0011
	S5	1.5 – 0	15	35	30	20	0.15	0.04	0.50	0.15	80	5000	20	0.001
	S6	3.0 – 0	50	25	15	10	0.13	0.04	0.50	0.13	70	5000	30	0.0012
	S7	3.5 – 0	50	25	15	10	0.11	0.04	0.50	0.11	70	10000	15	0.001
	S8	4.0 – 0	50	25	15	10	0.13	0.04	0.50	0.13	90	5000	20	0.0015
	S9	4.5 – 0	15	45	25	15	0.1	0.02	0.45	0.1	50	10000	30	0.0012
	S10	5.0 – 0	15	45	25	15	0.12	0.02	0.45	0.12	55	10000	35	0.0013
	S11	5.5 – 0	15	45	25	15	0.12	0.02	0.45	0.12	40	5000	40	0.0013
	S12	6.0 – 0	15	45	25	15	0.1	0.02	0.45	0.1	60	10000	35	0.0011
	S13	6.5 – 0	10	25	55	10	0.13	0.03	0.48	0.13	100	20000	50	0.0010
	S14	7.0 – 0	10	25	55	10	0.16	0.03	0.48	0.16	40	20000	45	0.0011
	S15	7.5 – 0	10	25	55	10	0.13	0.03	0.48	0.13	40	20000	40	0.0012
	S16	8.0 – 0	10	25	55	10	0.15	0.03	0.48	0.15	30	10000	30	0.0010
	S17	8.5 – 0	10	25	45	20	0.14	0.02	0.45	0.14	50	50000	50	0.0010
	S18	9.0 – 0	30	30	18	22	0.13	0.02	0.52	0.13	60	25000	35	0.0012
	S19	9.5 – 0	30	40	12	18	0.12	0.02	0.55	0.12	55	25000	20	0.0013
	S20	10.0 – 0	30	42	18	10	0.11	0.01	0.40	0.11	50	5000	15	0.0011
		Sediment Property												
	Sediment Type	Diameter	Density	Initial Porosity	Initial Permeability	Compacted Porosity	Compaction	Compacted Permeability	Erodibility					
	Coarse Grained Sand	1.0 mm	2.70 g/cm ³	0.21 m ³ /m ³	500 mD	0.25 m ³ /m ³	5000 KPa	50 mD	0.6					
	Fine Grained Sand	0.1 mm	2.70 g/cm ³	0.3 m ³ /m ³	100 mD	0.15 m ³ /m ³	2500 KPa	5 mD	0.45					
	Silt	0.01 mm	2.65 g/cm ³	0.38 m ³ /m ³	50 mD	0.12 m ³ /m ³	1200 KPa	2 mD	0.3					
	Clay	0.001 mm	2.65 g/cm ³	0.48 m ³ /m ³	5 mD	0.05 m ³ /m ³	500 KPa	0.1 mD	0.15					

Table 3. Lithofacies classification in the forward stratigraphic model; ~~showing the command used~~ in the property calculator tool in Petrel™.

Lithofacies Classification		
Facies Code	Lithofacies	Command Used in Petrel's Property Calculator
0	Marine Shale	If(Sand_fine>=0.19 And Sand_fine<=0.21 Or Silt>=0.19 And Silt<=0.2 Or Clay>=0.2 And Clay<=0.21 Or Depth_of_deposition>=-82 And Depth_of_deposition<=-78)
1	Muddy Shallow Bay Fill	If(Sand_fine>=0.36 And Sand_fine<=0.38 Or Silt>=0.18 And Silt<=0.2 Or Clay>0.18 And Clay<=0.19 Or Depth_of_deposition>=-30 And Depth_of_deposition<=-20)
2	Sandy Shallow Bay Fill	If(Sand_coarse>=0.65 And Sand_coarse<=0.73 Or Sand_fine>=0.18 And Sand_fine<=0.22 Or Silt>=0.18 And Silt<=0.2 Or Clay>=0.17 And Clay<=0.18 Or Depth_of_deposition>=-3 And Depth_of_deposition<=0)
3	Channel Fill Sandstone	If(Sand_coarse>=0.5 And Sand_coarse<=0.68 Or Sand_fine>=0.23 And Sand_fine<=0.25 Or Silt>=0.17 And Silt<=0.18 Or Depth_of_deposition>=0 And Depth_of_deposition<=2)
4	Lower Shoreface Units	If(Sand_coarse>=0.19 And Sand_coarse<=0.31 Or Sand_fine>=0.19 And Sand_fine<=0.24 Or Silt>=0.4 And Silt<=0.48 Or Clay>=0.19 And Clay<=0.31 Or Depth_of_deposition>=-83 And Depth_of_deposition<=50)
5	Middle Shoreface Units	If(Sand_coarse>=0.32 And Sand_coarse<=0.53 Or Sand_fine>=0.25 And Sand_fine<=0.32 Or Silt>=0.26 And Silt<=0.32 Or Clay>=0.19 And Clay<=0.21 Or Depth_of_deposition>=-38 And Depth_of_deposition<=-12)
6	Upper Shoreface Units	If(Sand_coarse>=0.53 And Sand_coarse<=0.72 Or Sand_fine>=0.28 And Sand_fine<=0.33 Or Silt>=0.16 And Silt<=0.21 Or Depth_of_deposition>=-10 And Depth_of_deposition<=6)
7	Distal Mouth Bar Units	If(Sand_fine>=0.23 And Sand_fine<=0.27 Or Silt>=0.38 And Silt<=0.43 Or Clay>=0.19 And Clay<=0.21 Or Depth_of_deposition>=-95 And Depth_of_deposition<=-80)
8	Proximal Mouth Bar Units	If(Sand_coarse>=0.53 And Sand_coarse<=0.71 Or Sand_fine>=0.27 And Sand_fine<=0.32 Or Silt>=0.16 And Silt<=0.21 Or Clay>=0.06 And Clay<=0.07 Or Depth_of_deposition>=-30 And Depth_of_deposition<=-27)
9	Tide Influenced Sandstones	If(Sand_coarse>=0.53 And Sand_coarse<=0.71 Or Sand_fine>=0.26 And Sand_fine<=0.31 Or Silt>=0.35 And Silt<=0.41 Or Depth_of_deposition>=-5 And Depth_of_deposition<=1)
10	Fluvial Channel Sandstones	If(Sand_coarse>=0.54 And Sand_coarse<=0.56 Or Sand_fine>=0.27 And Sand_fine<=0.29 Or Silt>=0.19 And Silt<=0.21 Or Depth_of_deposition>=-2 And Depth_of_deposition<=2)
11	Coal	Estimated as background attribute
12	Coastal plain fines	If(Silt>=0.31 And Silt<=0.43 Or Clay>=0.31 And Clay<=0.35 Or Depositional_depth>=-100 And Depositional_depth<=-40)
13	Marine Mudstone	If(Sand_fine>=0.36 And Sand_fine<=0.38 Or Silt>=0.4 And Silt<=0.52 Or Clay>=0.45 And Clay<=0.78 Or Depth_of_deposition>=-105 And Depth_of_deposition<=-90)

Lithofacies Classification		
Facies Code	Lithofacies	Command Used in Petrel's Property Calculator
0	Marine Shale	If(Sand_fine>=0.19 And Sand_fine<=0.21 Or Silt>=0.19 And Silt<=0.2 Or Clay>=0.2 And Clay<=0.21 Or Depth_of_deposition>=-82 And Depth_of_deposition<=-78)
1	Muddy Shallow Bay Fill	If(Sand_fine>=0.36 And Sand_fine<=0.38 Or Silt>=0.18 And Silt<=0.2 Or Clay>0.18 And Clay<=0.19 Or Depth_of_deposition>=-30 And Depth_of_deposition<=-20)
2	Sandy Shallow Bay Fill	If(Sand_coarse>=0.65 And Sand_coarse<=0.73 Or Sand_fine>=0.18 And Sand_fine<=0.22 Or Silt>=0.18 And Silt<=0.2 Or Clay>=0.17 And Clay<=0.18 Or Depth_of_deposition>=-3 And Depth_of_deposition<=0)
3	Channel Fill Sandstone	If(Sand_coarse>=0.5 And Sand_coarse<=0.68 Or Sand_fine>=0.23 And Sand_fine<=0.25 Or Silt>=0.17 And Silt<=0.18 Or Depth_of_deposition>=0 And Depth_of_deposition<=2)
4	Lower Shoreface Units	If(Sand_coarse>=0.19 And Sand_coarse<=0.31 Or Sand_fine>=0.19 And Sand_fine<=0.24 Or Silt>=0.4 And Silt<=0.48 Or Clay>=0.19 And Clay<=0.31 Or Depth_of_deposition>=-83 And Depth_of_deposition<=50)
5	Middle Shoreface Units	If(Sand_coarse>=0.32 And Sand_coarse<=0.53 Or Sand_fine>=0.25 And Sand_fine<=0.32 Or Silt>=0.26 And Silt<=0.32 Or Clay>=0.19 And Clay<=0.21 Or Depth_of_deposition>=-38 And Depth_of_deposition<=-12)
6	Upper Shoreface Units	If(Sand_coarse>=0.53 And Sand_coarse<=0.72 Or Sand_fine>=0.28 And Sand_fine<=0.33 Or Silt>=0.16 And Silt<=0.21 Or Depth_of_deposition>=-10 And Depth_of_deposition<=6)
7	Distal Mouth Bar Units	If(Sand_fine>=0.23 And Sand_fine<=0.27 Or Silt>=0.38 And Silt<=0.43 Or Clay>=0.19 And Clay<=0.21 Or Depth_of_deposition>=-95 And Depth_of_deposition<=-80)
8	Proximal Mouth Bar Units	If(Sand_coarse>=0.53 And Sand_coarse<=0.71 Or Sand_fine>=0.27 And Sand_fine<=0.32 Or Silt>=0.16 And Silt<=0.21 Or Clay>=0.06 And Clay<=0.07 Or Depth_of_deposition>=-30 And Depth_of_deposition<=-27)
9	Tide Influenced Sandstones	If(Sand_coarse>=0.53 And Sand_coarse<=0.71 Or Sand_fine>=0.26 And Sand_fine<=0.31 Or Silt>=0.35 And Silt<=0.41 Or Depth_of_deposition>=-5 And Depth_of_deposition<=1)
10	Fluvial Channel Sandstones	If(Sand_coarse>=0.54 And Sand_coarse<=0.56 Or Sand_fine>=0.27 And Sand_fine<=0.29 Or Silt>=0.19 And Silt<=0.21 Or Depth_of_deposition>=-2 And Depth_of_deposition<=2)
11	Coal	Estimated as background attribute
12	Coastal plain fines	If(Silt>=0.31 And Silt<=0.43 Or Clay>=0.31 And Clay<=0.35 Or Depositional_depth>=-100 And Depositional_depth<=-40)
13	Marine Mudstone	If(Sand_fine>=0.36 And Sand_fine<=0.38 Or Silt>=0.4 And Silt<=0.52 Or Clay>=0.45 And Clay<=0.78 Or Depth_of_deposition>=-105 And Depth_of_deposition<=-90)

Table 4. Porosity and Permeability ~~estimate in identified~~ estimates of lithofacies packages in the model area.

Code	Lithofacies	Average NPHI	Density Porosity	Estimated Porosity	KLOGH (mD)
0	Marine Shale	0.17 - 0.45	0.1	0.08 - 0.11	10.02 - 16.1
1	Muddy Shallow Bay Fill	0.17 - 0.42	0.1	0.08 - 0.13	23.85 - 102.3
2	Sandy Shallow Bay Fill	0.07 - 0.52	0.25	0.16 - 0.25	100.0 - 398.7
3	Channel Fill Sandstone	0.04 - 0.15	0.30	0.18 - 0.22	400.01 - 889.7
4	Distal Lower Shoreface	0.04 - 0.19	0.29	0.1 - 0.23	120.5 - 170.3
5	Proximal Shoreface	0.05 - 0.17	0.31	0.17 - 0.24	80.2 - 412.5
6	Upper Shoreface Units	0.09 - 0.11	0.28	0.21 - 0.26	650.2 - 1023.7
7	Distal Mouth Bar Units	0.08 - 0.17	0.27	0.09 - 0.17	170.5 - 223.1
8	Proximal Mouth Bar	0.05 - 0.59	0.12	0.19 - 0.21	130.5 - 314.3
9	Tide Influenced SS	0.14 - 0.46	0.26	0.15 - 0.20	220.0 - 512.6
10	Fluvial Sandstones	0.14 - 0.29	0.21	0.19 - 0.21	180.5 - 691.8
11	Coal	0.24 - 0.53	0.05	0.001	0.001
12	Coastal Plain Fines	0.43 - 0.49	0.06	0.04 - 0.12	5.2 - 34.6
13	Marine Mudstone	0.16 - 0.42	0.1	0.08 - 0.10	6.0 - 15.2

Code	Lithofacies	Avg. NPHI	Density Porosity	Estimated Porosity	KLOGH (mD)
0	Marine Shale	0.17 - 0.45	0.1	0.08 - 0.11	10.02 - 16.1
1	Muddy Shallow Bay Fill	0.17 - 0.42	0.1	0.08 - 0.13	23.85 - 102.3
2	Sandy Shallow Bay Fill	0.07 - 0.52	0.25	0.16 - 0.25	100.0 - 398.7
3	Channel Fill Sandstone	0.04 - 0.15	0.3	0.18 - 0.22	400.01 - 889.7
4	Distal Lower Shoreface	0.04 - 0.19	0.29	0.1 - 0.23	120.5 - 170.3
5	Proximal Shoreface	0.05 - 0.17	0.31	0.17 - 0.24	80.2 - 412.5
6	Upper Shoreface	0.09 - 0.11	0.28	0.21 - 0.26	650.2 - 1023.7
7	Distal Mouth Bar	0.08 - 0.17	0.27	0.09 - 0.17	170.5 - 223.1
8	Proximal Mouth Bar	0.05 - 0.59	0.12	0.19 - 0.21	130.5 - 314.3
9	Tidal Influenced Sandstone	0.14 - 0.46	0.26	0.15 - 0.20	220.0 - 512.6
10	Fluvial Sandstones	0.14 - 0.29	0.21	0.19 - 0.21	180.5 - 691.8
11	Coal	0.24 - 0.53	0.05	0.001	0.001
12	Coastal Plain Fines	0.43 - 0.49	0.06	0.04 - 0.12	5.2 - 34.6
13	Marine Mudstone	0.16 - 0.42	0.1	0.08 - 0.10	6.0 - 15.2

Table 5. ~~Comparison~~A comparison of a) porosity, and b) permeability estimates ~~in~~from selected intervals in the original ~~petrophysical model~~porosity/permeability models and forward modeling-based porosity and permeability models.

a. Validation Well Position 1							
	Porosity: GPM-Based Model					Porosity: Original Model	
	Depth (m)						
Models	5 m	10 m	15 m	25 m	35 m	Depth (m)	Average Porosity
R14	0.22	0.24	0.16	0.22	0.16	5	0.2
R20	0.16	0.19	0.26	0.18	0.15	10	0.25
R26	0.18	0.17	0.23	0.16	0.19	15	0.27
R36	0.22	0.21	0.19	0.22	0.21	25	0.16
R45	0.25	0.2	0.23	0.22	0.15	35	0.13
R49	0.21	0.17	0.22	0.17	0.18		
Validation Well Position 2							
	Porosity: GPM-Based Model					Porosity: Original Model	
	Depth (m)						
Models	5 m	10 m	15 m	25 m	35 m	Depth (m)	Average Porosity
R14	0.17	0.16	0.24	0.15	0.25	5	0.17
R20	0.21	0.22	0.2	0.21	0.23	10	0.21
R26	0.21	0.2	0.21	0.25	0.24	15	0.21
R36	0.2	0.22	0.21	0.21	0.19	25	0.17
R45	0.22	0.19	0.2	0.19	0.21	35	0.19
R49	0.26	0.24	0.23	0.16	0.21		

b. Validation Well Position 1							
	Permeability_Z (mD): GPM-Based Model					Permeability_Z: Original Model	
	Depth (m)						
Models	5 m	10 m	15 m	25 m	35 m	Depth (m)	Average Perm_Z
R14	163.95	312.38	69.84	310.16	508.2	5	352.74
R20	290.84	315.09	105.66	273.04	200.63	10	312.38
R26	375.92	203.81	166.23	189.92	348.12	15	201.08
R36	418.03	203.27	190.9	168.9	370.56	25	199.76
R45	337.6	412.67	199.66	156.71	305.92	35	508.2
R49	370.89	129.33	291.77	175.53	551.18		
Validation Well Position 2							
	Permeability_Z (mD): GPM-Based Model					Permeability_Z: Original Model	
	Depth (m)						
Models	5 m	10 m	15 m	25 m	35 m	Depth (m)	Average Perm_Z
R14	320.34	336.22	151.08	464.22	132.98	5	6.6
R20	122.66	209.15	161.3	230.58	208.48	10	883.6
R26	151.48	710.07	175.09	384.49	169.48	15	30.3
R36	184.74	344.99	157.08	420.15	136.14	25	496.99
R45	91.44	361.04	77.17	382.85	134.56	35	156.6
R49	134.01	721.73	137.42	636.48	290.06		

a. Validation Well Position 1					
	Depth (m)				
	5 m	10 m	15 m	25 m	35 m
Models	Measured Porosity				
Original Model	0.2	0.25	0.27	0.16	0.13
R14	0.22	0.24	0.16	0.22	0.16
R20	0.16	0.19	0.26	0.18	0.15
R26	0.18	0.17	0.23	0.16	0.19
R36	0.22	0.21	0.19	0.22	0.21