1 **InundatEd-v1.0: A HAND-based flood risk modeling system using a Discrete**
2 **Global Grid System**

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Abstract

Despite the high historical losses attributed to flood events, Canadian flood mitigation efforts have been hindered by a dearth of current, accessible flood extent/risk models and maps. Such resources often entail large datasets and high computational requirements. This study presents a novel, computationally efficient flood inundation modelling framework ("InundatEd") using the height above nearest drainage-based solution for Manning's equation, implemented in a big-data discrete global grid systems-based architecture with a web-GIS platform. Specifically, this study aimed to develop, present, and validate InundatEd through binary classification comparisons to recently observed flood events. The framework is divided into multiple swappable modules including: GIS pre-processing; regional regression; inundation model; and web-GIS visualization. Extent testing and processing speed results indicate the value of a DGGS-based architecture alongside a simple conceptual inundation model and a dynamic user interface.

Introduction:

The practice of flood modelling, which aims to understand, quantify, and represent the characteristics and impacts of flood events across a range of spatial and temporal scales, has long informed the sustainable management of watersheds and water resources including flood risk management (Handmer, 1980; Stevens & Hanschka, 2014; Teng et al., 2017, 2019; Towe et al., 2020). Flood modelling research has increased in response to such factors as predicted climate change impacts (Wilby & Keenan, 2012) and advancements in computer, GIS (Geographic Information Systems), and remote sensing technologies, among others (Kalyanapu, Shankar, Pardyjak, Judi, & Burian, 2011; Vojtek & Vojteková, 2016; Wang & Cheng, 2007).

Flood inundation modelling approaches can be broadly divided into three model classes: empirical (Schumann et al., 2009; Smith, 1997); hydrodynamic (Brunner, 2016, DHI, 2012); and simplified/conceptual (L'homme et al., 2008, Néelz & Pender, 2010). Empirical methods entail direct observation through methods such as remote sensing, measurements, and surveying, and have since evolved into statistical methods informed by fitting relationships to empirical data. Hydrodynamic models, incorporating three subclasses, viz; one-dimensional (Brunner, 2016; DHI, 2003), two-dimensional (DHI, 2012; Moulinec et. al., 2011), and three-dimensional (Prakash et. al., 2014; Vacondio et. al., 2011), consider fluid motion in terms of physical laws to derive and solve equations. The third model class, simple conceptual, has become increasingly well-known in the contexts of large study areas, data scarcity, and/or stochastic modeling and encompasses the majority of recent developments in inundation modelling practices (Teng et. al. 2017). Relative to the typically complex hydrodynamic model class, simple conceptual models simplify the physical processes and are characterized by much shorter processing times (Teng et al., 2017, 2019). A class of model which uses the output of a more complex model as a means of calibrating a relatively simpler model is also gaining popularity (Oubennaceur et al., 2019). While each class has contributed substantially to the advancement of flood risk mapping and forecasting practices, a consistent barrier has been the trade-off between computer processing time and model complexity (Neal, Dunne, Sampson, Smith, & Bates, 2018), especially with respect to two-dimensional and three-dimensional hydrodynamic models, which entail specialized expertise to derive and apply physical and fluid motion laws, require adequate data to resolve equations, and the computational resources to process the equations. Neal et al. (2018) summarized the proposed solutions to such challenges as relating to 1) modifications to governing equations or 2) code

69   parallelization, with the latter informing the method proposed in Oubennaceur et al. (2019). With

70   respect to 2D/3D hydrodynamic model code parallelization, Vacondio et al. (2017) listed two

71   approaches: classical (multi-treading or Open Multi-Processing and Message Passing Interface)

72   and Graphics Processing Units (GPUs). The GPU-accelerated method has been shown to decrease

73   execution times, while avoiding the use of supercomputers, for high-resolution, regional-scale

74   flood simulations (e.g., Ferrari et al. (2020), Vacondio et al. (2017), Wang & Yang (2020), and

75   Xing et al. (2019)). However, the GPU-accelerated method is still limited in terms of the hardware

76   requirement (specialized graphics cards), the use of uniform and/or non-uniform grids (Vacondio

77   et al. (2017)), and the need for specific, specialized modelling programs to handle the input data

78   required to solve complex hydrodynamic equations.

79

80   Several studies have introduced generic modelling frameworks that aim to provide robust

81   flood risk estimates with relatively little configuration. Winsemius et al. (2013) for example

82   developed GLOFRIS, a global-scale flood risk modelling framework comprised of global forcing

83   data, a global hydrological model, a flood routing model, and an inundation downscaling model.

84   While capable of providing flood risk at virtually any location on earth, the modelling framework

85   is fixed to the existing datasets and models used, which have significant uncertainty at the scales

86   considered. At a more local scale, Jamali et al. (2018) introduces a flexible flood inundation model

87   that integrates a 1D hydraulic model with a simple GIS-based flood inundation approach.

88   However, this loosely coupled approach still requires specification of a standalone hydraulic model

89   for each location at which it is implemented. There has been a recent stream of research aiming to

90   develop simple conceptual inundation models that preserve both the generality of GLOFIS and the

91   specificity of more local-scale models. Such simple conceptual inundation models offer another

92   potential avenue to handle limitations such as computation requirements and data scarcity. In turn,

93   areas and scales poorly served by standard hydrodynamic modelling may be provided with up-to

94   date flood extent maps. Platforms through which the public can view and interact with the flood

95   extent maps may also be developed (Tavares da Costa, 2019). One such simple conceptual

96   inundation model is the flood model based on Height Above Nearest Drainage (HAND) (Liu et.

97   al 2018). Zheng et al. (2018) estimated the River Channel Geometry and Rating Curve Estimation

98   Using HAND which gained interest from the community, industry, and government agencies.

99   Afshari et al. (2018) showed that, while HAND-based flood predictions can overestimate flood

100 depth, this method provides fast and computationally light flood simulations suitable for large
101 scales and hyper-resolutions. Although simple conceptual models using such methods as linear
102 binary classification and Geomorphic Flood Index (Samela et al., 2017, 2018) have been, and
103 continue to be, developed, the combination of simple conceptual flood methods with big-data
104 approaches remains largely uninvestigated (Tavares da Costa, 2019).

105

106 Recent advances in big data architectures may hold potential to retain enough model
107 complexity to be useful while providing computational speedups that support widespread and
108 system agnostic model development and deployment. There is an increasing need for examination
109 of the potential of decision-making through data-driven approaches in flood risk management and
110 investigation of a suitable software architecture and associated cohort of methodologies (Towe et
111 al., 2020).

112 Discrete global grid systems (DGGS) are emerging as a data model for a digital earth
113 framework (Craglia et al. 2012; Craglia et al., 2008). One of the more promising aspects of DGGS
114 data models to handle big spatial data is their ability to integrate heterogeneous spatial data into a
115 common spatial fabric. This structure is suitable for rapid model developments where models can
116 be split into unit processing regions. Furthermore, with the help of DGGS the model can be ported
117 to a decentralized big-data processing system and many computations can be scaled for millions
118 of unit regions. The Open Geospatial Consortium adopted a DGGS Abstract Specification in late
119 2017 and work is currently underway to develop standards for DGGS specification as a core
120 geospatial data model (OGC, 2017). This is the first use of a DGGS for flood modelling we are
121 aware of.

122 The Integrated Discrete Environmental Analytics System (IDEAS) is a recently developed
123 DGGS-based data model and modelling environment which implements a multi-resolution
124 hexagon tiling data structure within a hybrid relational database environment (Robertson,
125 Chaudhuri, Hojati, & Roberts, 2020). Notably, and in contrast to previous systems, the only special
126 installation entailed by the DGGS-based data spatial model is a relational database. As such,
127 DGGS-based data model can be ported to any software-hardware architecture as long as it supports
128 a relational database system. The system exploits the hardware capability of the database itself
129 which can potentially incorporate the following: GPU(s), distributed storage, and a cloud database.

130   In this paper we employ the IDEAS framework for the efficient computation, simulation,
131   analysis, and mapping of flood events for risk mitigation in a Canadian context. As such, the
132   novelty of this study is twofold: 1) the contribution of the new DGGS-based big spatial data model
133   to the field of flood modelling, and 2) the presentation of a web-interface which lets users compute
134   the inundation on the fly based on input discharge for select Canadian regions where flood risk
135   maps are either not publicly available or do not exist. Moreover, the properties and structure of the
136   DGGS-based spatial data model address a number of challenges and limitations faced by previous
137   flood modelling approaches in the literature. For instance, it is modular, making it easy to switch
138   between Regional Flood Frequency Analysis (RFFA)-based, HAND-based, or alternative models
139   without sacrificing the consistency of the framework. Likewise, the method by which Manning's
140   n is calculated can be easily interchanged. Another novel aspect of this framework is the
141   incorporation of Land Use Land Cover data in the estimation of the roughness coefficient
142   Manning's n instead of a constant value or a channel-specific value of Manning's n as is typically
143   used (Afshari et al., 2017; Zheng et al., 2018). In terms of the tradeoff between model complexity
144   and computation power, the IDEAS framework uses an integer-based addressing system which
145   makes it orders of magnitude more efficient than that of other, more traditional spatial data models
146   (i.e, raster, vector) (Mahdavi-Amiri et. al. 2015; Li & Stefanakis, 2020; Robertson et al., 2020).
147   This, in turn, benefits any and all spatial computations associated with flood modelling. Finally,
148   whereas most major spatial computations entail specialized software/code, in the DGGS-based
149   method the spatial relationship is embedded in the spatial-data model itself. Thus, the spatial
150   relationships need not be considered beyond the use of certain rules of the spatial-data model. The
151   overall efficiency and versatility provided by a DGGS framework can benefit the field of flood
152   risk mapping, which uses the spatial distribution of simulated floods to identify vulnerable
153   locations.

154   Access to flood risk maps can build the capacity of individuals to make informed and
155   sustainable investment and residence decisions in an age of climate concern and environmental
156   change (Albano et al., 2018). The current state of public knowledge of flooding risks is
157   unsatisfactory, with an estimated 94% of 2300 Canadian respondents in highly flood-prone areas
158   lacking awareness of the flood-related risks to themselves and their property, per a 2016 national
159   survey (Calamai & Minano, 2017; Thistlethwaite, Henstra, Brown, & Scott, 2018; Thistlethwaite,
160   Henstra, Peddle, & Scott, 2017). Calls for better transparency and access to reliable flood risk

161 maps and data with which to improve public awareness and understanding of flood risks is in line
162 with a contemporary trend toward more open and reproducible environmental models
163 (Gebetsroither-Geringer, Stollnberger, & Peters-Anders, 2018). There is an opportunity to utilize
164 big data architectures and recent developments in flood inundation modelling and risk assessment
165 technologies to make flood risk information, based on best flood modelling practices, more
166 accessible.

167   The aim of this paper is threefold: 1) propose a simple conceptual inundation model
168 implemented in big-data architecture; 2) test the model and its results through comparison to
169 known extents of previous flood events; and 3) present the resultant flood maps via an open source,
170 interactive web application.

171

172 **2. Methods**

173

174 **2.1 Overview**

175 The modelling component of InundatEd incorporated four general stages: 1) GIS pre-processing;
176 2) flood frequency analysis and regional regression; 3) the application of the catchment integrated
177 Manning's Equation; 4) upscaling the model to a discrete global grid systems data model. Sections
178 2.2.1 to 2.2.4 describe stages 1-4 respectively.

179   The second component of InundatEd's development was the design of a Web-GIS
180 interface, described in Section 2.3, which liaises with and between the big data architecture, the
181 flood models' outputs as defined by user inputs, and FEMA's Hazus depth-damage functions
182 (Nastev & Todorov, 2013) (Section S1). Section 2.4 subsequently links the Web-GIS interface
183 conceptually to previous sections by providing a summary of InundatEd's system structure and its
184 operation. Finally, simulated flood extents using InundatEd's methodology were compared to the
185 extents of observed, historical flood extent polygons within the Grand River watershed and the
186 Ottawa River watershed, provided respectively by the Grand River Conservation Authority and
187 Environment Canada. The comparison and testing process is described in Section 2.5.

188

189

190 **2.2. Modelling**

191

192 2.2.1 – Stage 1: GIS Pre-processing

193

194   The following GIS input data were obtained from Natural Resources Canada for the Grand River

195   and Ottawa River watersheds and cropped to their respective drainage areas of 6,800 square

196   kilometres (Li et al., 2016) and 146,000 square kilometers (Nix, 1987): Digital Elevation Models

197   (Canada Centre for Mapping and Earth Observation, 2015); river network vector shapefiles

198   (Strategic Policy and Innovation Centre, 2019); and Land Use Land Cover (LULC) (Canada

199   Centre for Remote Sensing, 2019). Figure 1 shows the input Digital Elevation Model with

200   elevation values given in metres, and the dams and gauging stations used in this study. The

201   resolution of the DEM and LULC data is 30m x 30m. The vertical accuracy of the DEM is 0.34 m

202   $\pm$ 6.22 m, i.e., 10 m at the 90% confidence level (Beaulieu & Clavet, 2007). The vertical datum

203   used is the Canadian Geodetic Vertical Datum of 2013 (CGVD2013). The stations used for station-

204   level discharge comparison are labeled in Figure 1. The uncertainty in the vertical dimension

205   affects the slopes of individual pixels, the upslope contributing area, and can potentially affect the

206   quality of extracted hydrologic features (Lee et al., 1992, 1996; Liu, 1994; Ehlschlaeger and

207   Shortridge, 1996). Hunter and Goodchild (1997), while investigating the effect of simulated

208   changes in elevation at different levels of spatial autocorrelation on slope and aspect calculations,

209   indicated the importance of a stochastic understanding of DEMs. The Monte Carlo method (Fisher

210   1991) could potentially shed some light on this kind of uncertainty. However, in our case it was

211   beyond the focus of our study and we considered the vertical uncertainty small enough to not affect

212   our large-scale flood modeling simulations. The remaining GIS input data is shown in

213   Supplementary Figure S1. Very small networks, independent of the higher-order channels, were

214   deleted from both regions. ArcGIS Desktop's Raster Calculator tool was used to burn the river

215   network vector into the DEM to ensure the consistency of the river network between the dem

216   delineated and observed. TauDEM (Terrain Analysis Using Digital Elevation Models) (Tarboton,

217   2005), an open-source tool for hydrological terrain analysis, was then used to determine drainage

218   directions and drainage accumulation (Tarboton & Ames, 2004) within the watersheds of interest.

219   Each watershed's drainage network was then established in TauDEM by defining a minimum

220   threshold of two square kilometres on the contributory area of each pixel for the Grand River

221   watershed and ten square kilometres for the Ottawa River watershed. Separately, a value of

222   Manning's n was determined for each 30 x 30 metre pixel of the study areas based on land use/

223   land cover attributes (Brunner, 2016). To this end, the input LULC classes (Canada Centre for

224   Remote Sensing, 2019) within the study watersheds were mapped to the nearest class of the similar

225   land cover classes documented in Chow (1959, Table 5-6) and Brunner (2016, Figure 3-19), from

226   which the respective values of Manning's n were used. Table 1 provides the utilized input LULC

227   classes, their respective description provided by NRCAN, and the employed n values. Height

228   Above Nearest Drainage (HAND) (Rahmati, Kornejady, Samadi, Nobre, & Melesse, 2018;

229   Garousi-Nejad, Tarboton, Aboutalebi, & Torres-Rua, 2019) was also calculated in TauDEM with

230   reference to the DEM and derived drainage network. Figure 2a provides a visual overview of this

231   stage of the modelling component.

232

233   2.2.2. Stage 2: Regional Regression and Flood Frequency Analysis

234   Perhaps one of the most popular methods of flood frequency analysis is the index flood

235   approach - a regional regression model based on annual maximum discharge data (Dalrymple,

236   1960; Hailegeorgis & Alfredsen 2017). A variant of the index flood approach, which entails flood

237   frequency analysis, has been employed to understand the characteristics of flood behavior at the

238   global level (Smith et. al., 2014). At regional scale Burn 1997 has discussed the catchment

239   procedure essential to undertake the flood frequency analysis. Faulkner et. al. (2016) devised the

240   procedure to estimate the design flood levels using the available station data. Regional

241   hydrological frequency analysis at ungauged sites is also studied by few researchers (Desai and

242   Ouarda 2021).

243   The index flood approach was used to derive the discharges by return period at sub-

244   catchment outlets. The model includes two sections: a) a relationship between index flood and

245   contributory upstream area for each hydrometric station and each subcatchment outlet (regional

246   regression); and b) a flood frequency analysis to estimate the quantile values of the departures,

247   with a departure defined as discharge at given station divided by the index flood of that same

248   station). The index flood approach entails the following assumptions: a) the flood quantiles at

249   any hydrometric site can be segregated into two components – an index flood and regional

250   growth curve (RGC); b) the index flood at a given location relates to the (sub)catchment

251   characteristics via a power-scaling equation, either in a simpler case which considers only

252   upstream contributory area or in a more complex case which incorporates land use/ land cover,

253   soil, and climate information; and c) within a homogeneous region the departure/ratio between

254   the index flood and discharge at hydrometric sites yields a single regional growth curve which

255   can relate the discharge and return period (Hailegeorgis & Alfredsen, 2017).

256   Per assumption a) (the flood quantiles at any hydrometric site can be segregated into two

257   components – an index flood and regional growth curve (RGC)), the index flood at each

258   hydrometric station is required. To this end, annual maximum discharge values (m^3s^{-1}) were

259   extracted within R (R Core Team, 2019) at hydrometric stations maintained by Environment

260   Canada within the Grand River and Ottawa River watersheds (HYDAT) (Hutchinson, 2016).

261   Only stations with a period of record >= 10 years of annual maximum discharge (England et al.

262   (2018); Faulkner, Warren, & Burn (2016)) were maintained (n = 32 and n = 54 respectively for

263   the Grand River watershed and the Ottawa River watershed). The minimum, median, and

264   maximum periods of record for the Grand River watershed were 12, 50, and 86 years,

265   respectively. Periods of record for the Ottawa River watershed ranged from a minimum of 10

266   years to a maximum of 58 years with a median of 36 years. A median annual maximum

267   discharge value ($\tilde{Q}$) was then calculated for each hydrometric station. As discussed in

268   Hailegeorgis & Alfredsen (2017), although the index flood is generally the sample mean of a set

269   of annual maximum discharge values, index floods have also been evaluated based on the sample

270   median (eg. Wilson et al., 2011) at the suggestion of Robson & Reed (1999). Finally, the index

271   flood values ($\tilde{Q}$) were used to normalize the observed annual maximum discharge values (Q) at

272   their respective station, resulting in a set of values designated as Qi, such that Qi = Q/ $\tilde{Q}$.

273   With respect to regional regression and assumption b) of the index flood method, a

274   generalized linear model was applied to relate $\log_{10}$ transformed $\tilde{Q}$ values to $\log_{10}$ transformed

275   upstream area values at each hydrometric station. The generalized linear model assumed an

276   ordinary least squares error distribution. The results of the generalized linear model for each

277   watershed allowed for the calculation of previously unknown $\tilde{Q}$ values for each subcatchment

278   outlet. In a more complex model (Fouad et. al. 2016), other catchment characteristics such as land

279   use/land cover, geology, etc. could be used. However, in the case of the proposed model the

280   correlations between the calculated and observed index floods, on the sole basis of discharge

281   records and a linear model relating upstream area, were high as discussed in the Results section.

282   Thus, the simpler method was used to estimate index floods and to relate index flood to

283   contributory area at hydrometric stations and subcatchment outlets. Thus, the regional regression

284   model derived a relationship between index flood ($\tilde{Q}$) and upstream contributory area for each

285   hydrometric station s or sub-catchment outlet. The relationship between index flood at station i or

286 at a subcatchment outlet $(\widetilde{Q^s})$ (median of annual maximum discharge) and upstream contributory

287 area (A_s) is given by:

$$\tilde{Q}^s = aA_s^c \quad (1)$$

289 where a is the index flood discharge response at a unit catchment outlet (or at a hydrometric

290 station) and c is the scaling constant. We took the logarithm of Equation (1) on both sides - a

291 procedure noted in Hailegeorgis & Alfredsen (2017) as used in Eaton, Church, & Ham (2002) -

292 yielding a linear relationship which was solved using the Ordinary Least Squares approach

293 (Haddad et al. (2011).

294   With respect to assumption c) of the index flood method, which assumes that a regional

295 growth curve can be applied to a homogenous area as outlined above, we attempted to fit a

296 distribution to the ratio of the annual maximum discharge values at each station to the

297 corresponding index flood. Hailegeorgis and Alfredsen (2017) discussed a regionalization

298 procedure which ensures the homogeneity of the station-level data over any region. However, due

299 to the limited availability of the discharge data we avoided such sub-sampling and carried out the

300 index flood method at the entire watershed scale (Faulkner, Warren, & Burn 2016). This, however,

301 has impacted the upper quantiles of the flood estimation when comparing to the station level data

302 (Section 3.1). A fundamental step of the analysis process is the selection of a suitable probability

303 distribution model, a common tool in hydrologic modelling studies. The model should account for

304 changes to the flow's extreme value characteristics in response to such factors as urbanization,

305 agriculture, resource extraction, or the operation of dams and weirs. Sometimes, natural hydrologic

306 peaks, such as the spring freshet, are exacerbated by antecedent conditions such as large snowpacks

307 and frozen soils, resulting in substantial flood events. While solutions to this problem have been

308 proposed in the literature, artificial abstraction fundamentally changes the extreme value

309 characteristics of the flow, thereby hindering the usability of most distributional forms (Kamal et.

310 al. 2017).

311   Many researchers have tried to address this problem by putting explicit assumptions on

312 types of non-stationarity affecting the river discharge and are able to devise a closed mathematical

313 formulation which enables the parametric distributions to handle such non-stationarity. However,

314 such methods typically entail knowledge of the specific design return periods of individual flood

315 prevention structures (Salas & Obeysekera, 2014), many of which are absent in our case. To

316 circumvent this problem, we used a non-parametric approach for the regional growth curve (RGC),

317   which requires no fundamental sample characteristics. Thus, modified flood records and limited

318   information notwithstanding, flood frequency estimation is possible using the index flood

319   approach. Per assumption c) of the index flood method, a log-spline non-parametric approach was

320   taken to model a RGC (Stone, Hansen, Kooperberg, & Truong, 1997) for each study watershed.

321   Specifically, the index flood values ($\tilde{Q}$) were used to normalize the observed annual maximum

322   discharge values (Q) at their respective station ($Q_i = Q/ \tilde{Q}$). The Q_i values (n= 1487 and n = 1248

323   for the Ottawa River watershed and the Grand River watershed, respectively) were then fitted to a

324   logspline distribution for their respective watershed. The discharge quantiles (Q_r) were extracted

325   for the following return periods (T, years): 1.25, 1.5, 2.0, 2.33, 5, 10, 25, 50, 100, 200, and 500.

326   The return periods were first converted to a cumulative distribution function:

327   Finally, flood quantile estimations were calculated for each return period as shown below:

328   $$Q_T^i = \widetilde{Q^i} q_T \quad (2)$$

329   such that T is a specified return period in years; Q_T^i is a quantile estimate of discharge for the

330   specified return period T (years) at a specified station i (or a subcatchment outlet); $\widetilde{Q^i}$ is the "index

331   flood" at the same station i (or at the same sub-catchment outlet); i = 1,2,…,N where N =32 for

332   the Grand River watershed or N= 54 for the Ottawa River watershed; and q_T is the regional growth

333   curve as described above. Figure 2b provides a visual accounting of the regional regression and

334   flood frequency analysis methodology described in this section.

335   Some of the limitations of this framework include the long-term flow records and

336   homogenous stations required for the creation of regional regression models. A dearth of long-

337   term data affects flood magnitude computations specifically for the upper quantiles (5T rule,

338   Section 3.1).

339

340   2.2.3 Stage 3: Catchment Integrated Manning's Equation

341   Manning's formula (Song et. al., 2017) is widely used to calculate the velocity and subsequently

342   the discharge of any cross-section of an open channel. The Manning's equation is given in SI units

343   by:

344   $$Q = \frac{1}{n} R_h^{\frac{2}{3}} A S^{\frac{1}{2}} \quad (3)$$

345   such that Q is discharge in cubic metres per second, A represents the cross-sectional area, n is a

346   roughness coefficient, R_h is the hydraulic radius, and S represents slope (fall over run) along the

347 flow path. Despite its widespread use, robustness, and relative ease of use, Manning's Equation

348 has an inherent problem which comes from the uncertain orientation of cross-sections. To mitigate

349 this problem, we integrated Manning's Equation along the drainage lines within the catchment,

350 accounting for the slope of each grid cell to yield bed area and derived the stage-discharge

351 relationship. This strategy uses hydrological terrain analysis, discussed previously in Section 2.2.1,

352 to determine the Height Above Nearest Drainage (HAND) of each pixel (Rodda, 2005; Rennó et

353 al., 2008). The HAND method determines the height of every grid cell to the closest stream cell it

354 drains to. In other words, each grid cell's HAND estimation is the water height at which that cell

355 is immersed. The inundation extent of a given water level can be controlled by choosing all the

356 cells with a HAND less than or equal to the given level. The water depth at every cell can then be

357 calculated as the water level minus the HAND value of the corresponding cell. The relevance of

358 HAND to the field of flood modelling has been demonstrated in the literature (Rodda, 2005, Nobre

359 et al., 2016). Its documented use notwithstanding, HAND's potential applications to the depiction

360 of stream geometry information and to the investigation of stage-discharge connections have not

361 been well investigated. Hydraulic methods of discharge calculation typically entail hydraulic

362 parameters derived from the known geometry of a channel. The knowledge of a channel's cross

363 sectional design is a requirement for many one-dimensional flood routing models, for instance the

364 one-dimensional St. Venant equation (Brunner, 2016). Even though the use of DEM interpolated

365 bathymetry, as used by our method, induces error in the modelling of flood inundation, it is a

366 necessity in the absence of bathymetry data. There are several instances in literature (Sanders,

367 2007) where the DEM interpolated bathymetry has been tested in place of actual bathymetry for

368 hydrodynamic flood modelling. Furthermore, the requirement of the cross-section being

369 perpendicular to the flow direction makes it an implicit problem and also dependent on the choice

370 of cross-section position as well as the distance at which the points are taken on the cross-section.

371 In the current practice of hand designing it makes it subjective and draws substantial uncertainty

372 in the inundation simulation. Alternatively, HAND-based models do not explicitly solve the

373 Manning's equation at individual cross-section, but rather solve for a catchment averaged version

374 of it, by considering a river as a summation of infinite cross-sections. As such, the inherent

375 uncertainty is avoided. However, the simplistic HAND-based model struggles to simulate proper

376 inundation extent in case of complex conditions such as meandering main channels and

377 confluences (Afshari et. al. 2017). This model doesn't capture the dynamic flow characteristics

378   such as backwater effects created by flood mitigation structures. Furthermore, the large flood depth

379   and low flow velocity in the natural rivers makes the river subcritical on many occasions,

380   specifically for large floodplains where the water slows down significantly. This causes the

381   backwater effect very far upstream of the flooding locations which is not simulated in HAND

382   based methods. Therefore, users have to be cautious in such cases.

383   The conceptual framework for implementing HAND to estimate the channel hydraulic

384   properties and rating curve is as follows: for any reach at water level h, all the cells with a HAND

385   value $<$ h compose the inundated zone F(h), which is a subarea of the reach catchment. The water

386   depth at any cell in the inundated zone F(h) is the difference between the reach-average water level

387   h and the HAND of that cell, $HAND_c$, which can be represented as: depth = $HAND_c$-h. Since a

388   uniform reach-average water level h is applied to check the inundation of any cell within the

389   catchment, the inundated zone F(h) refers to that reach level. The water surface area of any

390   inundated cell is equal to the area of the cell A_c. This case study uses 30 metre x 30 metre grid

391   cells, thus in this case $A_c = 900$ m^2. The channel bed area for each inundated cell is given by

392 $$A_s = A_c\sqrt{(1 + slope^2)} \ (4)$$

393   where slope is the surface slope of the inundated pixel expressed as rise over run or inverse tangent

394   of the slope angle. This equation approximates the surface area of the grid cell as the area of the

395   planar surface with surface slope, which intersects with the horizontal projected area of the grid

396   cell. The flood volume of each inundated pixel at a water depth of h can be calculated as V_c (h)=A_c

397   (h-$HAND_c$). If the reach length L is known, the reach-averaged cross section area for each pixel is

398   given by A_i=V_c/L. Similarly, the reach-averaged cross section wetted perimeter for each inundated

399   pixel P_i(h)= A_s/L. Therefore, the hydraulic radius for each inundated pixel is given by R_i=A_i/P_i.

400   Therefore, we can estimate the reach-averaged cross-section area $A = \sum_i A_i$, perimeter $P =$

401     $\sum_i P_i$, and hydraulic radius R= A/P for the entire flooded area. We compared the composite

402   Manning's n (Chow, 1959; Flintham & Carling, 1992; Pillai, 1962; Tullis, 2012) from 7 different

403   methods: the Colebatch method; the Cox method; the Horton Method; the Krishnamurthy Method;

404   the Lotter method; the Pavlovskii Method; and the Yen Method (McAtee, 2012). More details

405   about these methods are in the supplementary Section S2 of this paper.

406   Thus the discharge Q(h) corresponding to inundation height can be computed by the Manning's

407   equation and given by:

408 $$Q(h) = \frac{1}{n} R^{\frac{2}{3}} A S^{\frac{1}{2}} \quad (6)$$

409 where S is the slope of the river and n is the composite Manning's roughness coefficient. Figure

410 2c displays the sequence of methods outlined for the Catchment Integrated Manning's Equation

411 method.

412

413 2.2.4 Stage 4: Upscaling and Data Conversion

414 The proposed InundatEd inundation model simulates the flood-depth distributions for each

415 catchment independently. This makes this model suitable to be ported to a DGGS-based data

416 model and processing system. Following the GIS preprocessing, done in TauDEM as discussed in

417 Section 2.2.1, the required data was converted to a DGGS representation, as outlined in Robertson

418 et al., (2020). Supplementary Figure S2 for raster input data (S2a), polygon (vector) input data

419 (S2b), and network (directional polyline vector) input data (S2c). For raster data (S2a), the

420 bounding box is used to extract a set of DGGS cells, and then for each DGGS cell's centroid the

421 raster value is extracted. To convert polygon data to a DGGS data model, we sample from its

422 interior and its boundary separately using uniform sampling. Then each sample point is converted

423 into DGGS cells based on its coordinates and stored into IDEAS data model by aggregating both

424 sets of DGGS cells (Figure S2b). The same process for the border extraction is applied to the

425 polylines and networks, however with network data the order of the cells is also stored as a flag to

426 use in directional analysis (Figure S2c). Following conversion, the data was ported to a 40-node

427 IBM Netezza Database for subsequent calculations. General, systematic limitations of the

428 InundatEd IDEAS-based inundation model are discussed in Section 3.1.

429

430 **2.3 Web-GIS Interface**

431 The R/Shiny platform and the R-Studio development environment were used to design the user

432 interface and server components of an online web application, allowing users to query and interact

433 with the inundation model. Features of R specific to InundatEd's modelling workflow were its

434 support of the Hazus damage functions and its support for DGGS spatial data. Shown in Figure

435 3a, the InundatEd user interface offers widgets for the following user inputs: address (text);

436 discharge (slider); and return period (drop down), as well as tabs for viewing interactive graphs.

437 The InundatEd user interface also features an interactive map which leverages the Leafgl R

438   package (Appelhans & Fay, 2019) for seamless integration with the DGGS data model. Users may
439   click on the map to obtain point-specific depth information.
440

441   **2.4 InundatEd Flood Information System – System Structure Summary**
442   Figure 3b displays the overall system structure and linkages for the InundatEd flood information
443   system. GIS input data, as discussed in Section 2.2, were staged, pre-processed, and ported to the
444   database. Data querying was used to compute 'in-database' inundation (flood depth) and related
445   damages (methods outlined in Section 2.1) in response to user interface inputs to the R/Shiny UI.
446

447   **2.5 Flood Data Comparison and Model Testing**

448   2.5.0 Study Areas

449   As preliminary testing domains, we created flood inundation models for the Grand River Basin
450   and Ottawa River Basin respectively, both located in Ontario, Canada. Each basin has experienced
451   historical flooding and have implemented varying measures of flood control. Table 2 shows
452   different salient characteristics of these catchments. For the purposes of graphing and discussion
453   of station-specific period of record (number of years with a recorded annual maximum discharge)
454   on theoretical vs estimated flood quantiles, two stations from each study watershed were selected,
455   one each for high period of record and low period of record. For the Grand River watershed,
456   stations 02GA003 and 02GA047 were selected for high and low period of record, respectively.
457   For the Ottawa River watershed, stations 02KF006 and 02JE028 were selected, respectively.
458   "Theoretical quantiles" are here defined as the quantiles generated by our model based on the
459   logspline fit, which incorporates annual maximum discharge values from multiple stations across
460   each study watershed (Section 2.2.2 and Figure 3). In contrast, "estimated quantiles" are here
461   defined as the flood quantiles calculated simply by extracting the quantiles for the desired return
462   periods from the raw annual maximum discharge values observed at the hydrometric station of
463   interest.

464   2.5.1. Ottawa River Watershed

465   Four flood extent polygons (FEPs) provided by Natural Resources Canada (Natural Resources
466   Canada, 2018, 2020) from the May-June 2019 flood season were used as "observed" floods to test

467 the model outputs for the Ottawa River watershed. Each FEP represented a previously digitized

468 floodwater extent at a specified date/time.

469   A second criterion for selection was that the hydrometric station(s) intersected by the FEP

470 provided discharge data for the FEP's respective datetime. Two hydrometric stations which met

471 both criteria were selected: 02KF005 and 02KB001. The following procedure was followed for

472 each FEP using the corresponding hydrometric station (02KF005 or 02KB001), the station level

473 index flood ($\tilde{Q}$, previously calculated during Section 2.2.2), and the observed discharge (Q_{obs}). In

474 both cases, the logspline fit for the Ottawa River watershed, previously generated during Section

475 2.2.2, was also used.

476   The observed discharge (Q_{obs}) was divided by the corresponding hydrometric station's

477 index flood ($\tilde{Q}$) ($Q_i = Q_{obs} / \tilde{Q}$) The cumulative probability of Q_i was then converted to a return

478 period.

479

480 To generate each simulated flood for comparison to its observed counterpart, the methodology

481 outlined in Sections 2.2.2 and 2.2.3 was repeated with the four new return periods appended to

482 the original list of return periods in Section 2.2.2. Table 3 lists each FEP, the corresponding

483 intersected hydrometric station, the period of record used for each station to calculate $\tilde{Q}$, the

484 observed discharge, the resultant cumulative probability value, and the final return period used to

485 generate each simulated flood.

486

487 2.5.2. Grand River Watershed

488 Regulatory floodplain extent data (the greater of RP=100 or discharge from Hurricane Hazel,

489 "observed" flood extent) was obtained from the Grand River Conservation Authority (GRCA)

490 (Grand River Conservation Authority, 2019). However, analysis revealed that, at most hydrometric

491 stations in the Grand River watershed, the 100-year return period yielded higher discharge values

492 relative to the "Hurricane Hazel" storm. Thus, the 100-year return period could be used. The

493 estimated flood extent for RP=100 was generated per sections 2.2.1-2.2.3. Table S1 provides a

494 discharge comparison between the 100-year return period and the regulatory storm.

495

496 2.5.3. Flood Extent Comparisons

497   For both the Grand River watershed and the Ottawa River watershed, only those subcatchments
498   in close proximity to the observed flood extent polygons were retained for visualization
499   purposes. To this end, a criterion was applied to subcatchments in the Grand River watershed
500   requiring an intersection with the observed flood polygon of >= 20% of the subcatchment's area.
501   For the Ottawa River watershed, due to the use of station-specific observed discharges, an
502   additional criterion was applied: that a given subcatchment intersects with a network line with
503   contributory upstream area >= 80% and contributory upstream area <= 120% of the observed
504   upstream area of the hydrometric station (02KF005 or 02KB001). Table S2 provides by-
505   subcatchment areas of the observed flood extent polygons whose subcatchments were eliminated
506   based on the 20% intersection threshold. Per Table S2, one excluded subcatchment (10505) had
507   an intersection value >= 20%, attributable in part to the presence of a tributary along which it
508   was not expected that the return period would be properly scaled but which intersected the
509   subcatchment. Additionally, due to the pluvial nature of the flooding in that subcatchment, it was
510   once again expected that the return period as a function of the river discharge would not be
511   properly scaled without the presence of a hydrometric station to provide discharge information.

512   Binary classification metrics have been used to compare between observed and simulated
513   floods in cases where the focus is on extent, not depth (eg Papaioannou et al., 2016; Wing et al.,
514   2017; Chicco & Jurman, 2020). A binary classification (or 2x2 contingency) method was used to
515   compare the simulated flood extent rasters to the extents of their observed counterparts, whereby
516   a confusion matrix was generated for each subcatchment. Multiple accuracy measures were
517   calculated from the contingency tables to support the evaluation of the flood model, including:
518   True Positive Rate (TPR). True Negative Rate (TNR), Accuracy, Matthews Correlation
519   Coefficient (MCC) (Chicco & Jurman, 2020; Esfandiari et al., 2020; Rahmati et al., 2020), and
520   the Critical Success Index (CSI) (e.g., Papaioannou et al., 2016; Stephens & Bates, 2015). Both
521   the CSI and the MCC have been used in the context of flood model validation. The Critical
522   Success Index (CSI) is defined as:

523
$$CSI = \frac{TP}{TP + FN + FP} (7)$$

524   The Matthews Correlation Coefficient (MCC) is defined as:

525
$$MCC = \frac{TP \times TN - FP \times FN}{\sqrt{(TP+FP)(TP+FN)(TN+FP)(TN+FN)}} \ (8)$$

526   such that TP = true positive, TN = true negative, FP = false positive, and FN = false negative.

527

3. Results and Discussion

3.1 Model Processes and DGGS

530   Intermediate model outputs for the Grand River and Ottawa River watersheds - Height Above

531   Nearest Drainage, delineated river networks, and Manning's n- are displayed in Figure S3.

532   Figure 4 visualizes results for the Grand River watershed and for the Ottawa River watershed for

533   the following method components: calculation of hydrometric station upstream (contributory)

534   area; index flood regression as represented by the correlation of logged index discharge and

535   logged upstream area; and flood frequency as represented by discharge against a Gumbel

536   transformed return period (years), for the stations respectively representative of high and low

537   observations. Figures 4a and 4b plot the log of calculated upstream area against the log of

538   observed upstream area, yielding respective Pearson correlation coefficients of 0.99 and 0.63 for

539   the Grand River and Ottawa River watersheds. The relatively weak correlation of the Ottawa

540   River watershed arose primarily from the limited resolution (number of decimal places in lat-

541   long) of the station location information; incorrect reporting of station locations and/or their

542   drainage area (Environment Canada reported the drainage area as 0 for multiple stations); and

543   sometimes wrongly snapping stations to the tributaries rather than to the main river, particularly

544   in cases involving a wide river channel or braided river. However, this does not affect the model

545   itself, as we have used the station-specific drainage areas reported by Environment Canada to

546   create the regional regression model. With respect to regional regression, Figure 4c visualizes the

547   relationship between predicted index flood discharge and contributory upstream area, at

548   individual hydrometric stations, for the Grand River and Ottawa River watersheds (R = 0.83 and

549   0.95, respectively).The regional growth curves for both the Grand River watershed and the

550   Ottawa River watershed are shown in Figure 4d. To compare the proposed approach of using

551   log-spline distribution against a traditional parametric distribution we fitted a Generalized

552   Extreme Value (GEV) distribution to the RGC (Supplementary Figure S4). With respect to the

553   log-spline RGCs, AIC values of 1861.69 and 867.69 and (-2)(logliklihood) values of 1826.04

554   and 809.26 were reported for the Grand River watershed and Ottawa River watershed

555   respectively. The log-spline (-2)(logliklihood) values were lower than their GEV counterparts

556   (1837.56 and 880.12) for both watersheds. For the Ottawa River watershed, the log-spline AIC

557   value, 867.69, was also lower than that of its GEV counterpart (886.12). Furthermore, the use of

558   the log-spline distribution allows for a consistent method which can be applied readily across any

559   watershed without careful calibration of the distribution function. Thus, the log-spline

560   distribution was used for the regional growth curves. The lower values of the normalized

561   discharge shown in Figure 4d for higher return periods (2-3) for the Ottawa River watershed

562   suggest relatively more structural alterations within the watershed, for instance flood control and

563   dams, than the Grand River watershed (Ottawa Riverkeeper, 2020). The Grand River watershed

564   yielded relatively higher values of normalized discharge (>3) at higher return periods in Figure

565   4d. Figure 5 shows the comparison of estimated flood quantiles against theoretical flood

566   quantiles at an individual station from each study watershed. The stations - 02GA034 of the

567   Grand River watershed and 02KF001 of the Ottawa River watershed (Figure 1)- were selected

568   due to their long "discharge counts", referring to the number of years for which an annual

569   maximum discharge was recorded at each station. Specifically, station 02GA034 (5a) yielded a

570   discharge count of 101 and station 02KF001 (5b) yielded a discharge count of 84. Return periods

571   (T, years) have been converted in terms of the Gumbel reduced variable as follows:

572    $$Gumbel = -ln\left[ln\left(\frac{T}{T-1}\right)\right] (9)$$

573   The dotted lines on Figures 5a and 5b represent the 5T threshold - the return period limit beyond

574   which flood simulations can not be reasonably estimated. The 5T threshold requires that, for the

575   reasonable estimation of a quantile for a desired return period T, there be at least 5T years of data

576   (Hailegeorgis & Alfredsen, 2017; Jacob et al., 1999). As expected, the theoretical and estimated

577   return periods are comparable for low return periods. However, and as shown in Figure 5, the

578   theoretical and estimated quantiles deviate at lower RP values than the 5T threshold for both

579   stations. This disagreement between the theoretical and estimated quantiles recalls the assumption

580   of homogeneity for each watershed (Burn, 1997) - estimations of higher return periods, considering

581   the 5T rule, would require more observations. However, further sub-sampling the stations into

582   regional homogeneous groups would have reduced the data quantity substantially for each group.

583

3.2 Web-GIS Interface

A pre-alpha version of the InundatEd app is available at https://spatial.wlu.ca/inundated/. Source code for the most recent version of InundatEd will be publicly available on GitHub (Spatial Lab, 2020). The use of R/Shiny to develop InundatEd and its provision on GitHub encourages transparency, ongoing development, and response to user feedback and preferences.

3.3 Model Testing

Of the binary comparison results for the 7 composite Manning's n methods listed in Section 2.2.3, the Krishnamurthy method yielded the highest median CSI values (Table S3 for the Grand River watershed and Table S4 for the Ottawa River watershed). As such, it was selected for further visualization and discussion.

The following return periods (in years) were observed for FEPs intersecting hydrometric station 02KF005 in the Ottawa River watershed: 26.5, 16.52, and 25.96. Additionally, a return period of 42.69 years was observed for a FEP intersecting hydrometric station 02KB001 in the Ottawa River watershed. The 100-year return period was tested for the Grand River watershed. Binary classification results for the Grand River watershed are shown in Figure 6 for four comparison metrics: Critical Success Index, Matthews Correlation Coefficient, True Positive Rate, and True Negative Rate. Figure 7 presents Critical Success Index and Matthews Correlation Coefficient results for the four Ottawa River watershed cases, with True Positive and True Negative results presented in Supplementary Figure S5. Table 4 lists the number of subcatchments evaluated, the median CSI, and the median MCC for each of the 5 test return periods. The median values of additional metrics are provided in Table S5.

The median CSI values ranged from 0.581 to 0.849 (Table 4), with both of those values coming from the Ottawa River watershed (return periods 42.69 and 26.5, respectively). The median MCC values ranged from 0.743 (Ottawa RP 42.69) to 0.888 (Ottawa RP 26.5). The median CSI and MCC values for the Grand River watershed were 0.741 and 0.844, respectively. The results reported herein are comparable to, and in some cases exceed, previously published binary classification results. For instance, with respect to the MCC, an urban flood model produced by Rahmati et al. (2020) provided an MCC value of 0.76 when compared to historical flood risk areas.

614   Esfandiari et al. (2020) compared two flood simulations: a HAND-based flood model and a model

615   which combined HAND and machine learning to observe flood extents, resulting in a range of

616   MCC values from ~0.77 to ~0.85. Bates et al. (2021) achieved CSI values of 0.69 and 0.82 for a

617   100-year return period flood model of the conterminous United States at a 30m resolution. It must

618   be noted that direct comparisons between the works listed here and this study must be viewed with

619   caution, due to differences in methodologies, assumptions, data sources, data availability, and

620   return periods between the studies. Furthermore, the extent comparison scores are not necessarily

621   objective measures of performance of the simulation model. They can vary depending on the

622   severity of the flood, catchment characteristics, and quality of the benchmark data (Mason et. al.

623   2009, Stephens et al., 2014, Wing et. al. 2021).

624   Additionally, the median F_1 score (Chicco & Jurman, 2020) for the Grand River watershed was

625   0.85. The median F_1 scores for Ottawa River watershed return periods 26.5, 16.52, 25.96, and

626   42.69 were 0.96, 0.95, 0.95, and 0.94 respectively. Such results are approximately in line with

627   Pinos & Timbe (2019), who achieved F_1 values from 0.625 to 0.941 for 50-year RP floods using

628   a variety of 2D dynamic models. Afshari (2018) achieved F_1 values from 0.48 - 0.64 for the 10-

629   year, 100-year, and 500-year return periods when comparing a HAND-based simulation against a

630   HEC-RAS 2D control. Lim & Brandt (2019) determined that low-resolution DEMs are capable of

631   yielding relatively high comparison metrics (e.g. F_1 values approximately >= 0.80) in situations

632   where Manning's n varies widely over space. The connection between high values of Manning's

633   n and flood overestimation (false discovery) was also discussed. The Grand River watershed

634   yielded a median False Discovery Rate (FDR) of 0.117, and the four Ottawa River watershed cases

635   yielded respective median FDRs of 0.019, 0.01, 0.006, and 0.44 for the evaluated subcatchments.

636   The moderately high FDR value of 0.44 for the 42.69-year return period and the observed

637   overestimation of flood extent (discussed below) may be a result of high local Manning's n values.

638   In addition, the influences of flat terrain (Lim & Brandt, 2019) and anabranch must be considered

639   as it can disrupt the assumption of a single drainage direction for each pixel during sub-catchment

640   delineation. Additional factors potentially influencing the overestimation are the problems

641   inherent to HAND-based modeling, as discussed in section 2.2.3. The topography of the area of

642   the Ottawa River watershed wherein the extent comparisons were made is relatively flat with

643   multiple anabranches and thus can lead to chaotic network delineation. Although attempts were

644   made in this model to counter this impact and avoid slope values of 0 (the burning of the polyline

645   network into the DEM, Section 2.2.1 and Figure 2a), the use of the Manning's equation was still

646   compromised in certain areas and likely had a negative impact on the resultant flood simulations.

647

648   As noted in Lim & Brandt (2019), the reliability of the observed flood extent polygons also merits

649   comment. In this case study, the observed FEPs for the Ottawa River watershed were originally

650   digitized from remotely sensed data and thus carry forward the errors and uncertainties from prior

651   processing. The Grand River watershed's 100-year return period extent was also generated outside

652   of this study and potentially carries multiple sources of error and uncertainty. However, evaluation

653   of the exact extent to which errors present in the observed flood extent polygons could have

654   impacted the binary classification results was not an objective of this study.

655   Figure 8 visualizes the 100-year return period simulated flood for the Grand River

656   watershed. Inset maps are provided which highlight one subcatchment with a high CSI (A, CSI=

657   0.77) and two subcatchments with low CSIs (B, CSI =0.17 and 0.22). The simulated flood shown

658   in Figure 8A compares very well to the extent of its observed counterpart, consistent with the

659   relatively high CSI value. Notably, three hydrometric stations are located within the Figure 8A

660   subcatchment: 02GA014, 02GA027, and 02GA016. Per the methods in Section 2.2.2, station

661   02GA014 yielded a period of record of 54, 02GA027 yielded an insufficient (<10) period of record,

662   and station 02GA016 yielded a period of record of 58. The presence of the two hydrometric

663   stations with considerable periods of record likely strengthened the regional regression of the area

664   and contributed to the success of the simulated flood shown in Figure 8A. In contrast, within the

665   low-CSI (0.17 and 0.22) subcatchments shown in Figure 8B, the simulation considerably

666   overestimated the extent of the 100-year return period flood. The overestimation of the flood

667   extents observed in Figure 8B can likely be attributed, at least in part, to the following: a) multiple

668   upstream and downstream dams (Grand River Conservation Authority, 2000) and b) the channel

669   meanders - as discussed previously, the simple HAND-based model employed here is not robust

670   against channel complexities nor flow control structures such as dams. It must be recalled here that

671   the modular nature of the InundatEd model allows for the "swapping" of various flood modelling

672   methods, and thus could easily accommodate, for instance, shallow water equations. It is also

673   possible to include such operations in future versions of the model by either modifying the DEM

674   values to reflect flood control structures or by offsetting the discharge of the catchment based on

675   structure storage.

676

677 With respect to the Ottawa River watershed, Figure 9 highlights subcatchments whose comparison

678 between observed and simulated flood extents yielded low (A: CSI= 0.13) , moderate (B: CSI =

679 0.66 and D: CSI =0.65) and high (C: CSI = 0.87) CSI values.

680

681 Figure 9A shows the simulated and observed flood extents for return period 25.69. Two main

682 factors influencing the low CSI are readily apparent. The first is that the observed FEP appears

683 "cut off", not extending through most of the subcatchment. It is possible that the flood in the

684 remainder of the sub-catchment was simply not digitized during the observed FEP's generation,

685 especially given the subcatchment's position. However, of the area of the subcatchment intersected

686 by the observed FEP, the simulated flood has considerably underestimated the observed flood

687 extent. Figure 9B shows the extent comparison of the 42.69 -year return period in a subcatchment

688 of moderate CSI (0.66). Figure 9C illustrates a subcatchment of high CSI (0.87), characterized by

689 an overall underestimation in flood extent, barring a slight overestimation in one area. Figure 9D

690 (CSI = 0.65) shows a mixture of overestimation and underestimation.

691   Although the results for both the Grand River watershed and the Ottawa River watershed

692 suggest substantial agreement between the respective observed and simulated flood extents, a

693 number of considerations, including input data characteristics and metric bias, require that the

694 presented results be taken with caution and, in some cases, offer clear paths for improvement. With

695 respect to input data, the simulated floods presented within this case study are limited by the initial

696 use of a 30m x 30 DEM raster. As concluded by Papaioannou et al. (2016), floodplain modelling

697 is sensitive to both the resolution of the input DEM and to the choice of modelling approach.

698 Additionally, and as discussed in Section 2.2.3, there are some inherent limitations of the HAND-

699 based modeling approach.

700   Overall, the results indicated that the current iteration of the InundatEd flood model was

701 reasonably successful on the basis of moderate-high MCC values indirect comparisons against the

702 observed flooding extents. However, any weight assigned to this claim must, in addition to the

703 previously discussed caveats, recall that only extent and not depth was compared between the

704 observed and simulated floods. The use of the DGGS big-data architecture provides a promising

705 foundation for further work, such as the incorporation of the impacts of flood control structures,

706 on the InundatEd model.

3.4 Model Performance

There is a distinct contrast of runtimes between the DGGS method and those using a traditional, raster-based method for sub-catchments within the Grand River Watershed (n= 306 for each method) during the generation of respective RP 100 flood maps. The DGGS based storing and processing method is an order of magnitude faster than processing the HAND and catchment boundaries using raster and vector format. The mean runtime using the DGGS method (0.23 seconds) was significantly lower than the mean runtime using the raster-based method (3.98 seconds) at both the 99% confidence intervals ($p < 2.2e-16$). Thus, the efficiency of the proposed inundation model -coupled with a big-data Discrete Global Grids Systems architecture- is demonstrated with respect to processing times with limited input data. As the IDEAS framework and the InundatEd flood modelling method continue to develop, processing time benchmarks could be established to track and evaluate the model's robustness against increasing complexity (e.g., the integration of hydrological processing algorithms) and to facilitate comparisons with other inundation models.

3.5 Conclusions

We have tested a novel flood modelling and mapping system, implemented within a DGGS-based big data platform. In many parts of the world, including Canada, the widespread deployment of detailed hydrodynamic models has been hindered by complexities and expenses regarding input data and computational resources, especially the dichotomy between processing time and model complexity. This research proposes a novel solution to these challenges. First, we demonstrated the development of a flood modelling framework in a Discrete Global Grid Systems (DGGS) data model and the presentation of the models' outputs via an open-source R/Shiny interface robust against algorithm modifications and improvements. The DGGS data model efficiently integrates heterogeneous spatial data into a common framework, rapidly develops models, and can scale for thousands of unit processing regions through easy parallelization. Second, the computational framework has been implemented using a regional dataset over locations and at scales which have not been studied before. We successfully demonstrated the merit of the HAND-based inundation modelling to emulate the observed flooding extent for several historical and design floods. Third,

739 DGGS-powered analytics allow users to quickly visualize flood extents and depths for regions of
740 interest, with reasonable alignment with observed flooding events. Finally, we believe our flood-
741 inundation estimation method can address situations where good quality data is scarce and/or there
742 are insufficient resources for a complex model. To apply the model in a real time environment we
743 would need a discharge forecasting model or have real-time discharge data at the catchment outlet,
744 which could be used to compute the flood inundation using the pre-computed stage-discharge
745 relationship and inundation model.
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1139 **List of tables:**

1140

1141 Table 1. Values of Manning's n

NRCAN LULC Value	NRCAN Description	Manning's n
1	Temperate or sub-polar needleleaf forest	0.16
2	Sub-polar taiga needleleaf forest	0.16
5	Temperate or sub-polar broadleaf deciduous forest	0.16
6	Mixed forest	0.16
8	Temperate or sub-polar shrubland	0.1
10	Temperate or sub-polar grassland	0.035
12	Sub-polar or polar grassland-lichen-moss	0.035
13	Sub-polar or polar barren-lichen-moss	0.03
14	Wetland	0.1
15	Cropland	0.035
16	Barren lands	0.025
17	Urban	0.08
18	Water	0.04

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1172   Table 2. Study Watershed Characteristics

Characteristic	Grand River Watershed	Ottawa River Watershed
Drainage Area (km^2)	6,800 (Li et al., 2016)	146,000 (Nix, 1987)
Elevation range (masl)	173-535 (Lake Erie Source Protection Region Technical Team, 2008)	430 – 20 (Nix, 1987)
Geologic characteristics	Underlain by groundwater-rich, fractured, porous limestone bedrock; surface geology characterized by glacial till and moraine complexes (Liel et al., 2016)	Incorporates the geological subdivisions St. Lawrence Lowlands, Grenville Province, Superior Province, and Cobalt Plate within the region of the Canadian Shield (Environment and Climate Change Canada, 2019)
Approximate Population size	985,000 (Grand River Conservation Authority, 2014)	> 2,000,000 (Environment and Climate Change Canada, 2019)
Land Use / Land Cover	43% agriculture; 26.92% range-grass and pasture; 12% forests; 9.29 % urban areas; 1.8% wetlands (Veale & Cooke, 2017)	73% forested (Quebec); 85% mixed and deciduous forest, 15% boreal (middle-south and northern regions, respectively) (Environment and Climate Change Canada, 2019); 6% farmland; <2% developed (Werstuck & Coulibaly, 2017)
Average Annual Precipitation (mm)	800-900 (Kaur et al., 2019)	840 (Werstuck & Coulibaly, 2017)
Temperature	8-10 ° C average annual; moderate-to-cool temperate (Kaur et al., 2019)	21 - -10 °C average daily (Werstuck & Coulibaly, 2017)

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Table 3. Simulated Flood Generation – Ottawa River Watershed

Observed Flood Extent Polygon	Observed Date and Time (UTC)	Intersected Hydrometric Station	Station Period of Record (years)	Index Flood ($\tilde{Q}$, m³s⁻¹)	Observed Discharge (m³s⁻¹)	Logspline fit observation count	Cumulative Probability Value	Return Period (years)
FloodExtentPolygon_QC_ LowerOttawa_20190429_ 230713.shp	2019/04/29 23:07:13	02KF005	38	3400	5790	1487	0.962	26.5
FloodExtentPolygon_QC_ LowerOttawa_20190507_ 111329.shp	2019/05/07 11:13:29	02KF005	38	3400	5350	1487	0.939	16.52
FloodExtentPolygon_QC_ LowerOttawa_20190513_ 225800.shp	2019/05/13 22:58:00	02KF005	38	3400	5570	1487	0.961	25.96
FloodExtentPolygon_QC_ CentralOttawa_20190503_ 113004.shp	2019/05/03 11:30:04	02KB001	52	258	477	1487	0.977	42.69

Table 4. Binary Comparison Results

Watershed	Return Period (years)	Number of evaluated subcatchments	Median CSI	Median MCC
Grand River	100	71	0.741	0.844
Ottawa River	26.5	17	0.849	0.888
Ottawa River	16.52	21	0.785	0.826
Ottawa River	25.96	22	0.803	0.852
Ottawa River	42.69	7	0.581	0.743

List of Figures

Figure 1. GIS Input Data – Grand River Watershed (a) and Ottawa River Watershed (b) Topography. The maps are created in ArcGIS with the basemaps provided by © ESRI. The stations that are used later in Figure 5 comparison are labeled in the plot.

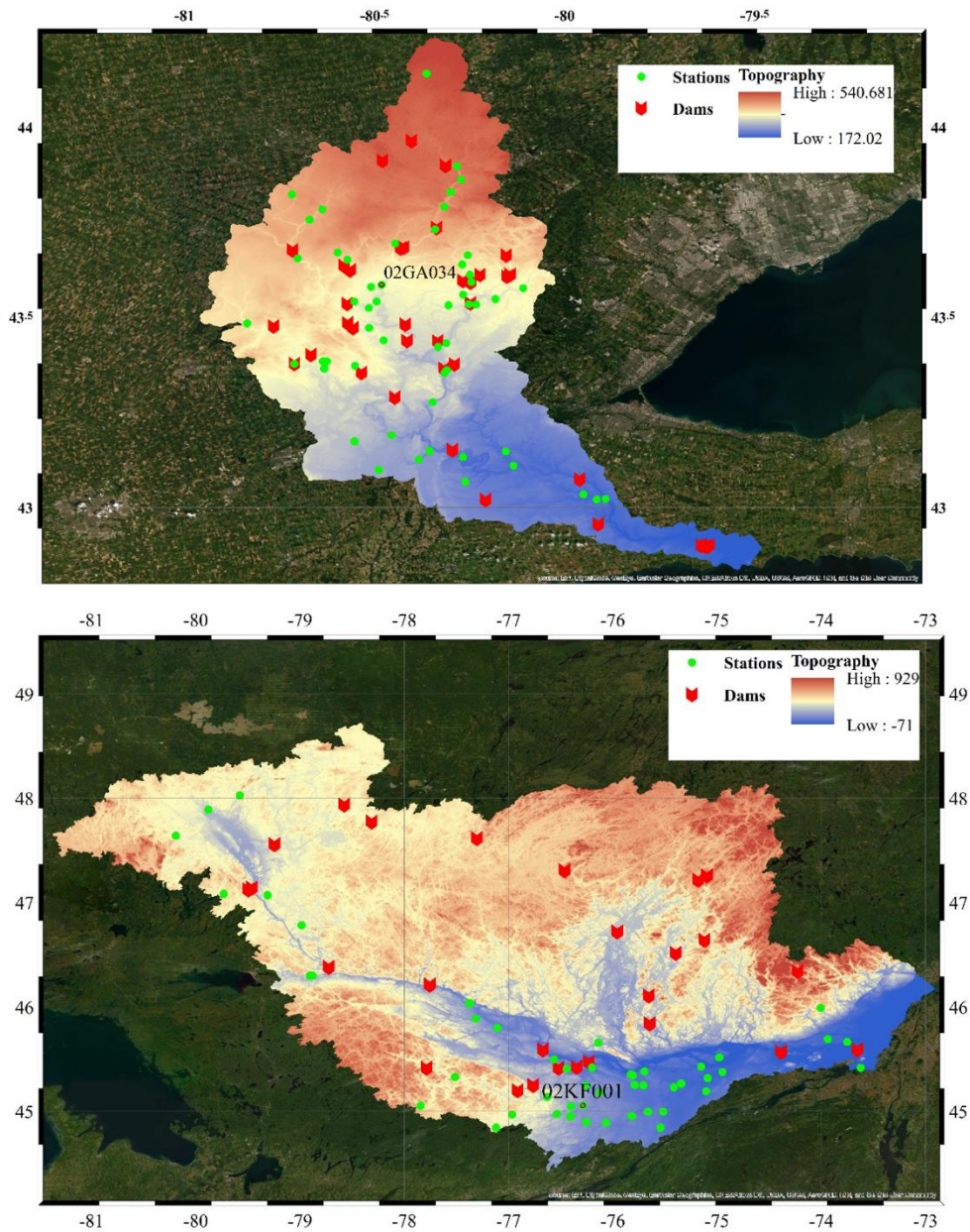



Figure 2. Flood model flowchart illustrating three sub-phases of overall modelling methodology:
a) GIS Pre-processing; b) Flood frequency analysis and regional regression; and c) HAND-based solution of Manning's Equation

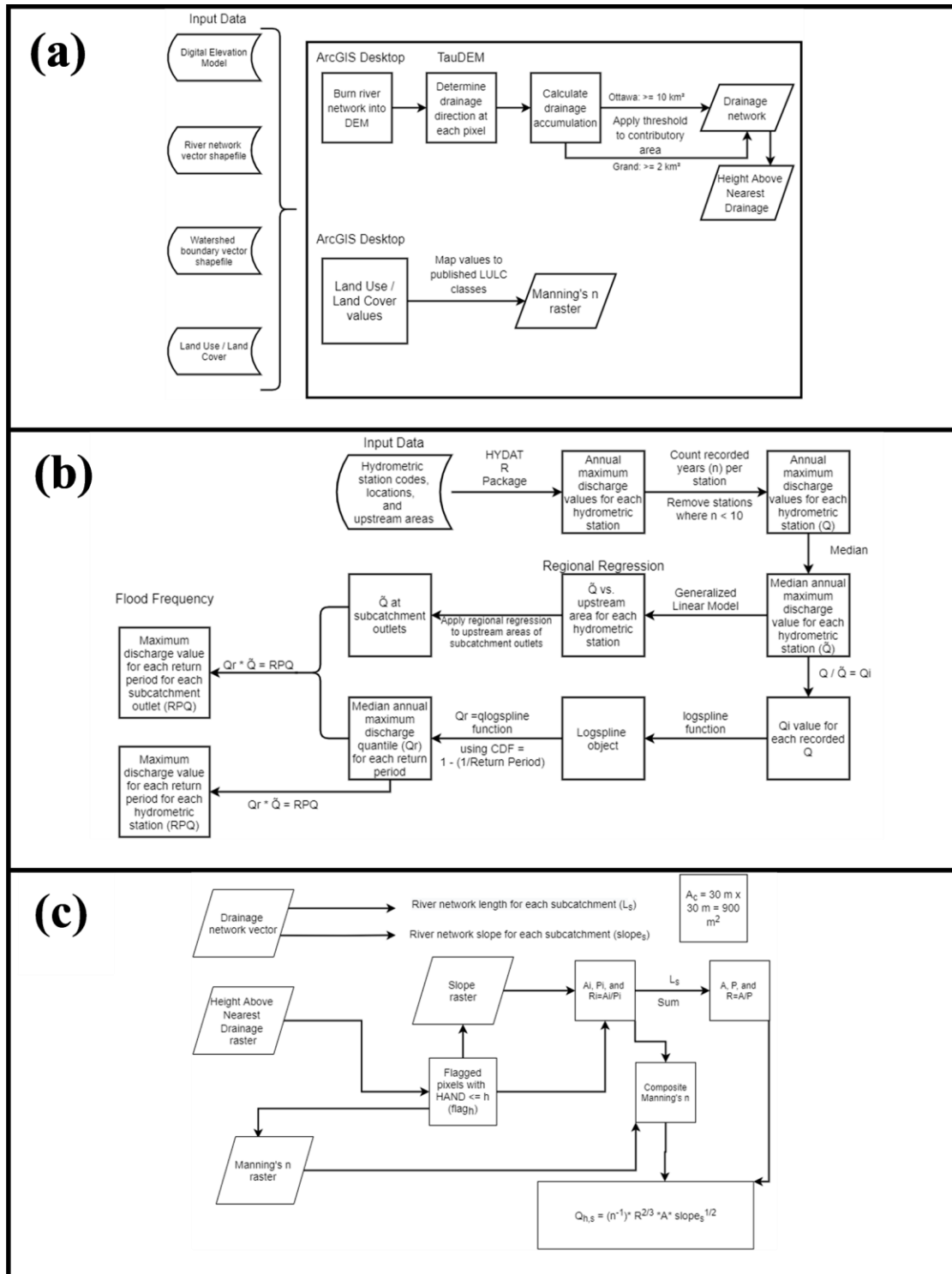



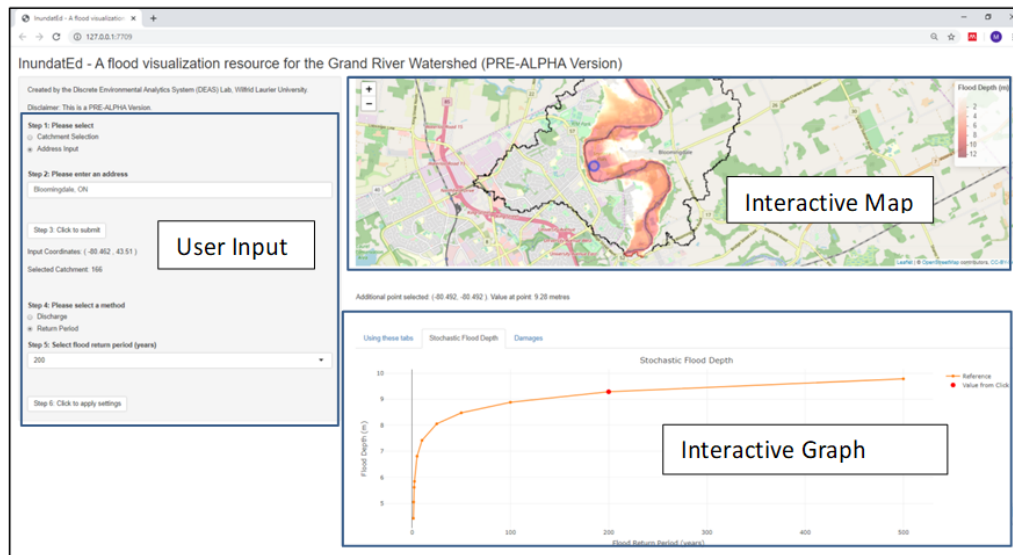
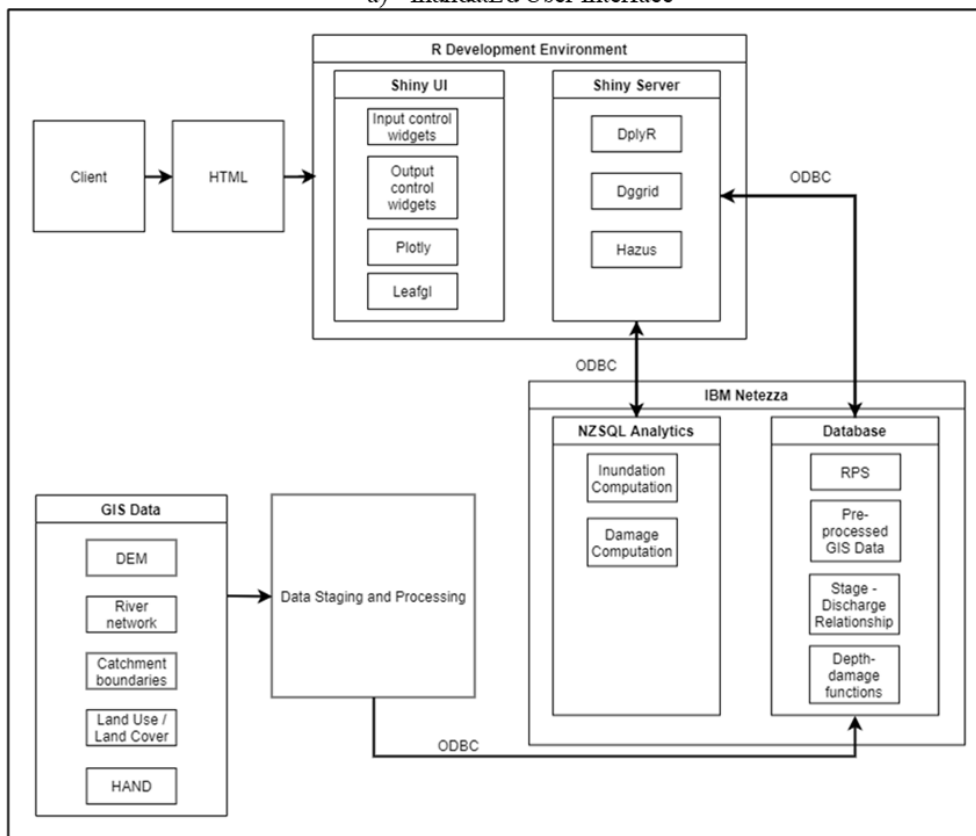
Figure 3. InundatEd User Interface (a) and System Diagram (b). The basemap is created in Leaflet using © OpenStreetMap contributors 2020. Distributed under a Creative Commons BY-SA License

a) InundatEd User Interface

b) InundatEd System Diagram

Figure 4. Flood frequency and regional regression plots

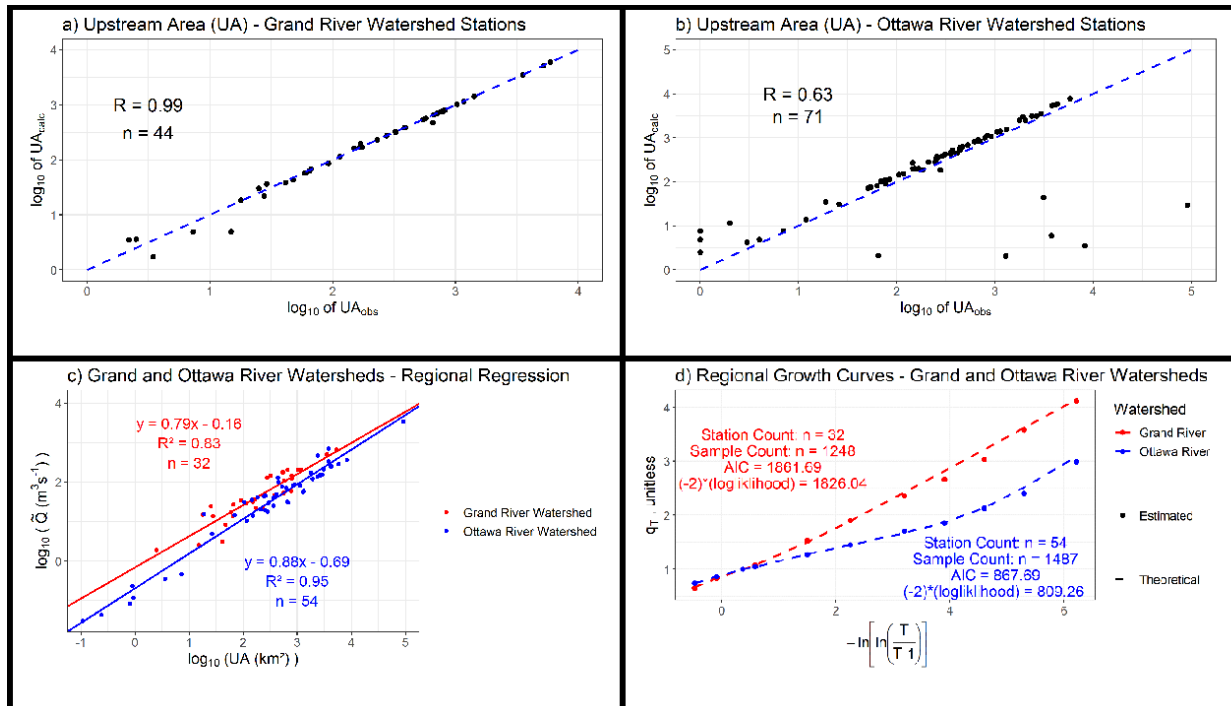



Figure 5. Theoretical Versus Estimated Flood Quantiles

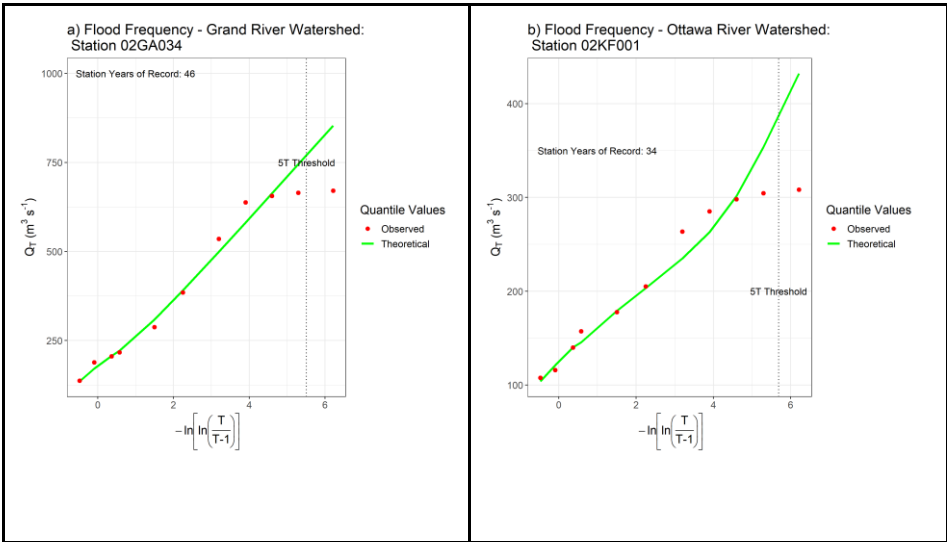



Figure 6. Binary Classification Results – Grand River Watershed

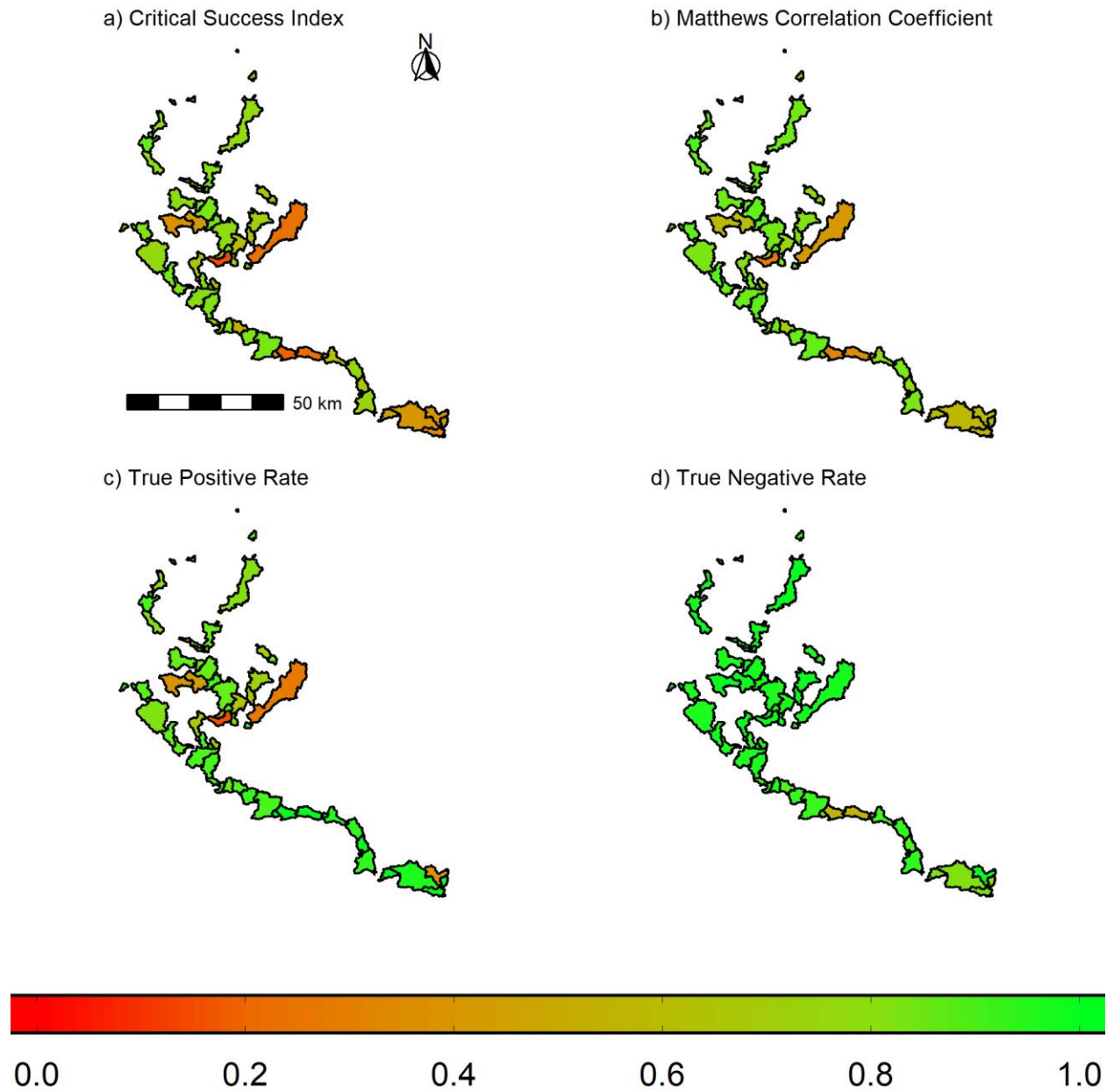



Figure 7. Binary Classification Results – Ottawa River Watershed

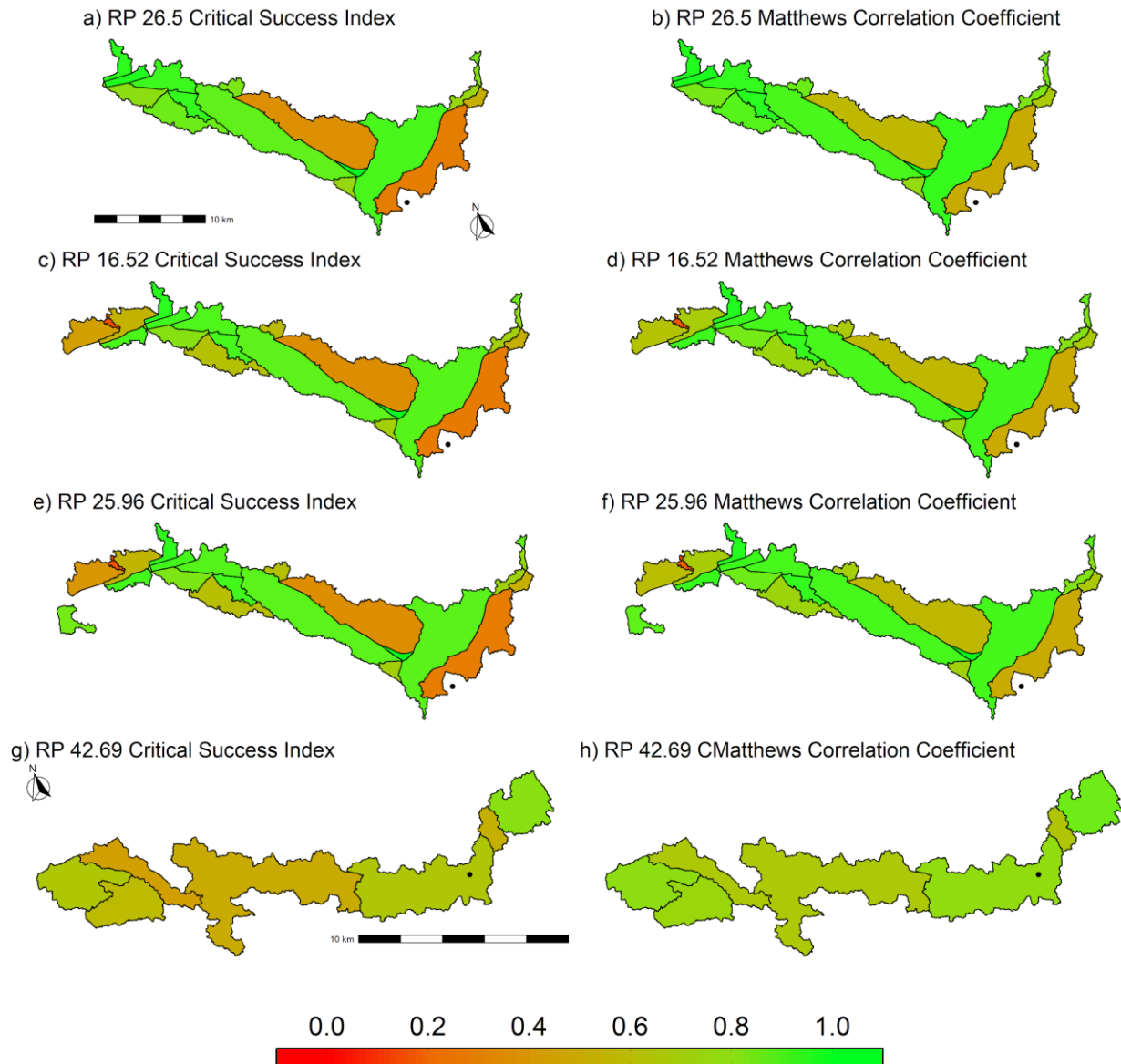



Figure 8. Simulated Flood and Insets – Grand River Watershed 100-Year Return Period

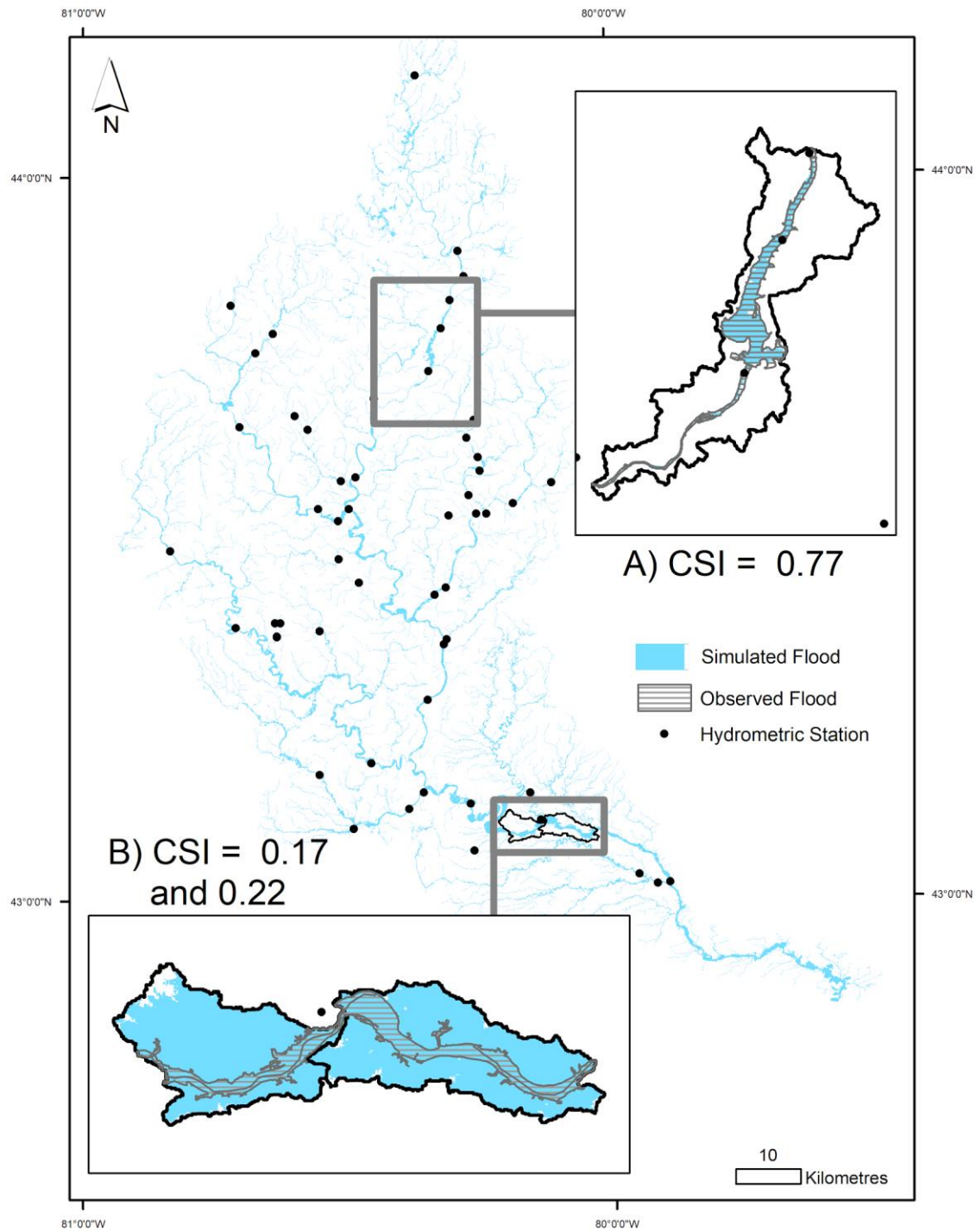
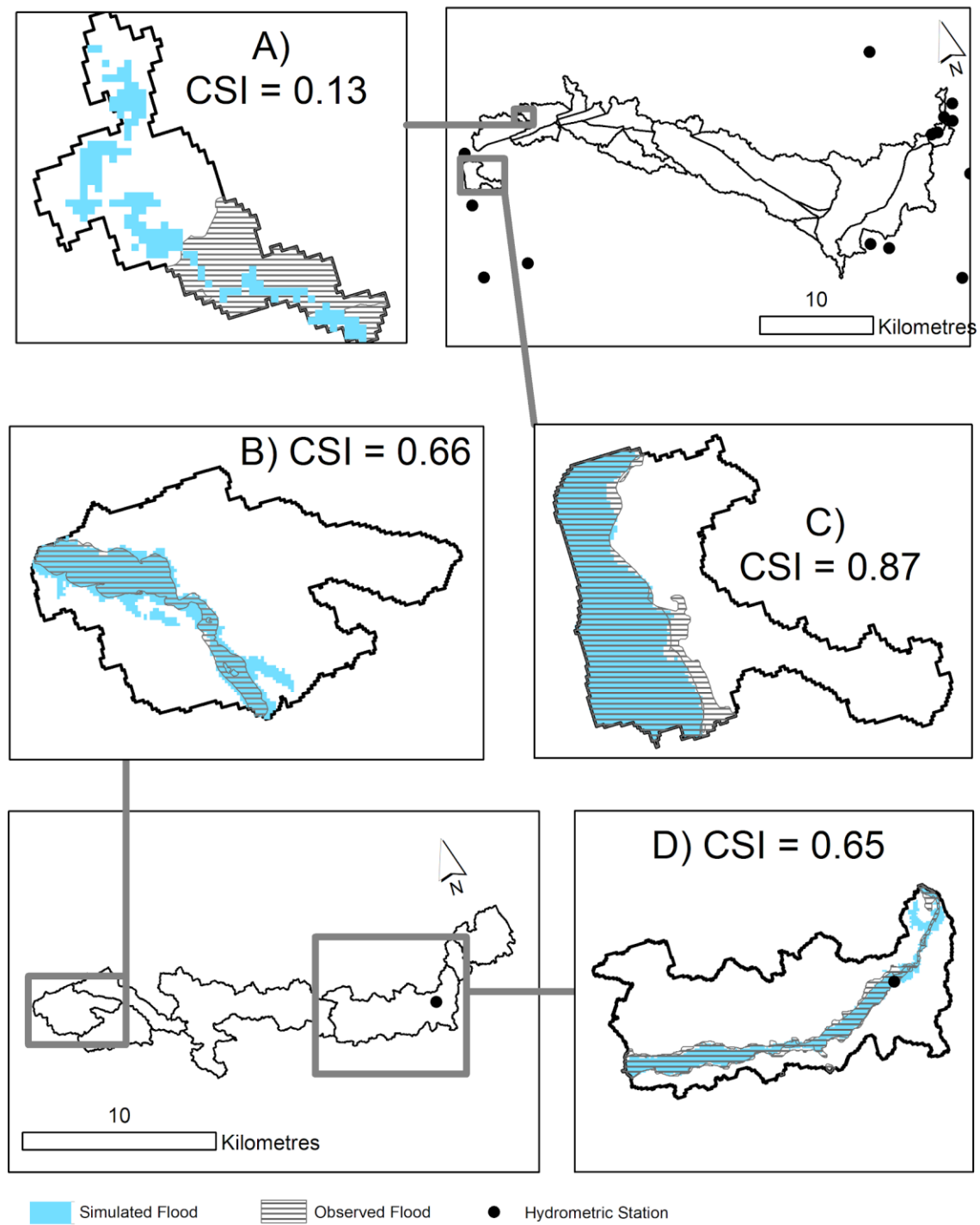



Figure 9. Observed and Simulated Flood Extents– Ottawa River Watershed

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Conflicts of interest/Competing interests

The authors declare that there are no competing interests.

Availability of data and material

Any data that support the findings of this study, not already publicly available, are available from the corresponding author, C. Chaudhuri, upon reasonable request.

Author Contribution

The idea behind this research was conceived, implemented, and written equally by all the authors.

Code availability

The current version of InnundatEd is available from the project GitHub website: https://github.com/thespatiallabatLaurier/floodapp_public. The exact version of the model used to produce the results used in this paper is archived on Zenodo (*10.5281/zenodo.4095618*)