A framework to evaluate IMEX schemes for atmospheric models

Oksana Guba[1], Mark A. Taylor[1], Andrew M. Bradley[1], Peter A. Bosler[1], and Andrew Steyer[1]

[1]Sandia Natl. Laboratories, PO Box 5800, MS 1321, Albuquerque, NM, 87175 USA

Correspondence: Oksana Guba (onguba@sandia.gov)

Abstract. We present a new evaluation framework for implicit and explicit (IMEX) Runge-Kutta timestepping schemes. The new framework uses a linearized nonhydrostatic system of normal modes. We utilize the framework to investigate ~~the~~ stability of IMEX methods and their dispersion and dissipation ~~for~~ of gravity, Rossby, and acoustic waves. We test the new framework on a variety of IMEX schemes and use it to develop and analyze a set of ~~2nd order~~ second-order low-storage IMEX Runge-Kutta methods with high CFL. We show that the new framework is more selective than the 2D acoustic system previously used in ~~the~~ literature. Schemes that are stable for the 2D acoustic system are not stable for the system of normal modes.

1 Introduction

Differences in phase speeds between slow and fast waves in atmospheric models motivate development of timestepping schemes with an implicit component, to avoid expensive ~~time step~~ timestep restrictions imposed by fast waves on explicit methods. The nonlinearity of the equations ~~often imposes~~ and the expense of solving globally coupled linear equations often impose a prohibitive cost on the solvers required by fully implicit methods, and hybrid implicit-explicit (IMEX) schemes that leverage the strengths of both have become common. Here, we develop a new framework for evaluating IMEX methods for atmospheric modeling.

We follow approaches from Durran and Blossey (2012); Weller et al. (2013); Lock et al. (2014); Rokhzadi et al. (2018), and others to present an evaluation framework that is simpler than a full 3D model while still containing the challenges associated with the presence of both slow and fast modes. Our framework is based on the normal mode analysis for systems introduced in Thuburn et al. (2002a, b) and Thuburn and Woollings (2005).

We focus on IMEX Runge-Kutta (RK) methods and their use in our primary application, the High Order Method Modeling Environment (HOMME) dynamical core (Dennis et al., 2012; Taylor et al., 2020). HOMME is the nonhydrostatic atmospheric dynamical core of the U. S. Dept. of Energy Exascale Earth System Model's (E3SM) (Rasch et al., 2019) atmosphere component. HOMME is formulated in Horizontally-Explicit Vertically-Implicit (HEVI) form and is well-suited for IMEX RK schemes ~~where~~ in which terms that carry vertically propagating acoustic waves are treated implicitly.

We adapt the techniques of Thuburn and Woollings (2005), hereafter TW2005, to the specific system of equations and prognostic variables in HOMME as well as other dynamical cores. ~~Namely~~In particular, we use a system of normal modes for a mass-based vertically-Lagrangian coordinate system with a Lorenz-staggered vertical discretization. We construct a spacetime operator for this system and study its properties, including stability, dispersion, and dissipation. Compared ~~to~~ with the previ-

ously used 2D acoustic system and the compressible Boussinesq equations (Durran and Blossey, 2012; Weller et al., 2013; Lock et al., 2014; Rokhzadi et al., 2018), this system provides more complexity and more closely resembles the equations used in modern dynamical cores. It contains a full set of modes: east- and west-propagating acoustic and gravity waves and westward-propagating Rossby waves. It is linearized about a hydrostatic reference state and ~~uses the common constant pressure~~ has the commonly used constant-pressure boundary condition at the model top.

Using the new framework, we develop a family of ~~second order, high CFL, low storage~~ second-order, high-CFL, low-storage IMEX RK schemes and analyze their suitability for operational use in E3SM's ~~high resolution~~ high-resolution science campaigns.

The remainder of this paper is structured as follows. In Section 2 we present the linearized system of equations associated with our formulation of the nonhydrostatic dynamics equations and compute its ~~spacial~~ spatial numerical dispersion properties. Section 3 introduces the spacetime operator and describes our analysis of its numerical stability properties. In Section 4 we compare the stability diagrams of several schemes and develop a new family of IMEX RK methods with desirable stability and storage properties. In Section 4.4 we investigate convergence of IMEX methods with respect to vertical resolution. Section 5 concludes.

2 Linearized system for normal modes

In this section we define the linearized system of equations that corresponds to the HOMME nonhydrostatic dynamics model. ~~We recover analytical and numerical frequencies for spacial discretization of the system and confirm that the discretization (which we~~ Then we present a discretization—which we broadly define here to include ~~choice~~ the choices of prognostic variables, equation of state, boundary conditions, and ~~staggering)~~ staggering—of this system corresponding to HOMME's discretization. We obtain analytical and numerical frequencies for respectively the analytical and discretized systems and confirm that the discretization is nearly optimal. Therefore, ~~later the system can be used~~ we can subsequently use the system to investigate properties of IMEX spacetime operators.

2.1 Description of the system

In Thuburn et al. (2002a, b) and TW2005, the Euler equations for a dry adiabatic atmosphere are simplified to study normal modes. Various approximations about the geometry and Coriolis terms are made, and the systems are linearized about a hydrostatic reference state at rest. Furthermore, TW2005 presents such systems for different choices for thermodynamic variables, vertical coordinates, and equations of state. We use a vertical coordinate based on hydrostatic pressure (Laprise, 1992), where hybrid pressure levels are located on constant s surfaces, and s is the vertical Lagrangian coordinate satisfying $\dot{s} = 0$, following Lin (2004). Therefore, we adopt ~~system~~ the system of equations (20)–(24) in TW2005 for the shallow atmosphere

approximation and a Lagrangian vertical coordinate:

$$u_t = fv - \left(\frac{1}{\rho^r} \frac{\partial p}{\partial x} + \frac{\partial \phi}{\partial x} \right) \tag{1}$$

$$v_t = -fu - \left(\frac{1}{\rho^r} \frac{\partial p}{\partial y} + \frac{\partial \phi}{\partial y} \right) \tag{2}$$

$$w_t = -g \frac{\sigma}{\sigma^r} - \frac{1}{\sigma^r} \frac{\partial p}{\partial \theta} \tag{3}$$

$$\phi_t = gw \tag{4}$$

$$\sigma_t = -\sigma^r \left(\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} \right). \tag{5}$$

Here u, v, and w are velocity components, p is pressure, ρ is density, ϕ is geopotential, g is the gravity constant, f is the Coriolis parameter, σ is pseudo-density defined with respect to the vertical coordinate (see Taylor et al. (2020) for details), and θ is potential temperature. The superscript r denotes variables defined by reference profiles of a linearized hydrostatic steady state with constant temperature T_0. The subscript t denotes partial differentiation with respect to time. Variables u, v, w, ϕ, p, and σ are first-order perturbed quantities, about the reference state, as follows from linear analysis.

After substituting ~~single mode~~ single-mode solutions in which each field is proportional to $\exp(ik_x x + il_y y - i\omega t)$, this formulation is equivalent to the system of equations (20)–(24) in the isentropic coordinate from TW2005. With inclusion of the β ~~-effect~~ effect as in equations (55)–(56) of TW2005, this system is as follows:

$$-i\omega u = fv + \frac{ik_x}{K^2} \beta u - ik_x \left(\frac{p}{\rho^r} + \phi \right) \tag{6}$$

$$-i\omega v = -fu + \frac{ik_x}{K^2} \beta v - il_x \left(\frac{p}{\rho^r} + \phi \right) \tag{7}$$

$$-i\omega w = -g \frac{\sigma}{\sigma^r} - \frac{p_\theta}{\sigma^r} \tag{8}$$

$$-i\omega \phi = gw \tag{9}$$

$$-i\omega \sigma = -\sigma^r (ik_x u + il_x v), \tag{10}$$

with linearized equation of state (EOS)

$$\frac{p}{p^r} = \frac{1}{1-\kappa} \frac{\sigma}{\sigma^r} - \frac{1}{1-\kappa} \frac{\phi_\theta}{\phi^r_\theta}. \tag{11}$$

We also retain a version of system (6)–(10) with time derivatives in the left hand side:

$$u_t = fv + \frac{ik_x}{K^2} \beta u - ik_x \left(\frac{p}{\rho^r} + \phi \right) \tag{12}$$

$$v_t = -fu + \frac{ik_x}{K^2} \beta v - il_x \left(\frac{p}{\rho^r} + \phi \right) \tag{13}$$

$$w_t = -g \frac{\sigma}{\sigma^r} - \frac{p_\theta}{\sigma^r} \tag{14}$$

$$\phi_t = gw \tag{15}$$

$$\sigma_t = -\sigma^r (ik_x u + il_x v). \tag{16}$$

In addition to the variables and constants defined above, $\kappa = R/c_p$ is a thermodynamic constant and k_x and l_x are horizontal wavenumbers with $K^2 = k_x^2 + l_x^2$. Here and later in the text, the subscript x in k_x and l_x does not denote differentiation in x. ~~We keep such notations~~; we use this notation to be consistent with ~~notations~~ the symbols for horizontal and vertical wavenumbers introduced in Weller et al. (2013); Lock et al. (2014). The subscript θ denotes partial differentiation with respect to potential temperature. In (6)–(10), (11), and (12)–(16), the variables ρ^r, σ^r, p^r, and derivative ϕ_θ^r are variables defined by the reference profile of a linearized hydrostatic steady state with constant temperature T_0. ~~Variables~~ The variables u, v, w, ϕ, p, and σ are first-order perturbed quantities about the reference state. All variables are scalar quantities.

We note that since $\dot{\theta} = 0$, the linear system associated with the TW2005 isentropic model is equivalent to the linear system derived with a vertically-Lagrangian coordinate. We use the same bottom boundary condition (BC) $\phi = 0$ for systems (6)–(10) and (12)–(16) as in TW2005~~, but a different top BC.~~ We replace the rigid lid boundary condition with a constant pressure boundary condition, which for ~~perturbed pressure~~ the perturbed-pressure variable becomes $p_{\text{top}} = 0$. This BC is more typical for a mass-based vertical coordinate.

We define meridional wave number $l_x = 0$, temperature of reference state $T_0 = 250$ K, depth of domain in ~~vertical~~ the vertical direction $D = 10^5$ m, Coriolis parameters $\beta = 1.619 \times 10^{-11}\,\text{s}^{-1}\text{m}^{-1}$ and $f = 1.031 \times 10^{-4}\,\text{s}^{-1}$, gravitational acceleration $g = 9.80616\,\text{ms}^{-2}$, and thermodynamic constants $R = 287.05\,\text{Jkg}^{-1}\text{K}^{-1}$ and $c_p = 1005.0\,\text{Jkg}^{-1}\text{K}^{-1}$.

To study the dispersion properties of system (6)–(10), we choose horizontal wavenumber $k_x = 2\pi/10^6\,\text{m}^{-1}$ and set the number of vertical levels $n_{\text{lev}} = 20$. Dispersion and dissipation diagrams of the spacetime operators are also computed with the same n_{lev} and k_x to match frequencies and eigenvectors of the spacetime operators with ones from the ~~spacial~~ spatial discretization.

To form a spacetime operator using Eqs. (12)–(16) and study the stability of IMEX schemes, we set $n_{\text{lev}} = 72$, to emulate the default configuration of E3SM, and vary k_x throughout a representative parameter space resolvable by anticipated ~~high resolution~~ high-resolution models. In regimes ~~where~~ in which stability is controlled by the Courant-Friedrichs-Lewy (CFL) condition associated with acoustics modes, we desire an IMEX method ~~where the~~ whose stability will not depend on the number of vertical levels. In Sect. 4.4 we study the stability of IMEX schemes for a varying number of vertical levels.

2.2 ~~Analytic~~ Analytical frequencies and dispersion relations

The problem of finding frequencies ω in system (6)–(10) is equivalent to investigating ~~a~~ the spectrum of a differential operator. Since we replace ~~boundary conditions~~ the boundary condition at the top of the model, we obtain a slightly different dispersion relation for internal modes compared ~~to~~ with previous work. ~~And~~ Additionally, in contrast ~~with~~ to TW2005, there are no external modes in our system.

To derive the dispersion relation from (6)–(10), we follow Sect. 3 of TW2005 and Thuburn et al. (2002b). The dispersion relation is independent of the choice of vertical coordinate and is most easily found using the height coordinate, z. In TW2005 the hydrostatic equation, elimination, and use of the EOS yield the ODE, ~~Eq.~~ equation (57)

$$(\partial_z + A)(\partial_z + B)p + C = 0, \tag{17}$$

where the constants A and B are related to the static stability and sound speed, respectively, of the isothermal reference state and $C(\omega)$ is a cubic function of the frequency ω. Expressions for $A, B, A, B,$ and C are defined as in TW2005, equation (58). As in TWS2002b, we make the change of variable $\tilde{p} = p \exp\left(\frac{(A+B)z}{2}\right)$ to obtain

$$\tilde{p}_{zz} + a\tilde{p} = 0, \quad a(\omega) = C(\omega) - \frac{(B-A)^2}{4}. \tag{18}$$

120   In our setting, ODE (18) has bottom boundary condition

$$\tilde{p}_z + \frac{B-A}{2}\tilde{p} = 0 \tag{19}$$

at $z = 0$ and top boundary condition $\tilde{p} = 0$ at $z = D$.

We first assume $a > 0$. Cases The cases $a < 0$, and $a = 0$ are discussed below. With $m = \sqrt{a}$ and a solution of form $\tilde{p}(z) = c_1 \sin(mz) + c_2 \cos(mz)$, we recover obtain the internal modes. From the top boundary condition we recover

$$0 = \tilde{p}(D) = c_1 \sin(mD) + c_2 \cos(mD) \quad \Rightarrow \quad c_2 = -c_1 \tan(mD).$$

From the bottom boundary condition we recover

$$0 = \tilde{p}_z(0) + \frac{B-A}{2}\tilde{p}(0) = c_1 m + c_2 \frac{B-A}{2} \quad \Rightarrow \quad c_2 = -c_1 \frac{2m}{B-1} \frac{2m}{B-A}.$$

Combining these, we obtain a condition on wavenumber m:

$$\tan(mD) = \frac{2m}{B-A}. \tag{20}$$

125   In TW2005, the internal modes obey $m = n\pi/D$, where $n > 0$ is the mode number. In (20), for large m, wavenumbers are close to $\frac{n\pi}{D} + \frac{\pi}{2D}$, where n is a positive integer.

Due to the nonlinearity of Eq. (20) with respect to m, wavenumbers m obeying Eq. (20) are found numerically in Matlab by solving Eq. (20) for the first n_{lev} values of m_i, $i \in \{1, \ldots, n_{\text{lev}}\}$, $n_{\text{lev}} = 20$. We recover three wave branches, acoustic, gravity, and Rossby, by solving the quintic equation

130
$$a(\omega) = C(\omega) - \frac{(B-A)^2}{4} = m_i^2, \tag{21}$$

that follows from substituting $a = m_i^2$ in Eq. (18), and solving for ω for each m_i. Three branches of internal waves are plotted as solid blue lines in Fig. 1.

External modes are derived assuming $a < 0$ in Eq. (18). Solutions are then represented by $\tilde{p}(z) = c_1 e^{mz} + c_2 e^{-mz}$, $m = \sqrt{-a}$. This leads to the equation

135
$$\tanh(mD) = \frac{2m}{B-A}, \tag{22}$$

which does not have a solution , as follows. First, rewrite it as $\tanh(\tilde{m}) = \frac{2\tilde{m}}{(B-A)D}$ with $\tilde{m} = mD$. Since $\frac{2}{(B-A)D} > 3$, the line $\frac{2\tilde{m}}{(B-A)D}$ and the curve $\tanh \tilde{m}$ do not intersect except at the origin. The origin is not a solution since we assumed $a < 0$

and thus $m \neq 0$. Similarly, the choice $a = 0$ cannot have solutions satisfying the boundary conditions for our particular value of D.

140 Analytically, one can recover external modes if the depth of the domain, D, is ~~bigger~~larger. We searched for values m in Eq. (22) for $D = 40000$ m and $D = 50000$ m and used these values in Eq. (21). We obtained five real roots with magnitudes of order 10^{-6}, 10^{-3}, and 10^{-2}, as expected. We were unable to locate external modes in discretized systems with large domain sizes. To search, we examined eigenvalues and eigenvectors ~~(using the fact that~~ external modes have zero vertical structure in ~~vertical velocity)~~the vertical velocity coordinate.

145 2.3 Numerical frequencies ~~for~~ in the HOMME discretization

To discretize the right hand side of systems (12)–(16) and (6)–(10) vertically in space, we use a Lorenz staggering and place u, v, and σ at the midpoints of the model's n_{lev} vertical levels and ϕ and w at its $n_{\text{lev}} + 1$ level interfaces. This staggering is denoted $[wz, uv\sigma]$. Due to the choice of boundary conditions, ϕ and w are zero at the bottom of the domain; therefore, we solve only for their n_{lev} interface values, excluding the bottom interface. The total vector length in the discretized system is $5n_{\text{lev}}$.

150 Our placement of variables requires four discrete operators: one to interpolate ϕ from interfaces to midlevels, one to approximate the derivative ϕ_θ at midlevels, one to interpolate σ from midlevels to interfaces, and one to approximate the derivative p_θ on interfaces. Derivatives are formed using second-order finite differencing with constant level spacing $,$ $\Delta\theta$. Interpolation to and from midlevels is implemented via simple averaging of neighbor values. Applying these operators at each level and interface, we can now write the discretization of system (12)–(16) as ~~a matrix equation ,~~the matrix equation

155 $$U_t = \mathbf{M}U_{~~.~~}.$$
(23)

Matrix $\mathbf{M}$ ~~is of~~ has size $5n_{\text{lev}} \times 5n_{\text{lev}}$. The eigenvalues of $\mathbf{M}$ are discrete representations of quantities $-i\omega$ in (6)–(10) ~~and ,~~ and the eigenvectors of $\mathbf{M}$ correspond to the three branches of waves, Rossby, gravity, ~~or~~and acoustic.

We compute the numerical eigenvalues of $\mathbf{M}$ with Matlab, then match a vertical mode to each numerical eigenvalue. To find a vertical mode, we wrote a routine to count zeros in ~~an~~ the imaginary eigenvector part that corresponds to w. For the five 160 smallest wavenumbers we diagnose $n = 1/3$ manually. A few solutions for the highest wavenumbers for Rossby and gravity waves become oscillatory~~and counting zeros for them is inaccurate. We~~. Counting zeros for these is inaccurate; instead, we diagnose them using the monotonicity of numerical eigenvalues.

The numerical dispersion relation for the discretization of system (6)–(10) is plotted in Fig. 1, with blue diamonds for westward propagating waves with $\omega < 0$ and red stars for eastward propagating waves with $\omega > 0$. As in TW2005, system 165 $[wz, uv\sigma]$, which is characterized by its staggering, choice of prognostic variables, and EOS, is in category 2b. Categories for discretizations are defined in TW2005. The ~~most~~ optimal category is category 1~~for methods with~~; methods in this category have numerical dispersion very close to analytical. The next most optimal methods belong to the set of Category 2 methods. Category 2b methods have a ~~near~~nearly optimal dispersion relation~~with overestimated Rossby frequencies~~. Rossby frequencies are overestimated, as shown in Fig. 1, where numerical frequencies for the Rossby branch for large mode numbers are ~~bigger~~ 170 larger by absolute value (Rossby frequencies are negative) than their analytical counterparts.
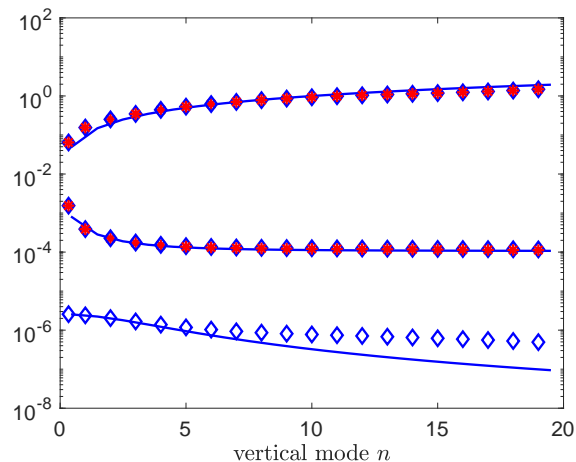
6

Figure 1. Analytical and numerical dispersion relation for system (6)–(10) . Solid blue curves, from top to bottom, are acoustic, gravity, and Rossby branches of analytical solutions for ω. Blue diamonds are negative numerical eigenvalues and red stars are positive numerical frequencies ω.

3 Stability of IMEX methods from eigenvalues of a spacetime operator

In the previous section we evaluated the properties of the spatial discretization for system (6)–(10) . We now combine the spatial discretization with a temporal discretization and then evaluate the resulting spacetime operator.

3.1 Spacetime operator

175 Similarly to Weller et al. (2013) and Lock et al. (2014), we form a spacetime operator from system (12)–(16) and compute its spectrum numerically. To be stable, the eigenvalues of the spacetime operator should lie on or inside of the unit circle.

The spacetime operator is defined by the underlying IMEX scheme. Given a linear ODE

$$y_t = \mathbf{S}y + \mathbf{N}y, \tag{24}$$

where $\mathbf{S}$ and $\mathbf{N}$ are the stiff and nonstiff parts already discretized in space~~. The~~, the spacetime operator $\mathbf{Q}$ can be formed from the double Butcher tableau of explicit (left) and implicit (right) tables associated with a particular IMEX scheme,

$$
\begin{array}{c|c}
c & \mathbf{A} \\
\hline
& b^T
\end{array}
\qquad
\begin{array}{c|c}
\hat{c} & \hat{\mathbf{A}} \\
\hline
& \hat{b}^T
\end{array}.
$$

Here $\mathbf{A}$ denotes the explicit matrix for an IMEX scheme and has no relation with the constant A used in Sect. 2.2. ~~We keep~~
180 ~~both notations as is due to their use in literature~~ We follow the literature in using this notation.

Matrices The matrices $\mathbf{A} = \{a_{j_1 j_2}\}$ and $\hat{\mathbf{A}} = \{\hat{a}_{j_1 j_2}\}$, $j_1, j_2 = 1, ..., \nu$, where ν is the number of stages, and vectors $\mathbf{c} = \{c_{j1}\}$ and $\hat{\mathbf{c}} = \{\hat{c}_{j1}\}$ which determine the location of internal stages, obey the constraints $c_{j_1} = \sum_{j_2} a_{j_1 j_2}$ and $\hat{c}_{j_1} = \sum_{j_2} \hat{a}_{j_1 j_2}$. The weight vectors are $\mathbf{b} = \{b_{j2}\}$ and $\hat{\mathbf{b}} = \{\hat{b}_{j2}\}$. Upper-diagonal and diagonal coefficients of the explicit matrix by definition are zero: $a_{j_1 j_2} = 0$, $j_1 \leq j_2$. We are only interested in diagonally implicit Runge-Kutta (DIRK) methods; therefore, in the implicit matrix $\hat{a}_{j_1 j_2} = 0$ for $j_1 < j_2$.

Later we refer to order of accuracy conditions for IMEX schemes, as defined, for example, in Rokhzadi et al. (2018). First-order conditions are

$$\sum_{j_1} b_{j_1} = \sum_{j_1} \hat{b}_{j_1} = 1. \tag{25}$$

Second-order conditions include the first-order conditions, conditions for each table, and the following coupling conditions for the explicit and implicit tables:

$$\sum_{j_1} b_{j_1} c_{j_1} = \sum_{j_1} \hat{b}_{j_1} \hat{c}_{j_1} = \sum_{j_1} \hat{b}_{j_1} c_{j_1} = \sum_{j_1} b_{j_1} \hat{c}_{j_1} = \frac{1}{2}. \tag{26}$$

For details on how to construct a spacetime operator, see Lock et al. (2014), Eq. (29) or (41), where the spacetime operator is either a scalar or a 3×3 matrix and is called an amplification factor. Here, the spacetime operator is a $(5n_{\text{lev}}) \times (5n_{\text{lev}})$ matrix.

To form a spacetime operator from system (12)–(16), we should define its stiff and nonstiff parts. For the stiff part, represented by matrix $\mathbf{S}$, we consider the right-hand side terms of the equations for vertical velocity and geopotential,

$$-g\frac{\sigma}{\sigma^r} - \frac{p_\theta}{\sigma^r} \qquad \text{and} \qquad gw.$$

It can be shown analytically (Steyer et al., 2019) or numerically, using Matlab scripts for this project, that the eigenvalues of $\mathbf{S}$ coincide with frequencies for acoustic waves. All other terms in the right-hand side of Eqs. (6)–(10) contribute to the nonstiff matrix $\mathbf{N}$. Unlike in the 2D acoustic system (Lock et al., 2014), the spectrum of $\mathbf{N}$ does not coincide with the slow modes of system (12)–(16), and $\mathbf{N}$ is not linear in k_x, in the sense that $\mathbf{N} \neq k_x \mathbf{N}_0$ for some constant operator $\mathbf{N}_0$.

3.2 Stability diagrams

To investigate the numerical stability of timestepping schemes, it is common to refer to the 2D acoustics system (Weller et al., 2013; Lock et al., 2014; Steyer et al., 2019)

$$\boldsymbol{y}_t = -ik_x \begin{pmatrix} 0 & 0 & 1 \\ 0 & 0 & 0 \\ c_s^2 & 0 & 0 \end{pmatrix} \boldsymbol{y} - ik_z \begin{pmatrix} 0 & 0 & 0 \\ 0 & 0 & 1 \\ 0 & c_s^2 & 0 \end{pmatrix} \boldsymbol{y}, \tag{27}$$

with horizontal wave number k_x, vertical wave number k_z, and $k_x = 2\pi/T_x$ and $k_z = 2\pi/T_z$ for wavelengths T_x and T_z. In this system, the spacetime operator has three eigenvalues, which we denote by λ. They are functions of C_x and C_z, $\lambda = \lambda(C_x, C_z)$,

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for Courant numbers $C_x = c_s k_x \Delta t$ and $C_z = c_s k_z \Delta t$, where c_s is the speed of sound and k_x and k_z are horizontal and vertical wavenumbers, respectively. The full stability diagram can then be plotted as a function of C_x and C_z or related quantities.

The relation $\lambda = \lambda(C_x, C_z)$ does not hold for system (12)–(16) and its corresponding spacetime operator. In this system, the eigenvalues are functions of three parameters, $\lambda = \lambda(k_x, \Delta t, n_{\text{lev}})$. For each k_x and Δt, there are $5n_{\text{nlev}}$ eigenvalues. To study the stability properties in this three-dimensional parameter space, we consider two regimes. We first set $n_{\text{lev}} = 72$, to emulate the default configuration of E3SM, and vary k_x throughout a representative parameter space resolvable by anticipated high-resolution models. In the second regime, we fix k_x to the highest frequency resolvable by a model with 3 km grid spacing and consider a range of vertical levels. As we are interested in IMEX methods that treat vertical acoustic waves implicitly, an ideal method should remain stable for all choices of n_{lev}.

In the first regime, we plot stability diagrams with horizontal wavelength T_x on the horizontal axis and Δt on the vertical axis. We vary T_x from approximately 2 to 220 km and the timestep range from 0.5 to 400 s. For each k_x and Δt, we compose a spacetime operator that corresponds to a particular IMEX method. The operator's eigenvalues are computed numerically using one of Matlab's solvers. The largest-magnitude eigenvalue is saved to an array that is then plotted on a stability diagram. We declare a spacetime operator stable if its largest-magnitude eigenvalue has magnitude less than $1 + \epsilon_{\text{tol}}$, with $\epsilon_{\text{tol}} = 10^{-12}$. In our diagrams, stable regions are colored white.

3.3 Diagrams for dispersion and dissipation

Knowing the eigenpairs $(-i\omega_k, \boldsymbol{m}_k)$ of the space operator $\mathbf{M}$ as in Eq. (23) and the eigenpairs $(\lambda_j, \boldsymbol{q}_j)$ of the IMEX spacetime operator $\mathbf{Q}$, we recover additional properties of each IMEX scheme.

For small timesteps Δt, we expect the relationship between the space operator $\mathbf{M}$ and the spacetime operator $\mathbf{Q}$ constructed for Δt step to be

$$\boldsymbol{q}_j \simeq \boldsymbol{m}_k \quad \text{and} \quad \lambda_j = l_j e^{-i\tilde{\omega}_j \Delta t} \tag{28}$$

for some real $l_j > 0$ and real $\tilde{\omega}_j$. We also expect each pair $(\boldsymbol{q}_j, \boldsymbol{m}_k)$ to be uniquely matched.

Ideally, $l_j = 1$ and $\tilde{\omega}_j = \omega_k$; that is, there are no dissipation or dispersion errors from timestepping. In practice, we observe at least some numerical dissipation from applying an IMEX scheme, especially for acoustic waves.

To make dissipation and dispersion diagrams, we use the Munkres algorithm (Munkres, 1957) and its Matlab implementation (Cao, 2020 (accessed March 22, 2020) to uniquely match each $\boldsymbol{q}_j$ with $\boldsymbol{m}_k$ using the cost function $-\frac{<\boldsymbol{m}_k, \boldsymbol{q}_j>}{|\boldsymbol{m}_k||\boldsymbol{q}_j|}$, where $< \cdot, \cdot >$ denotes an inner product. Then we examine the corresponding eigenvalue λ_j from the spacetime operator and compute its absolute value l_j and its $\tilde{\omega}_i$ from Eq. (28). We discuss dissipation and dispersion diagrams further in Sect. 4.3, where we apply them for the family of IMEX methods M2.

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4 Selectiveness of new framework

In Sect. 4.1 we provide an example of a scheme that appears to be stable for many practical choices of ~~time steps~~ timesteps if it is analysed with system (27) but is unstable for these timesteps if analysed with the system of normal modes (12)–(16) . We also apply the new framework for two schemes presented in Giraldo et al. (2013) and Rokhzadi et al. (2018).

4.1 Scheme M1

In tables (29) we present a 6-stage IMEX scheme based on one of the explicit Runge-Kutta methods in Kinnmark, I. and Gray, W. (1984b). The explicit table, (29), left, is a low storage, ~~3nd order method with~~ third-order method with a high CFL of $\sqrt{15} \approx 4$. We construct the implicit table, (29), right, using a ~~backward Euler~~ backward-Euler method for all implicit stages except the last one. The last stage is constructed to have three positive coefficients, including a nonzero coefficient on the main diagonal of matrix $\hat{\mathbf{A}}$, and to obey the ~~2nd order~~ second-order convergence conditions for IMEX methods, (25)–(26). The method has the same time locations of explicit and implicit internal stages and is ~~2nd order~~ second-order accurate. It satisfies a stiffly accurate condition~~,~~; that is, the last row of $\hat{\mathbf{A}}$ matches components of $\hat{\boldsymbol{b}}$.

$$
\begin{array}{c|cccccc|cccccc}
0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\
1/5 & 1/5 & 0 & 0 & 0 & 0 & 0 & 1/5 & 0 & 1/5 & 0 & 0 & 0 & 0 \\
1/5 & 0 & 1/5 & 0 & 0 & 0 & 0 & 1/5 & 0 & 0 & 1/5 & 0 & 0 & 0 \\
1/3 & 0 & 0 & 1/3 & 0 & 0 & 0 & 1/3 & 0 & 0 & 0 & 1/3 & 0 & 0 \\
1/2 & 0 & 0 & 0 & 1/2 & 0 & 0 & 1/2 & 0 & 0 & 0 & 0 & 1/2 & 0 \\
1 & 0 & 0 & 0 & 0 & 1 & 0 & 1 & 5/18 & 5/18 & 0 & 0 & 0 & 8/18 \\
\hline
 & 0 & 0 & 0 & 0 & 1 & 0 & & 5/18 & 5/18 & 0 & 0 & 0 & 8/18
\end{array}
\tag{29}
$$

4.1.1 Plotting details

We plot three stability diagrams for the M1 scheme: Fig. 2(a), with axes $(k_x \Delta t, k_z \Delta t)$~~and~~; Fig. 2(b)~~with $(T_x, \Delta t)$ axes for~~, with axes $(T_x, \Delta t)$ for the 2D acoustics system (27); and Fig. 2(c)~~with $(T_x, \Delta t)$ axes for~~, with axes $(T_x, \Delta t)$ for the system of normal modes (12)–(16) . In Fig. 2(a) the x-axis $k_x \Delta t$ varies from 10^{-4} to $10^{0.1}$ and the y-axis $k_z \Delta t$ varies from 10^{-4} to 10^2. ~~For spacing we use logarithmic scale and~~ In each dimension, we use 100 ~~sampling~~ logarithmically spaced points. As in Lock et al. (2014) and Steyer et al. (2019), for each pair of $k_x \Delta t$ and $k_z \Delta t$, the spacetime operator from Eq. (27) is computed using IMEX method M1 given by tables (29).

Figures 2(b) and 2(c) use the horizontal wavenumber k_x that corresponds to ~~wavelengths~~ the wavelength T_x. In the figures, T_x varies from approximately $2\,\mathrm{km}$ to $220\,\mathrm{km}$~~with logarithmic spacing for~~, with 100 ~~sampling~~ logarithmically spaced points. Since the acoustic system (27) requires k_z, for Fig. 2(b) we make k_z span the range $K_0 = k_x \times [10^{-2}, 10^4]$. On the y-axis, the timestep varies from $0.5\,\mathrm{s}$ to $400\,\mathrm{s}$~~with logarithmic spacing for~~, again with 100 ~~sampling~~ logarithmically spaced points. For each pair of $(k_x, \Delta t)$, we compute a set of spacetime operators based on $k_z \in K_0$ via the same procedure as for Fig. 2(a). If for

each k_z the operator is stable, then point $(T_x, \Delta t)$ is stable in Fig. 2(b). We chose to ~~plot T_x wavelengths on~~ use wavelength on the x-axes of ~~stability diagrams instead of wavenumbers~~ the stability diagrams, rather than wavenumber, to make it easier to identify horizontal resolutions.

Figure 2(c) is generated identically to Fig. 2(b) except that its results come from the system (12)–(16) . Since ~~its spatially discretized version~~ the spatially discretized system is discretized in the vertical direction, there is no need to define k_z.

~~Stability~~ These stability diagrams are not scaled by the number of stages in the IMEX methods.

4.1.2 Stability of the M1 schemes

When using the stability diagrams in Figs. 2(a,b) based on the 2D acoustic system, as in Lock et al. (2014), the scheme appears stable for reasonable timesteps and resolutions as indicated by the large white (stable) regions. Both figures show that the stability of the IMEX scheme is the same as the stability of its explicit table, which is defined by Courant number $S_{M1} \approx 4$, as follows. In Fig. 2(a) a straight vertical line going through a point $k_x \Delta t = S_{M1}$ remains in the white region, and in Fig. 2(b) the stable (white) region lies below the straight line with slope 1 ~~,~~ that goes through the point that corresponds to values $(S_{M1}/(c_s k_x), \Delta t)$. Indeed, the approximate values $T_x = 2000$ m, $\Delta t = 4$ s, $k_x = 0.0031$ m^{-1}, and $c_s = 317$ ms^{-1}, which is ~~value of~~ the speed of sound of the constant reference state in system (12)–(16) , satisfy the last condition.

However, in Fig. 2(c), timesteps based solely on the stability of the explicit table in (29) are not stable. That is, the 2D acoustic system in Eq. (27) does not have enough complexity to indicate that the method can be unstable in practice. Compared to Eq. (27), the system of normal modes contains a full set of modes: east- and west-propagating acoustic and gravity waves and westward-propagating Rossby waves. It is linearized about a non-constant hydrostatic reference state and has ~~commonly used constant pressure~~ the commonly used constant-pressure boundary condition at the model top.

4.2 Schemes ARK2(2,3,2)(Giraldo et al., 2013) and IMEX-SSP2(2,3,2)(Rokhzadi et al., 2018)

In Rokhzadi et al. (2018) one of the ARK2(2,3,2) methods from Giraldo et al. (2013) is compared ~~to~~ with a new scheme, IMEX-SSP2(2,3,2). The family of ARK2(2,3,2) schemes is characterized by parameter a_{32} in the explicit table (Giraldo et al., 2013). In Rokhzadi et al. (2018), the authors choose the method with $a_{32} = \frac{1}{6}(3 + 2\sqrt{2})$, which we denote here as ARK2(2,3,2)(1). Rokhzadi et al. (2018) apply optimization to derive an ARK2 method with improved accuracy, stability, and strong stability preserving (SSP) properties ~~as compared~~ relative to ARK2(2,3,2)(1) for a linear wave equation, the ~~2-D~~ 2D acoustics system, the compressible Boussinesq equations, and the van Der Pol equation as in Durran and Blossey (2012), Weller et al. (2013), and Lock et al. (2014). We compare these two methods and method ARK2(2,3,2) with $a_{32} = 0.85$~~(~~, which we denote ARK2(2,3,2)(2)~~)~~, using our system of normal modes (12)–(16) . We conclude that ARK2(2,3,2)(2) and IMEX-SSP2(2,3,2) have very similar stability properties, as shown in Fig. 3 (b) and (c), but the stable (white) region for ARK2(2,3,2)(1) is significantly smaller, as shown in Fig. 3 (a).
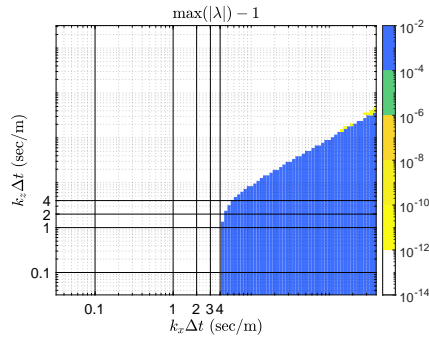
(a) 2D acoustics system, $(k_x \Delta t, k_z \Delta t)$ axes
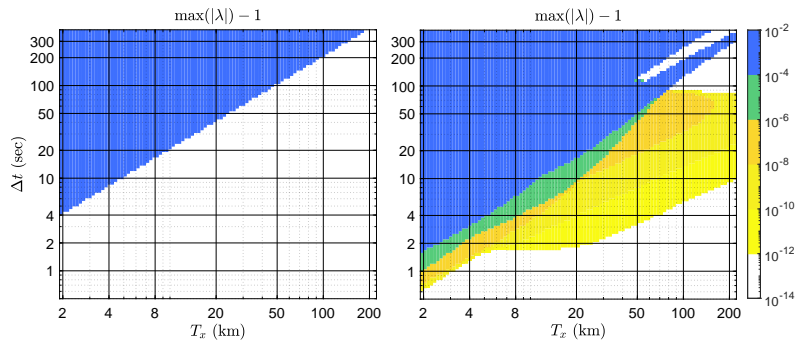
(b) 2D acoustics system, $(T_x, \Delta t)$ axes   (c) System of normal modes, $(T_x, \Delta t)$ axes

Figure 2. Example of selectiveness of the new framework using M1 method: the stability diagram (c) based on the system of normal modes ~~deems~~ determines scheme M1 ~~as is~~ unstable for practical applications, while ~~stable~~ timesteps that are stable in the stability diagrams (a,b) based on the 2D acoustic system look acceptable.

4.3   ~~Set~~ A set of ~~low storage~~low-storage, ~~high CFL~~ high-CFL IMEX schemes~~M2~~

290   We develop a set of ~~M2 methods using a 2nd order~~methods we denote M2 using a second-order, explicit, low-storage, ~~CFL of 4~~ CFL-4 Runge-Kutta scheme from Kinnmark, I. and Gray, W. (1984a). ~~Low storage, high CFL~~ Low-storage, high-CFL methods developed in Kinnmark, I. and Gray, W. (1984a) and Kinnmark, I. and Gray, W. (1984b) are used in HOMME, the nonhydrostatic atmospheric dynamical core of the U. S. Dept. of Energy Exascale Earth System Model's (E3SM) atmosphere component. It is practical to extend existing explicit RK schemes to IMEX RK methods. We analyze the stability, dispersion, 295   and dissipation properties of these M2 schemes using the system of normal modes (12)–(16) .

(a) ARK2(2,3,2)(1) (b) ARK2(2,3,2)(2) (c) IMEX-SSP2(2,3,2)
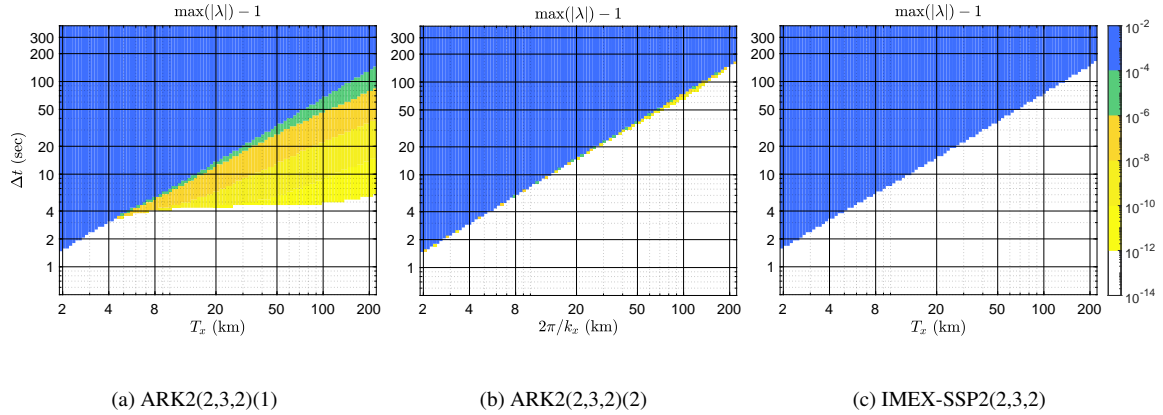
Figure 3. Schemes analyzed in ~~(Rokhzadi et al., 2018)~~ Rokhzadi et al. (2018) and ~~the~~ ARK2(2,3,2)(2) scheme: (a) ARK2(2,3,2)(1), (b) ARK2(2,3,2)(2), (c) IMEX-SSP2(2,3,2).

4.3.1 Definitions

We start with the ~~2nd order explicit table ,~~ second-order explicit table (30), left, from one of ~~the~~ methods in Kinnmark, I. and Gray, W. (1984a). For the implicit table ~~,~~ (30), right, we choose the same times for internal stages and make all but ~~last implicit stages backward Euler. Internal backward Euler~~ the last implicit stage backward-Euler. Internal backward-Euler stages provide stability and do not affect ~~2nd order~~ the second-order accuracy conditions for IMEX given by Eqs. (25)~~–~~(26).

~~The~~ M2 methods vary ~~by~~ only in their last implicit stage~~only~~. We require the last implicit stage to obey a stiffly accurate condition and have only nonnegative entries in its table. The last stage is defined by the vector $\boldsymbol{d}$, whose entries correspond to the last row of the implicit Butcher tableau, as shown in table (30), right. Moreover, here we ~~only consider~~ consider only schemes with at most three nonzero entries ~~of~~ in $\boldsymbol{d}$ ~~due to considerations about computational cost.~~ to limit storage. In practice, using ~~an~~ IMEX method in a 3D model with topography will require storing geopotential and vertical velocity terms for each internal stage that corresponds to $d_{j_1} \neq 0$, $j_1 < \nu$. Therefore, we focus on methods that limit such storage space.

$$
\begin{array}{c|cccccc}
0 & 0 & 0 & 0 & 0 & 0 & 0 \\
1/4 & 1/4 & 0 & 0 & 0 & 0 & 0 \\
1/6 & 0 & 1/6 & 0 & 0 & 0 & 0 \\
3/8 & 0 & 0 & 3/8 & 0 & 0 & 0 \\
1/2 & 0 & 0 & 0 & 1/2 & 0 & 0 \\
1 & 0 & 0 & 0 & 0 & 1 & 0 \\
\hline
 & 0 & 0 & 0 & 0 & 1 & 0
\end{array}
\qquad
\begin{array}{c|cccccc}
0 & 0 & 0 & 0 & 0 & 0 & 0 \\
1/4 & 0 & 1/4 & 0 & 0 & 0 & 0 \\
1/6 & 0 & 0 & 1/6 & 0 & 0 & 0 \\
3/8 & 0 & 0 & 0 & 3/8 & 0 & 0 \\
1/2 & 0 & 0 & 0 & 0 & 1/2 & 0 \\
1 & d_1 & d_2 & d_3 & d_4 & d_5 & d_6 \\
\hline
 & d_1 & d_2 & d_3 & d_4 & d_5 & d_6
\end{array}
\tag{30}
$$

Name	Last stage	Vector $\boldsymbol{d}$	Order
M2a		$\boldsymbol{d} = (3/11, 0, 3/11, 0, 0, 5/11)$	2
M2b		$\boldsymbol{d} = (0, 0, 3/5, 0, 0, 2/5)$	2
M2c		$\boldsymbol{d} = (2/7, 2/7, 0, 0, 0, 4/11)$	2
M2be	backward-Euler	$\boldsymbol{d} = (0, 0, 0, 0, 0, 1)$	1
M2cn	Crank-Nicolson	$\boldsymbol{d} = (1/2, 0, 0, 0, 0, 1/2)$	2
M2cno	Crank-Nicolson with off-centering	$\boldsymbol{d} = (1/2 - 0.02, 0, 0, 0, 0, 1/2 + 0.02)$	1

Table 1. The M2 schemes.

where

$$(d_1, d_2, d_3, d_4, d_5, d_6) = \boldsymbol{d}.$$

We consider the first- and second-order variants of the M2 methods listed in Table 1.

Variants M2a, M2b, and M2c, where M2c was introduced in Steyer et al. (2019), are second-order methods with good stability properties; their dispersive and dissipative characteristics are different, as shown below in Fig. 4. Variants M2be and M2cn are the two extremes of the M2 family. In M2be the last stage is the backward-Euler method. Thus, it is first-order accurate, and we expect this scheme to be the most stable but also the most dissipative. We expect method M2cn, which has the Crank-Nicolson method for the last stage, to have no dissipation for hyperbolic problems like ours. We also analyze method M2cno, whose last stage is the Crank-Nicolson method with off-centering, since off-centering is a common approach to stabilize timestepping schemes (Durran and Blossey, 2012; Staniforth et al., 2006).

4.3.2 Stability diagrams and dispersion/dissipation diagrams

Stability diagrams for the M2 schemes are shown in Figs. 4(a-c) and 5(a-c) which follow the plotting procedures described in Sect. 4.1.1. We plot numerical frequencies of the space operator $\mathbf{Q}$ and the spacetime operator $\mathbf{M}$ to evaluate how the numerical-timestepping methods preserve the frequencies ω from the space discretization $\mathbf{Q}$. Hyperbolicity of the system (12)–(16) implies exact time integration will conserve the frequencies. Inexact time integration will introduce errors, which we evaluate below. We also evaluate numerical damping since exact time integration has none. Note that we compare the properties of the spacetime operator with those of the space operator integrated exactly in time, but we do not compare solutions of the spacetime operator with analytical solutions of system (12)–(16) . This choice of comparison focuses on the numerical errors due solely to the timestepping methods.

Dispersion and dissipation plots are shown below the stability diagrams, for the spacetime operator $\mathbf{Q}$ with eigenpairs $(\lambda_j, \boldsymbol{q}_j)$, in Figs. 4(d-f) and 5(d-f). In each figure, $\Delta t = 50$ s and $n_{\text{lev}} = 20$. The top plots show numerical frequencies
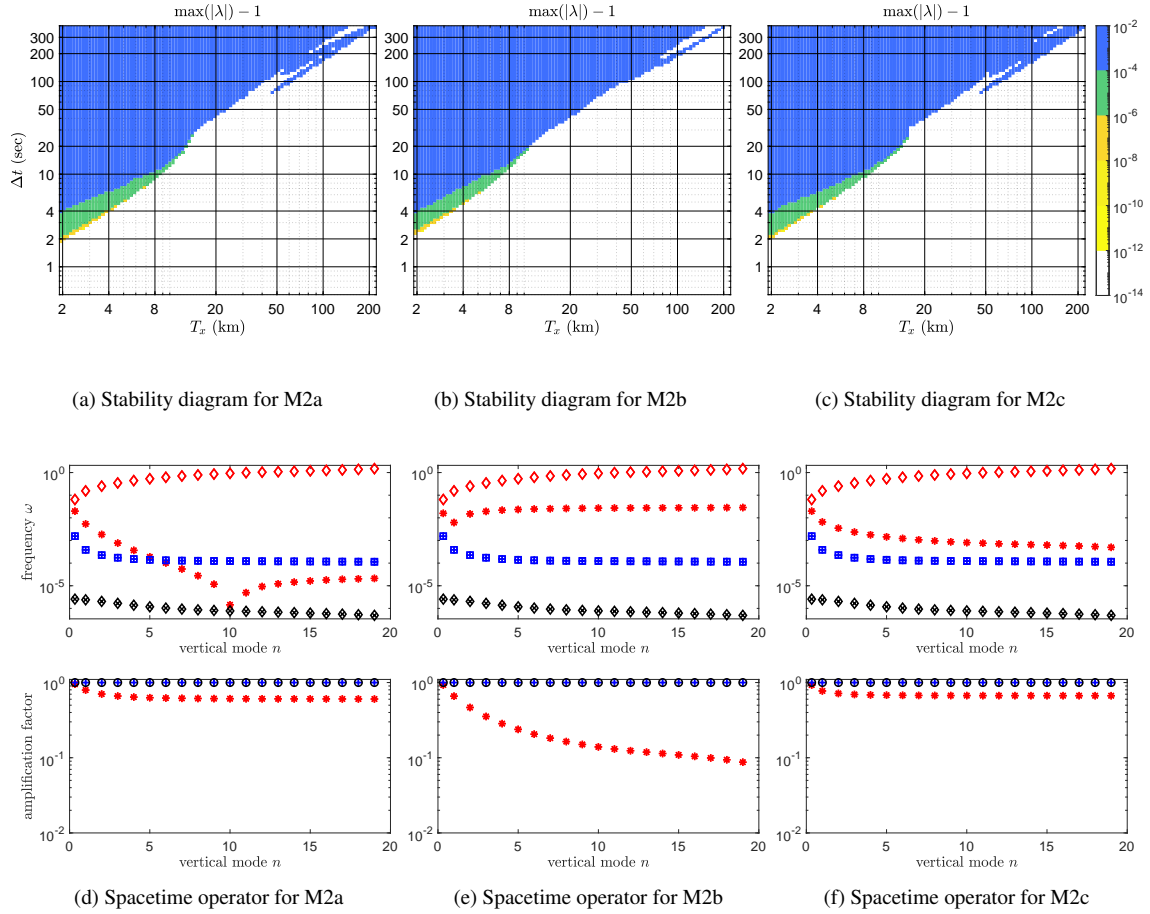
14

(a) Stability diagram for M2a   (b) Stability diagram for M2b   (c) Stability diagram for M2c

(d) Spacetime operator for M2a   (e) Spacetime operator for M2b   (f) Spacetime operator for M2c

Figure 4. Properties of M2 schemes: ~~Stability diagrams and~~ stability, dispersion~~/~~, and dissipation diagrams.

λ_j vs. vertical mode number. Red diamonds are numerical frequencies of the space operator for east- and west-propagating acoustic waves. Blue squares represent east- and west-propagating gravity waves for the space operator. Black diamonds are frequencies for west-propagating Rossby waves for the space operator. Red stars, blue plus signs, and black stars are for corresponding branches of the spacetime operator. Vertical mode number and wave characterization are obtained ~~from~~ by uniquely matching eigenvector q_j ~~with~~ to its counterpart, eigenvector m_k, of the space operator M~~(also computed for~~, also computed using 20 vertical levels~~)~~.

~~Bottom~~ The bottom plots in Figs. 4(d-f) and 5(d-f) show the amplification factors of eigenvalues, $|\lambda_j|$, for the spacetime operator. ~~There,~~ The red stars, blue plus signs, and black stars are for acoustic, gravity, and Rossby waves~~correspondingly~~, respectively. Each plot shows amplification factors near 1 for gravity and Rossby waves, with additional damping of the acoustic modes. We discuss these differences further in the next section.

(a) Stability diagram for M2be (b) Stability diagram for M2cn (c) Stability diagram for M2cno

(d) Spacetime operator for M2be (e) Spacetime operator for M2cn (f) Spacetime operator for M2cno
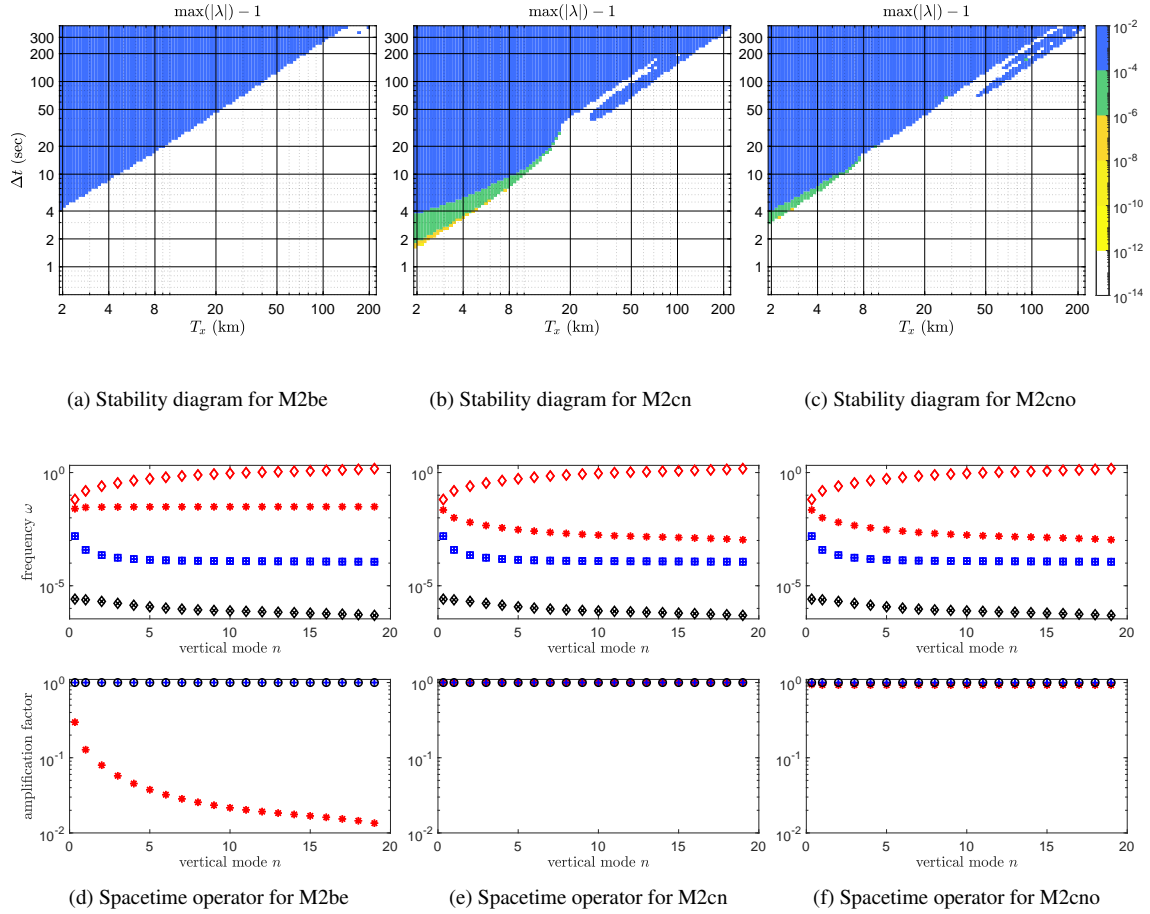
Figure 5. Properties of M2 schemes: ~~Stability diagrams and~~ stability, dispersion~~/~~, and dissipation diagrams.

4.3.3 Analysing the M2 schemes

Due to their different final stages, the M2 schemes have different stability properties and dispersive and dissipative characteristics. To evaluate stability, we focus on ~~regions of smallest spatial resolutions~~ the regions having smallest spatial resolution and highest wavenumbers, since ~~those are~~ these are the regions where nonhydrostatic effects are most prominent. ~~Thus stability evaluation~~ Evaluation of stability is easy: ~~bigger~~ larger stable (white) regions ~~translate to~~ imply larger stable Δt for those methods.

As expected, due to the presence of the last backward-Euler stage in the implicit table, the M2be scheme is the most stable. Recall that analytically for hyperbolic problems, the ~~backward Euler~~ backward-Euler method is unconditionally stable and is very dissipative. For the M2be method, the largest stable Δt at $T_x = 2$ km is approximately 4 ~~sec~~s, which is at least ~~2× larger than~~ twice as large as the largest stable Δt for the other schemes.

It is desirable to have an IMEX method with stability properties similar to those of an explicit method used for the nonstiff part of the system (24). In other words, it is desirable to be able to integrate a nonhydrostatic system using an IMEX method with a timestep as large as the timestep used to integrate a hydrostatic system using an explicit Runge-Kutta method. Therefore, we compare the stability of the IMEX method M2be with the stability of the Runge-Kutta method consisting of the explicit table in M2be, a method we denote MExplicit, when it is applied to the nonstiff part of equation (24). The stability region of M2be in Fig. 5(a) is almost as big as the stability region of MExplicit (not shown here) up to a minor difference at approximate wavelength $T_x = 220$ km. That is, the stability region of M2be is the biggest region we could possibly get from an IMEX scheme whose explicit table is part of the M2 set.

It is harder to rank schemes using dispersion and dissipation diagrams. All schemes preserve the dispersion and dissipation relations for gravity and Rossby waves to a high degree. But they perform very differently for acoustic waves. Method M2be has the largest dissipation for acoustic waves and is the only scheme that does not have regions of negative group velocity for acoustic waves. Method M2cn has opposite characteristics: it does not damp acoustic waves, and the errors in the acoustic frequencies are much larger. M2cno, a first-order variation of M2cn, has dispersion errors very similar to M2cn while introducing low-degree dissipation into acoustic waves.

Since acoustic waves can be considered insignificant for atmospheric applications due to their low energy, one is tempted to discard numerical errors in the dispersion and dissipation of acoustic waves. However, there is an argument (Thuburn, 2012) that correct representation of even energetically weak waves in the atmosphere is crucial for accurate restoration of hydrostatic balance.

Among other second-order schemes, M2a, M2b, and M2c, it is hard to declare a clear winner. Due to its smaller largest stable Δt at $T_x = 2$ km and large dispersion errors, M2a may be less competitive. Compared with M2c, M2b has slightly larger maximum stable Δt at $T_x = 2$ km and its errors in dispersion for acoustic waves are smaller, but its dissipation is larger. Indeed, its larger dissipation is probably what causes its better stability compared with M2c. However, depending on the evaluation criteria, M2c can be viewed as a better scheme than M2b. For example, it has less dissipation and its dispersion is very similar to that of the Crank-Nicolson method, which is widely used for hyperbolic problems.

4.3.4 Role of the implicit table

We chose to limit our search for a suitable M2 method by varying only the vector d in the implicit table. Since the second-order accuracy conditions for the M2 family depend only on the last implicit stage, we make all other implicit stages, stages 2–5, use the backward-Euler method to presumably maximize stability. One could also try to use Crank-Nicolson or off-centered Crank-Nicolson methods for implicit stages 2–5.

To understand how the implicit stages influence dissipation of acoustic waves, we consider the expression for the final solution of Eq. (24) using Lock et al. (2014), Eq. (15), and the definition of the M2 family in Eq. (30):

$$\boldsymbol{y}^{n+1} = \boldsymbol{y}^n + \Delta t\,\boldsymbol{N}(\boldsymbol{y}^{(5)}, t^n + \Delta t) + d_1\,\Delta t\,\boldsymbol{S}(\boldsymbol{y}^n, t^n) + d_2\,\Delta t\,\boldsymbol{S}\left(\boldsymbol{y}^{(2)}, t^n + \frac{1}{4}\Delta t\right) + d_3\,\Delta t\,\boldsymbol{S}\left(\boldsymbol{y}^{(3)}, t^n + \frac{1}{6}\Delta t\right) \quad (31)$$

$$+ \quad d_4\,\Delta t\,\boldsymbol{S}\left(\boldsymbol{y}^{(4)}, t^n + \frac{3}{8}\Delta t\right) + d_5\,\Delta t\,\boldsymbol{S}\left(\boldsymbol{y}^{(5)}, t^n + \frac{1}{2}\Delta t\right) + d_6\,\Delta t\,\boldsymbol{S}\left(\boldsymbol{y}^{(6)}, t^n + \Delta t\right). \quad (32)$$

Scheme M2cn, given by its final implicit stage $(d_1, ..., d_6) = (1/2, 0, 0, 0, 0, 1/2)$, does not have dissipation. For M2cn, the solution $\boldsymbol{y}^{n+1}$ is directly influenced by intermediate implicit stages ~~2-5 only via~~ 2–5 only by the nonstiff term. Also, its final implicit stage is represented by the Crank-Nicolson method, known to be nondissipative for hyperbolic problems. We conclude that both of these facts contribute to the lack of dissipation in M2cn. Scheme M2be has final implicit stage $(d_1, ..., d_6) = (0, 0, 0, 0, 0, 1)$, which gives the ~~backward Euler~~ backward-Euler method. Similarly to the ~~backward Euler~~ backward-Euler method for hyperbolic problems, M2be is very dissipative.

We suggest that the dispersion and dissipation of acoustics waves can be tuned by working only with the implicit table of any method.

4.4 Stability properties with respect to vertical resolution

For an explicit timestepping method, the most restrictive CFL condition is usually that associated with the vertically propagating acoustic ~~waves~~ wavesm and the stable timestep ~~would decrease~~ decreases linearly with $\Delta z = D/n_{\text{lev}}$. Ideally, with an implicit treatment of vertical acoustic waves, an IMEX method should remain stable as n_{lev} is increased, and the stability should be controlled only by the CFL condition associated with the horizontal resolution.

To analyze this aspect of various IMEX methods, we fix k_x to the highest frequency resolvable by a model with 3 km grid spacing and vary the number of vertical levels from $n_{\text{lev}} = 20$ to $n_{\text{lev}} = 100$. We plot the method's stability as a function of n_{lev} using a logarithmic scale (up to rounding to the nearest integer) and 50 ~~sampling points. Stability~~ sample points. The stability diagrams are made very similarly to the ones in Fig. 4~~, with only difference of~~; the only difference is the horizontal axis, which now ~~defines~~ is n_{lev}. We vary Δt from 1 to 10 s with logarithmic spacing and 100 samples. Note that the horizontal axis is not defined by a vertical wavenumber, k_z, because for any fixed resolution Δz the model supports waves with many vertical wavenumbers.

Figure 6 contains stability diagrams for schemes M1, ARK2(2,3,2)(1), ARK2(2,3,2)(2), and M2b. For schemes M1 and ARK2(2,3,2)(1), the stability is independent of Δz, as desired, only for up to approximately $n_{\text{lev}} = 57$ ($\Delta z \simeq 175$ m). In Figs. 6(a,b) the stable region for the approximate interval $n_{\text{lev}} \in [20, 57]$ ($\Delta z \in [175, 500]$ m) is under a straight line ~~with~~ for some $\Delta t = \Delta t_0$. For finer Δz ~~stability~~, the stable regions lie below a line with a constant slope for both schemes.

In contrast, for methods ARK2(2,3,2)(2) and M2b, stability is always controlled by the horizontal resolution: in Fig. 6(c) the stable region is below the horizontal line $\Delta t_0 \simeq 7.2$ s. To further support this conclusion, we also computed eigenvalues of the spacetime operator for method M2b, $\Delta t = 7$ s, and a few large values of n_{lev}, up to 600. The spacetime operator for all large n_{lev} was stable.
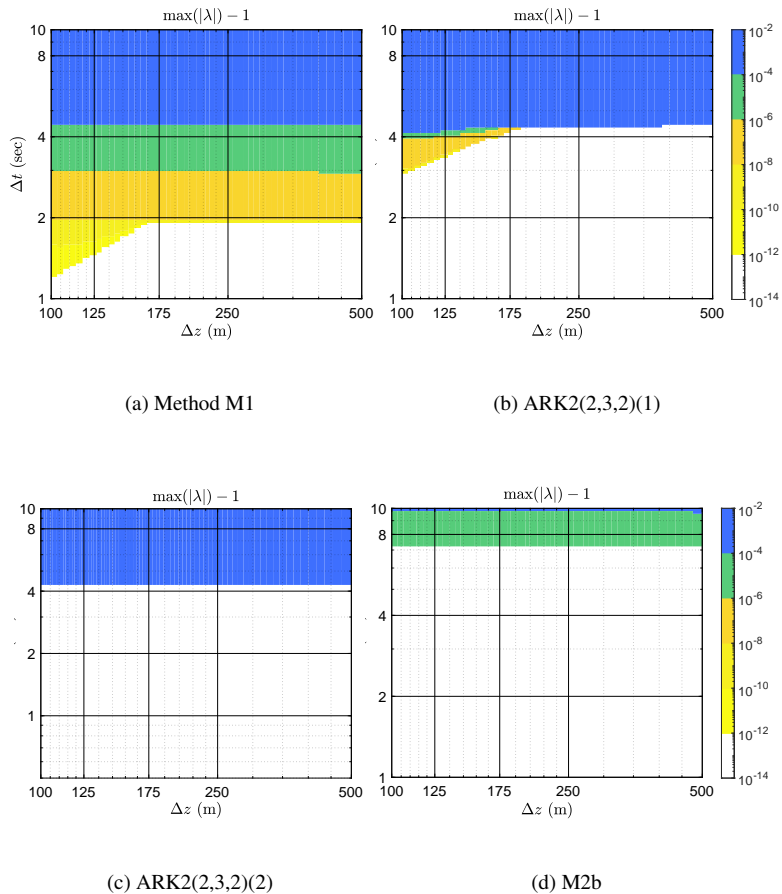
(a) Method M1   (b) ARK2(2,3,2)(1)

(c) ARK2(2,3,2)(2)   (d) M2b

Figure 6. Stability diagrams with respect to varying n_{lev}.

We do not present stability diagrams for Δz studies for other methods from this paper because they are identical to Fig. 6(c) up to the value of Δt_0. That is, the stability of methods IMEX-SSP2(2,3,2) and M2 methods is controlled by the horizontal wavelengths.

5   Conclusions

We developed a new framework to evaluate IMEX RK methods for atmospheric modeling. The framework uses a system of normal modes and is proven to be simple but more selective than the 2D acoustics system used in the literature. For example, the M1 method from Sect. 4.1 appears to be stable for a large set of timesteps and resolutions when using the 2D acoustics system. If the method is evaluated with the system of normal modes, it is unstable for the same set of timesteps and resolutions.

The new framework gives us insight to develop a set of second-order, ~~low storage, high CFL~~ low-storage, high-CFL IMEX RK methods to use in atmospheric dynamical cores. Furthermore, we use the spacetime operator built with the system of normal modes to investigate dispersion and dissipation of IMEX RK schemes for three types of waves, gravity, Rossby, and
425 acoustic.

One extension of this work would be to investigate selectiveness of the framework based not on the system of normal modes (12)–(16) but on a system of compressible Boussinesq equations as in Durran and Blossey (2012).

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