- 1 Dear editor,
- 2 Thank you very much for your efforts in the review process. We are happy to receive such good news!

3 We have made some minor changes according to the manuscript preparation requests of GMD, such

- 4 as: Changing "Figure" to "Fig.", changing "Section" to "Sect.", embedding fonts into the figures,
- 5 changed the table design to only have horizontal lines, double-checked the references and other minor
- 6 changes. Lastly we added to units to the RMSE in the abstract as requested.
- 7 We hope these details (and attached manuscript mark-up) sufficiently describes the manuscript changes
- 8 made. We are looking forward to the proof version of our manuscript.
- 9 Sincerely,
- 10 Bram Droppers on behalf of all co-authors

Simulating human impacts on global water resources using 1

VIC-5 2

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10 Correspondence to: Bram Droppers (bram.droppers@wur.nl) Abstract. Questions related to historical and future water resources and scarcity have been addressed by several macro-scale hydrological models. One of these models is the Variable Infiltration Capacity (VIC) model. However, further model developments were needed to holistically assess anthropogenic impacts on global water resources using VIC.

Our study developed VIC-WUR, which extends the VIC model with: (1) integrated routing, (2) surface and groundwater use for various sectors (irrigation, domestic, industrial, energy₂ and livestock), (3) environmental flow requirements for both surface and groundwater systems, and (4) dam operation. Global gridded datasets on sectoral demands were developed separately and used as an input to the VIC-WUR model.

20 Simulated national water withdrawals were in line with reported FAO national annual withdrawals (R² 21adjusted $\underline{\mathbb{R}}^2 > 0.8$), both per sector as well as per source. However, trends in time for domestic and 22 industrial water withdrawal were mixed compared to other previous studies. GRACE monthly terrestrial 23 water storage anomalies were well represented (global mean RMSE of 1.9 mm and 3.5 mm for annual 24 and interannual anomalies respectively), while groundwater depletion trends were overestimated. The 25 implemented human impact modules increased simulated streamflow performance for 370 out of 462 human-impacted GRDC monitoring stations, mostly due to the effects of reservoir operation. An 26 27 assessment of environmental flow requirements indicates that global water withdrawals have to be severely limited (by 39 %) to protect aquatic ecosystems, especially for groundwater withdrawals. 28

29 VIC-WUR has potential for studying impacts of climate change and anthropogenic developments on

30 current and future water resources and sectoral specific-water scarcity. The additions presented here

31 make the VIC model more suited for fully-integrated worldwide water-resource assessments.

32 1 Introduction

33 Questions related to historical and future water resources and scarcity have been addressed by several 34 macro-scale hydrological models over the last few decades (Liang et al., 1994; Alcamo et al., 1997; 35 Hagemann and Gates, 2001; Takata et al., 2003; Krinner et al., 2005; Bondeau et al., 2007; Hanasaki et al., 2008b; Vanvan Beek and Bierkens, 20082009; Best et al., 2011). Early efforts focussed on the 36 37 simulation of natural water resources and the impacts of land cover and climate change on water 38 availability (Oki et al., 1995; Nijssen et al., 2001a; Nijssen et al., 2001b). Recently, a larger focus has 39 been on incorporating anthropogenic impacts, such as water withdrawals and dam operations, into water 40 resource assessments (Alcamo et al., 2003; Haddeland et al., 2006b; Biemans et al., 2011; Wada et al., 41 2011b; Hanasaki et al., 2018).

42 Global water withdrawals increased eight-fold over the last century and are projected to increase further 43 (Shiklomanov, 2000; Wada et al., 2011a). Although water withdrawals are only a small fraction of the total global runoff (Oki and Kanae, 2006), water scarcity can be severe due to the variability of water in 44 45 both time and space (Postel et al., 1996). Already severe water scarcity is experienced by two-thirds of 46 the global population for at least part of the year (Mekonnen and Hoekstra, 2016). To stabilize water 47 availability for different sectors (e.g. irrigation, hydropower, and domestic uses) dams and reservoirs were built, which are able to strongly affect global river streamflow (Nilsson et al., 2005; Grill et al., 48 49 2019). In addition, groundwater resources are being extensively exploited to meet increasing water demands (Rodell et al., 2009; Famiglietti, 2014). 50

51 One of widely-used macro-scale hydrological models is the Variable Infiltration Capacity (VIC) model. 52 The model was originally developed as a land-surface model (Liang et al., 1994), but has been mostly used as a stand-alone hydrological model (Abdulla et al., 1996; Nijssen et al., 1997) using an offline 53 54 routing module (Lohmann et al., 1996; Lohmann et al., 1998a, b1998b, a). Where land-surface models 55 focus on the vertical exchange of water and energy between the land surface and the atmosphere, hydrological models focus on the lateral movement and availability of water. By combining these two 56 57 approaches, VIC simulations are strongly process-based and this, in turn, provides a good basis for climate-impact modelling. 58

59 VIC has been used extensively in studies ranging from: coupled regional climate model simulations 60 (Zhu et al., 2009; Hamman et al., 2016), combined river streamflow and water-temperature simulations 61 (van Vliet et al., 2016), hydrological sensitivity to climate change (Hamlet and Lettenmaier, 1999; 62 Nijssen et al., 2001a; Chegwidden et al., 2019), global streamflow simulations (Nijssen et al., 2001b), sensitivity in flow regulation and redistribution (Voisin et al., 2018; Zhou et al., 2018), and real-time 63 drought forecasting (Wood and Lettenmaier, 2006; Mo, 2008). Several studies used VIC to simulate the 64 65 anthropogenic impacts of irrigation and dam operation on water resources (Haddeland et al., 2006a; Haddeland et al., 2006b; Zhou et al., 2015; Zhou et al., 2016) based on the model setup of Haddeland et 66 67 al. (2006b). However, further developments were needed to holistically assess anthropogenic impacts on global water resources using VIC (Nazemi and Wheater, 2015a, b; Döll et al., 2016; Pokhrel et al., 68 2016). 69

70 Firstly, the VIC model did not yet include groundwater withdrawals or water withdrawals from 71 domestic, manufacturing, and energy (thermoelectric) sources. Although these sectors use less water 72 than irrigation (Shiklomanov, 2000; Grobicki et al., 2005; Hejazi et al., 2014) they are locally important 73 actors (Gleick et al., 2013)(Gleick et al., 2013), especially for the water-food-energy nexus (Bazilian et 74 al., 2011). Sufficient water supply and availability are essential for meeting a range of local and global 75 sustainable development goals related to water, food, energy, and ecosystems (Bijl et al., 2018). 76 Secondly, environmental flow requirements (EFRs) were often neglected (Pastor et al., 2014), even 77 though they are "necessary to sustain aquatic ecosystems which, in turn, support human cultures, economies, sustainable livelihoods, and well-being" (Brisbane Declaration, 2017). Anthropogenic 78 79 alterations already strongly affect freshwater ecosystems (Carpenter et al., 2011), with more than a 80 quarter of all global rivers experiencing very high biodiversity threats (Vorosmarty et al., 2010). By 81 neglecting EFRs, sustainable water availability for anthropogenic uses is overestimated (Gerten et al., 82 2013). Lastly, while the model setup of Haddeland et al. (2006b) already included important anthropogenic impact modules (i.e. irrigation and dam operation), these were not fully integrated yet. 83 84 Therefore multiple successive model runs were required (see SectionSect. 2.1) which was 85 computationally expensive, especially for global water resources assessments.

4

Recently version 5 of the VIC model (VIC-5) was released (Hamman et al., 2018), which focussed on 86 87 improving the VIC model infrastructure. These improvements provide the opportunity to fully integrate 88 human-impacts into the VIC model framework, while reducing computation times. Here the newly 89 developed VIC-WUR model is presented (named after the developing team at Wageningen University 90 and Research). The VIC-WUR model extends the existing VIC-5 model with several modules that 91 simulate the anthropogenic impacts on water resources. These modules will implement previous major 92 works on anthropogenic impact modelling as well as integrate environmental flow requirements into 93 VIC-5. The modules include: (1) integrated routing, (2) surface and groundwater use for various sectors 94 (irrigation, domestic, industrial, energy and livestock), (3) environmental flow requirements for both 95 surface and groundwater systems, and (4) dam operation.

96 The next section first describes the original VIC-5 hydrological model (SectionSect. 2.1), which 97 calculates natural water resource availability. Subsequently the integration of the anthropogenic impact 98 modules, which modify the water resource availability, are described (SectionSect. 2.2). Global 99 anthropogenic water uses for each sector are also estimated (SectionSect. 2.3). To assess the capability 100 of the newly developed modules, the VIC-WUR results were compared with FAO national water 101 withdrawals by sector and by source (FAO, 2016)(FAO, 2016); Huang et al. (2018), Steinfeld et al. 102 (2006)Steinfeld et al. (2006), and Shiklomanov (2000) data on water withdrawals by sector; GRACE 103 terrestrial water storage anomalies (NASA, 2002)(NASA, 2002); GRDC streamflow timeseries (GRDC, 104 2003)(GRDC, 2003); and Yassin et al. (2019) and Hanasaki et al. (2006) data on reservoir operation 105 (SectionSect. 3.2). VIC-WUR simulations results are also compared with various other state-of-the-art 106 global hydrological models. Lastly, the impacts of adhering to surface and groundwater environmental 107 flow requirements on water availability are assessed (SectionSect. 3.3). This assessment is included to 108 indicate the effects of the newly integrated surface and groundwater environmental flow requirements 109 on worldwide water availability.

110 2 Model development

111 2.1 VIC hydrological model

112 The basis of the VIC-WUR model is the Variable Infiltration Capacity model version 5 (VIC-5) (Liang 113 et al., 1994; Hamman et al., 2018). VIC-5 is an open source macro-scale hydrological model that 114 simulates the full water and energy balance on a (latitude - longitude) grid. Each grid cell accounts for 115 sub-grid variability in land cover and topography, and allows for variable saturation across the grid cell. 116 For each sub-grid the water and energy balance is computed individually (i.e. sub-grid do not exchange 117 water or energy between one another). The methods used to calculate the water and energy balance are 118 summarized in Appendix A, mainly based on the work of Liang et al. (1994). For the description of the global calibration and validation of the water balance one is referred to Nijssen et al. (2001b). 119

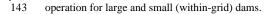
120 VIC version 5 (Hamman et al., 2018) upgrades did not change the model representation of physical 121 processes, but improved the model infrastructure. Improvements include the use of NetCDF for 122 input/output and the implementation of parallelization through Message Passing Interface (MPI). These 123 changes increase computational speed and make VIC-5 better suited for (computationally expensive) 124 global simulations. The most significant modification that enables new model applications is that VIC-125 5 also changed the processing order of the model. In previous versions all timesteps were processed for 126 a single grid cell before continuing to the next cell (time-before-space). In VIC-5 all grid cells are 127 processed before continuing to the next timestep (space-before-time). This development allows for 128 interaction between grid cells every timestep, which is important for full integration of the anthropogenic 129 impact modules, especially water withdrawals and dam operation.

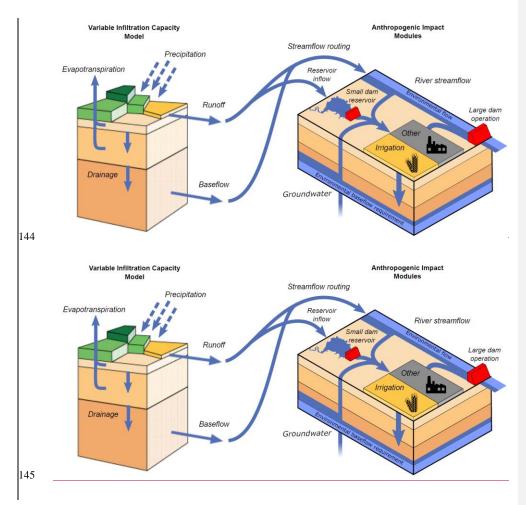
For example, surface and subsurface runoff routing to produce river streamflow was typically done as a post-process operation (Lohmann et al., 1996; Hamman et al., 2017), due to the time-before-space processing order of previous versions. In order for reservoirs to account for downstream water demand, an irrigation demand initialization was required. This initialization could either be an independent offline dataset (Voisin et al., 2013a)(Voisin et al., 2013a) or multiple successive model runs (Haddeland et al., 2006b). Since VIC-5 uses the space-before-time processing order, irrigation water demands and runoff routing could be simulated each timestep. The routing post-process was replaced by our newly

- 137 developed routing module, which simulates routing sequentially (upstream-to-downstream) based on
- the Lohmann et al. (1996) equations.

139 2.2 Anthropogenic-impact modules

140 VIC-WUR extends the existing VIC-5 though the addition of several newly implemented
141 anthropogenic-impact modules (FigureFig. 1). These modules include sector-specific water withdrawal
142 and consumption, environmental flow requirements for both surface and groundwater systems, and dam





146Figure 1: Schematic overview of the VIC-WUR model that includes the VIC-5 model (left) and several anthropogenic147impact modules, (right). Water from river streamflow, groundwater, and small (within-grid) reservoirs are available148for withdrawal. Surface and groundwater withdrawals are constrained by environmental flow requirements.149Withdrawn water is available for irrigation, domestic, industrial, energy, and livestock use. Unconsumed irrigation150water is returned to the soil column of the hydrological model. Unconsumed water for the other sectors is returned to151the river streamflow. Small reservoirs fill using surface runoff from the cell they are located, while large dam reservoirs152operate solely on rivers streamflow.

153 2.2.1 Water withdrawal and consumption

154 In VIC-WUR, sectoral water demands need to be specified for each grid cell (SectionSect. 2.3). To meet 155 water demands, water can be withdrawn from river streamflow, small (within-grid) reservoirs, and 156 groundwater resources. Streamflow withdrawals are abstracted from the grid cell discharge (as 157 generated by the routing module) and reservoir withdrawals are abstracted from small dam reservoirs 158 (located in the cell). Groundwater withdrawals are abstracted from the third layer soil moisture and an 159 (unlimited) aquifer below the soil column. Aquifer abstractions represent renewable and non-renewable 160 abstractions from deep groundwater resources. Subsurface runoff is used to fill the aquifer if there is a 161 deficit.

162 The partitioning of water withdrawals between surface and ground water resources is data driven 163 (similar to e.g. Döll et al., 2012; Voisin et al., 2017; Hanasaki et al., 2018). Partitioning was based on 164 the study of Döll et al. (2012), who estimated groundwater withdrawal fractions for each sector in around 165 15.000 national and sub-national administrative units. These groundwater fractions were based mainly 166 on information from the International Groundwater Resources Assessment Centre (IGRAC; un-167 igrac.org) database. Surface water withdrawals were partitioned between river streamflow and small 168 reservoirs relative to water availability. Groundwater withdrawals were first withdrawn from the third 169 soil layer, second from the (remaining) river streamflow resources and lastly from the groundwater 170 aquifer. This order was implemented to avoid overestimation of non-renewable groundwater 171 withdrawals as a result of errors in the partitioning data. Aquifer withdrawals are additionally limited 172 by the pumping capacity from Sutanudjaja et al. (2018), who estimated regional pumping capacities 173 based on information from IGRAC.

Water can also be withdrawn from the river streamflow of other 'remote' cells in delta areas. Since rivers cannot split in the routing module, the model is unable to simulate the redistribution of water resources in dendritic deltas. Therefore, streamflow at the river mouth is available for use in delta areas (partitioned based on demand) to simulate the actual water availability. Delta areas were delineated bythe global delta map of Tessler et al. (2015).

179 In terms of water allocation, under conditions where water demands cannot be met, water withdrawals 180 are allocated to the domestic, energy, manufacturing, livestock, and irrigation sector in that order. 181 Withdrawn water is partly consumed, meaning the water evaporates and does not return to the 182 hydrological model. Consumption rates were set at 0.15 for the domestic and 0.10 for the industrial 183 sector, based on the data of Shiklomanov (2000). The water consumption in the energy sector was based on Goldstein and Smith (2002) and varies per thermoelectric plant based on the fuel type and cooling 184 185 system. For the livestock sector the assumption was made that all withdrawn water is consumed. 186 Unconsumed water withdrawals for these sectors are returned as river streamflow. For the irrigation 187 sector, consumption was determined by the calculated evapotranspiration. Unconsumed irrigation water 188 remains in the soil column and eventually returns as subsurface runoff.

189 2.2.2 Environmental flow requirements

190 Water withdrawals can be constrained by environmental flow requirements (EFRs). These EFRs specify 191 the timing and quantity of water needed to support terrestrial river ecosystems (Smakhtin et al., 2004; 192 Pastor et al., 2019). Surface and groundwater withdrawals are constrained separately in VIC-WUR, 193 based on the EFRs for streamflow and baseflow respectively. EFRs for streamflow specify the minimum 194 river streamflow requirements while EFRs for baseflow specify the minimum subsurface runoff 195 requirements (from groundwater to surface water). Since baseflow is a function groundwater 196 availability, baseflow requirements are used to constrain groundwater (including aquifer) withdrawals. 197 Various EFR methods are available (Smakhtin et al., 2004; Richter et al., 2012; Pastor et al., 2014). Our 198 study used the Variable Monthly Flow (VMF) method (Pastor et al., 2014) to calculate the EFRs for 199 streamflows. VMF calculates the required streamflow as a fraction of the natural flow during high (30 200 %), intermediate (45 %) and low (60 %) flow periods, as described in Appendix B. The VMF method 201 performed favourably compared to other hydrological methods, in 11 case studies where EFRs were 202 calculated locally (Pastor et al., 2014). The advantage of the VMF method is that the method accounts 203 for the natural flow variability, which is essential to support freshwater ecosystems (Poff et al., 2010). 204 EFR methods for baseflow have been rather underdeveloped compared to EFR methods for streamflow. 205 However, a presumptive standard of 90 % of the natural subsurface runoff through time was proposed 206 by Gleeson and Richter (2018), as described in Appendix B. This standard should provide high levels of ecological protection, especially for groundwater dependent ecosystems. 207 208 Note that part of the EFRs for baseflow are already captured in the EFRs for streamflow, especially 209 during low-flow periods that are usually dominated by baseflows. However, the EFRs for baseflow 210 specifically limit local groundwater withdrawals while EFRs for streamflow include the accumulated 211 runoff from upstream areas. Also, the chemical composition of groundwater derived flows is inherently 212 different, making them a non-substitutable water flow for environmental purposes (Gleeson and Richter,

213 2018).

214 2.2.3 Dam operation

215 Due to the lack of globally available information on local dam operations, several generic dam operation 216 schemes were developed for macro-scale hydrological models to reproduce the effect of dams on natural 217 streamflow (Haddeland et al., 2006a; Hanasaki et al., 2006; Zhao et al., 2016; Rougé et al., 2019; Yassin et al., 2019). In VIC-WUR a distinction is made between 'small' dam reservoirs (with an upstream area 218 219 smaller than the cell area) and 'large' dam reservoirs, similar to Hanasaki et al. (2018), Wisser et al. 220 (2010a) and Döll et al. (2009). Small dam reservoirs act as buckets that fill using surface runoff of the 221 grid-cell they are located in and reservoirs storage can be used for water withdrawals in the same cell. 222 Large dam reservoirs are located in the main river and used the operation scheme of Hanasaki et al. (2006), as described in Appendix C. 223

The scheme distinguishes between two dam types: (1) dams that do not account for water demands downstream (e.g. hydropower dams or flood protection dams) and (2) dams that do account for water demand downstream (e.g. irrigation dams). For dams that do not account for demands, dam release is aimed at reducing annual fluctuations in discharge. For dams that do account for demands, dam release is additionally adjusted to provide more water during periods of high demand. The operation scheme
was validated by Hanasaki et al. (2006) for 28 reservoirs and was used in various other studies (Hanasaki
et al., 2008b; Döll et al., 2009; Pokhrel et al., 2012b; Voisin et al., 2013b; Hanasaki et al., 2018). Here,
the scheme was adjusted slightly to account for monthly varying EFRs and to reduce overflow releases,
which is described in Appendix C.

The Global Reservoir and Dam (GRanD) database (Lehner et al., 2011) was used to specify location, capacity, function (purpose), and construction year of each dam. The capacity of multiple (small- and large) dams located in the same cell were combined.

236 2.3 Sectoral water demands

237 VIC-WUR water withdrawals are based on the irrigation, domestic, industry, energy, and livestock 238 water demand in each grid-cell. Water demands represent the potential water withdrawal, which is 239 reduced when insufficient water is available. Irrigation demands were estimated based on the 240 hydrological model while water demands for other sectors are provided to the model as an input. 241 Domestic and industrial were estimated based on several socioeconomic predictors, while energy and 242 livestock water demands were derived from power plant and livestock distribution data. Due to data 243 limitations the energy sector was incomplete, and energy water demands were partly included in the 244 industrial water demands (which combined the remaining energy and manufacturing water demands). 245 For more details concerning sectoral water demand calculations the reader is referred to Appendix D.

246 2.3.1 Irrigation demands

Irrigation demands were set to increase soil moisture in the root zone so that water availability is not limiting crop evapotranspiration and growth. The exception is paddy rice irrigation (Brouwer et al., 1989), where irrigation was also supplied to keep the upper soil layer saturated. Water demands for paddy irrigation practices are relatively high compared to conventional irrigation practices due to increased evaporation and percolation. Therefore, the crop irrigation demands for these two irrigation practices were calculated and applied separately (i.e. in different sub-grids). Note that multiple cropping seasons are included based on the MIRCA2000 land-use dataset (Portmann et al., 2010) (see
 SectionSect. 3.1 for more details).

Total irrigation demands also included transportation and application losses. Note that transportation and application losses are not 'lost' but rather returned to the soil column without being used by the crop. The water loss fraction was based on Frenken and Gillet (2012), who estimated the aggregated irrigation efficiency for 22 United Nations sub-regions. Irrigation efficiencies were estimated based on the difference between AQUASTAT reported irrigation water withdrawals and calculated irrigation water requirements (Allen et al., 1998), using data on crop information (e.g. growing season, harvest area) from AQUASTAT.

262 2.3.2 Domestic and industrial demands

Domestic and industrial water withdrawals were estimated based on Gross Domestic Product (GDP) per capita and Gross Value Added (GVA) by industries respectively (from Bolt et al. (2018), Feenstra et al. (2015) and World bank (2010); see Appendix D for more details). These drivers do not fully capture the multitude of socioeconomic factors that influence water demands (Babel et al., 2007). However, the wide availability of data allows for extrapolation of water demands to data-scarce regions and future scenarios (using studies such as Chateau et al. (2014)).

269 Domestic water demands per capita (used for drinking, sanitation, hygiene, and amenity uses) were 270 estimated similar to Alcamo et al. (2003). Demands increased non-linearly with GDP per capita due to 271 the acquisition of water using appliances as household become richer. A minimum water supply is 272 needed for survival, and the saturation of water using appliances sets a maximum on domestic water 273 demands. Industrial water demands (used for cooling, transportation, and manufacturing) were 274 estimated similar to Flörke et al. (2013) and Voß and Flörke (2010). Industrial demands increased 275 linearly with GVA (as an indicator of industrial production). Since industrial water intensities (i.e. the 276 water use per production unit) vary widely between different industries (Flörke and Alcamo, 2004; 277 Vassolo and Döll, 2005; Voß and Flörke, 2010), the average water intensity was estimated for each country. Both domestic and industrial water demands were also influenced by technologicaldevelopments that increase water-use efficiency over time, as in Flörke et al. (2013).

280 Domestic water demands varied monthly based on air temperature variability as in Huang et al. (2018) 281 (based on Wada et al. (2011b)). Using this approach, water demands were higher in summer than in 282 winter, especially for counties with strong seasonal temperature differences. Domestic water demand per capita were downscaled using the HYDE3.2 gridded population maps (Goldewijk et al., 2017). 283 284 Industrial water demands were kept constant throughout the year. Industrial demands were downscaled from national to grid cell values using the NASA Back Marble night-time light intensity map (Roman 285 286 et al., 2018). National industrial water demands were allocated based on the relative light intensity per 287 grid cell for each country.

288 2.3.3 Energy and livestock demands

289 Energy water demands (used for cooling of thermoelectric plants) were estimated using data from van 290 Vliet et al. (2016). Water use intensity for generation (i.e. the water use per generation unit) was 291 estimated based on the fuel and cooling system type (Goldstein and Smith, 2002), which was combined 292 with the generation capacity. Note that the data only covered a selection of the total number of 293 thermoelectric power plants worldwide. Around 27 % of the total (non-renewable) global installed 294 capacity between 1980 and 2011 was included in the dataset due to lack of information on cooling 295 system types for the majority of thermoelectric plants. To avoid double counting, energy water demands 296 were subtracted from the industrial water demands.

Livestock water demands (used for drinking and animal servicing) were estimated by combining the Gridded Livestock of the World (GLW3) map (Gilbert et al., 2018) with the livestock water requirement reported by <u>Steinfeld et al. (2006)Steinfeld et al. (2006)</u>. Eight varieties of livestock were considered: cattle, buffaloes, horses, sheep, goats, pigs, chicken, and ducks. Drinking water demands varied monthly based on temperature as described by <u>Steinfeld et al. (2006)Steinfeld et al. (2006)</u>, whereby drinking water requirements were higher during higher temperatures.

303 3 Model application

304 3.1 Setup

VIC-WUR results were generated between 1979 and 2016, excluding a spin-up period of one year (analysis period from 1980 to 2016). The model used a daily timestep (with a 6-hourly timestep for snow processes) and simulations were executed on a 0.5° by 0.5° grid (around 55 km at the equator) with three soil layers per grid cell. Soil and (natural) vegetation parameters were the same as in Nijssen et al. (2001c) (disaggregated to 0.5°), who used various sources to determine the soil (Cosby et al., 1984; Carter and Scholes, 1999) and vegetation parameters (Calder, 1993; Ducoudre et al., 1993; Sellers et al., 1994; Myneni et al., 1997).

Nijssen et al. (2001c) used the Advanced Very High Resolution Radiometer vegetation type database (Hansen et al., 2000) to spatially distinguish 13 land cover types. The land cover type 'cropland' in the original land-cover dataset was replaced by cropland extents from the MIRCA2000 cropland dataset (Portmann et al., 2010). MIRCA2000 distinguishes the monthly growing area(s) and season(s) of 26 irrigated and rain-fed crop types around the year 2000. Crop types were aggregated into three land cover types: rain-fed, irrigated, and paddy rice cropland. The natural vegetation was proportionally rescaled to make up discrepancies between the natural vegetation and cropland extents.

Cropland coverage (the cropland area actually growing crops) varied monthly based on the crop growing areas of MIRCA2000. The remainder was treated as bare soil. Cropland vegetation parameters (e.g. Leaf Area Index (LAI), displacement, vegetation roughness and albedo) vary monthly based on the crop growing seasons and the development-stage crop coefficients of the Food and Agricultural Organisation (Allen et al., 1998).

The latest WATCH forcing data Era Interim (aggregated to 6 hourly), developed by the EU Water and Global Change (WATCH; Harding et al., 2011) project, was used as climate forcing (WFDEI; Weedon et al., 2014). The dataset provides gridded historical climatic variables of minimum and maximum air temperature, precipitation (as the sum of snowfall and rainfall, GPCC bias-corrected), relative humidity, pressure, and incoming shortwave and longwave radiation. For naturalized simulations only the routing module was used. For the human-impact simulations the sectoral water withdrawals and dam operation modules were turned on in the model simulations. For the EFR-limited simulations water withdrawals and dam operations were constrained as described.

332 3.2 Validation and evaluation

In order to validate the VIC-WUR human-impact modules, water withdrawal, terrestrial total water storage anomalies, <u>and</u> streamflow and reservoir operation simulations were compared with observations. The validation specifically focused on the effects of the newly included human-impact modules, meaning that streamflow and total-water storage anomaly results are shown for river basins that are strongly influenced by human activities. A general validation for streamflow and terrestrial total water storage anomalies (including basins with limited human activities) is shown in Appendix E.

339 3.2.1 Sectoral water withdrawals

340 Simulated global domestic, industrial, livestock, and irrigation mean water withdrawals were 310, 771, 341 36, and 2202 km3 year-1 respectively for the period of 1980 to 2016. Sectoral water withdrawals were 342 compared with FAO national annual water withdrawals (FAO, 2016)(FAO, 2016), monthly withdrawal 343 data from Huang et al. (2018), and annual withdrawal data from Shiklomanov (2000) and Steinfeld et 344 al. (2006)Steinfeld et al. (2006). For the latter studies, water withdrawals were aggregated by region 345 (world, Africa, Asia, Americas, Europe and Oceania). Note that Huang et al. (2018) irrigation water 346 withdrawals integrate results of four other macro-scale hydrological models (WaterGAP, H08, LPJmL, 347 PCR-GLOBWB), using the same land-use and climate setup as our study. Results from individual 348 macro-scale hydrological models are also shown.

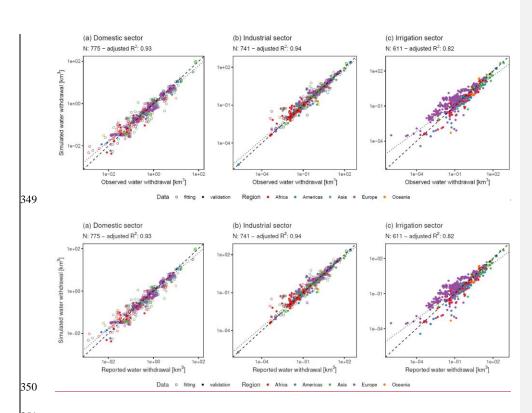
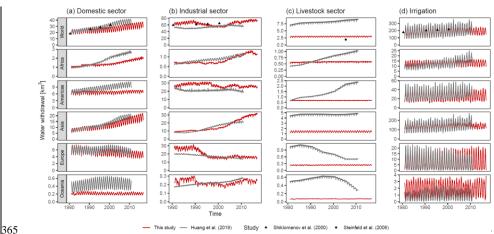
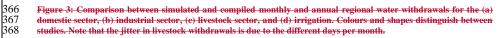
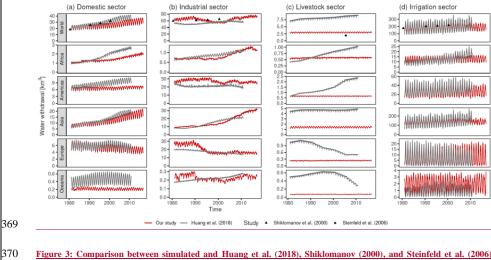


Figure 2: Comparison between simulated and <u>FAO</u> reported national annual water withdrawals for the (a) domestic, (b) industrial, and (c) irrigation sector. Colours distinguish between regions. Open circles were also used in the calibration of the water withdrawal demands. The dashed line indicates the 1:1 ratio and the spotted line indicates the simulated best linear fit. Note the log-log axis which is used to display the wide range of water withdrawals. The **R**² adjusted <u>R</u>² is also based on the log values.

356 Simulated domestic, industrial, and irrigation water withdrawals correlated well to reported national 357 water withdrawals, with adjusted R² of 0.93, 0.94, and 0.82 for domestic, industrial, and irrigation water 358 withdrawal respectively (Figure Fig. 2a-c). Generally, smaller water withdrawals were overestimated 359 and larger water withdrawals were underestimated. Differences for the domestic and industrial sector 360 were small and probably related to the fact that smaller countries were poorly delineated on a 0.5° by 0.5° grid. However, irrigation differences were larger with overestimations of irrigation water 361 362 withdrawals in (mostly) Europe. Since irrigation water demands are the results of the simulated water balance, overestimations would indicate a regional underestimation of water availability for Europe or 363 364 differences in irrigation efficiency.









374 When domestic, industrial, and livestock water withdrawals were compared to other studies, results were

375 mixed (figureFig. 3a-c). Simulated domestic withdrawals followed a similar trend in time. However,

376 simulated domestic water withdrawals trends were overall somewhat underestimated with a mean bias

377 of 54 km³ year⁻¹ compared to Huang et al. (2018). Asia is the main contributor to the global underestimation, but results are similar in most regions. Simulated industrial water withdrawal were (mostly) higher in our study with a mean bias of 107 km³ year⁻¹ compared to Huang et al. (2018) but only a mean bias of 5 km³ year⁻¹ compared to Shiklomanov (2000). Also, industrial water withdrawal trends in time were less consistent.

Withdrawal differences for the domestic and industrial sector are probably due to the limited data availability. Our approach to compute water demands was data-driven and sensitive to data gaps (as opposed to Huang et al. (2018) who also combined model results). For example, domestic withdrawal data for China was not available before 2007 and industrial withdrawal data was limited before 1990. Also, data on the disaggregation of industrial sectors (e.g. energy and mining) was limited, which can be important sectors in the water-food-energy nexus.

For livestock water withdrawals there is a large discrepancy between the Huang et al. (2018) and **Steinfeld et al.** (2006)Steinfeld et al. (2006). Both studies used similar livestock maps, but there was large differences in livestock water intensity [litre animal⁻¹ year⁻¹]. Since our study used <u>Steinfeld et al.</u> (2006)Steinfeld et al. (2006) to estimate livestock water intensity, our results were closer to their values (slightly higher due to the inclusion of buffaloes, horses, and ducks). Note that Huang et al. (2018) shows trends in livestock water withdrawals while our study used static livestock maps.

394 Table 1: GlobalAverage annual global irrigation water withdrawals as calculated by several global hydrological models. 395 ***Includes livestock withdrawals.

		Representative			
Model	Irrigation withdrawal [km3 year 1]		Reference	-	Formatted: Font: Not Bold
		years			Formatted: Line spacing: Double
				\mathbb{H}	Formatted: Font: Not Bold, Not Superscript/ Subscript
VIC-WUR	2202 (± 60)	1980-2016	Our study		Formatted: Font: Not Bold
**>0	(a) 2810	(a) 1995	(a) Hanasaki et al. (2008a)		Formatted: Font: Not Bold, Not Superscript/ Subscript
H08	(b) 2544 (± 75)	(b) 1984 - 2013	(b) Hanasaki et al. (2018)	/	Formatted Table
MATSIRO	(a) 2158 (± 134)	(a) 1983 - 2007	(a) Pokhrel et al. (2012a)	١	Formatted: Font: Not Bold
	(b) 3028 (± 171)	(b) 1998 - 2002	(b) Pokhrel et al. (2015)		
LPJmL	2555	1971 - 2000	Rost et al. (2008)		
PCR-GLOB	(a) 2644	(a) 2010	(a) Wada and Bierkens (2014)		Formatted: English (United Kingdom)
FCK-0LOD	(b) 2309 <u>***</u>	(b) 2000 - 2015	(b) Sutanudjaja et al. (2018)		Formatted: English (United Kingdom)
WaterGAP	(a) 3185	(a) 1998-2002	(a) Döll et al. (2012)		Formatted: English (United Kingdom)

1		(b) 2400	(b) 2003 - 2009	(b) Döll et al. (2014)		Formatted: English (United Kingdom)
	WBM	2997	2002	Wisser et al. (2010b).		Formatted: English (United Kingdom)
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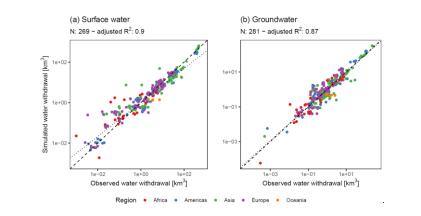
Simulated irrigation water withdrawals were within range of other macro-scale hydrological model estimates (Table 1). Simulated monthly variability in irrigation water withdrawals is reduced compared to the compiled results of Huang et al. (2018) (FigureFig. 3d), especially in Asia. Also, trends in time are less pronounces as can be seen in Africa. These differences may indicate a relative low weather/climate sensitivity of evapotranspiration in VIC-WUR, as annual and interannual weather changes affect irrigation water demands to a lesser degree.

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402 3.2.2 Groundwater withdrawals and depletion

413

Simulated global mean withdrawals were 2327 and 992 km3 year-1 for surface and groundwater 403 respectively for the period of 1980 to 2016. Of the global groundwater withdrawals, 334 km³ year⁻¹ 404 405 contributed to groundwater depletion. Simulated ground and surface water withdrawals and terrestrial 406 total water storage anomalies were compared FAO national annual water withdrawals (FAO, 407 2016)(FAO, 2016) and monthly storage anomaly data from the GRACE satellite (NASA, 2002).(NASA, 408 2002). GRACE satellite total water storage anomalies were used to validate total water storage dynamics 409 as well as groundwater exploitation contributing to downward trends in total water storage. Groundwater 410 depletion results from other macro-scale hydrological models are shown as well. In order to compare 411 the simulation results to the GRACE dataset, a 300km gaussian filer was applied to the simulated data 412 (similar to Long et al. (2015)).



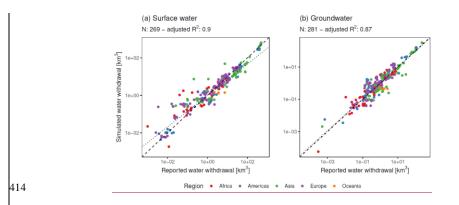
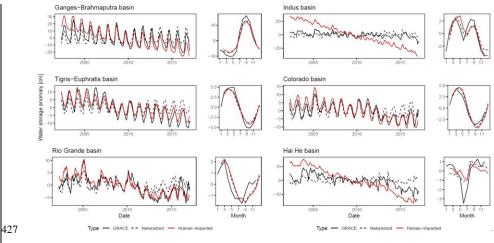


Figure 4: Comparison between simulated and <u>FAO</u> reported national annual water withdrawals from (a) surface water
and (b) groundwater. Colours distinguish between regions. The dashed line indicates the 1:1 ratio and the spotted line
indicates the simulated best linear fit. Note the log-log axis which is used to display the wide range of water withdrawals.
The R²-adjusted <u>R²</u> is also based on the log values.

419 Simulated surface and groundwater withdrawals correlated well to the reported national water withdrawals, with adjusted R² of 0.90 and 0.87 for surface and groundwater respectively (Figure Fig. 4a-420 421 b). Surface water withdrawals were overestimated for low withdrawals and underestimated for large 422 withdrawals. There is a weak correlation (-0.35) between the underestimations in surface water 423 withdrawals and the overestimation in groundwater withdrawals, meaning water withdrawal differences 424 could be related to the partitioning between surface and groundwater resources. Also, it is likely that 425 low water demands are overestimated (as discussed in SectionSect. 3.2.1), resulting in an overestimation 426 of low surface water withdrawals.



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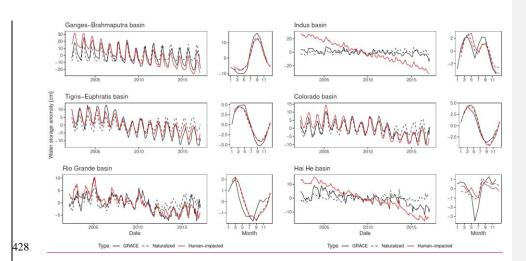


Figure 5: Comparison between simulated and <u>GRACE</u> observed monthly terrestrial total water storage anomalies.
 Figures indicate timeseries and multi-year mean average for naturalized simulations (dashed), human-impacted simulations (red), and observed (black) terrestrial total water storage anomalies.

432 Simulated monthly terrestrial water storage anomalies correlated well to the GRACE observations, with 433 mean annual and inter-annual Root Mean Squared Error (RMSE) of 1.9 mm and 3.5 mm respectively. 434 The difference between annual and inter annual performance was primarily due to the groundwater 435 depletion process (FigureFig. 5). Simulated groundwater depletion was (mostly) overestimated (e.g. 436 Indus and Hai He basins), with higher declining trends in terrestrial total water storage for most basins. 437 However, compared to other macro-scale hydrological models, simulated groundwater withdrawal and 438 exploitation was within range (Table 2), even though total groundwater withdrawals were relatively 439 high. 440 indicate withdrawal that 441 442

443 and de Graaf et al. (2017)). For example, processes such as wetland recharge and groundwater flows

444 between cells are not simulated, even though these could decrease groundwater depletion

⁴⁴⁵Table 2: GlobalAverage annual global
hydrological models.groundwater withdrawals and depletion as calculated by several global
hydrological models.

Model	Groundwater withdrawal [km3 year-1]	Groundwater depletion [km3 year-1]	Representative years	Reference
VIC-WUR	992 (± 51)	316 (± 63)	1980 - 2016	Our study
H08	789 (± 30)	182 (± 26)	1984 - 2013	Hanasaki et al. (2018)
MATSIRO	570 (± 61)	330	1998 - 2002	Pokhrel et al. (2015)
GCAM		(a) 600	(a) 2005	(a) Kim et al. (2016)
		(b) 550	(b) 2000	(b) Turner et al. (2019)
PCR-	(a) 952	(a) 304	(a) 2010	(a) Wada and Bierkens (2014)
GLOB	(b) 632	(b) 171	(b) 2000 - 2015	(b) Sutanudjaja et al. (2018)
WaterGAP	(a) 1519	(a) 250	(a) 1998-2002	(a) Döll et al. (2012)
WaterOAI	(b) 888	(b) 113	(b) 2000 - 2009	(b) Döll et al. (2014)
groundwate	e FAO compa r is overestim	rison, these results see ated. However, conclu-	ems to indicate	that withdrawal partitioning towar groundwater depletion are limited idy (as discussed by Konikow (20)
and de Graa	af et al. (2017)). For example, proces	sses such as wet	land recharge and groundwater flow

452 3.2.3 Discharge modification

453 Simulated discharge was compared to GRDC station data (GRDC, 2003)(GRDC, 2003) for various 454 human-impacted rivers. Stations were selected if the upstream area was larger than 20,000 km2, matched the simulated upstream area at the station location, and the available data spanned more than 2 years. 455 456 Subsequently, stations where the human-impact modules did not sufficiently impacted discharge were 457 omitted. In order validate the reservoir operation more thoroughly, simulated reservoir inflow, storage, 458 and release was compared with operation data from Hanasaki et al. (2006) and Yassin et al. (2019). 459 Reservoirs were included if the simulated storage capacity (which is the combined storage capacity of 460 all large dams in a grid) was similar to observed storage capacity.

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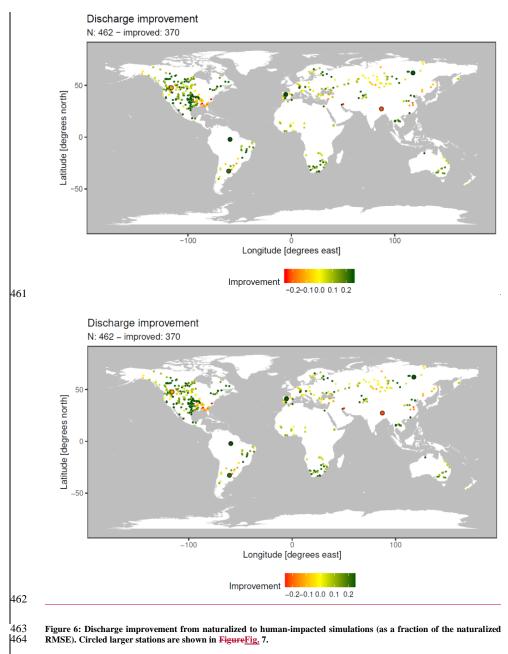


Figure 6: Discharge improvement from naturalized to human-impacted simulations (as a fraction of the naturalized RMSE). Circled larger stations are shown in FigureFig. 7.

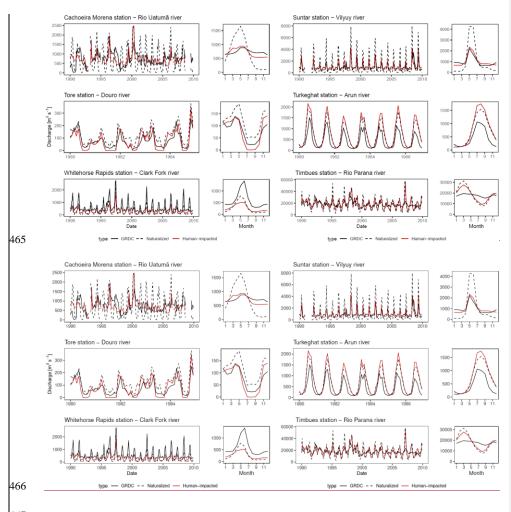
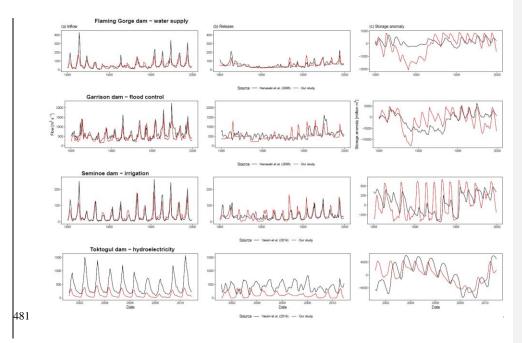


Figure 7: Comparison between simulated and <u>GRDC</u> observed discharge. Figures indicate timeseries and multi-year average of for naturalized simulations (dashed), human-impacted simulations (red), and observed (black) discharge. The inclusion of the human-impact modules improved discharge performance, measured in RMSE, for 370 out of 462 stations (80 %; FigureFig. 6 and 7). Improvements were mainly due to the effects of reservoir operation on discharges (e.g. Cachoeira Morena and Suntar stations), but also due to withdrawal reductions (e.g. Tore station). Reservoir effects on discharge were sometimes underestimated however (e.g. Timbues station).

Decreased performance was mostly related to under or overestimations of (calibrated) natural streamflow which was subsequently exacerbated by reservoir operation and water withdrawals. For example, the Clark Fork river naturalized streamflow was underestimated, which was subsequently further underestimated by the human-impact modules (Whitehorse Rapids station). Also, increases in discharge due to groundwater withdrawals could increase naturalized streamflow (e.g. Turkeghat station). Further improvements to discharge performance would most likely require either a recalibration of the VIC model parameters.



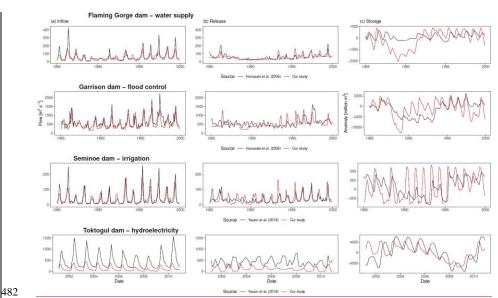




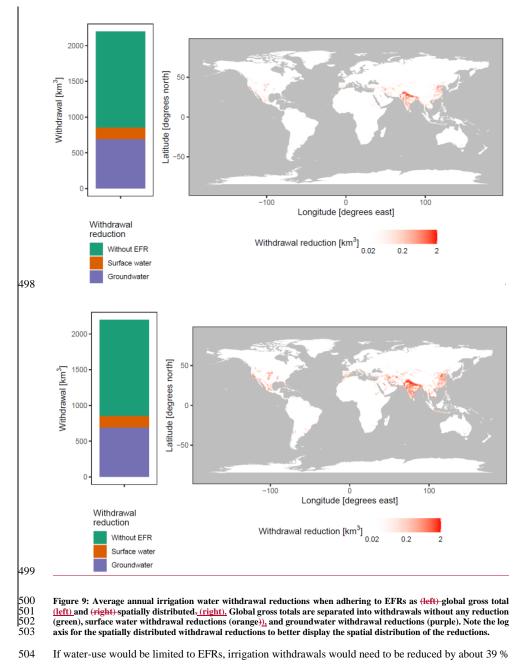
Figure 8: Comparison between simulated and <u>Hanasaki et al. (2006) and Yassin et al. (2019)</u> observed reservoir operation. Figures indicate timeseries and multi-year averages of (a) inflow, (b) release, and (c) storage anomalies for human-impacted simulations (red) and observations (black).

For individual reservoirs, operation characteristics were generally well simulated (Figure Fig. 8), with 487 reductions in annual discharge variations (e.g. Flaming Gorge and Garrison dams) and increased water 488 release for irrigation (e.g. Seminoe dam). However, due to changes in locally simulated and actual inflow, dam operation can take on different characteristics (e.g. Toktogul dam). Also, peak discharge 489 490 events caused by reservoir overflow (as also described by Masaki et al. (2018)) were not always sufficiently represented in the observations (e.g. Garisson dam). These differences indicate locally 491 varying reservoir operation strategies. Several studies have developed reservoir operation schemes that 492 493 can be calibrated to the local situation (Rougé et al., 2019; Yassin et al., 2019). However, worldwide 494 implementations of these operation schemes remains limited by data availability.

495 **3.3** Integrated environmental flow requirements

496 In order to assess the impact and capabilities of the newly integrated environmental flow requirements

497 (EFRs) module, simulated water withdrawals with and without adhering to EFRs were compared.



505 (851 km³ year⁻¹) (FigureFig. 9a). Under the strict requirements used in our study, 81 % (693 km³ year⁻¹

¹) of the reduction could be attributed to limitations imposed on groundwater withdrawals. Subsequently, the impact of the environmental flow requirements (if adhered to) would be largest in groundwater dependent regions (FigureFig. 9b). Note that, due to the full integration of EFRs, downstream surface water withdrawals increased by 98 km³ year⁻¹ when limiting groundwater withdrawals on top of limiting surface water withdrawals, due to increase subsurface runoff.

511 Reductions due to EFRs were similar to Jägermeyr et al. (2017), who calculated irrigation withdrawal 512 reductions of 41 % (997 km³ year⁻¹) assuming only surface water abstractions. In our study, surface 513 water reductions were smaller since the strict groundwater requirements increases subsurface runoff to 514 surface waters. It can be discussed to what extent the EFRs for baseflow were too constricting, since 515 they were based on the relatively stringent EFR for streamflow of Richter et al. (2012) (10 % of the 516 natural streamflow). However, in the absence of any other standards, this baseflow standard remains the 517 best available. Note that, even when accounting for EFRs for baseflow on a grid scale, withdrawals 518 could still have local and long-term impacts that are not captured by the model. The timing, location, 519 and depth of groundwater withdrawals are important factors due to their interactions with the local 520 geohydrology, as discussed by Gleeson and Richter (2018).

521 4 Conclusion

522 <u>4 Conclusions</u>

The VIC-WUR model introduced in this paper aims to provide new opportunities for global water resource assessments using the VIC model. Accordingly, several anthropogenic impact modules, based on previous major works, were integrated into the VIC-5 macro-scale hydrological model: domestic, industrial, energy, livestock₂ and irrigation water withdrawals from both surface water and groundwater as well as an integrated environmental flow requirement module and dam operation module. Global gridded datasets on domestic, industrial, energy₂ and livestock demand were developed separately and used to force the VIC-WUR model. 530 Simulated national water withdrawals were in line with reported national annual withdrawals (R² 531 adjusted $\mathbb{R}^2 > 0.8$; both per sector as per source). However, the data-oriented methodology used to derive 532 sectoral water demands resulted in different withdrawal trends over time compared to other studies 533 (Shiklomanov, 2000; Huang et al., 2018). While the current setup to estimate sectoral water demands is 534 well suited for future water withdrawal estimations, there are various other approaches (e.g. Alcamo et al., 2003; Vassolo and Döll, 2005; Shen et al., 2008; Hanasaki et al., 2013; Wada and Bierkens, 2014). 535 536 As the model setup of VIC-WUR allows for the evaluation of other sectoral water demand inputs (on various temporal aggregations), several different approaches can be used depending on the focus region 537 538 and data-availability for calibration. Terrestrial water storage anomaly trends were well simulated (mean annual and inter-annual RMSE of 1.9 mm and 3.6 mm respectively), while groundwater exploitation 539 540 was overestimated. Overestimated groundwater depletion rates are likely related to an over-partitioning 541 of water withdrawals to groundwater. The implemented human impact modules increased simulated 542 discharge performance (370 out of 462 stations), mostly due to the effects of reservoir operation.

An assessment of the effect of EFRs shows that, when one would adhere to these requirements, global water withdrawals would be severely limited (39 %). This limitation is especially the case for groundwater withdrawals, which, under the strict requirements used in our study, need to be reduced by 81 %.

547 VIC-WUR has potential for studying impacts of climate change and anthropogenic developments on 548 current and future water resources and sectoral specific-water scarcity. The additions presented here 549 make the VIC model more suited for fully-integrated worldwide water-resource assessments and 550 substantially decrease computation times compared to Haddeland et al. (2006a).

551 <u>5 Appendices</u>

552 51_Code availability

All code for the VIC-WUR model is freely available at github.com/wur-wsg/VIC (tag VIC-WUR.2.1.0
 DOI 10.5281/zenodo.3934325) under the GNU General Public License, version 2 (GPL-2.0). VIC

555	WUR documentation can be found at viewur.readthedoes.io. The original VIC model is freely available
556	at github.com/UW Hydro/VIC (tag VIC.5.0.1; DOI 10.5281/zenodo.267178) under the GNU General
557	Public License, version 2 (GPL 2.0). VIC documentation can be found at vic.readthedoes.io.
558	Documentation and scripts concerning input data used in our study is freely available at
559	github.com/bramdr/VIC_support (tag VIC-WUR.2.1.0; DOI 10.5281/zenodo.3934363) under the GNU
560	General Public License, version 3 (GPL-3.0).

561 6 Appendix

562 6.15.1 Appendix A: VIC water and energy balance

563 In VIC each sub-grid computes the water and energy balance individually (i.e. sub-grid do not exchange water or energy between one another). For the water balance, incoming precipitation is partitioned 564 between evapotranspiration, surface and subsurface runoff, and soil water storage. Potential 565 566 evapotranspiration is based on the Penman-Monteith equation without the canopy resistance 567 (Shuttleworth, 1993). The actual evapotranspiration is calculated by two methods, based on whether the 568 land cover is vegetated or not (bare soil). Evapotranspiration of vegetation is constrained by stomatal, 569 architectural and aerodynamic resistances and is partitioned between canopy evaporation and 570 transpiration based on the intercepted water content of the canopy (Deardorff, 1978; Ducoudre et al., 571 1993). Bare soil evaporation is constrained by the saturated area of the upper soil layer. The saturated 572 area is variable within the grid since (as the model name implies) the infiltration capacity of the soil is 573 assumed heterogeneous (Franchini and Pacciani, 1991). Saturated areas evaporate at the potential 574 evaporation rate while in unsaturated areas evaporation is limited. Surface runoff is produced by 575 precipitation over saturated areas. Precipitation over unsaturated areas infiltrates into the upper soil layer 576 and drains through the soil layers based on the gravitational hydraulic conductivity equations of Brooks 577 and Corey (1964). Brooks and Corey (1964). In the first and second layer water is available for 578 transpiration, while the third layer is assumed to be below the root zone. From the third layer baseflow 579 is generated based on the non-linear Arno conceptualization (Franchini and Pacciani, 1991). Baseflow increases linearly with soil moisture content when the moisture content is low. At higher soil moisturecontents the relation is non-linear, representing subsurface storm-flows.

582 For the energy balance, incoming net radiation is partitioned between sensible, latent, and ground heat 583 fluxes and energy storage in the air below the canopy. The energy storage below the canopy is omitted 584 if it is considered negligible (e.g. the canopy surface is open or close to the ground). The latent heat flux is determined by the evapotranspiration as calculated in the water balance. The sensible heat flux is 585 586 calculated based on the difference between the air and surface temperature and the ground heat flux is calculated based on the difference between the soil and surface temperature. Since the incoming net 587 588 radiation is also a function of the surface temperature (specifically the outgoing longwave radiation), 589 the surface temperature is solved iteratively. Subsurface ground heat fluxes are calculated assuming an 590 exponential temperature profile between the surface and the bottom of the soil column, where the bottom 591 temperature is assumed constant. Later model developments included options for finite difference 592 solutions of the ground temperature profile (Cherkauer and Lettenmaier, 1999), spatial distribution of 593 soil temperatures (Cherkauer and Lettenmaier, 2003), a quasi-2-layer snow-pack snow model (Andreadis et al., 2009), and blowing snow sublimation (Bowling et al., 2004). 594

595 6.25.2 Appendix B: EFRs for surface and groundwater

VIC-WUR used the Variable Monthly Flow (VMF) method (Pastor et al., 2014) to limit surface water withdrawals. The VMF method (Pastor et al., 2014) calculates the EFRs for streamflow as a fraction of the natural flow during high (Eq. A.1), intermediate (Eq. A.2), and low (Eq. A.3) flow periods. The presumptive standard Gleeson and Richter (2018) is used to limit groundwater withdrawals (including aquifer groundwater withdrawals). This standard calculates the EFRs for baseflow as 90 % of the natural subsurface runoff through time (Eq. A.4). Here, daily instead of monthly EFRs were used to better capture the monthly flow variability.

$$603 \quad EFR_{s,d} = 0.6 \cdot NF_{s,d} \qquad \qquad \text{Eq. (A.1)}$$

604 where $NF_{s,d} \leq 0.4 \cdot NF_{s,y}$

605 $EFR_{s,d} = 0.45 \cdot NF_{s,d}$ Eq. (A.2)

31

606 where $0.4 \cdot MF_{s,y} < NF_{s,d} \le 0.8 \cdot NF_{s,y}$

607
$$EFR_{s,d} = 0.3 \cdot NF_{s,d}$$
 Eq. (A.3)
608 where $NF_{s,d} > 0.8 \cdot NF_{s,y}$

$$609 \quad EFR_{h,d} = 0.9 \cdot NF_{h,d}$$
 Eq. (A.4)

610 Where $EFR_{s,d}$ is the daily EFRs for streamflow [m³ s⁻¹], $EFR_{b,d}$ the daily EFRs for baseflow [m³ s⁻¹], 611 $NF_{s,d}$ is the average natural daily streamflow [m³ s⁻¹], and $NF_{s,y}$ is the average natural yearly streamflow 612 [m³ s⁻¹], and $NF_{b,d}$ is the average natural daily baseflow [m³ s⁻¹].

EFRs for streamflow and baseflow were based on VIC-WUR naturalized simulations between 1980 and
2010. Average natural daily flows were calculated as the interpolated multi-year monthly average flow
over the simulation period.

616 6.35.3 Appendix C: Dam operation scheme

617 VIC-WUR used a dam operation scheme based on Hanasaki et al. (2006). Target release (i.e. the 618 estimated optimal release) was calculated at the start of the operational year. The operational year starts 619 at the month where the inflow drops below the average annual inflow, and thus the storage should be at 620 its desired maximum. The scheme distinguished between two dam types: (1) dams that did not account 621 for water demands downstream (e.g. hydropower dams or flood control) and (2) dams that did account 622 for water demands downstream (e.g. irrigation dams). The original scheme of Hanasaki et al. (2006) 623 also accounts for EFRs, which were fixed at half the annual mean inflow. Other studies lowered the 624 requirements to a tenth of the mean annual inflow, increasing irrigation availability and preventing 625 excessive releases (Biemans et al., 2011; Voisin et al., 2013b). In our study the original dam operation scheme was adapted slightly to account for monthly varying EFRs. 626

For dams that did not account for demands, the initial release was set at the mean annual inflow corrected
by the variable EFRs (Eq. A.5). For dams that did account for demands, the initial release was increased
during periods of higher water demand. If demands were relatively high compared to the annual inflow,
the release was corrected by the demand relative to the mean demand (Eq. A.6). If demands were

631 relatively low compared to the annual inflow, release was corrected based on the actual water demand

632 (Eq. A.7).

634
$$R'_{m} = EFR_{s,m} + (I_{y} - EFR_{s,y})$$
 Eq. (A.5)

 $635 \qquad where D_y = 0$

636
$$R'_m = EFR_{s,m} + (I_y - EFR_{s,y}) * \frac{D_m}{D_y}$$
 Eq. (A.6)

637 where
$$D_y > 0$$
 and $D_y > (I_y - EFR_{s,y})$

638
$$R'_m = EFR_{s,m} + (I_y - EFR_{s,y}) - D_y + D_m$$
 Eq. (A.7)

639 where
$$D_y > 0$$
 and $D_y \le (I_y - EFR_{s,y})$

640 Where R'_m is the initial monthly target release $[m^3 \ s^{-1}]$, $EFR_{s,m}$ is the average monthly EFR for 641 streamflow demand $[m^3 \ s^{-1}]$, I_y is the average yearly inflow $[m^3 \ s^{-1}]$, $EFR_{s,y}$ is the average yearly EFR 642 for streamflow $[m^3 \ s^{-1}]$, D_m is the average monthly water demand $[m^3 \ s^{-1}]_{\perp}$ and D_y is the average yearly 643 water demand $[m^3 \ s^{-1}]$.

As in Hanasaki et al. (2006), the initial target release was adjusted based on storage and capacity. Target release was adjusted to compensate differences between the current storage and the desired maximum storage (Eq. A.8). Target release was additionally adjusted if the storage capacity is relatively low compared to the annual inflow, and unable to store large portions of the inflow for later release (Eq. A.9).

$$649 R_m = k \cdot R'_m Eq. (A.8)$$

650 where
$$c \ge 0.5$$

651
$$R_m = \left(\frac{c}{0.5}\right)^2 \cdot k \cdot R'_m + \left\{1 - \left(\frac{c}{0.5}\right)^2\right\} \cdot I_m$$
 Eq. (A.9)

 $652 \qquad where \ 0 \le c \le 0.5$

Where I_{klm} is the average monthly inflow [m³ s⁻¹], *c* the capacity parameter [-] calculated as the storage capacity divided by the mean annual inflow, and *k* the storage parameter [-] calculated as current storage divided by the desired maximum storage. The desired maximum storage was set at 85 % of the storage capacity as recommended by Hanasaki et al. (2006).

Water inflow, demand and EFRs were estimated based on the average of the past five years. Water demands were based on the water demands of downstream cells. Only a fraction of water demands were taken into account, based on the fraction of discharge the dam controlled. For example: if a dam controlled 70 % of the discharge of a downstream cell, than 70 % of its demands were taken into account. Fractions smaller than 25 % were ignored.

662 The original dam operation scheme of Hanasaki et al. (2006) was shown to produce excessively high 663 discharge events due to overflow releases (Masaki et al., 2018). These overflow releases occurred due to a mismatch between the expected and actual inflow. In our study, dam release was increased during 664 665 high-storage events to prevent overflow and accompanying high discharge events. If dam storage was 666 above the desired maximum storage, target dam release was increased to negate the difference (Eq. A.10). If dam storage was below the desired minimum storage, release is decreased (Eq. A.11). Dam 667 release was adjusted exponentially based on the relative storage difference: small storage differences 668 669 were only corrected slightly, but if the dam was close to overflowing or emptying, the difference was 670 corrected strongly.

671
$$R_a = R_m + \frac{(S - C\alpha)}{\gamma} \cdot \left(\frac{\frac{S}{C} - \alpha}{1 - \alpha}\right)^b$$
Eq. (A.10)

 $672 \qquad where S > C\alpha$

673
$$R_a = R_m + \frac{(S - C(1 - \alpha))}{\gamma} \cdot \left(\frac{(1 - \alpha) - \frac{S}{C}}{1 - \alpha}\right)^b$$
Eq. (A.11)

674 where $S < C(1-\alpha)$

675	Where R_a is the actual dam release [m ³ s ⁻¹], S the dam storage capacity [m ³], α the fraction of the capacity
676	that is the desired maximum [-], β the exponent determining the correction increase [-][-], and γ the

677 parameter determining the period when the release is corrected [s^{-1}]. In testing the exponent and period

678 were tuned to 0.6 and 5 days respectively.

679 6.45.4 Appendix D: Water demand

680 6.4.15.4.1 Fitting and validation data

Data on irrigation, domestic, and industrial water withdrawals were based on the AQUASTAT database
(FAO, 2016)(FAO, 2016), EUROSTAT database (EC, 2019)(EC, 2019) and United Nations World
Water Development Report (Connor, 2015). Data on GDP per capita and GVA waswere abstracted from
the Maddison Project Database 2018 (Bolt et al., 2018), Penn World Table 9.0 (Feenstra et al., 2015)
and World Bank Development Indicators (World bank, 2010).

Available data for domestic an industrial withdrawals were divided into a dataset used for parameter fitting (80 %) and a dataset used for validation (20 %). Domestic water demands were estimated for each United Nations sub-region, and thus <u>the</u> data was divided per sub-region to ensure a good global coverage of data. In the same manner industrial water demand were divided per country. In case there is only a single data <u>pointentry</u>, the <u>data</u>entry was added to both the fitting and validation data.

691 6.4.25.4.2 Irrigation sector

692 Conventional irrigation demands were calculated when soil moisture contents drop below the critical 693 threshold where evapotranspiration will be limited. Demands were set to relieve water stress (Eq. A.12). 694 Paddy irrigation demands were set to always keep the soil moisture content of the upper soil layer 695 saturated (Eq. A.13), similar to Hanasaki et al. (2008b) and Wada et al. (2014). For paddy irrigation, the 696 saturated hydraulic conductivity of the upper soil layer was reduced by its cubed root to simulate 697 puddling practices, as recommended by the CROPWAT model (Smith, 1996).(Smith, 1996). Total irrigation demands were adjusted by the irrigation efficiency (Eq. A.14). Paddy irrigation used an 698 699 irrigation efficiency of 1 since the water losses were already incorporated in the water demand 700 calculation.

701
$$ID'_{conventional} = (W_{cr,1} + W_{cr,2}) - (W_1 + W_2)$$
 Eq. (A.12)

702 where $W_1 + W_2 < W_{cr,1} + W_{cr,2}$

35

$$703 \qquad ID'_{paddy} = W_{max,1} - W_1$$

704 where $W_1 < W_{max,1}$

$$705 \quad ID = ID' * IE \qquad \qquad \text{Eq. (A.14)}$$

Where $ID'_{conventional}$ is the conventional crop irrigation demand [mm], ID'_{paddy} is the paddy crop irrigation demand [mm], ID is the total irrigation demand [mm], W_1 and W_2 are the soil moisture contents of the first and second soil layer respectively [mm], W_{cr} is the critical soil moisture content [mm], W_{max} the maximum soil moisture content [mm], and IE is the irrigation efficiency [mm mm⁻¹].

Eq. (A.13)

710 6.4.35.4.3 Domestic sector

711 Domestic water demands were represented by using a sigmoid curve for the calculation of structural 712 domestic water demands (Eq.A.15) and a efficiency rate for the calculation of water-use efficiency 713 increases (Eq. A.16). These equations differ slightly from Alcamo et al. (2003) since our study used the 714 base 10 logarithms of GDP and water withdrawals per capita as they provided a better fit.

715
$$DSW_y = DSW_{min} + (DSW_{max} - DSW_{min}) * \frac{1}{1 + e^{-f(GDP_y - o)}}$$
 Eq. (A.15)

716
$$DW_y = 10^{DSW_y} \cdot TE^{y-y_{base}}$$
 Eq. (A.16)

717 Where *DSW* is the yearly structural domestic withdrawal [log10 m³ cap⁻¹], *DW* the yearly domestic 718 withdrawal [m³ cap⁻¹], $\frac{DW_{min}DSW_{min}}{DSW_{min}}$ the minimum structural domestic withdrawal [log10 m³ cap⁻¹], 719 $\frac{DW_{max}DSW_{max}}{DSW_{max}}$ the maximum structural domestic withdrawal (without technological improvement) 720 [log10 m³ cap⁻¹], *GDP* the yearly gross domestic product [log10 USD_{equivalent} cap⁻¹], *f* [-] and *o* [log10 721 USD_{equivalent}] the parameters that determine the range and steepness of the sigmoid curve, *y* the year 722 index, *TE* the technological efficiency rate [-], and *y_{base}* the base year (taken to be 1980).

723 DW_{min} was set at 7.5 l cap⁻¹ d⁻¹ based on the World Health Organisation standard (Reed and Reed, 2013),724 DW_{max} was estimated at around 450 l cap⁻¹ y⁻¹ based on a global curve fit, and *TE* was set at 0.995, 0.99,725and 0.98 for developing, transition and developed countries respectively (United Nations development726status classification) based on Flörke et al. (2013). Curve parameters f and o were estimated for the 23727United Nations sub-regions based on the GDP per capita and domestic water withdrawal data. In case36

728 insufficient data was available to calculate parameters values, regional (4 sub-regions) or global (4 sub-

729 regions) parameter estimates were used.

730 6.4.45.4.4 Industrial sector

731 Industrial water demands were represented by using a linear formula for the calculation of structural

industrial water demands (Eq. A.17) and a efficiency rate for the calculation of water-use efficiencyincreases (Eq. A.18).

734	$ISW_y = ISW_{int} \cdot GVA_y$	Eq. (A.	17)

735 $IW_y = ISW_y \cdot TE^{y-y_{base}}$ Eq. (A.18)

Where *ISW* is the yearly structural industrial withdrawal $[m^3]$, $\frac{HW_{int}(SW_{int})}{HW_{int}}$ the country specific industrial water intensity $[m USD_{equivalent}^{-1}]$, *IW* the yearly industrial withdrawal $[m^3]$, *GVA* the yearly gross value added by industry $[USD_{equivalent}]$, *y* the year index, y_{base} the base year (taken to be the year when the industrial water intensity is determined), and *TE* the technological efficiency rate [-].

740 *TE* was set at 0.976 and 1 for OECD and non-OECD countries respectively before the year 1980, 0.976

between the years 1980 and 2000 and 0.99 after the year 2000 based on Flörke et al. (2013). Industrial water intensities were estimated for the 246 United Nations countries based on the GVA and industrial water withdrawal data. In case insufficient data was available to calculate the industrial water intensities, either sub-regional (56 countries), regional (17 countries) or global (9 countries) intensities estimates were used.

746 6.4.5<u>5.4.5</u> Energy sector

For each thermoelectric power plant the water intensity was combined with their generation to calculate
the water demands (Eq. A.19). Actual generation is estimated by adjusting the installed generation
capacity by 46 % for fossil, 72 % for nuclear, and 56 % for biomass power plants (based on EIA national
annual generation data (EIA, 2013)(EIA, 2013))

 $751 \qquad EW_y = EW_{int} \cdot G_y$

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Eq. (A.19)

753	yearly generation for each plant [MWh], and y the year index.	
754	The energy water demands were subtracted from the industrial water demands at the location of each	
755	power plant. In cases where the grid cell industrial water demand was less than the energy water demand,	
756	national industrial water demands were lowered. In cases where even the national industrial water	
757	demands were less than the national energy water demand (3 countries), the energy water demands were	
758	lowered instead. Energy demands were lowered until 10 % of the national industrial water demand	
759	remains, to ensure some spatial coverage of industrial and energy water demands.	
760	6.4.65.4.6 Livestock sector	
761	Livestock water demands were estimated by combining the livestock population with the water	
762	requirements for each livestock variety (Eq. A.20).	
763	$LW_y = LW_{int} \cdot L $ Eq. (A.20)	
764	Where <i>LW</i> is the yearly livestock withdrawal $[m^3]$, <i>LW</i> _{int} the livestock water intensity $[m^3 \text{ livestock}^{-1}]$,	Formatted: Font: Italic
765	L the livestock number for each variety [livestock].	Formatted: Font: Italic Formatted: Font: Italic
766	6-55.5 Appendix E: General performance	
767	VIC-WUR monthly discharge and monthly terrestrial total water storage anomalies were compared with	
768	observations from the GRDC dataset (GRDC, 2003)(GRDC, 2003) and GRACE satellite dataset	
769	(NASA, 2002)(NASA, 2002) for eight major river basins (not included in the main text; Fig. A1).	
770	Discharge stations were selected if the upstream area was larger than 10000 m2, matched the simulated	

Where EW is the yearly energy withdrawal $[m^3]$, EW_{int} the energy water intensity $[m^3 MWh^{-1}]$, G the

upstream area at the station location,): Amazon, Congo, Lena, Volga, Yangtze, Danube, Columbia, and

Mississippi river basins. A 300km gaussian filer has been applied to the total water storage simulation

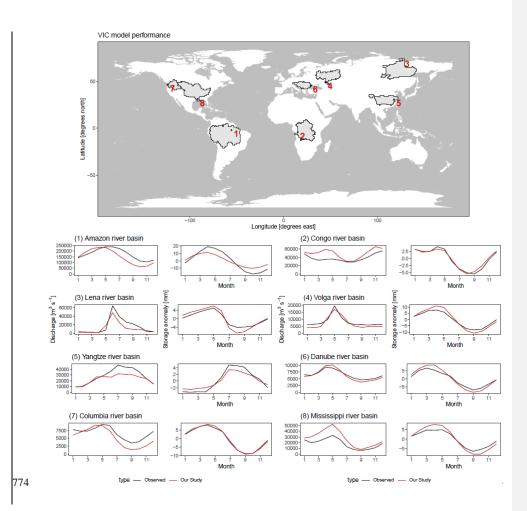
752

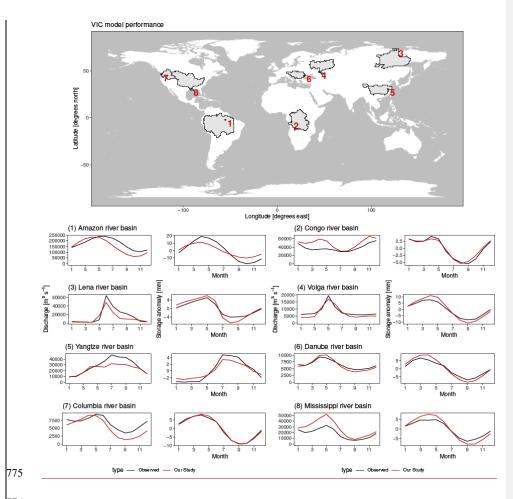
771

772

773

data (similar to Long et al. (2015)).





 776
 Figure A1: Comparison between simulated and <u>GRDC and GRACE</u> observed discharge and terrestrial total water

 777
 storage anomalies. Figures indicate multi-year averages of human-impacted simulations (red) and observations (black).

778 <u>6 Code availability</u>

779	All code for the VIC-WUR model is freely available at github.com/wur-wsg/VIC (tag VIC-WUR.2.1.0;
780	DOI 10.5281/zenodo.3934325) under the GNU General Public License, version 2 (GPL-2.0). VIC-
781	WUR documentation can be found at vicwur.readthedocs.io. The original VIC model is freely available
782	at github.com/UW-Hydro/VIC (tag VIC.5.0.1; DOI 10.5281/zenodo.267178) under the GNU General
783	Public License, version 2 (GPL-2.0). VIC documentation can be found at vic.readthedocs.io.
784	Documentation and scripts concerning input data used in our study is freely available at
I	40

786 <u>General Public License, version 3 (GPL-3.0).</u>

787 7 Author contribution

- 788 Bram Droppers and Wietse H.P. Franssen developed and tested the model additions introduced in VIC-
- 789 WUR. Bram Droppers generated and analysed the results. Michelle T.H. van Vliet, Bart Nijssen and
- 790 Fulco Ludwig provided overall oversight and guidance. Bram Droppers prepared the manuscript with
- 791 contributions from all co-authors.

792 8 Competing interests

793 The authors declare that they have no conflict of interest.

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