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#### apportionment and Source sensitivity analysis: two methodologies with two different purposes.

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### Abstract

- 12 In this work are reviewed the existing methodologies for source
- apportionment and sensitivity analysis to identify key differences 13
- 14 and stress their implicit limitations. The emphasis is laid on the
- differences between source "impacts" (sensitivity analysis) and 15
- "contributions" (source apportionment) obtained by using four 16
- different methodologies: brute force top-down, brute force bottom-17
- up, tagged species and DDM. A simple theoretical example to 18
- 19 compare these approaches is used highlighting differences and
- potential implications for policy. When the relationships between 20
- 21 concentration and emissions are linear, impacts and contributions are
- 22 equivalent concepts. In this case, source apportionment may be used
- 23
- for air quality planning purposes and vice versa, sensitivity analysis
- 24 may be used for quantifying sources contributions.
- However, this study demonstrates that when the relationship 25
- between emissions and concentrations is non-linear, sensitivity 26
- 27 approaches are not suitable to retrieve source contributions and
- 28 source apportionment methods are not appropriate to evaluate the
- 29 impact of abatement strategies. Moreover, when using sensitivity
- 30 analysis for planning, it is important to note that, under non-linear
- 31 circumstances, the calculated impacts will only provide information
- 32 for the exact conditions (e.g. emission reduction share) that are
- 33 simulated.

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Keywords: source apportionment, sensitivity analysis, abatement strategies,
 air quality planning

#### 1. Introduction

The concentration of a pollutant at a given location generally results from direct emissions and from interactions in the atmosphere among different emission precursors, emitted by a variety of sources. For example, particulate matter (denoted here as PM) results from the interaction and combination of 5 precursors (PPM, NO<sub>x</sub>, SO<sub>2</sub>, NH<sub>3</sub>, and VOC) which can be emitted by different activity macro-sectors (e.g. residential, transport, industrial and

48 agriculture).

Abatement strategies aim at reducing the precursor's emission of the different activity sector to reduce pollutant concentrations but these strategies are challenging to design because of the complex relationships that link precursors and pollutants.

Two different approaches are currently used to support air quality decision makers: source apportionment and sensitivity analysis.

- Source apportionment quantifies the **contribution** of an emission source (or precursor) to the concentration of one pollutant at one given location.
- Sensitivity analysis estimates the <u>impact</u> on pollutant concentration that results from a change of one or more emission sources.

The main objective of this work is to review the existing methodologies, identify key differences and stress their implicit limitations. We will particularly focus on the differences between concentration "impacts" (sensitivity) and "contributions" (source apportionment) obtained with different methodologies. We make use of a simple theoretical example to compare the approaches, highlight differences and potential implications in terms of policy. In the following sections, we analyze first how these methodologies work

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in a simple linear case before generalizing it to more complex non-73 linear situations.

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# 2. Linear simplification and implications

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Let's consider C a pollutant concentration at one location that is a function of three variables  $(E_1, E_2 \text{ and } E_3)$ , i.e. the emissions of three precursors or sources within a given domain:  $C = C(E_1, E_2, E_3)$ . For a linear relationship between the function C and the three variables  $E_1$ ,  $E_2$  and  $E_3$ , we can write:

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$$C(E_1, E_2, E_3) = C(0, 0, 0) + P_1 E_1 + P_2 E_2 + P_3 E_3$$
 (1)

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where  $P_1$ ,  $P_2$  and  $P_3$  are three constant coefficients.

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On the other hand, the sensitivity of the concentration to a change of a given emission source can be quantified via partial derivatives. For expression (1) this gives:

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$$\frac{\partial C}{\partial E_1} = P_1$$
;  $\frac{\partial C}{\partial E_2} = P_2$ ;  $\frac{\partial C}{\partial E_3} = P_3$ 

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In Clappier et al. (2017) the coefficients  $(P_1, P_2 \text{ and } P_3)$  are referred to "potencies". The Authors used this concept of "potencies" to analyze the model response to emission changes in different European countries.

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The consequences of a linear relationship between concentration and emission sources are twofold:

- 98 1) all higher order derivatives (order 2 and beyond) are null, 99 including those involving two or more emission sources (crossed 100 derivatives) as the impact of a change in one emission source is
- 101 independent from all others.
- 102 2) the first-order partial derivatives are constant and can therefore be 103 calculated with finite differencing, between any couple of emission

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levels, for example a base case (denoted BC) and a background (denoted as 0).

106 The potency equations then read as:

$$P_1 = \frac{\Delta C_0^{BC_1}}{E_1^{BC}} \ ; \ P_2 \ = \frac{\Delta C_0^{BC_2}}{E_2^{BC}} \ ; P_3 = \frac{\Delta C_0^{BC_3}}{E_3^{BC}}$$

108  
109 with 
$$\Delta C_0^{BC_1} = C(E_1^{BC}, 0,0) - C(0,0,0),$$
  
110  $\Delta C_0^{BC_2} = C(0, E_2^{BC}, 0) - C(0,0,0)$   
111  $\Delta C_0^{BC_3} = C(0,0, E_3^{BC}) - C(0,0,0)$ 

Together with "potencies", Clappier et al. also introduce the concept of "potential", defined as the concentration change resulting from a total reduction of the emissions (from BC to 0). The "potential" can be calculated via relation (1) applied between the base-case and background levels as:

$$\Delta C_0^{BC} = \Delta C_0^{BC_1} + \Delta C_0^{BC_2} + \Delta C_0^{BC_3}$$
 (2)

120 where  $\Delta C_0^{BC} = C(E_1^{BC}, E_2^{BC}, E_3^{BC}) - C(0,0,0)$ 

Equation (2) can directly be used for source apportionment purpose, with  $\Delta C_0^{BC_1}$  the concentration change resulting from a total reduction of the emission source (or precursor)  $E_1$ , reflecting the contribution of  $E_1$  to the base case concentration. Similarly  $\Delta C_0^{BC_2}$  and  $\Delta C_0^{BC_3}$  are the contributions of  $E_2$  and  $E_3$ . Equation (2) shows that, in the linear case, the concentration change resulting from a simultaneous reduction of all emission sources  $(\Delta C_0^{BC})$  is equal to the sum of the emission sources contributions.

131 In the next sections, we will explore how this simple conclusion 132 changes when non-linear relationships are considered. In particular, 133 we will assess which implications (and limitations) these non-134 linearities have in terms of source apportionment and sensitivity 135 analysis.

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# 3. Brute Force method

The "brute force" method consists in estimating the concentration change by performing and subtracting two simulations, one with and the second without a specific emission source to be analysed (Blanchard, 1999; Yarwood et al., 2004).

In non-linear situations, the concentration change resulting from a set of emission sources is not anymore equivalent to the sum of the concentration changes resulting from emission sources changed individually. In the following, we will refer to the work of Stein and Alpert (1993) who proposed an approach to decompose an overall impact into single (one emission source only) and combined

### 3.1. Bottom-up formulation

(multiple emission sources) impacts.

We consider here three emission precursors  $E_1$ ,  $E_2$  and  $E_3$  that are changing from a low (denoted as "L") to a high level (denoted as "H"). In a bottom-up approach, the low emission level is chosen as the reference. With these definitions and notations, the impact on concentration resulting from a change of one only of the three precursor's emissions can be written as follows:

$$\begin{split} &\Delta C_L^{H_1} = C(E_1^H, E_2^L, E_3^L) - C(E_1^L, E_2^L, E_3^L) \\ &\Delta C_{\bar{L}}^{H_2} = C(E_1^L, E_2^H, E_3^L) - C(E_1^L, E_2^L, E_3^L) \\ &\Delta C_L^{H_3} = C(E_1^L, E_2^L, E_3^H) - C(E_1^L, E_2^L, E_3^L) \end{split}$$

While the impact on concentration resulting from the simultaneous changes of two or three precursor's emissions would be written as:

$$\begin{split} &\Delta C_{\bar{L}}^{H_1,H_2} = C(E_1^H, E_2^H, E_3^L) - C(E_1^L, E_2^L, E_3^L) \\ &\Delta C_{\bar{L}}^{H_1,H_3} = C(E_1^H, E_2^L, E_3^H) - C(E_1^L, E_2^L, E_3^l) \\ &\Delta C_{\bar{L}}^{H_2,H_3} = C(E_1^L, E_2^H, E_3^H) - C(E_1^L, E_2^L, E_3^L) \\ &\Delta C_{\bar{L}}^{\bar{H}} = C(E_1^H, E_2^H, E_3^H) - C(E_1^L, E_2^L, E_3^L) \end{split}$$

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- Using a similar notation, the decomposition of Stein and Alpert applied to 2 variables ( $E_1$  and  $E_2$ ) would read as:
- 168  $\Delta C_{\bar{l}}^{H_1, H_2} = \Delta C_{\bar{l}}^{H_1} + \Delta C_{\bar{l}}^{H_2} + \hat{C}^{int}$  (3)

 $\Delta C_{\bar{L}} = \Delta C_{\bar{L}} + \Delta C_{\bar{L}} + C^{int}$ (3)

where  $\Delta C_{\bar{L}}^{H_1}$  and  $\Delta C_{\bar{L}}^{H_2}$  are the impacts induced by the change in emission sources  $E_I$  and  $E_2$  taken independently and  $\Delta C_{\bar{L}}^{H_1,H_2}$  the impact induced from  $E_I$  and  $E_2$  taken simultaneously.

175 It is clear from (3) that the impact of a simultaneous change of two 176 emission sources is not equivalent to the sum of the individual 177 impacts, as highlighted by the additional term  $\hat{C}^{int}$ . This term that 178 quantifies the interaction between the two emission sources can be 179 calculated using (3) as:

 $\hat{C}^{int} = \hat{C}_{\bar{l}}^{H_1, H_2} = \Delta C_{\bar{l}}^{H_1, H_2} - \Delta C_{\bar{l}}^{H_1} - \Delta C_{\bar{l}}^{H_2}$  (4)

The Stein and Alpert formulation can similarly be applied with 3
emission sources:

 $\Delta C_{\bar{L}}^{\bar{H}} = \Delta C_{\bar{L}}^{H_1} + \Delta C_{\bar{L}}^{H_2} + \Delta C_{\bar{L}}^{H_3} + \hat{C}^{int}$  (5)

186 Where  $\Delta C_L^{H_1}$ ,  $\Delta C_L^{H_2}$  and  $\Delta C_{\bar{L}}^{H_3}$  are the impact on concentration resulting from single emission changes in the sources and 188

 $\hat{C}^{int} = \hat{C}_{\bar{L}}^{H_1, H_2} + \hat{C}_{\bar{L}}^{H_1, H_3} + \hat{C}_{\bar{L}}^{H_2, H_3} + \hat{C}_{\bar{L}}^{H_1, H_2, H_3} \tag{6}$ 

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190 where  $\hat{C}_{L}^{H_1,H_2}$ ,  $\hat{C}_{\bar{L}}^{H_1,H_3}$  and  $\hat{C}_{\bar{L}}^{H_2,H_3}$  are the double interaction terms that
191 can be further decomposed via equation (4).  $\hat{C}_{\bar{L}}^{H_1,H_2,H_3}$  is the triple
192 interaction term (between  $E_I$ ,  $E_2$ ,  $E_3$ ) which can be decomposed by
193 combining (5) and (6) as:

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$$\begin{split} \hat{C}_{\bar{L}}^{H_{1},H_{2},H_{3}} &= \Delta C_{\bar{L}}^{\bar{H}} - \Delta C_{\bar{L}}^{H_{1}} - \Delta C_{\bar{L}}^{H_{2}} - \Delta C_{\bar{L}}^{H_{3}} \\ &\Delta C_{\bar{L}}^{H_{1},H_{2}} - \Delta C_{\bar{L}}^{H_{1},H_{3}} - \Delta C_{\bar{L}}^{H_{2},H_{3}} \end{split}$$

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### 3.2. Top-down formulation

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In a top-down formulation, the highest emission level is chosen as reference. The Stein Alpert formulation for three precursors can then be expressed similarly to the bottom-up formulation as:

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$$\Delta C_{\bar{L}}^{\bar{H}} = \Delta C_{L_1}^{\bar{H}} + \Delta C_{L_2}^{\bar{H}} + \Delta C_{L_3}^{\bar{H}} + \hat{C}^{int}$$
 (7)

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where  $\Delta C_{L_1}^{\overline{H}}$ ,  $\Delta C_{L_2}^{\overline{H}}$  and  $\Delta C_{L_3}^{\overline{H}}$  are the impacts on concentration induced by reducing  $E_1$ ,  $E_2$  and  $E_3$  independently whereas  $\hat{C}^{int}$  is the interaction term which itself can be decomposed into a series of double interactions and a triple interaction terms:

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$$\hat{C}^{int} = \hat{C}^{\bar{H}}_{L_1,L_2} + \hat{C}^{\bar{H}}_{L_1,L_3} + \hat{C}^{\bar{H}}_{L_2,L_3} + \hat{C}^{\bar{H}}_{L_1,L_2,L_3} \tag{8}$$

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209 It is important to stress that the top-down single impacts are not 210 equivalent to their bottom-up counterparts. The relation between 211 these bottom-up and top-down impacts can be expressed as (here for 212 the case of E<sub>3</sub>):

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$$\Delta C_{L_2}^{\bar{H}} = C(E_1^H, E_2^H, E_3^H) - C(E_1^H, E_2^H, E_3^L)$$

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$$\Delta C_{L_3}^H = C(E_1^H, E_2^H, E_3^H) - C(E_1^L, E_2^L, E_3^L) - [C(E_1^H, E_2^H, E_3^L) - C(E_1^L, E_2^L, E_3^L)]$$

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$$\Delta C_{L_3}^{\overline{H}} = \Delta C_{\overline{L}}^{\overline{H}} - \Delta C_{\overline{L}}^{H_1 H_2} \tag{9}$$

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Using equations (3), (4), (5) and (6), equation (9) can be reexpressed as:

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$$\Delta C_{L_3}^{\bar{H}} = \Delta C_{\bar{L}}^{H_3} + \hat{C}_{\bar{L}}^{H_1, H_3} + \hat{C}_{\bar{L}}^{H_2, H_3} + \hat{C}_{\bar{L}}^{H_1, H_2, H_3} \tag{10}$$

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In other words, the top-down impact on concentration of an emission source (obtained by switching off the emission source while all others remain unchanged) is not equivalent to its bottom-up counterpart, (obtained by switching on the emission source while all others are switched off). Relation (10) indeed clearly shows that additional interaction terms need to be considered. The implications resulting from these differences are highlighted in Section 5 in which some theoretical examples are described.

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## 4. Source apportionment and sensitivity analysis

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# 4.1. Tagged species techniques

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Equation (2) shows that, when the relationship between concentration and several emission sources is linear, the contribution of a specific source (source apportionment) can be computed as the impact on concentration obtained by a full reduction of this source (sensitivity). Moreover, the sum of the impacts on concentration obtained by reduction of the single sources  $(\Delta C_0^{BC_1} + \Delta C_0^{BC_2} + \Delta C_0^{BC_3})$  is equivalent to the impact on concentration resulting from a simultaneous abatement of all sources ( $\Delta C_0^{BC}$ ). In such a case, the concentration impacts are equal to source contributions and source apportionment and sensitivity analysis lead to similar results. This is not the case, however, when the relationship between concentrations and emissions is nonlinear. In their approach, Stein and Alpert express the difference between the impact caused by a simultaneous abatement and the sum of the impacts caused by individual abatement as interactions among the different sources. The Stein and Alpert formulation applied between the base-case and background levels is very close to equation (2) but with an additional term that accounts for interactions:

$$\Delta C_0^{BC} = \Delta C_0^{BC_1} + \Delta C_0^{BC_2} + \Delta C_0^{BC_3} + \hat{C}^{int}$$

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Because the interaction terms cannot not be attributed to a single emission source as they represent the interaction between two and more emission sources, the Stein and Alpert methodology does not allow identifying the full contribution of each individual source. It cannot therefore be used for source apportionment purpose, unless the interaction terms are negligible as in the linear case.

Unlike the Stein and Alpert methodology, the tagged species methodology is designed for source apportionment purposes. This methodology tags each precursor and quantifies its contribution (in terms of mass) to the pollutant concentration.

Tagged algorithms are implemented in several chemical transport model systems (Yarwood et al., 2004; Wagstrom et al., 2008, ENVIRON, 2014; Bhave et al., 2007; Wang et al., 2009; Kranenburg et al., 2013).

In tagging approaches, the effect of the full reduction of all sources is directly expressed as the sum of the source contributions:

$$\Delta C_0^{BC} = \delta C_1 + \delta C_2 + \delta C_3$$

where  $\delta C_1$ ,  $\delta C_2$ ,  $\delta C_3$  are the contributions of sources  $E_1$ ,  $E_2$  and  $E_3$  resulting from the tagged species approach resolution.

Tagging methodologies split the interaction terms into fractions and attribute these fractions to the source contributions, on the basis of mass weighting factors.

$$\delta C_1 = \Delta C_0^{BC_1} + \alpha \hat{C}^{int}$$

Because the tagged species approach mixes interaction terms and single concentration impacts into sources contributions, it is not suitable to estimate the effect of emission reduction when non-linearities are present (Burr and Zhang 2011a, 2011b). Indeed these two types of terms may react in very different ways to emission reductions. This fact is detailed in the examples provided below.

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On the other hand, the strength of this method is that it allows for a direct comparison of the source contributions with measurements (or measurement based methods like receptor models).

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4.2. DDM

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The decoupled direct method (DDM) is designed to estimate sensitivities to emission changes (Dunker et al., 1984; Dunker et al., 2002). It aims to compute only the first order derivatives (which correspond to the potencies mentioned in paragraph 2).

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$$\frac{\partial C}{\partial E_1}$$
;  $\frac{\partial C}{\partial E_2}$ ;  $\frac{\partial C}{\partial E_3}$ 

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The Taylor formula is applied at first order to calculate the concentration change between two emission levels (denoted H and L).

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$$\Delta C_{L}^{\overline{H}} = \Delta E_{1} \frac{\partial C}{\partial E_{1}} \bigg|_{H} + \Delta E_{2} \frac{\partial C}{\partial E_{2}} \bigg|_{H} + \Delta E_{3} \frac{\partial C}{\partial E_{3}} \bigg|_{H}$$

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with 
$$\Delta E_1 = E_1^H - E_1^L$$
,  $\Delta E_2 = E_2^H - E_2^L$ ,  $\Delta E_3 = E_3^H - E_3^L$ 

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In the linear case, the first order derivatives are constant and the first
 order approximation of the Taylor formula gives the exact
 expression of the impact on concentration of an emission change
 between H and L. When the emission-concentration relationship is
 nonlinear, the first derivatives are not constants. The first order

Taylor formula cannot take into account the nonlinear effects. It is a linear approximation based on derivatives computed at a given

317 emission reference level (level H in our example). The estimation of

the impact on concentration of an emission change between H and L

is accurate enough if level L is close enough to level H.

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321 The HDDM method (Hakami et al., 2003) aim to increase the

322 accuracy of the DDM method by computing second order

323 derivatives.

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- 324 DDM (and HDDM) gives similar information to the Stein Alpert
- 325 formulation applied with the Brute force top-down approach
- 326 (because the reference level is H). For the same reason than for the
- 327 Stein Alpert approach, these two methods are suitable for source
- apportionment purpose only if the relation between concentration
- and emission is close to linearity.
- 330 DDM (and HDDM) approximates the impact on concentration from
- an emission change between the two level H and L, using
- derivatives computed at level H. This impact is accurate enough if
- the level L is close enough to the reference level H.

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5. Example

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In this section, examples are designed to illustrate the differences in terms of contribution and impact estimates when the approaches discussed previously are used. In these examples, we focus on the formation of particulate matter (PM) in the atmosphere and only consider three formation processes: direct emissions (primary PM denoted as PPM); formation through reactions with nitrogen oxides (NO<sub>2</sub>) and ammonia (NH<sub>3</sub>) and formation through reactions with sulphur oxide (SO<sub>2</sub>) and NH<sub>3</sub>. These reactions pathways are summarised by the following system of reactions:

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- 348 PPM  $\rightarrow$  PM[PPM] 349 NO<sub>2</sub> + NH<sub>3</sub>  $\rightarrow$  PM[NH<sub>4</sub>NO<sub>3</sub>]
- 350  $SO_2 + 2 NH_3 \rightarrow PM[(NH_4)_2SO_4]$

351

- This system is further simplified by assuming that all reactions have
- 353 comparable kinetics (reaction speed) and have reached their
- equilibrium. From these three reactions, 1 PM mole can be produced
- by 1 PPM mole, by the combination of 1 NH<sub>3</sub> and 1 NO<sub>2</sub> moles or
- by the combination of 1 SO<sub>2</sub> and 2 NH<sub>3</sub> moles.

- We also limit our examples to emissions from three activity sectors.
- 359 The residential sector (R) only emits PPM and NO<sub>2</sub>, the agricultural
- sector (A) only emits NH<sub>3</sub> and the industrial sector (I) only emits
- 361 PPM and SO<sub>2</sub> (Figure 1). We assume for convenience that no

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background pollution is present (i.e. there is no PM when all emissions are zero).

# 5.1. Non-limited regime

In this first example, the quantity of precursors (in terms of mass) is large enough to feed all reactions. The agricultural sector emits 150  $NH_3$  moles which can react with 50  $NO_2$  moles emitted by the residential sector and 50  $SO_2$  moles emitted by industrial sector. 100 PPM moles are emitted by the residential sector as well by the industrial sector.

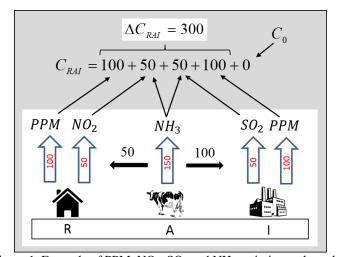


Figure 1. Example of PPM, NO<sub>2</sub>, SO<sub>2</sub> and NH<sub>3</sub> emissions released by three activity sectors: residential (R), agricultural (A) and industrial (I). For convenience, no units are associated to emissions and concentrations

Let's first calculate the PM concentration produced with and without each of the sources:

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- No source:  $C_0$  is the PM concentration obtained when all emissions are set to zero. Since we assumed a zero background pollution,
- $C_0 = 0$ .

- One source only:  $C_R$  (resp.  $C_A$  and  $C_I$ ) is the PM concentration reached when only the residential (resp. agricultural and industrial) sector releases emissions:
  - $C_R$  = 100 produced by PPM emissions (NO<sub>2</sub> emissions do not produce PM as no NH<sub>3</sub> is available).
- $-C_A = 0$  because NO<sub>2</sub> and SO<sub>2</sub> are not available to react with NH<sub>3</sub>.
  - $C_I = 100$  produced by the PPM emissions (SO<sub>2</sub> emissions do not produce PM as no NH<sub>3</sub> is available).

<u>Two sources</u>:  $C_{RA}$   $C_{RI}$ , and  $C_{AI}$  are the concentrations obtained when two (out of three) activity sectors release their emissions simultaneously (the RA subscripts correspond to residential and agriculture, RI to residential and industrial, AI to agriculture and industrial):

- $-C_{RA} = 150$ : 100 produced by PPM emissions from the residential sector and 50 produced by the 50 NO<sub>2</sub> released by the residential sector reacting with the 50 NH<sub>3</sub> emitted by agriculture (100 NH<sub>3</sub> moles remain unused).
- $C_{RI}$  = 200 : 100 produced by PPM emissions from the residential sector and 100 produced by PPM emissions from the industrial sector.
- $C_{AI}$  = 150 : 100 produced by PPM industrial emissions and 50 from the combination of 50 SO<sub>2</sub> (industry) and 100 NH<sub>3</sub> (agriculture).

- 413 <u>Three sources:</u> *C<sub>RAI</sub>* is the concentrations obtained when all 414 emissions are released simultaneously.
- $C_{RAI} = 300 : 200$  from PPM (residential and industry), 50 from reaction between NO<sub>2</sub> and NH<sub>3</sub> and 50 from reaction between SO<sub>2</sub> and NH<sub>3</sub>.

Brute-force Bottom-up (BF-BU) method

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- 421 The contribution of each activity sector is calculated as the
- 422 concentration change resulting from a 100% emission increase from
- 423 the lowest emission level (previously denoted "L" or background) to
- the highest level (denoted as "H", the base case  $C_{RAI}$  obtained with 424
- 425 all emissions)

426

427 In a bottom-up approach, the concentration associated with the 428 lowest emission level is considered as the reference. Concentration 429 impacts are then computed by difference between any situation (e.g.

430 one, two or three sources present) and this reference.

431

432 - with one source: 
$$\Delta C_R^{BU}$$
  
433  $\Delta C_A^{BU}$ 

$$\begin{array}{l} \Delta C_R^{BU} = C_R - C_0 = 100 \\ \Delta C_A^{BU} = C_A - C_0 = 0 \\ \Delta C_I^{BU} = C_I - C_0 = 100 \end{array}$$

$$\Delta C_I^{BU} = C_I - C_0 = 100$$

- with two sources: 
$$\Delta C_{RA}^{BU} = C_{RA} - C_0 = 150$$

$$\begin{array}{l} \Delta C_{RA}^{BU} = C_{RA} - C_0 = 150 \\ \Delta C_{RI}^{BU} = C_{RI} - C_0 = 200 \\ \Delta C_{AI}^{BU} = C_{AI} - C_0 = 150 \end{array}$$

$$\Delta C_{AI}^{BO} = C_{AI} - C_0 = 150$$

438 439

440 - with three sources: 
$$\Delta C_{RAI} = C_{RAI} - C_0 = 300$$
441

442 To calculate the interaction terms, we use the Stein-Alpert

formulation using Eq. (5) and Eq. (6): 443

$$\Delta C_{RAI} = \Delta C_R^{BU} + \Delta C_A^{BU} + \Delta C_I^{BU} + \hat{C}_{RA}^{BU} + \hat{C}_{RI}^{BU} + \hat{C}_{RI}^{BU} + \hat{C}_{RAI}^{BU}$$

445 446

444

from which the interaction terms are obtained by application of (4)

447 and (6):

448

$$\hat{C}_{RA}^{BU} = \Delta C_{RA}^{BU} - \Delta C_{R}^{BU} - \Delta C_{A}^{BU} = 50$$

$$C_{RI}^{BU} = \Delta C_{RI}^{BU} - \Delta C_{R}^{BU} - \Delta C_{I}^{BU} = 0$$

$$C_{AI}^{BU} = \Delta C_{AI}^{BU} - \Delta C_{A}^{BU} - \Delta C_{I}^{BU} = 50$$

$$\begin{split} \hat{C}_{RA}^{BU} &= \Delta C_{RA}^{BU} - \Delta C_{R}^{BU} - \Delta C_{A}^{BU} = 50 \\ \hat{C}_{RI}^{BU} &= \Delta C_{RI}^{BU} - \Delta C_{R}^{BU} - \Delta C_{I}^{BU} = 0 \\ \hat{C}_{AI}^{BU} &= \Delta C_{AI}^{BU} - \Delta C_{A}^{BU} - \Delta C_{I}^{BU} = 50 \\ \hat{C}_{RAI}^{BU} &= \Delta C_{RAI} - \Delta C_{R}^{BU} - \Delta C_{A}^{BU} - \Delta C_{I}^{BU} - \hat{C}_{RA}^{BU} - \hat{C}_{RI}^{BU} - \hat{C}_{RI}^{BU} = 0 \end{split}$$

- As can be seen from this example, the system behaves non-linearly 450
- and the interaction terms (e.g.  $\hat{\mathcal{C}}_{RA}^{BU}$ ) are not-zero. Moreover the sum of the individual impacts ( $\Delta C_R^{BU} + \Delta C_A^{BU} + \Delta C_I^{BU} = 200$ ) 451
- 452
- 453 underestimates the overall impact ( $\Delta C_{RAI} = 300$ ). These results are
- 454 graphically represented in Figure 2 (third column).

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# Brute-force Top-down (BF-TD) method

In a BF-TD approach, the higher emission level (base case,  $C_{RAI}$ ) is the reference and the impact of each activity sector is calculated as the concentration change resulting from a 100% emission decrease (of one, two or three sources) from this reference to the background level.

- with one source: When all emissions from one sector are reduced (e.g. residential), the other two sector remain active (agricultural and industry). In this case, the Top-down impact is the difference between the base case concentration and the concentration resulting from the agricultural and industrial emissions only. A similar reasoning can be made for all sectors:

$$\begin{array}{l} \Delta C_{R}^{TD} = C_{RAI} - C_{AI} = 150 \\ \Delta C_{A}^{TD} = C_{RAI} - C_{RI} = 100 \\ \Delta C_{I}^{TD} = C_{RAI} - C_{RA} = 150 \end{array}$$

 with two sources: The Top-down impact due to a full reduction of two sectors (e.g. residential and agriculture) is similarly computed as the difference between the base case concentration and the concentration resulting from the remaining sector (industry).

$$\begin{array}{l} \Delta C_{RA}^{TD} = C_{RAI} - C_{I} = 200 \\ \Delta C_{RI}^{TD} = C_{RAI} - C_{A} = 300 \\ \Delta C_{AI}^{TD} = C_{RAI} - C_{R} = 200 \end{array}$$

  with three sources: The impact resulting from the simultaneous reduction of all three sources is similar in the Top-down and Bottom-up approaches:

$$\Delta C_{RAI} = C_{RAI} - C_0 = 300$$

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- 493 The interaction terms can be obtained in a similar way to the
- 494 bottom-up approach by using the Stein and Alpert formulation for
- 495

$$\Delta C_{RAI} = \Delta C_R^{TD} + \Delta C_A^{TD} + \Delta C_I^{TD} + \hat{C}_{RA}^{TD} + \hat{C}_{RI}^{TD} + \hat{C}_{AI}^{TD} + \hat{C}_{RAI}^{TD}$$

The interaction terms are given by: 498

$$C_{RA}^{TD} = \Delta C_{RA}^{TD} - \Delta C_{R}^{TD} - \Delta C_{A}^{TD} = -50$$

$$C_{RA}^{TD} = \Delta C_{RA}^{TD} - \Delta C_{RA}^{TD} = 0$$

$$C_{RI} = \Delta C_{RI} - \Delta C_{R} - \Delta C_{I} = 0$$

$$\hat{C}_{AI}^{TD} = \Delta C_{AI}^{TD} - \Delta C_{A}^{TD} - \Delta C_{I}^{TD} = -50$$

$$\hat{C}_{RA}^{TD} = \Delta C_{RA}^{TD} - \Delta C_{R}^{TD} - \Delta C_{A}^{TD} = -50$$

$$\hat{C}_{RI}^{TD} = \Delta C_{RI}^{TD} - \Delta C_{R}^{TD} - \Delta C_{I}^{TD} = 0$$

$$\hat{C}_{AI}^{TD} = \Delta C_{AI}^{TD} - \Delta C_{A}^{TD} - \Delta C_{I}^{TD} = -50$$

$$\hat{C}_{RAI}^{TD} = \Delta C_{RAI}^{TD} - \Delta C_{R}^{TD} - \Delta C_{A}^{TD} - \Delta C_{I}^{TD} - \hat{C}_{RA}^{TD} - \hat{C}_{RI}^{TD} - \hat{C}_{AI}^{TD} = 0$$

500

- With this approach, a non-linear behavior is also observed and 501
- 502 interaction terms are not zero. It is also interesting to note that the
- triple interaction term  $(\hat{\mathcal{C}}_{RAI}^{TD})$  is null. The sum of the individual 503
- 504
- impacts ( $\Delta C_R^{TD} + \Delta C_A^{TD} + \Delta C_I^{TD} = 400$ ) overestimates the overall impact ( $\Delta C_{RAI} = 300$ ). We further discuss these aspects at the end of 505
- 506 this section. These results are graphically represented in Figure 2
- 507 (fourth and fifth columns).

508 509 510

# Tagged species approach

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- 512 Compared to Brute-force, the tagged species approach calculates the
- 513 share of each source to the overall concentration change. These
- 514 shares are referred to as contributions and have the main property
- 515 that the sum of the individual contributions is equal to the overall
- 516 concentration impact, by definition, i.e.:

517

$$\Delta C_{RAI} = \delta C_R^{TAG} + \delta C_A^{TAG} + \delta C_I^{TAG}$$

518 519

- 520 The sector contributions are computed by tracking the mass of their
- 521 emitted species contributing to PM formation (in our example:
- 522 PM[PPM],  $PM[NH_4NO_3]$  and  $PM[(NH_4)_2SO_4]$ )

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- PM[PPM] is formed from PPM. The 100 moles from the residential sector lead to 100 moles of PM. The same applies to the 100 moles from industry.
- 528 PM[NH<sub>4</sub>NO<sub>3</sub>] is formed by combination of NH<sub>3</sub> and NO<sub>2</sub>. The 529 share between these two contributions is obtained by application 530 of stoichiometric molar mass ratios:

$$a_1 = \frac{[NO_3]_m}{[NO_3]_m + [NH_4]_m} = 0.78$$

532
533 In our example, 50 moles of PM[NH<sub>4</sub>NO<sub>3</sub>] are formed by combination of NO<sub>2</sub> (50 moles) from the residential sector and NH<sub>3</sub> (50 moles) from agriculture. The contribution attributed to

NO<sub>2</sub> is  $50 \times a_1$  whereas the contribution attributed to NH<sub>3</sub> is  $50 \times (1 - a_1)$ .

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- PM[(NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub>] is formed by combination of NH<sub>3</sub> and SO<sub>2</sub>. The following stoichiometric mass ratio is used:

$$a_2 = \frac{[SO_4]_m}{[SO_4]_m + 2[NH_4]_m} = 0.73$$

The contribution attributed to SO<sub>2</sub> is  $50 \times a_2$  whereas the contribution attributed to NH<sub>3</sub> is  $50 \times (1 - a_2)$ .

The contribution of each sector is then obtained as the sum of their precursor contribution shares as follows:

550 
$$\delta C_R^{TAG} = 100 + 50 \times a_1 = 138.7$$
  
 $\delta C_A^{TAG} = 50 \times (1 - a_1) + 50 \times (1 - a_2) = 24.9$   
 $\delta C_I^{TAG} = 100 + 50 \times a_2 = 136.4$   
551

- By definition the sum of the contributions ( $\delta C_R^{TAG} + \delta C_A^{TAG} +$
- $\delta C_I^{TAG} = 300$ ) is exactly equal to the overall concentration impact
- 554  $(\Delta C_{RAI} = 300)$ .

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556 Note that a decomposition of the non-linear interaction terms 557 obtained in the top-down or bottom-up approach, using the above 558 stoichiometric ratios would lead to similar results than the tagged 559 approach. These results are graphically represented in Figure 2 560 (second column).

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# **DDM**

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In this methodology, delta concentrations and interaction terms are estimated with first order partial derivatives computed from the highest emission level (base case in our example). Being a sensitivity approach using level H as reference, DDM shows clear analogies with the BF-TD.

569 570 571

$$\left. \frac{\partial c}{\partial \alpha_R} \right|_{TD} = 150$$
  $\left. \frac{\partial c}{\partial \alpha_A} \right|_{TD} = 100$   $\left. \frac{\partial c}{\partial \alpha_I} \right|_{TD} = 150$ 

572 573 574

where  $\alpha_R$  ,  $\alpha_A$  and  $\alpha_I$  are percentage emission changes from the base case for the residential, agricultural and industrial sectors.

575 576 The first-order derivatives are evaluated using finite differencing 577 between the base case and a level characterised by emissions that are 578 10% lower for each activity sector.

579 The concentration changes resulting from a 100% emission 580 reduction (i.e. between the base case and the zero emission case) 581 could be estimated by setting  $\alpha_R$ ,  $\alpha_A$  and  $\alpha_I$  to unity.

582

$$\begin{split} \Delta C_R^{HDDM} &= \frac{\partial C}{\partial \alpha_R} \bigg|_{TD} = 150 \\ \Delta C_A^{HDDM} &= \frac{\partial C}{\partial \alpha_A} \bigg|_{TD} = 100 \\ \Delta C_I^{HDDM} &= \frac{\partial C}{\partial \alpha_I} \bigg|_{TD} = 150 \end{split}$$

583 584 585

586

We see from this last example that both the total PM and the contribution of the sources are then comparable with those obtained Geosci. Model Dev. Discuss., https://doi.org/10.5194/gmd-2017-161 Manuscript under review for journal Geosci. Model Dev.

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with the BF-TD method. Their interpretation is similar (Figure 2, sixth column).

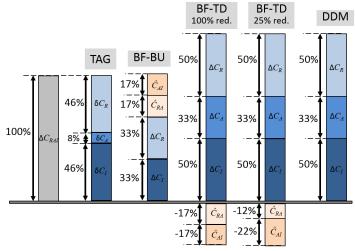


Figure 2. Schematic representation of the allocation of PM to its sources in the non-limited example. The expected total PM is displayed in the grey bar on the left.

 In the linear case (second paragraph) we have seen that a single source contribution can be computed as the impact resulting from a full reduction of this source. However, source contributions and concentration impacts should not be confused as they are different in most situations. The example presented in this paragraph illustrates this clearly for a non-linear system. Indeed the contributions of the single sources computed by the tagged species approach ( $\delta C_R^{TAG} = 138$ ;  $\delta C_A^{TAG} = 24$ ;  $\delta C_I^{TAG} = 136$ ) differ from the concentration impacts resulting from a total abatement of these single sources computed by the BF-TD ( $\Delta C_R^{TD} = 150$ ;  $\Delta C_A^{TD} = 100$ ;  $\Delta C_I^{TD} = 150$ ) method. Moreover, the sum of the concentration impacts obtained with either the BF-TD approach for single sources does not equal the total concentration impact ( $\Delta C_{RAI} = 300$ ). This is also valid for any selection of two sectors ( $\Delta C_R^{TD} + \Delta C_A^{TD} = 250 \neq \Delta C_{RA}^{TD} = 200$ ). Note

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that similarly to BF-TD, the concentration impacts computed as increases from the background (BF-BU) show the same behaviour  $(\Delta C_R^{BU} + \Delta C_A^{BU} = 100 \neq \Delta C_{RA}^{BU} = 150)$ .

 $(\Delta C_R^{BU} + \Delta C_A^{BU} = 100 \neq \Delta C_{RA}^{BU} = 150)$ 

Figure 3 shows that the impact on concentration is proportional to the emission reduction indicating that the relationship between emission and concentration changes is linear. However, this example also illustrates the fact that linearity encompasses two aspects: 1) the interaction terms are zero  $(\hat{C}^{int} = 0)$ ; 2) the ratios between concentration change and emission changes  $(\Delta C/\Delta E)$  remain constant, regardless of the calculation bounds (denoted "H" and "L" in Section 4). In the current example the ratios  $\Delta C/\Delta E$  are constant (linear trend of  $\Delta C$  on Figure 3) but the relationship between concentration and emission is not linear because of the non-zero interaction terms (not shown)  $(\hat{C}_{RA}^{TD} = -50)$  and  $\hat{C}_{AI}^{TD} = -50$ ). However, even with zero interaction terms, we can still observe a non-linear behaviour with the emission reduction percentage. The evaluation of linearity therefore requires two tests: one to quantify the interaction terms and the second to assess the deviation from a linear trend with respect to the emission reduction percentage.

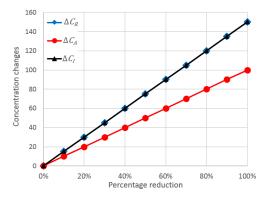


Figure 3: Evolution of the concentration changes resulting from different percentage of source abatement (Top down approach) for the three sectors (Residential, Agricultural and Industrial).

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# 5.2. Limited regime

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This example is similar to the previous, except that the emissions of NH<sub>3</sub> are reduced from 150 to 100 moles.

640 641 When all sources release emissions, the 100 moles of NH<sub>3</sub> are shared into 100/3=33.3 moles which react with NO<sub>2</sub> to form 33.3 642 643 moles of PM[NH<sub>4</sub>NO<sub>3</sub>] and 100×2/3=66.6 moles which react with 644 SO<sub>2</sub> to give 33.3 moles of PM[(NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub>]. Because the mass of

NH<sub>3</sub> is not enough to react with all the NO<sub>2</sub> and SO<sub>2</sub> mass, 16.7 645 646 moles of NO<sub>2</sub> and 16.7 moles of SO<sub>2</sub> remain unused.

Note that when the agricultural source is active with one only of the two other sources (residential or industrial) the NH<sub>3</sub> 100 moles are then sufficient to consume all the NO<sub>2</sub> or SO<sub>2</sub> and lead to 50 moles of PM in either case.

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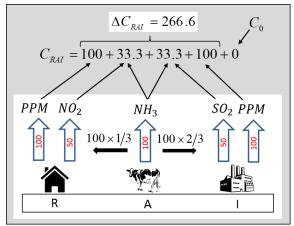


Figure 3. Example with three sources in an ammonia-limited regime. The mass emitted by each source is expressed in moles.

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> The PM concentrations obtained when one or two sources are active are similar to the previous example:

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```
C_0 = 0 ; C_R = 100 ; C_A = 0 ; C_I = 100 C_{RA} = 150 ; C_{RI} = 200 ; C_{AI} = 150
659
660
```

But the result differ when all sources are active:  $C_{RAI} = 266.6$  (200 from PPM (residential industry), 33.3 from reaction between NO<sub>2</sub> and NH<sub>3</sub> and 33.3 from reaction between SO<sub>2</sub> and NH<sub>3</sub>).

## **Bottom-up brute-force method (BF-BU)**

The BF-BU approach computes all concentration impacts from the background concentration  $(C_0)$ . The Stein-Alpert terms are similar to the non-limited case, excepted for  $\Delta C_{RAI}$  and  $\hat{C}_{RAI}$ :

671		
672	$\Delta C_R^{BU} = 100$	$\hat{C}_{RA}^{BU} = 50$
673	$\Delta C_A^{BU} = 0$	$\hat{C}_{RI}^{BU}=0$
674	$\Delta C_I^{BU} = 100$	$\hat{C}_{AI}^{BU} = 50$
675	$\Delta C_{RAI} = 266.6$	$\hat{C}_{RAI} = -33.3$

The limiting effect of NH<sub>3</sub> appears only in the negative triple interaction term ( $\hat{C}_{RAI}$ ).

### **Top-down brute-force method (BF-TD)**

The Top-down approach uses the base case  $(C_{RAI})$  concentration as reference to compute the concentration impact. In this case, all Stein-Alpert terms are different from the non-limited regime:

$$\Delta C_R^{TD} = 116.6$$
  $\hat{C}_{RA}^{TD} = -16.6$   $\Delta C_{RAI}^{TD} = 66.6$   $\hat{C}_{RI}^{TD} = 33.3$   $\Delta C_{I}^{TD} = 116.6$   $\hat{C}_{AI}^{TD} = -16.6$   $\hat{C}_{RAI} = -33.3$ 

### **Tagged approach**

The contribution of each source is computed similarly to the nonlimited regime. The productions of 33.3 moles of PM[NH<sub>4</sub>NO<sub>3</sub>] and

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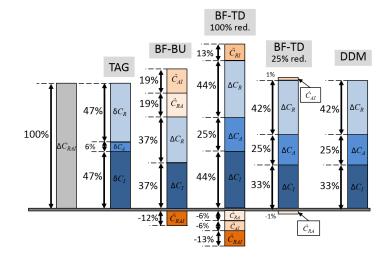
33.3 moles of PM[(NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub>] are split among the different sectors using the stoichiometric coefficients  $a_1$  and  $a_2$ :

699 
$$\delta C_R^{TAG} = 100 + 33.3 * a_1 = 125.8$$
  
 $\delta C_A^{TAG} = 33.3 * (1 - a_1) + 33.3 * (1 - a_2) = 16.6$   
 $\delta C_I^{TAG} = 100 + 33.3 * a_2 = 124.2$ 

# **DDM**

As shown below, DDM only considers first derivatives, which are not suitable to estimate higher order interaction terms. The calculation of the first order derivatives in this example gives:

$$\begin{split} \Delta C_R^{HDDM} &= \frac{\partial C}{\partial \alpha_R} \bigg|_{TD} = 111.5 \\ \Delta C_A^{HDDM} &= \frac{\partial C}{\partial \alpha_A} \bigg|_{TD} = 66.7 \\ \Delta C_R^{HDDM} &= \frac{\partial C}{\partial \alpha_I} \bigg|_{TD} = 88.1 \end{split}$$



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Figure 4. Schematic representation of the allocation of PM to its
 sources in the ammonia-limited example. The expected total PM is
 displayed in the grey bar on the left.

The main difference with respect to the non-limited regime is the appearance of a triple interaction term that will also lead to differences between the BF-TD and the DDM approaches, given the fact that the latter only accounts for first order terms.

In comparison to the non-limited regime, the calculation of the concentration impacts resulting from different percentage of emission reduction shows non-linear trends (Figure 5). A discontinuity appears at 50% reduction for the abatement of industrial emissions. This discontinuity corresponds to a change of chemical regime. Below the 50% reduction level , the quantity of NH $_3$  is not sufficient to feed the reactions with NO $_2$  and SO $_2$  (with no SO $_2$  reduction, 50 moles of NO $_2$  and 50 moles of SO $_2$  would require 150 moles of NH $_3$  but only 100 are available) while beyond this 50% reduction level the quantity of NH $_3$  is then enough to feed the reactions with NO $_2$  and SO $_2$  (with 50% SO $_2$  reduction, 50 moles of NO $_2$  and 25 moles of SO $_2$  requires 100 moles of NH $_3$ ).

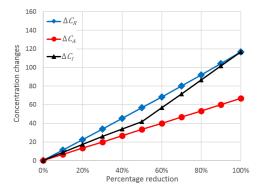


Figure 5: Evolution of the concentration changes resulting from different percentage of source abatement (Top down approach) for the three sectors (Residential, Agricultural and Industrial).

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737 The methodologies presented in this section aim at decomposing the 738 impact of an ensemble of sources into different terms attributed to 739 each individual sources. The terms computed by methodologies 740 designed for source apportionment (like TAG) are named source 741 contributions. Their sum is always equal to the combined impact of 742 all sources. On the other hand, the terms computed by sensitivity 743 analysis represent the emission change of each individual source and 744 their sum is equal to the combined impact of all sources only if the 745 relationship between emissions and concentrations is linear (see 746 Section 2). In non-linear situations, the source contributions 747 computed for source apportionment and the source impacts 748 computed for sensitivity analysis are different (see Figure 4 where 749 column 2 shows different results than column 3 or 4). Non-linearity 750 also imply that the calculation of the source impacts depends from 751 the bounds used to estimate the concentration changes (denoted "H" 752 and "L" in Section 4). The BF-BU and BF-TD (columns 3 and 4 in 753 Figure 4) give different results because they are not using the same 754 reference level ("L" for the BU and "H" for the TD as defined in 755 Section 4). Moreover, the results depend from the percentage of 756 emission changes applied to calculate the source impacts as 757 demonstrated by the different source impacts computed with the BF-758 TD for 100% and 25% emission reductions (columns 4 and 5 in 759 Figure 4). We expect that lower percentage emission reductions 760 generate less non-linearity and lead to a better agreement between 761 the BF-TD and the DDM method (columns 5 and 6 in Figure 4). 762 In synthesis, the second example illustrates that all the 763 methodologies tested to find source contributions and source 764 impacts give different results when the relationship emissions-765 concentrations is non-linear. It is therefore important to determine 766 the degree of non-linearity in order to understand the range of 767 applicability of each methodology and apply it for the right purpose.

### 6. Conclusions

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When pollutant concentrations exceed the thresholds set in the legislation, competent authorities must take actions to abate pollution. In the European legislation (Directive 2008/50/EC) both

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source apportionment and planning are requested when designing air quality plans. In practice, source apportionment is often used for planning purposes. It is indeed intuitive to use source apportionment to detect the activity sectors that need to be tackled in priority in an air quality plan. On the other hand, sensitivity analysis is often used as an approach to derive source contributions (e.g. SHERPA, FASST, GAINS...).

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In this work, we compared the two above mentioned approaches and investigated their domain of application. While sensitivity analysis refers to impacts to characterize the concentration change resulting from a given emission change, source apportionment aims to quantify contributions, by attributing a fraction of the pollutant concentration to each emission source. In the case of linear relationships between concentration and emissions, impacts and contributions are equivalent concepts. Source apportionment may then be used for air quality planning purposes and vice versa, sensitivity analysis may be used for quantifying sources contributions.

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In many cases, however, linearity is not a valid assumption. In such cases, sensitivity approaches cannot be used to retrieve source apportionment information, unless non-linear interaction terms are explicitly accounted for. On the other hand, source apportionment approaches (e.g. tagged species approach) intrinsically account for these non-linear interactions into their source contributions. But because it mix interaction terms and impacts, which may react in opposite directions, source apportionment should not be used to evaluate the impact of abatement strategies Even when using sensitivity analysis for planning, it is important to note that, under non-linear conditions, the calculated impacts will only provide information for the exact conditions that are considered. Impacts for an emission reduction of 50% are only valid for exactly that percentage of reduction and extrapolation to air quality planning with any other emission reduction levels would be inappropriate, unless additional scenarios are tested. Along the same line of reasoning, the importance of the non-linear interaction terms (among precursors) should be quantified as well when assessing the

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811 impact of more sources or precursors. Finally, these non-linear 812 interaction terms are in most cases not constant with the emission 813 reduction intensities, which would imposes the further need to 814 quantify them for different levels of emission reduction. 815 816 Fortunately, not all cases are so complex to require the full 817 quantification of all non-linear interaction terms. Thunis et al. (2015) showed that for yearly average relationships between emission and 818 concentration changes, linearity is a realistic assumption, implying 819 820 the possible use of source apportionment and sensitivity analysis for 821 both purposes. Some integrated assessment tools (e.g. GAINS, 822 SHERPA) take advantage of this assumption to retrieve source 823 apportionment information from calculated CTM sensitivities. 824 Although non-linearities are important for short-term time averages 825 (e.g. daily means, episodes), they are likely not associated to every 826 process. For instance, non-linear interactions are expected to be 827 more relevant for secondary pollutants, especially under limited 828 regimes. The challenge consists, therefore, in screening the system 829 for significant non-linearities and account for them by calculating 830 explicitly the relevant non-linear interaction terms. 831 832 One main strength of source apportionment approaches is to provide 833 contribution estimates that can be cross validated with source 834 apportionment derived from measurements (i.e. receptor modelling, 835 for a detailed description see e.g. Belis et al., 2013). This step is 836 crucial for the evaluation of chemistry transport models. 837 838 7. Code availability No specific code is attached to this work as all presented examples 839 840 can easily be replicated. 841 References 842 843 844 2008/50/EC, D. Directive 2008/50/EC of the European Parliament 845 and of the Council of 21 May 2008 on ambient air quality and

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