

Supplement of

Gas-phase chemistry in the online multiscale NMMB/BSC Chemical Transport Model: Description and evaluation at global scale

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1 Statistical Measures

There are several metrics that are used by the modeling community to evaluate performances of AQMs (U.S.EPA, 1991; Cox and Tikvart, 1990; Russell and Dennis, 2000). The statistical indicators selected in this study are: Correlation coefficient (r : Eq. 1) , Mean Bias (MB: Eq. 2) and Root Mean Square Error (RMSE: Eq.3).

$$r = \frac{1}{N} \frac{\sum_{i=1}^N (O_i - \bar{O})\Delta(P_i - \bar{P})}{\sigma_O \Delta \sigma_P} \quad (1)$$

$$MB = \frac{\sum_{i=1}^N (P_i - O_i)}{N} \quad (2)$$

$$RMSE = \sqrt{\frac{1}{N} \sum_{i=1}^N (P_i - O_i)^2} \quad (3)$$

where σ is the standard deviation and P and O denote the vector of model output and the vector observations, respectively. No threshold has been applied in the computation of the statistics.

2 Figures

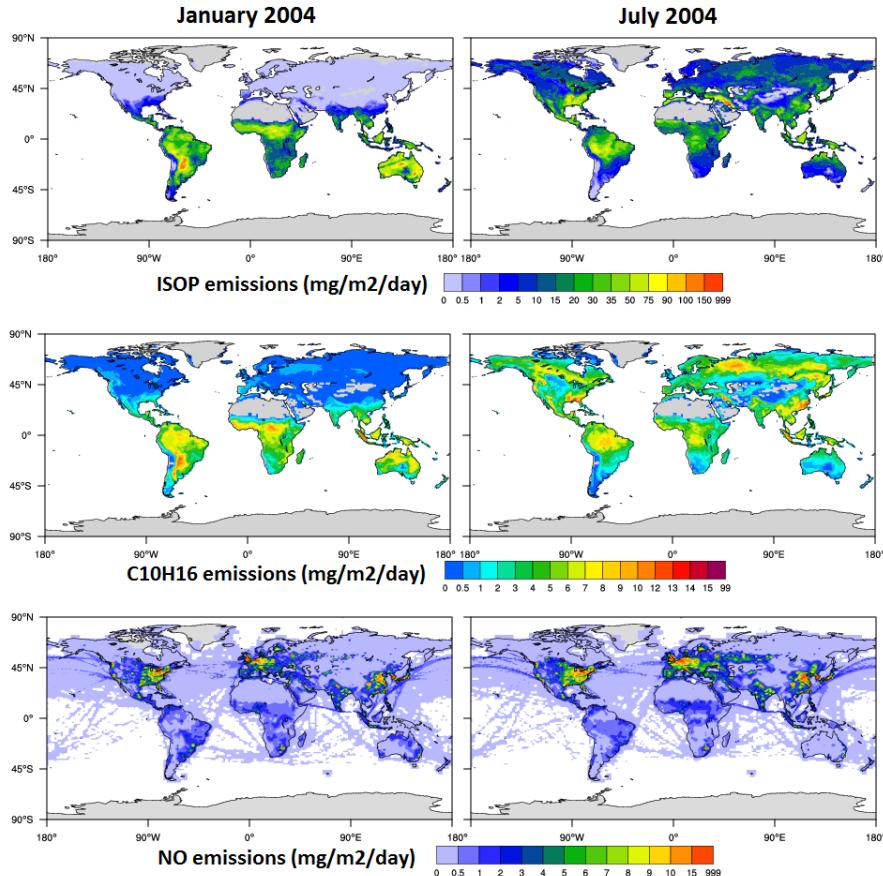


Figure S1: Biogenic emissions of isoprene (upper panel) and monoterpane (middle panel), from the on-line model MEGAN, and anthropogenic emissions of NO, from ACCMIP inventory, for January and July 2004 used in this model simulation

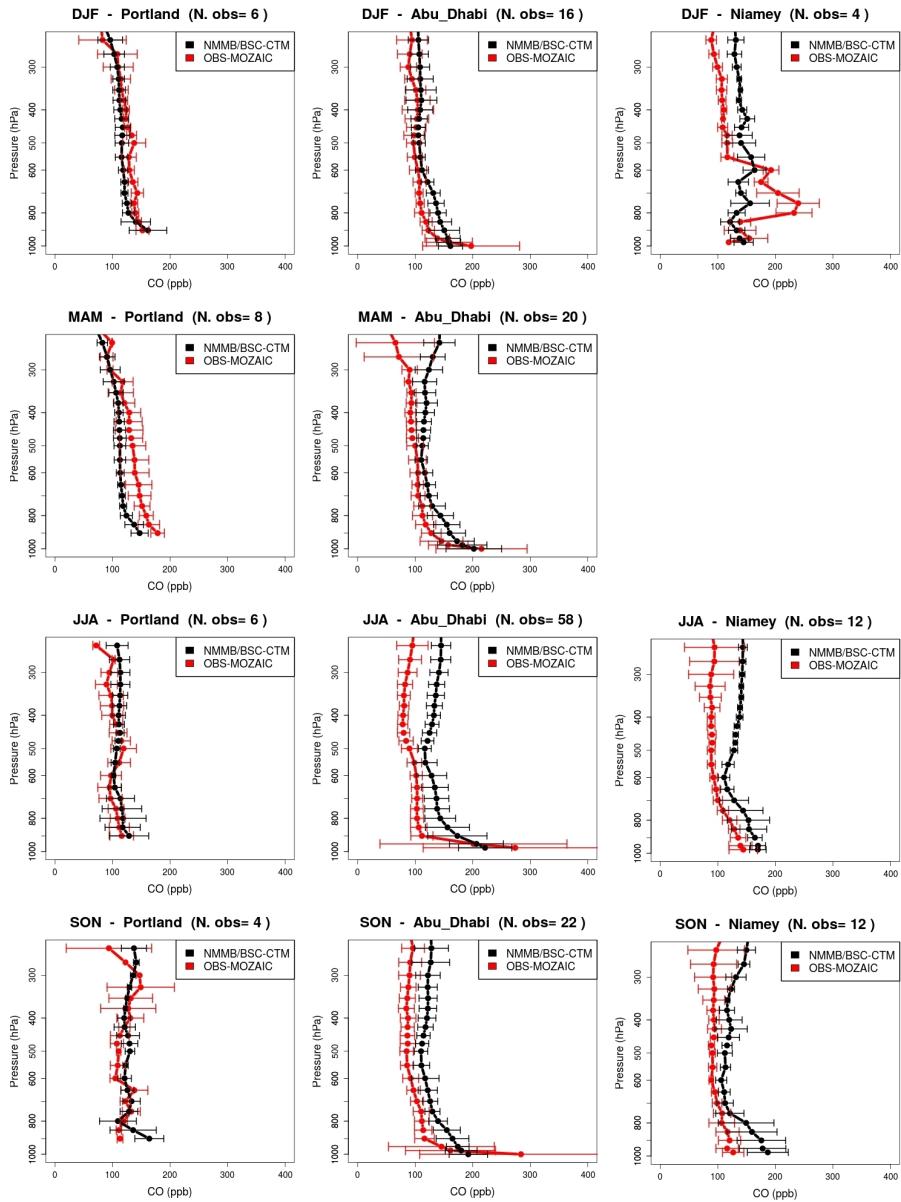


Figure S2: CO vertical profile seasonal averages over Portland, Abu Zabi and Niamey (from left to right) for the whole year 2004. Observations are in a solid red line and model data in a solid black line. The number of observations flights is given on the top of each plot.

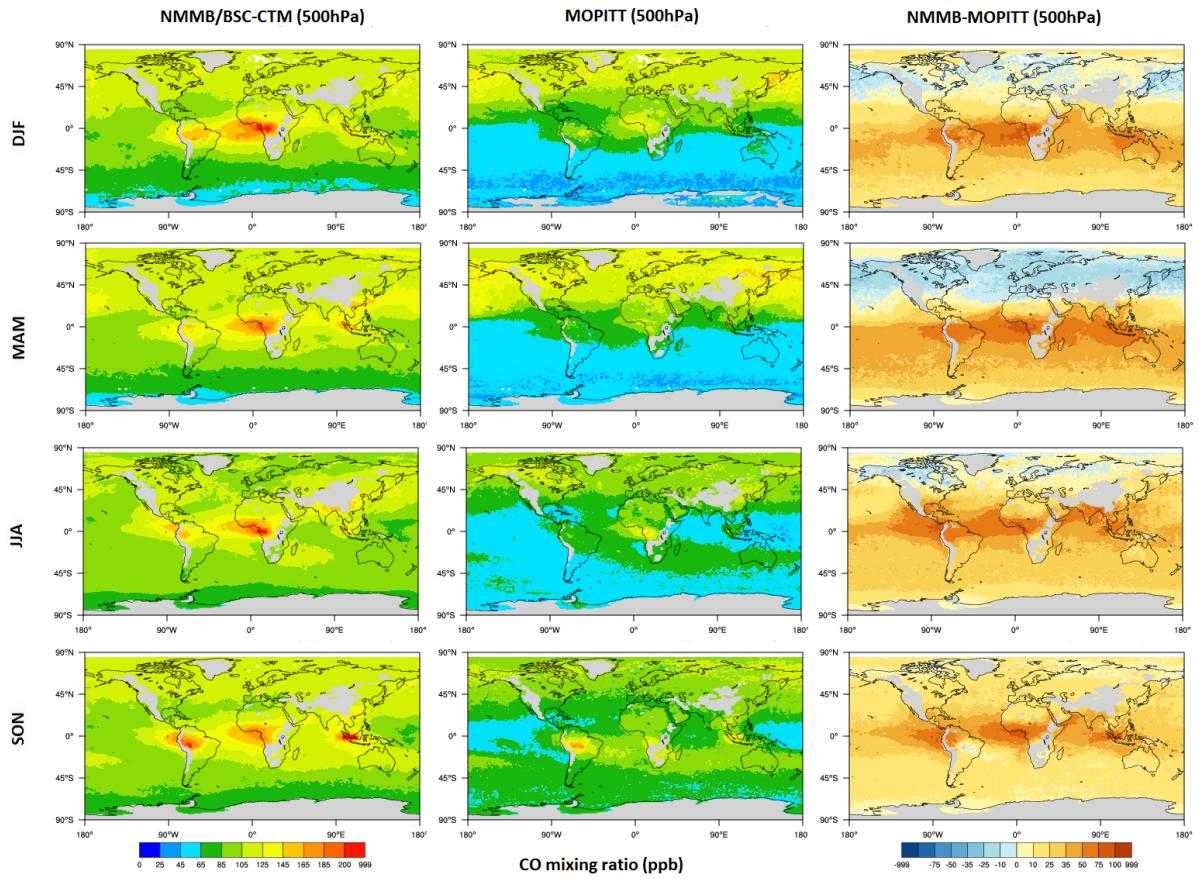


Figure S3: Comparison of modeled NMMB/BSC-CTM CO mixing ratio at 500hPa against satellite data (MOPITT) for (from top) DJF, MAM, JJA, and SON for the whole year 2004 in ppb. NMMB/BSC-CTM data is displayed in the left panel, MOPITT data in the middle panel and the bias in the right panel.

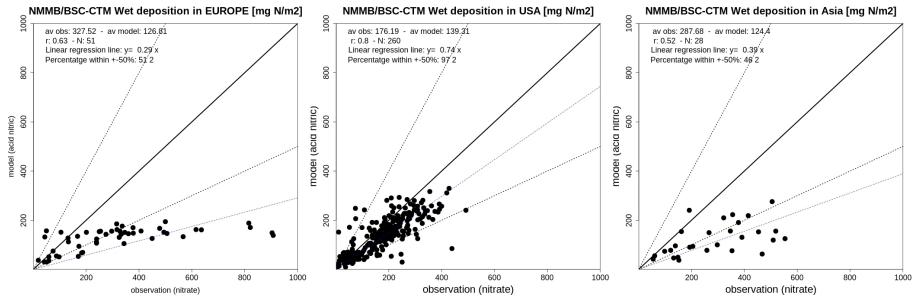


Figure S4: Scatter plots of the simulated HNO_3 versus nitrate measurements for three networks: Europe (left panel), USA (middle panel) and Asia (right panel). Dashed lines have slopes equal to 2 and 0.5. The dotted line is the result of the linear regression fitting through the origin.

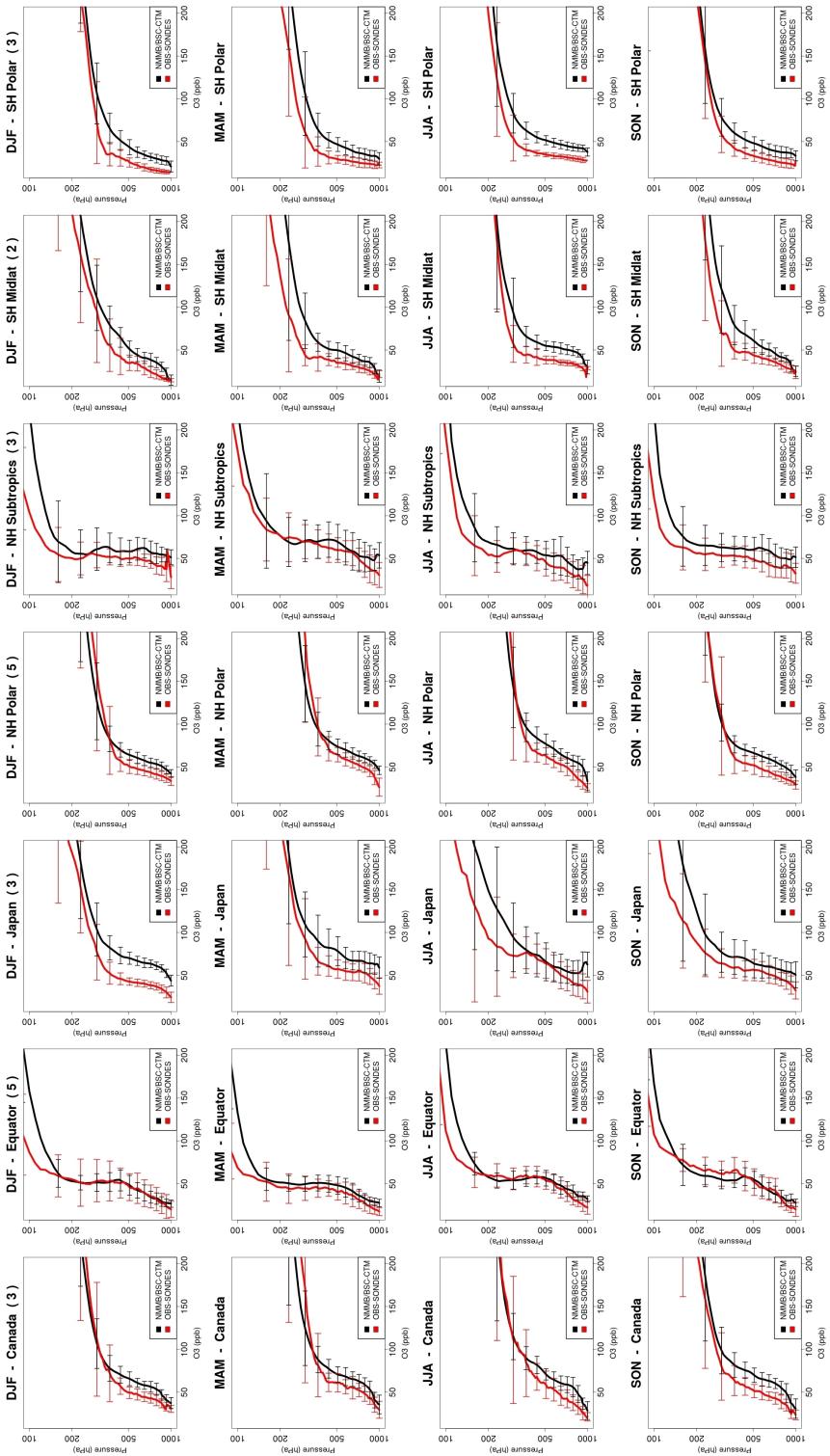


Figure S5: Comparison of ozonesonde measurements (red lines) and simulated (black lines) seasonal vertical profiles of O_3 (ppb) and standard deviations (horizontal lines). The region name and the number of stations, using brackets, are given above each plot.

3 Tables

Table S1: The chemical trace species for the CB05 chemical mechanism included in gas-phase tropospheric chemistry version of NMMB/BSC-CTM.

Species name	Description	Species name	Description
NO	Nitric oxide	SO ₂	Sulfur dioxide
NO ₂	Nitrogen dioxide	MEO ₂	Methylperoxy radical
O ₃	Ozone	MEOH	Methanol
O	Oxygen atom in the O ³ (P) electronic state	MEPX	Methylhydroperoxide
O ¹ D	Oxygen atom in the O ¹ (D) electronic state	FACD	Formic acid
OH	Hydroxyl radical	ETHA	Ethane
HO ₂	Hydroperoxy radical	ROOH	Higher organic peroxide
H ₂ O ₂	Hydrogen peroxide	AACD	Acetic and higher carboxylic acids
NO ₃	Nitrate radical	PACD	Peroxyacetic and higher peroxycarboxylic acids
N ₂ O ₅	Dinitrogen pentoxide	PAR	Paraffin carbon bond (C-C)
HONO	Nitrous acid	ROR	Secondary alkoxy radical
HNO ₃	Nitric acid	ETH	Ethene
PNA	Peroxynitric acid (HNO ₄)	OLE	Terminal olefin carbon bond (R-C=C)
CO	Carbon monoxide	IOLE	Internal olefin carbon bond (R-C=C-R)
FORM	Formaldehyde	ISOP	Isoprene
ALD2	Acetaldehyde	ISPD	Isoprene product (lumped methacrolein, methyl vinyl ketone, etc.)
C ₂ O ₃	Acetylperoxy radical	TERP	Terpene
PAN	Peroxyacetyl nitrate	TOL	Toluene and other monoalkyl aromatics
ALDX	Propionaldehyde and higher aldehydes	XYL	Xylene and other polyalkyl aromatics
CXO ₃	C ₃ and higher acylperoxy radicals	CRES	Cresol and higher molecular weight phenols
PANX	C ₃ and higher peroxyacetyl nitrates	TO ₂	Toluene-hydroxyl radical adduct
XO ₂	NO to NO ₂ conversion from alkylperoxy (RO ₂) radical	OPEN	Aromatic ring opening product
XO ₂ N	NO to organic nitrate conversion from alkylperoxy (RO ₂) radical	CRO	Methylphenoxy radical
NTR	Organic nitrate (RNO ₃)	MGLY	Methylglyoxal and other aromatic products
ETOH	Ethanol		
SULF	Sulfuric acid (gaseous)		

Table S2: The gas-phase CB05 chemical mechanism reactions applied in the NMMB/BSC-CTM. The first column describes the reactants, the second the products and the third displays the coefficients to compute the full rate expressions for each reaction.

Reactants	Products	Rate expression
O + O ₂ + M	→ O ₃ + M	6.0E-34*(300/T) ^{2.4}
O ₃ + NO	→ NO ₂	3.0E-12*exp(T/1500)
O + NO ₂	→ NO	5.6E-12*exp(180/T)
O + NO ₂	→ NO ₃	K ₀ = 2.5E-31*exp(300/T) ^{1.8} K _∞ =2.2E-11*exp(300/T) ^{0.7}
O + NO	→ NO ₂	K ₀ =9.0E-32*exp(300/T) ^{1.5} K _∞ =3.0E-11
NO ₂ + O ₃	→ NO ₃	1.2E-13*exp(T/2450)
O(¹ D) + M	→ O + M	2.1E-11*exp(102/T)
O(¹ D) + H ₂ O	→ 2.000*OH	2.2E-10
O ₃ + OH	→ HO ₂	1.7E-12*exp(T/940)
O ₃ + HO ₂	→ OH	1.0E-14*exp(T/490)
NO ₃ + NO	→ 2.000*NO ₂	1.5E-11*exp(170/T)
NO ₃ + NO ₂	→ NO + NO ₂	4.5E-14*exp(T/1260)
NO ₃ + NO ₂	→ N ₂ O ₅	K ₀ = 2.0E-30 *(300/T) ^{4.4} K _∞ = 1.4E-12*(300/T) ^{0.7}
N ₂ O ₅ + H ₂ O	→ 2.000*HNO ₃	2.5E-22
N ₂ O ₅ + H ₂ O + H ₂ O	→ 2.000*HNO ₃	1.8E-39
N ₂ O ₅	→ NO ₃ + NO ₂	K ₀ = 1.0E-03*exp(11000/T) ^{3.5} K _∞ = 9.7E+14*exp(T/11080) ^{0.1} F _c = 0.45 n= 1.0
NO + NO + O ₂	→ 2.000*NO ₂	3.3E-39*exp(530/T)
NO + NO ₂ + H ₂ O	→ 2.000*HONO	5.0E-40
NO + OH	→ HONO	7.0E-31*exp(300/T) ^{2.6} 3.6E-11*exp(300/T)-0.1
OH + HONO	→ NO ₂	1.8E-11*exp(T/390)
HONO + HONO	→ NO + NO ₂	1.0E-20
NO ₂ + OH	→ HNO ₃	K ₀ =2.0E-30*exp(300/T) ^{3.0} K _∞ =2.5E-11
OH+ HNO ₃	→ NO ₃	K ₀ =2.4E-14*exp(460/T) K ₂ = 2.7E-17*exp(2199/T) K ₃ = 6.5E-34*exp(1335/T)
HO ₂ + NO	→ OH + NO ₂	K ₀ =3.5E-12*exp(250/T)
HO ₂ + NO ₂	→ PNA	K ₀ =1.8E-31*exp(300/T) ^{3.2} K _∞ =4.7E-12 F _c =0.6
PNA	→ HO ₂ +NO ₂	K ₀ =4.1E-5*exp(T/10650) K _∞ =4.8E15*exp(T/11170) F _c =0.6
OH + PNA	→ NO ₂	1.3E-12*exp(380/T)
HO ₂ + HO ₂	→ H ₂ O ₂	K ₁ =2.3E-13*exp(600/T) K ₂ =1.7E-33*exp(1000/T)
HO ₂ +HO ₂ +H ₂ O	→ H ₂ O ₂	K ₁ =3.22E-34*exp(2800/T) K ₂ =2.38E-54*exp(3200/T)

Table S2: Continued from previous page

Reactants	Products	Rate expression
OH + H ₂ O ₂	→ HO ₂	2.9E-12*exp(T/160)
O ¹ D + H ₂	→ OH + HO ₂	1.1E-10
OH + H ₂	→ HO ₂	5.5E-12*exp(T/2000)
OH + O	→ HO ₂	2.2E-11*exp(120/T)
OH + OH	→ O	4.2E-12*exp(T/240)
OH + OH	→ H ₂ O ₂	K ₀ =6.9E-31*exp(300/T) ^{1.0} K _∞ =2.6E-11
OH + HO ₂	→	4.8E-11*exp(250/T)
HO ₂ + O	→ OH	3.0E-11*exp(200/T)
H ₂ O ₂ + O	→ OH + HO ₂	1.4E-12*exp(-2000/T)
NO ₃ + O	→ NO ₂	1.0E-11
NO ₃ + OH	→ HO ₂ + NO ₂	2.2E-11
NO ₃ + HO ₂	→ HNO ₃	3.5E-12
NO ₃ + O ₃	→ NO ₂	1.0E-17
NO ₃ + NO ₃	→ 2.000*NO ₂	8.5E-13*exp(T/2450)
XO ₂ + NO	→ NO ₂	2.6E-12*exp(365/T)
XO ₂ N + NO	→ NTR	2.6E-12*exp(365/T)
XO ₂ + HO ₂	→ ROOH	7.5E-13*exp(700/T)
XO ₂ N + HO ₂	→ ROOH	7.5E-13*exp(700/T)
XO ₂ + XO ₂	→	6.8E-14
XO ₂ N + XO ₂ N	→	6.8E-14
XO ₂ + XO ₂ N	→	6.8E-14
NTR + OH	→ HNO ₃ + HO ₂ + 0.330*FORM+	5.9E-13*exp(360/T)
ROOH + OH	→ XO ₂ + 0.500*ALD2 + 0.500*ALDX	3.01E-12*exp(190/T)
OH + CO	→ HO ₂	K ₁ = 1.44E-13 K ₂ =3.43E-33
OH + CH ₄	→ MEO ₂	2.45E-12*exp(T/1775)
MEO ₂ + NO	→ FORM + HO ₂ + NO ₂	2.8E-12*exp(300/T)
MEO ₂ + HO ₂	→ MEPX	4.1E-13*exp(750/T)
MEO ₂ + MEO ₂	→ 1.370*FORM+ 0.740*HO ₂ + 0.630*MEOH	9.5E-14*exp(390/T)
MEPX + OH	→ 0.700*MEO ₂ + 0.300*XO ₂ + 0.300*HO ₂	3.8E-12*exp(200/T)
MEOH + OH	→ FORM + HO ₂	7.3E-12*exp(T/620)
FORM + OH	→ HO ₂ + CO	9.0E-12
FORM + O	→ OH + HO ₂ + CO	3.4E-11*exp(T/1600)
FORM + NO ₃	→ HNO ₃ +HO ₂ + CO	5.8E-16
FORM + HO ₂	→ HCO ₃	9.7E-15*exp(625/T)
HCO ₃	→ FORM + HO ₂	2.4E+12*exp(T/7000)
HCO ₃ + NO	→ FACD+ NO ₂ + HO ₂	5.6E-12
HCO ₃ + HO ₂	→ MEPX	5.6E-15*exp(2300/T)
FACD + OH	→ HO ₂	4.0E-13
ALD2 + O	→ C ₂ O ₃ + OH	1.8E-11*exp(T/1100)
ALD2 + OH	→ C ₂ O ₃	5.6E-12*exp(270/T)
ALD2 + NO ₃	→ C ₂ O ₃ + HNO ₃	1.4E-12*exp(T/1900)
C ₂ O ₃ + NO	→ MEO ₂ + NO ₂	8.1E-12*exp(270/T)
PAN	→ C ₂ O ₃ + NO ₂	K ₀ = 4.9E-3*exp(12100/T) K _∞ = 5.4E16*exp(T/13830) F _c =0.3
C ₂ O ₃ + HO ₂	→ 0.800*PACD+ 0.200*AACD+ 0.200*O ₃	4.3E-13*exp(1040/T)
C ₂ O ₃ + MEO ₂	→ 0.900*MEO ₂ + 0.900*HO ₂ + FORM+ 0.100*AACD	2.0E-12*exp(500/T)

Table S2: Continued from previous page

Reactants	Products	Rate expression
$\text{C}_2\text{O}_3 + \text{XO}_2$	$\rightarrow 0.900*\text{MEO}_2 + 0.100*\text{AACD}$	$4.4\text{E}-13*\exp(1070/\text{T})$
$\text{C}_2\text{O}_3 + \text{C}_2\text{O}_3$	$\rightarrow 2.000*\text{MEO}_2$	$2.9\text{E}-12*\exp(500/\text{T})$
$\text{PACD} + \text{OH}$	$\rightarrow \text{C}_2\text{O}_3$	$4.0\text{E}-13*\exp(200/\text{T})$
$\text{AACD} + \text{OH}$	$\rightarrow \text{MEO}_2$	$4.0\text{E}-13*\exp(200/\text{T})$
$\text{ALDX} + \text{O}$	$\rightarrow \text{CXO}_3 + \text{OH}$	$1.3\text{E}-11*\exp(\text{T}/870)$
$\text{ALDX} + \text{OH}$	$\rightarrow \text{CXO}_3$	$5.1\text{E}-12*\exp(405/\text{T})$
$\text{ALDX} + \text{NO}_3$	$\rightarrow \text{CXO}_3 + \text{HNO}_3$	$6.5\text{E}-15$
$\text{CXO}_3 + \text{NO}$	$\rightarrow \text{ALD2} + \text{NO}_2 + \text{HO}_2 + \text{XO}_2$	$6.7\text{E}-12*\exp(340/\text{T})$
$\text{CXO}_3 + \text{NO}_2$	$\rightarrow \text{PANX}$	$K_0=2.7\text{E}-28*\exp(300/\text{T})^{7.1}$ $K_\infty=1.2\text{E}-11*\exp(300/\text{T})^{0.9}$ $F_c=0.3$
PANX	$\rightarrow \text{CXO}_3 + \text{NO}_2$	
$\text{PANX} + \text{OH}$	$\rightarrow \text{ALD2} + \text{NO}_2$	$3.0\text{E}-13$
$\text{CXO}_3 + \text{HO}_2$	$\rightarrow 0.800*\text{PACD} + 0.200*\text{AACD} + 0.200*\text{O}_3$	$4.3\text{E}-13*\exp(1040/\text{T})$
$\text{CXO}_3 + \text{MEO}_2$	$\rightarrow 0.900*\text{ALD2} + 0.900*\text{XO}_2 + \text{HO}_2 +$	$2.0\text{E}-12*\exp(500/\text{T})$
$\text{CXO}_3 + \text{XO}_2$	$\rightarrow 0.100*\text{AACD} + 0.100*\text{FORM}$	
$\text{CXO}_3 + \text{CXO}_3$	$\rightarrow 0.900*\text{ALD2} + 0.100*\text{AACD}$	$4.4\text{E}-13*\exp(1070/\text{T})$
$\text{CXO}_3 + \text{C}_2\text{O}_3$	$\rightarrow 2.000*\text{ALD2} + 2.000*\text{XO}_2 + 2.000*\text{HO}_2$	$2.9\text{E}-12*\exp(500/\text{T})$
$\text{PAR} + \text{OH}$	$\rightarrow \text{MEO}_2 + \text{XO}_2 + \text{HO}_2 + \text{ALD2}$	$2.9\text{E}-12*\exp(500/\text{T})$
	$0.870*\text{XO}_2 + 0.130*\text{XO}_2\text{N} + 0.110*\text{HO}_2 +$	
	$0.060*\text{ALD2} - 0.110*\text{PAR} + 0.760*\text{ROR} +$	$8.1\text{E}-13$
	$0.050*\text{ALDX}$	
	$0.960*\text{XO}_2 + 0.600*\text{ALD2} + 0.940*\text{HO}_2 -$	
ROR	$\rightarrow 2.100*\text{PAR} + 0.040*\text{XO}_2\text{N} + 0.020*\text{ROR} +$	$1.\text{E}+15*\exp(\text{T}/8000)$
	$0.500*\text{ALDX}$	
ROR	$\rightarrow \text{HO}_2$	$1.6\text{E}+3$
$\text{ROR} + \text{NO}_2$	$\rightarrow \text{NTR}$	$1.5\text{E}-11$
	$0.200*\text{ALD2} + 0.300*\text{ALDX} + 0.300*\text{HO}_2 +$	
$\text{O} + \text{OLE}$	$\rightarrow 0.200*\text{XO}_2 + 0.200*\text{CO} + 0.200*\text{FORM} +$	$1.\text{E}-11*\exp(\text{T}/280)$
	$0.010*\text{XO}_2\text{N} + 0.200*\text{PAR} + 0.100*\text{OH}$	
	$0.800*\text{FORM} + 0.330*\text{ALD2} +$	
$\text{OH} + \text{OLE}$	$\rightarrow 0.620*\text{ALDX} + 0.800*\text{XO}_2 + 0.950*\text{HO}_2 -$	$3.2\text{E}-11$
	$0.700*\text{PAR}$	
	$0.180*\text{ALD2} + 0.740*\text{FORM} +$	
$\text{O}_3 + \text{OLE}$	$\rightarrow 0.320*\text{ALDX} + 0.220*\text{XO}_2 + 0.100*\text{OH} +$	$6.5\text{E}-15*\exp(\text{T}/1900)$
	$0.330*\text{CO} + 0.440*\text{HO}_2 - 1.000*\text{PAR}$	
$\text{NO}_3 + \text{OLE}$	$\rightarrow \text{NO}_2 + \text{FORM} + 0.910*\text{XO}_2 + 0.090*\text{XO}_2\text{N} +$	$7.0\text{E}-13*\exp(\text{T}/2160)$
	$0.560*\text{ALDX} + 0.350*\text{ALD2} - 1.000*\text{PAR}$	
$\text{O} + \text{ETH}$	$\rightarrow \text{FORM} + 1.700*\text{HO}_2 + \text{CO} + 0.700*\text{XO}_2 +$	$1.04\text{E}-11*\exp(\text{T}/792)$
$\text{OH} + \text{ETH}$	$\rightarrow \text{XO}_2 + 1.560*\text{FORM} + 0.220*\text{ALDX} + \text{HO}_2$	$K_0=1.0\text{E}-28*\exp(300/\text{T})^{0.8}$ $K_\infty=8.8\text{E}-12$
$\text{O}_3 + \text{ETH}$	$\rightarrow \text{FORM} + 0.630*\text{CO} + 0.130*\text{HO}_2 +$	$1.2\text{E}-14*\exp(\text{T}/2630)$
$\text{NO}_3 + \text{ETH}$	$\rightarrow \text{NO}_2 + \text{XO}_2 + 2.0*\text{FORM}$	$3.3\text{E}-12*\exp(\text{T}/2880)$
$\text{IOLE} + \text{O}$	$\rightarrow 1.240*\text{ALD2} + 0.660*\text{ALDX} + 0.100*\text{HO}_2 +$	$2.3\text{E}-11$
$\text{IOLE} + \text{OH}$	$0.100*\text{XO}_2 + 0.100*\text{CO} + 0.100*\text{PAR}$	
$\text{IOLE} + \text{O}_3$	$\rightarrow 1.300*\text{ALD2} + 0.700*\text{ALDX} + \text{HO}_2 + \text{XO}_2$	$1.0\text{E}-11*\exp(550/\text{T})$
	$0.650*\text{ALD2} + 0.350*\text{ALDX} +$	
	$0.250*\text{FORM} + 0.250*\text{CO} + 0.500*\text{O}$	$8.4\text{E}-15*\exp(\text{T}/1100)$
	$+ 0.500*\text{OH} + 0.500*\text{HO}_2$	

Table S2: Continued from previous page

Reactants	Products	Rate expression
IOLE + NO ₃	$1.180^*ALD2 + 0.640^*ALDX + HO_2 + NO_2$ $0.440^*HO_2 + 0.080^*XO_2 + 0.360^*CRES +$	$9.6E-13*exp(T/270)$
TOL + OH	$0.560^*TO_2 + 0.765^*TOLRO_2$ $0.900^*NO_2 + 0.900^*HO_2 + 0.900^*OPEN +$	$1.8E-12*exp(355/T)$
TO ₂ + NO	0.100^*NTR	$8.1E-12$
TO ₂	CRES + HO ₂	4.2
OH + CRES	$0.400^*CRO + 0.600^*XO_2 + 0.600^*HO_2 +$ 0.300^*OPEN	$4.1E-11$
CRES + NO ₃	CRO + HNO ₃	2.2E-11
CRO + NO ₂	NTR	1.4E-11
CRO + HO ₂	CRES	5.5E-12
OPEN + OH	$XO_2 + 2.000^*CO + 2.000^*HO_2 + C_2O_3 +$ FORM $0.030^*ALDX + 0.620^*C_2O_3 +$	$3.0E-11$
OPEN + O ₃	$0.700^*FORM + 0.030^*XO_2 + 0.690^*CO +$ $0.080^*OH + 0.760^*HO_2 + 0.200^*MGLY$ $0.700^*HO_2 + 0.500^*XO_2 + 0.200^*CRES +$	$5.4E-17*exp(T/500)$
OH + XYL	$0.800^*MGLY + 1.100^*PAR + 0.300^*TO_2 +$ 0.804^*XYLRO_2	$1.7E-11*exp(116/T)$
OH + MGLY	XO ₂ + C ₂ O ₃	1.8E-11
O + ISOP	$0.750^*ISPD + 0.500^*FORM + 0.250^*XO_2 +$ $+ 0.250^*HO_2 + 0.250^*CXO_3 + 0.250^*PAR$	$3.6E-11$
OH + ISOP	$0.912^*ISPD + 0.629^*FORM + 0.991^*XO_2 +$ $+ 0.912^*HO_2 + 0.089^*XO_2N + ISOPRXN$ $0.650^*ISPD + 0.600^*FORM + 0.200^*XO_2$	$2.54E-11*exp(407.6/T)$
O ₃ + ISOP	$+ 0.066^*HO_2 + 0.266^*OH + 0.200^*CXO_3 +$ $0.150^*ALDX + 0.350^*PAR + 0.066^*CO$ $0.200^*ISPD + 0.800^*NTR + XO_2 +$	$7.86E-15*exp(T/1912)$
NO ₃ + ISOP	$0.800^*HO_2 + 0.200^*NO_2 + 0.800^*ALDX +$ 2.400^*PAR $1.565^*PAR + 0.167^*FORM + 0.713^*XO_2 +$	$3.03E-12*exp(T/448)$
OH + ISPD	$0.503^*HO_2 + 0.334^*CO + 0.168^*MGLY +$ $0.252^*ALD2 + 0.210^*C_2O_3 + 0.250^*CXO_3 +$ 0.120^*ALDX $0.114^*C_2O_3 + 0.150^*FORM +$	$3.36E-11$
O ₃ + ISPD	$0.850^*MGLY + 0.154^*HO_2 + 0.268^*OH +$ $0.064^*XO_2 + 0.020^*ALD2 + 0.360^*PAR +$ 0.225^*CO $0.357^*ALDX + 0.282^*FORM + 1.282^*PAR$	$7.1E-18$
NO ₃ + ISPD	$+ 0.925^*HO_2 + 0.643^*CO + 0.850^*NTR +$ $0.075^*CXO_3 + 0.075^*XO_2 + 0.150^*HNO_3$	$1.0E-15$
TERP + O	$0.150^*ALDX + 5.12^*PAR + TRPRXN$ $0.750^*HO_2 + 1.250^*XO_2 + 0.250^*XO_2N +$	$3.6E-11$
TERP + OH	$0.280^*FORM + 1.66^* PAR + 0.470^*ALDX +$ TRPRXN $0.570^*OH + 0.070^*HO_2 + 0.760^*XO_2 +$ $0.180^*XO_2N + 0.240^*FORM + 0.001^*CO +$	$1.5E-11*exp(449/T)$
TERP + O ₃	$7.000^*PAR + 0.210^*ALDX + 0.390^*CXO_3 +$ TRPRXN $0.470^*NO_2 + 0.280^*HO_2 + 1.030^*XO_2 +$	$1.2E-15*exp(T/821)$
TERP + NO ₃	$0.250^*XO_2N + 0.470^*ALDX + 0.530^*NTR +$ TRPRXN	$3.7E-12*exp(175/T)$

Table S2: Continued from previous page

Reactants	Products	Rate expression
SO ₂ + OH	→ SULF + HO ₂ + SULRXN	K ₀ = 3.0E-31*exp(300/T) ^{3.3} K _∞ = 1.5E-12
OH + ETOH	→ HO ₂ + 0.900*ALD2 + 0.050*ALDX + 0.100*FORM + 0.100*XO ₂	6.9E-12*exp(T/230)
OH + ETHA	→ 0.991*ALD2 + 0.991*XO ₂ + 0.009*XO ₂ N + HO ₂ + 0.200*ISPD + 0.800*NTR + XO ₂ +	8.7E-12*exp(T/1070)
NO ₂ + ISOP	→ 0.800*HO ₂ + 0.200*NO + 0.800*ALDX + 2.400*PAR	1.5E-19

Table S3: Photolysis reactions applied in the NMMB/BSC-CTM

Reactants	Products
$\text{NO}_2 + \text{hv}$	$\rightarrow \text{NO} + \text{O}$
$\text{O}_3 + \text{hv}$	$\rightarrow \text{O}$
$\text{O}_3 + \text{hv}$	$\rightarrow \text{O}^1\text{D}$
$\text{NO}_3 + \text{hv}$	$\rightarrow \text{NO}_2 + \text{O}$
$\text{NO}_3 + \text{hv}$	$\rightarrow \text{NO}$
$\text{HONO} + \text{hv}$	$\rightarrow \text{NO} + \text{OH}$
$\text{H}_2\text{O}_2 + \text{hv}$	$\rightarrow 2.000*\text{OH}$
$\text{PNA} + \text{hv}$	$\rightarrow 0.610*\text{HO}_2 + 0.610*\text{NO}_2 + 0.390*\text{OH} + 0.390*\text{NO}_3$
$\text{HNO}_3 + \text{hv}$	$\rightarrow \text{OH} + \text{NO}_2$
$\text{N}_2\text{O}_5 + \text{hv}$	$\rightarrow \text{NO}_2 + \text{NO}_3$
$\text{NTR} + \text{hv}$	$\rightarrow \text{NO}_2 + \text{HO}_2 + 0.330*\text{FORM} + 0.330*\text{ALD2} + 0.330*\text{ALDX} - 0.660*\text{PAR}$
$\text{FORM} + \text{hv}$	$\rightarrow 2.000*\text{HO}_2 + \text{CO}$
$\text{FORM} + \text{hv}$	$\rightarrow \text{CO}$
$\text{ALD2} + \text{hv}$	$\rightarrow \text{MEO}_2 + \text{CO} + \text{HO}_2$
$\text{PAN} + \text{hv}$	$\rightarrow \text{C}_2\text{O}_3 + \text{NO}_2$
$\text{PANX} + \text{hv}$	$\rightarrow \text{CXO}_3 + \text{NO}_2$
$\text{PACD} + \text{hv}$	$\rightarrow \text{MEO}_2 + \text{OH}$
$\text{ALDX} + \text{hv}$	$\rightarrow \text{MEO}_2 + \text{CO} + \text{HO}_2$

References

- W. M. Cox and J. A. Tikvart. A statistical procedure for determining the best performing air quality simulation model . *Atmospheric Environment. Part A. General Topics*, 24(9):2387 – 2395, 1990. ISSN 0960-1686. doi: [http://dx.doi.org/10.1016/0960-1686\(90\)90331-G](http://dx.doi.org/10.1016/0960-1686(90)90331-G). URL <http://www.sciencedirect.com/science/article/pii/096016869090331G>.
- A. Russell and R. Dennis. NARSTO critical review of photochemical models and modeling . *Atmospheric Environment*, 34(12–14):2283 – 2324, 2000. ISSN 1352-2310. doi: [http://dx.doi.org/10.1016/S1352-2310\(99\)00468-9](http://dx.doi.org/10.1016/S1352-2310(99)00468-9). URL <http://www.sciencedirect.com/science/article/pii/S1352231099004689>.
- U.S.EPA. Guideline for Regulatory Application of the Urban Airshed Model. Technical report, EPA-450/4-91-013. U.S. Environmental Protection Agency, Office of Air Quality Planning and Standards, Research Triangle Park, NC., 1991.