J. D. Annan (Editor)

While an editor comment is not formally required at this stage, I would like to encourage the authors to prepare a revised manuscript that takes account of the suggestions of the two helpful reviews.

Anonymous Referee #1

We thank the referee for her/his comments, and give our responses in detail below.

General Comments: This paper presents methodology for the ECCO v4 reanalysis with specific attention paid to changes in the current version. It also tries to address the controllability of the system, which is a very interesting and important question.

Since ECCO is a well-established reanalysis product that the authors rightly point out has been used in many scientific studies, the refinement of the product is very relevant to GMD. The paper presents advances that are extremely suitable for addressing questions within the scope of EGU. The controllability analysis in this paper is novel and potentially useful in addressing scientific questions as well as improving future state estimation projects. As the authors documented, this iteration of ECCO has enough modifications and improvements from the previous version to be considered a substantial advance in modeling science. Furthermore, since ECCO v4 will undoubtedly be used in future studies, it is important for this documentation to be published.

The new changes to ECCO are well documented and changes are clearly outlined. The system is obviously very large and complex, so there is excellent direction to references if the readers want to learn more about different aspects. In this way, what is new and what is previously done is clearly stated and documented. I believe that the description is complete enough that others can use the freely available code that the authors describe and reproduce the author's results. Tools are also provided to apply the framework to other applications.

The paper is well written and largely free of errors. The title is appropriate and it is clearly stated which model version is being described. The abstract is sufficient in summarizing the contents of the paper. Furthermore, the appendices are thorough and appropriate for this type of paper. I have a few minor suggestions for clarifications and a few typos that I will list below, but I think this is a very good paper that is very appropriate for this journal and should be published with only technical corrections. **Thanks.**

Specific Comments:

Page 3679, line 25 – It would be nice to have a little more elaboration on why it is tempting to attribute global mean sensitivity to discrete choices to omission of hydrology modeling over other explanations.

Sentence now refers to the "omission of atmospheric, continental, etc. modeling" more generally and as "merely a working hypothesis". The unclear reference to "hydrology" was expanded and is now stated between parentheses as an example to explain why we favor this hypothesis.

Page 3688, Line 28/Figure 10 – Fig. 10 shows misfits in ECCO v4 that are lower than other ECCO versions and other products. For the broad misfits that are still present, are there thoughts on how these can be addressed in future versions?

Further optimization (adjoint iterations) may simply be needed as stated in section 5.4, which now includes an explicit reference to Fig10.

Minor corrections:

Page 3681, Line 1 - commas around "for example"

Done.

Page 3686, Line 10 – Add the appendix number **Done.**

Anonymous Referee #2

We thank the referee for her/his comments, and give our responses in detail below.

This contribution is appropriate to the journal, it reports significant new work and new concepts, and I recommend that it be accepted, although I ask for some minor revisions.

This contribution has two aspects.

The first is a noble effort to document a very complicated modeling and assimilation system so others can both understand and work with the output and even reproduce the runs. It provides a comprehensive (and mostly well-written) description of the model and state estimation framework, and it is hard to suggest much that has been left out or needs more explanation. I am not enough of an expert to challenge, or even deeply check, many of the detailed model equations, but I trust that they are correct.

Thanks.

The system is working, as the fits show, and the recent improvements to the system are very impressive. Their discussion of weaknesses is particularly interesting, and it is good they acknowledge that error analysis is a weakness. This is in contrast to the "competing" ROMS assimilation system, which has well-developed uncertainty tools, even though it is not automatically-generated. This sparks a comment that the only reference to ROMS is Shchepetkin and McWilliams for the modified Adams-Bashforth time step, but I guess that given the purpose of this contribution, it is not necessary to provide a survey of models.

The two efforts maybe complement each other rather than compete with each other. In particular the MITgcm adjoint is typically run continuously over multiple decades to carry continuous state estimation, while the ROMS adjoint is geared toward sequential data assimilation. Uncertainty quantification may indeed be further developed in data assimilation than in state estimation as suggested by the referee, but the two problems are quite different. Not unlike Moore et al 2011 for ROMS, the present paper focuses on presenting one system rather than comparing them. A reference to Moore et al 2011 was added in the concluding section.

The second aspect is a detailed analysis of many runs of the same assimilation system to look at the sensitivity to a wide variety of model changes: "structural" and "parametric". This is made possible by the impressive the modesty of the v4 computation requirements. I had somehow thought that this computation would be beyond reach, but it is not.

quoting from the text: "Advanced usage of ECCO v4 may include re-running forward model solutions (the state estimate in particular) or its adjoint. Computational requirements are modest –the 20 year forward model integration typically takes between 6 and 12 h on 96 processors."

As noted by the referee, this is an advantage of ECCO v4. This point is now stressed in the concluding section, with a reference to the Appendix containing this quote.

Although the analysis here is welcome and very well done, there are a few things left out. A main question I would suggest be addressed is whether the adjustments of the mixing parameters are needed to compensate for the resolution of the model, in which case their spatial patterns may have little to do with real mixing. I agree that they are a

very convenient way to allow model errors, and, combined with adjustment of fluxes at the ocean surface, presumably allow the elimination of biases in temperature or salinity. While these adjustments produce a large reduction in the misfit to hydrographic data, it would help the curious reader to have the author's discussion of the likelihood of compensating errors.

The curious reader was already referred to the separate paper that assesses the mixing parameters geography in section 4.4. This reference is now placed at the end of section 5.2 and extended to discuss error compensation. The need for additional investigation is also now further stressed in the concluding section.

Phrased another way, the inclusion of these controls moves the

ECCO framework closer to the "weak constraint 4D-Var" used elsewhere, including ROMS, where error (control) terms can be included in every model equation at every grid point and time. This can make it easy to fit observations by deprecating the model dynamics, so a cautious approach is needed.

A major difference with weak constraint 4D-var however is that the chosen approach does not introduce source/sink terms of unknown nature in the model equations. Modifications of model parameters within acceptable ranges does not equate with deprecating model dynamics. The estimated parameters are of course uncertain, which is now further emphasized at the end of section 5.2.

In fact, the entire discussion of the model metrics responding to various controls and configurations could be made clearer. (and please write "Tables 3 and 8" instead of "Tables 3–8", which implies all the tables in between, too.) For example, is global mean temperature and salinity surface or total depth? If total depth, it's hard to see how mixing parameters could affect them much, since they redistribute the heat and the model is forced with fluxes. In addition, the conclusions drawn from the comparing the response magnitudes across different metrics were not convincing. I am especially skeptical of the bootstrap correlation calculations. So a bit more clarity here would help the dumber readers like me.

Section 5.1 was streamlined and clarified. Global means are computed over "total depth" but can react to any ocean model change since the surface buoyancy and freshwater forcing is computed through bulk formulae, which is now recalled in section 5.1. The use of bootstrapping is now further motivated.

Detailed suggestions:

first, please spell-check the manuscript. e.g. "abscence" on page 3662. "estime", and so on.

Done.

also there are many mismatched plurals, e.g. "slow models drifts" on page 3681. or page 3693: "internal-waves dynamics" (should be: internal-wave dynamics) Most of these are trivial, but can slow down the reading.

Done.

Finally, the Conclusion section seems to be a bit redundant in places, repeating "expert choices" when it doesn't seem necessary.

One of the two instances of "expert choices" in the conclusion was removed.

Abstract:

I found the following phrase confusing: "Both components are publicly available and highly integrated with the MITgcm" I suggest: "Both components are publicly available. The ECCO framework is highly integrated with the MITgcm"

Sentence was revised accordingly.

I also found the phrase "model-data constraints" to be confusing. I suggest "observational and model constraints", or something more specific.

Sentence was revised accordingly.

In fact, the word "constraints" is often added to "observational" in the text, where "observations" alone might be better. Much of the time "observational constraints" is correct, referring to constraining the model to match observations, but sometimes it seems to just mean observations. There are many variations, e.g. "observed data constraints", and I suggest going through and regularizing the terminology so that it is always the same, and observations are just "observations".

`constraint' was removed when un-necessary (in section 4.3 and elsewhere). `data' was generally preferred to `observations'. Terminology was regularized throughout the paper.

for example on page 3684: "A permanent issue is the need for additional data constraints, particularly in the abyss (Wunsch and Heimbach, 2014)." This implies that the observations exist, but were not used as constraints. I don't think this is what is meant, however. I suggest: "A permanent issue is the need for additional observations, particularly in the abyss (Wunsch and Heimbach, 2014)."

Sentence was revised accordingly.

The description of the grid could be a little clearer: Page 3658: "Poleward of 57 N, LLC is topologically equivalent to CS minus one cube face (Fig. 1)." then, later: "Between the LL sector and the Arctic cap, the grid makes a gradual, conformal transition that is evident in Fig. 3 between 57 and 67 N."

I suggest these two sentences be put adjacent, and perhaps a little more detail on how the grid transitions from LL in a sector to something like the CS, if that is indeed what happens. And/or just move up the reference to Appendix A so it comes at the start instead of end, and the reader can look at that before puzzling about the short summary.

Paragraph was revised accordingly.

This also applies to the Southern Cap, where the text says: "To the South of 70 S, LLC is topologically equivalent to a pillow case that would have two vertices in each hemisphere (Fig. 2, right panel)."

I first thought "hemisphere" meant east and west, and was confused, but they mean north and south; this could be rephrased just to say there are two vertices for the conformal grid on the southern cap and they are on land. No need for the pillow case. Paragraph was revised accordingly.

just a comment: The downside of the specialized grid is the complication of the analysis (page 3656), and I would be surprised if the Matlab toolbox could eliminate that entirely, but it is a very important part of the package.

page 3665: the "C-D" scheme is referenced without defining it. Please move up the definition, or refer to the defining section.

Done.

Figure 4: caption for lower panels should be clarified. Is it streamfunction at the surface or at 2000m?

Caption now specifies "for the vertically integrated flow".

The text should perhaps also say explicitly that the streamfunction is changed more by the C-D scheme than the customized viscosity, although the rms vertical velocity is also reduced more by the C-D scheme.

More explicit Fig. references were added where this point was already made.

I was surprised that the v4 solution was forced directly by wind stress instead of a bulk formula. I had thought that the ECCO framework had previous specified atmospheric fields and let bulk formulae compute the fluxes. Is this the case? If so, does the new approach not take account of stress modifications by surface currents or temperature

fronts? Please give a little more detail.

As already stated in the text, bulk formula are used to compute buoyancy and mass fluxes. For wind stress, both options are available as part of the model as now noted in section 3.5. The simple approach chosen in ECCO v4 accounts for wind stress errors directly, which is now more clearly stated. The referee's point regarding neglected stress modifications by surface currents was added.

section 4, page 3668: J is a SQUARED distance from the obs. same comment on next page, section 4.1

'squared' is now always appended before 'distance'.

figure 6 caption needs some editing for grammar (e.g. "bottom panel show" (add s), "all biweekly period" (add s))

in fact, all the captions could do with a little proof-reading. It is tedious to list the typos. term: "regression" tests: This is not regression as I usually see the word. I would characterize these as checksum experiments, or reproducibility checks...? Maybe this could be explained a little.

Captions were proof-read. We have further qualified `regression test' and added a textbook reference for this term in Appendix F. We prefer to retain the term "regression test", since it appears to be well understood to clearly distinguish between testing new features (not part of this) and testing that nothing has unexpectedly been changed (the goal of these tests). "Reproducibility tests" is not an ideal phrase, since the tests operate in the context of numerical and computational optimizations that may change reproducibility at the bit-wise level, but not change macroscopic behavior of a solution.

I particularly like Appendix G: the "solution history" section, as that is often a dark secret in state estimation. The model, parameters, and observations evolve during the iterations, and so reproducibility is difficult or impossible. I applaud the authors for listing the details, as part of their documentation of the solution. This disclosure could be helpful to others attempting related projects.

Thanks. Reproducing the detailed optimization and revision steps that led to this state estimate would admittedly be challenging. We should stress however that any ECCO v4 user can easily reproduce the state estimate solution. As far as we know this is a unique capability amongst ocean or atmospheric `re-analysis' products.

page 3702: "Revision 4 iteration 10 consisted in a filtering of atmospheric control parameters adjustments to reduce irregularities in the forcing that had appeared during adjoint iterations."

I suggest rephrasing or adding details to be clearer: was it space and/or time filtering?
`Filtering' was replaced with `trimming', which seems more accurate. This was done by subtracting leading EOFs, as now stated in the paper.

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ECCO version 4: an integrated framework for non-linear inverse modeling and global ocean state estimation

G. Forget¹, J.-M. Campin¹, P. Heimbach^{1,2,3}, C. N. Hill¹, R. M Ponte⁴, and C. Wunsch⁵

Correspondence to: G. Forget (gforget@mit.edu)

¹Dept. of Earth, Atmospheric and Planetary Sciences, Massachusetts Institute of Technology, Cambridge MA 02139, USA

²Institute for Computational Engineering and Sciences, The University of Texas at Austin, Austin, TX 78712, USA

³Jackson School of Geosciences, The University of Texas at Austin, Austin, TX 78712, USA

⁴Atmospheric and Environmental Research, Inc., Lexington MA 02421, USA

⁵Dept. of Earth and Planetary Sciences, Harvard University, Cambridge, MA 02139, USA

Abstract

This paper presents the ECCO v4 non-linear inverse modeling framework and its baseline solution for the evolving ocean state over the period 1992–2011. Both components are publicly available and highly integrated with the MITgcm. They are both subjected to regular, automated regression tests. The modeling framework includes sets of global conformal grids, a global model setup, implementations of model-data constraints and adjustable data constraints and control parameters, an interface to algorithmic differentiation, as well as a grid-independent, fully capable Matlab toolbox. The reference baseline ECCO v4 solution is a dynamically consistent ocean state estimate (ECCO-Production, release 1) without un-identified sources of heat and buoyancy, which any interested user will be able to reproduce accurately. The solution is an acceptable fit to most data and has been found physically plausible in many respects, as documented here and in related publications. Users are being provided with capabilities to assess model-data misfits for themselves. The synergy between modeling and data synthesis is asserted through the joint presentation of the modeling framework and the state estimate. In particular, the inverse estimate of parameterized physics was instrumental in improving the fit to the observed hydrography, and becomes an integral part of the ocean model setup available for general use. More generally, a first assessment of the relative importance of external, parametric and structural model errors is presented. Parametric and external model uncertainties appear to be of comparable importance and dominate over structural model uncertainty. The results generally underline the importance of including turbulent transport parameters in the inverse problem.

1 Introduction

The history of inverse modeling in oceanography goes back at least four decades (see Wunsch, 2006, for a general presentation). The canonical oceanographic inverse problem as implemented by Wunsch (1977) consisted in estimating the time mean absolute ocean circulation from synoptic, ship-based, hydrography transects. The physical model combined thermal-wind shear (diagnosed from observations) and a continuity equation. The model parameter to be estimated (i.e. the control vector) was the "reference level velocity". Least squares provide an adequate formulation to this inverse problem, and a practical method to avoid mis-interpreting geophysical noise (synoptic eddies, internal waves, etc.) for time mean ocean circulation features (Wunsch, 1977).

The original implementation has been extended substantially over subsequent decades, and some of the key technical developments are worth recalling (see also Wunsch and Heimbach, 2013a, for a review of the state of the art), as they provide the context for the present work. Non-linearities were introduced (Mercier, 1986) to incorporate optimal interpolation of hydrographic data in the inverse problem. While diapycnal and horizontal diffusion were also introduced early on (Schott and Zantopp, 1980; Olbers et al., 1985), the need for extending the inversion problem to parameterized advective eddy transports (Gent and Mcwilliams, 1990) was not fully appreciated until the study of Ferreira et al. (2005).

Time dependency and the use of Lagrange multipliers (i.e. the adjoint method) were first introduced in ocean inverse modeling by Thacker and Long (1988) and Holland and Malanotte-Rizzoli (1989) and applied to general circulation models by Tziperman and Thacker (1989) and Tziperman et al. (1992a, b). Later on algorithmic differentiation (AD) was introduced, making the use of Lagrange multipliers more practical (Griewank, 1992; Giering and Kaminski, 1998). Its application (Marotzke et al., 1999; Heimbach et al., 2002, 2005) to the Massachusetts Institute of Technology general circulation model (MITgcm; Marshall et al., 1997; Adcroft et al., 2004b) allowed for implementation of the time varying non-linear inverse problem, as envisioned by Wunsch and Minster (1982) and Wunsch (1984), to the case of actual observations data (Stammer et al., 2002; Ferron and Marotzke, 2003).

The MITgcm AD capabilities remain exceptional amongst general circulation models. Over the last decade, in the context of the Estimating the Circulation and Climate of the Ocean (ECCO) project, the MITgcm non-linear inverse modeling framework (using the adjoint method and algorithmic differentiation) has become a common tool for data synthesis, applied by many investigators to derive ocean state estimates (Stammer et al., 2004; Wunsch et al., 2007; Köhl et al., 2007; Köhl and Stammer, 2008; Forget et al., 2008b; Wunsch and Heimbach, 2009; Hoteit et al., 2009; Forget, 2010; Mazloff et al., 2010; Köhl et al., 2012; Speer and Forget, 2013; Köhl, 2014; Losch et al., 2014; Dail and Wunsch, 2014).

General circulation models implement the primitive equations, which extend far beyond the physics and numerics used in common inverse box models. On the one hand, they readily provide a versatile tool for dynamical interpolation of virtually all types of observations. On the other hand, numerical modeling has to be regarded as an integral part of non-linear inverse modeling, and as a primary responsibility of groups carrying ocean state estimation. Indeed, the quality of the model and the adequacy of its settings determine the physical consistency of ocean state estimates. Hence the state estimation group at MIT has become a main contributor of MITgcm code including, but not limited to the estimation framework implementation implementation of the estimation framework. Furthermore, the development of the new ECCO version 4 (ECCO v4) estimate described here started with an extensive revisit of MITgcm settings.

These considerations prompt the joint depiction of forward model setup and estimation framework developments as part of ECCO v4, and of the baseline solution of the non-linear inverse model. The overarching goal, which is essential to the oceanographic community, is the unification of the two pillars of science, namely observations (emphasis here is on data of global coverage) and theory (of which general circulation models are a vehicle). Thus, the synergy between data analysis and modeling is a guiding thread of this paper.

As a complement to this paper, and a number of associated publications, the setup and baseline solution of ECCO v4 are thoroughly documented by an extended suite of diagnostics (the "standard analysis" provided as Supplement) that users can readily download or reproduce. Daily and monthly regression tests are run for, respectively, a few time steps and 20 years. This will allow, for the foreseeable future, any user to generate additional output that may be needed for extended data-model data and model analyses. Thus, the authors aim to provide ECCO v4 as a fully-integrated non-linear inverse modeling framework including its baseline time-dependent solution that any interested user can readily start from, analyze and/or accurately re-run.

The foundation of the ECCO v4 model setup is a set of global grids of the earth surface (Sect. 2). The design, implementation and specification of the forward model setup and of the estimation framework are presented in Sects. 3 and 4 respectively. The baseline ECCO v4 solution (the ECCO-Production ECCO v4, release 1 state estimate) is the subject of Sect. 5, which is followed by conclusions and perspectives (Sect. 6).

Global grids 2

The most visible grid improvement, as compared with earlier ECCO configurations, is the extension of the gridded domain to the Arctic. This limitation of ECCO estimates produced until 2008 was due to the use of a latitude-longitude grid (LL; left panel of Fig. 1) that simply follows straight lines in spherical-polar projection, and requires an exponentially decreasing time step when approaching the North polePole.

The cubed-sphere grid (CS; center panel in Fig. 1) has been successfully used in various MITgcm calculations (e.g., Menemenlis et al., 2005a; Marshall et al., 2007b) resolving the Arctic. The CS grid is a conformal mapping of a sphere to a cube surface, such that each face contains one sixth of the so gridded earth (Rančić et al., 1996; Purser and Rančić, 1998). At its 8 vertices (cube corners), CS grid lines converge exponentially as resolution increases, but more slowly than for LL at geographic poles.

However, a number of shortcomings of CS have been noted. First, loss of orthogonality near the cube corner corners is exacerbated when increasing horizontal resolution. Second, some of the vertices have to be placed on ocean-covered areas, and have an exceedingly high resolution, requiring unnecessarily small time steps. Third, such grids represent an obstacle for new users who were accustomed to latitude-longitude grids. These considerations led to the design of the Lat-Lon-Cap grid (LLC; right panel in Fig. 1) such that

- 1. the grid reverts to a simple LL sector between 70° S and 57° N;
- 2. grid vertices are located over land;
- 3. grid heterogeneities remain acceptable at $\frac{1}{48}^{\circ}$ resolution.

At mid-latitudes, within the LL sector, the LLC grid is locally isotropic with grid spacing varying in $cos(\varphi)$, where φ denotes latitude. At low latitudes LLC is refined in the meridional direction to better resolve the tropical system of zonal currents¹. Grid scaling properties are shown in more detail in Figs. 2 and 3. The LL sector mesh derives from a simple analytic formulation based of geographic latitude and longitude. Users who may not be particularly invested in high latitude research may skip over the rest of this section, and simply extract the LL sector (70° S and 57° N) out of global LLC fields (see Sect. "Code availability").

Poleward of 57° N, LLC is topologically equivalent to CS minus one cube face (Fig. 1). Details of the grid generation method are reported in Appendix A. The vertices of the *Arctic* cap are placed at a latitude of 67° N and in a specific orientation such that they all fall over land (Fig. 2, middle panel). For any given Arctic face dimension, LLC has the added advantage of an increased resolution in the Arctic as compared with CS, which has vertices at 45N. The LLC grid is specifically designed for ocean simulations, whereas the CS grid is more suitable for atmospheric simulations. ². Between the LL sector and the Arctic cap, the grid makes a gradual, conformal transition that is evident in Fig. 3 between 57 and 67° N. To the South south of 70° S, LLC is topologically equivalent to a pillow case that would have two vertices in each hemisphere (Fig. 2, right panel). The vertices has two vertices that are again placed over land at a latitude of 80° S and away from the Ross and Weddell ice shelves (Fig. 2, right panel). Details of the grid generation method are reported in Appendix A.

Looking beyond the immediate need for a truly global coarse resolution grid, we chose to generate a parent $\frac{1}{48}^{\circ}$ global grid³. The main advantages of this approach are that a full suite of lower resolution grids readily descend from the parent grid, and that the entire suite of commensurate grids share grid lines. Thus, in principle, one can easily nest back and forth between grids of different resolution. These global grids are being used in a number of

¹An alternative version of LLC that remains locally isotropic in the tropics is also available.

²For any given Arctic face dimension, LLC has the added advantage of an increased resolution in the Arctic as compared with CS, which has vertices at 45° N.

³The resolution along the equator is quoted as $\frac{1}{48}$ ° (see Fig. 3 for details).

model setups at 1° resolution (Danabasoglu et al., 2014; Marshall et al., 2014; Köhl, 2014) and at full resolution (D. Menemenlis, personal communication, 2014).

The parent $\frac{1}{48}$ ° global grid has 17280 longitudinal grid cells. It is labelled "LLC4320" since the common face dimension (i.e. the number of points along one quarter of earth circumference at the equator) is 4320. This grid size was chosen to maximize the number of integer factors available for coarsening the parent grid and for partitioning the computational domain in parallel computer environments⁴. It has 64 whole integer factors in total, so that the $\frac{1}{48}$ ° grid can readily, accurately be coarsened to, e.g., $\frac{1}{24}$ °, $\frac{1}{16}$ °, $\frac{1}{12}$ °, $\frac{1}{8}$ °, $\frac{1}{6}$ °, $\frac{1}{4}$ °, $\frac{1}{3}$ °, $\frac{1}{2}$ °, 1°, 2° or 4°. This is a desirable property for a long-term project such as ECCO, in which spatio-temporal resolution is expected to increase in the future as computing capability and observational data base will keep increasing. A high degree of factorization also provides a convenient basis for down-scaled regional computations that employ boundary conditions from the state estimate (Sect. 5).

Advanced gridding has clear advantages from the standpoint of numerical ocean modeling. It can however put additional burdens on users of ocean model output who may find themselves coding the same diagnostics over and over again to accommodate different grids. One common approach is to distribute fields that were interpolated to a simpler grid (e.g., LL). This approach however, however, tends to introduce sizable errors (e.g., in areal integrals and transports). A different and simple approach to the analysis of model output is chosen here that does not alter the results but alleviates the burden of grid specifics when analyzing model output - the "gcmfaces" analysis framework that mimics the gridded earth decomposition of general circulation models in Matlab (Appendix C).

Model configuration

The model configuration presented below is the ECCO v4 setup used in state estimation (Sects. 4 and 5) and based on the LLC90 grid (Sect. 2). Variants of the ECCO v4 setup

⁴Number 17 280 is known as the compositorial of 10, i.e the product of composite numbers less than or equal to 10 (see Wells, 2011).

are also used in un-optimized model simulations (Danabasoglu et al., 2014; Marshall et al., 2014). The setup uses fully supported options of MITgcm software, is archived and regularly benchmarked subjected to regression testing (Appendix F), and is freely available along with the MITgcm itself (Sect. "Code availability").

The MITgcm, as configured in ECCO v4, solves the hydrostatic, Boussinesq equations (Marshall et al., 1997) using the z^* rescaled height vertical coordinate (Adcroft and Campin, 2004) and the vector-invariant form of the momentum equation (Adcroft et al., 2004a). This latter choice yields a discretized momentum equation without metric terms, which simplifies the handling of elaborate grids such as LLC90 (Sect. 2). This section summarizes the model equations, settings, and new MITgcm features (MITgcm Group, 2002; Adcroft et al., 2004b) used in ECCO v4. The novelty here largely resides in additions of forward model features to the body of adjointed codes (Sect. 4) and in their use in the state estimate (Sect. 5). Table 1 provides a list of basic model settings.

The relative importance of various model settings generally depends on the ocean state characteristic of interest. Here, a selection of ocean state characteristics is made amongst squared model-data differences distances (see Sect. 4), monthly time series of global mean quantities, and time-averaged meridional transports (Table 2). The selected characteristics in Table 2 are representative of the multi-faceted nature of ocean state estimation. These characteristics are used to gauge perturbations of 2020-year solutions to various model settings (Table 3) - and to estimated model parameter adjustments (see Sects. 4 and 5). They are also used to benchmark verify state estimate re-runs and model revisions (first 3 rows of Table 3; Appendix F) and to gauge the sensitivity of the state estimate to adjusted control parameters (Sect. 5). F).

3.1 **Basic equations**

For a water column that extends from the bottom at z = -H to the free surface at $z = \eta$, the z^* vertical coordinate is defined as $z = \eta + s^*z^*$ with the scaling factor $s^* = 1 + \eta/H$. In this section, the notation ∇_{z^*} indicates the nabla operator at constant z^* , i.e., in a plane of constant z^* value. The z^* coordinate set of equations was introduced by Adcroft and Campin (2004) (their Eqs. 9–11 and 13). Written in vector-invariant formulation they read:

$$\frac{\partial \boldsymbol{v}}{\partial t} + (f + \zeta)\hat{\boldsymbol{k}} \times \boldsymbol{v} + \nabla_{z^*}\mathsf{KE} + w\frac{\partial \boldsymbol{v}}{\partial z} + g\nabla_{z^*}\eta + \nabla_h\Phi' = \boldsymbol{D}_{z^*,\boldsymbol{v}} + \boldsymbol{D}_{\perp,\boldsymbol{v}} + \boldsymbol{\mathcal{F}}_{\boldsymbol{v}}$$
(1)

$$\frac{\partial \Phi'}{\partial z} = g \frac{\rho'}{\rho_c} \tag{2}$$

$$\frac{1}{H}\frac{\partial \eta}{\partial t} + \nabla_{z^*}(s^*v) + \frac{\partial w}{\partial z^*} = s^*\mathcal{F}$$
(3)

$$\frac{\partial(s^*\theta)}{\partial t} + \nabla_{z^*}(s^*\theta v_{\text{res}}) + \frac{\partial(\theta w_{\text{res}})}{\partial z^*} = s^*(\mathcal{F}_{\theta} + D_{\sigma,\theta} + D_{\perp,\theta})$$
(4)

$$\frac{\partial(s^*S)}{\partial t} + \nabla_{z^*}(s^*Sv_{\mathsf{res}}) + \frac{\partial(Sw_{\mathsf{res}})}{\partial z^*} = s^*(\mathcal{F}_S + D_{\sigma,S} + D_{\perp,S}) \tag{5}$$

where v is the horizontal velocity, $w^* = w/s^*$ is the vertical velocity in z^* coordinates⁵, \hat{k} is the vertical unity vector, f and $\zeta = \nabla \times v$ are the planetary and relative vorticity vertical component, KE is the horizontal kinetic energy, q is gravity, ρ' is the density anomaly relative to the constant Boussinesq density ρ_c ($\rho = \rho_c + \rho'$), Φ' is the pressure anomaly scaled by constant density ($\Phi' = p'/\rho_c$), θ and S are the potential temperature and salinity, $D_{z^*}, D_{\perp}, D_{\sigma}$ are subgrid-scale (SGS) processes parameterized as mixing horizontally, vertically or along iso-neutral surfaces, and $\mathcal{F}_{m{v}},~\mathcal{F},~\mathcal{F}_{m{ heta}},~\mathcal{F}_{S}$ are the forcing terms which are generally concentrated at the surface. Fields θ and S are advected (in Eqs. 4 and 5) by the residual-mean velocity field $(v_{res}, w_{res}) = (v, w) + (v_b, w_b)$ where (v_b, w_b) is the bolus velocity parameterizing the effect of unresolved eddies (Gent and Mcwilliams, 1990, GM hereafter).

The z^* coordinate formulation introduces a major difference in the continuity equation (Eq. 3) as compared to the z coordinate. Thus, even in the abscence absence of freshwater input ($\mathcal{F}=0$), the divergence of the 3-D flow field (u,v,w) is no longer zero. Then,

⁵For practical reason, the vertical velocity calculated by the model (w per Eq. 3) is neither the z^* vertical velocity w^* nor the true vertical velocity that would contain additional contributions (Adcroft and Campin, 2004, see their Eq. 4).

within the continuity equation, the rate of change of sea-surface elevation (the first term in Eq. 3) is uniformly distributed along the water column (as denoted by the 1/H scaling). The vertical velocity component w is obtained diagnostically from the continuity equation (Eq. 3). Furthermore, the horizontal momentum equation (Eq. 1) differs from the z coordinate case by the expression of horizontal pressure gradient (Adcroft and Campin, 2004, Eq. 15):

$$\nabla_h \Phi' = \nabla_{z^*} \Phi' + g \frac{\rho'}{\rho_c} \nabla_{z^*} \left(\eta \left(1 + \frac{z^*}{H} \right) \right) \tag{6}$$

where the second term represents the effect of gravity acting on the slope of constant z^* surface. The vertical momentum equation (Eq. 2) is reduced to the hydrostatic balance and sea-water density ρ is evaluated using the Jackett and McDougall (1995) equation of state in which pressure is assumed to be a function of only depth ($p = -\rho_c g z^*$) so that any compressible effect is completely removed.

Apart from the horizontal grid and the vertical coordinate z^* , the choice of time-stepping options used in ECCO v4 represents another major change compared to previous ECCO configurations. The time-discretized version of Eqs. (1)–(5) is reported in Appendix B, which is particularly important to understand budget and other diagnostics (Appendix C). In summary, the staggered time step approach is used, along with Adams-Bashforth 3 (AB-3) time stepping for momentum advection and the Coriolis term, 3rd third order Direct Space Time tracer advection (DST-3; a multi-dimensional scheme), and 3rd third order implicit tracer vertical advection (unconditionally stable). These options improve the model stability, allowing for a longer time step. Thus, the time step restriction due to the Coriolis term in the Arctic is alleviated by the use of AB-3 ($\Delta t = 1\,\mathrm{h}$ was unstable with AB-2 and $\epsilon_{\mathrm{AB}} \sim 0.1$). Also, the chosen combination of staggered time-stepping and tracer advection schemes increases the stability limit related to internal-wave speed. With these choices a time step of $\Delta t = 1 \, \text{h}$ is used with the LLC90 grid (Table 1).

3.2 Volume and tracer conservation

ECCO v4 uses a non-linear free surface combined with *real freshwater flux* forcing and the z^* coordinate. This approach allows to include material exchanges through the free surface in a physically intuitive way (Campin et al., 2008) and to achieve exact tracer conservation, both locally and globally (Campin et al., 2004). To illustrate this point, it is useful to start from the vertical integral of Eqs. (3)–(5), which is

$$\frac{\partial \eta}{\partial t} + \nabla \cdot \int_{-H}^{\eta} v \, dz = (PmE)/\rho_c \tag{7}$$

$$\frac{\partial}{\partial t}((\eta + H)\overline{\theta}) + \nabla \cdot \int_{-H}^{\eta} \theta \, \boldsymbol{v}_{\text{res}} \, \mathrm{d}z = Q_{\text{net}}/(\rho_{\text{c}} C_p) + \int_{-H}^{\eta} D_{\sigma,\theta} \, \mathrm{d}z \tag{8}$$

$$\frac{\partial}{\partial t}((\eta + H)\overline{S}) + \nabla \cdot \int_{-H}^{\eta} S \, \boldsymbol{v}_{\text{res}} \, \mathrm{d}z = S_{\text{flux}}/\rho_{\text{c}} + \int_{-H}^{\eta} D_{\sigma,S} \, \mathrm{d}z \tag{9}$$

where the overbar denotes vertical averaging according to $\overline{\varphi} = \frac{1}{(\eta + H)} \int_{-H}^{\eta} \varphi \, dz$.

The forcing terms \mathcal{F} , \mathcal{F}_{θ} , \mathcal{F}_{S} in Eqs. (3)–(5) are concentrated at or near the surface (unless geothermal heating at the bottom is active) and have been replaced by their integral form in Eqs. (7)–(9), namely the net fresh-water input at the surface (PmE, in kg m⁻² s⁻¹), the net heat flux into the water column (Q_{net} , in W m⁻²) and the salt-flux at the surface (S_{flux} , in g m $^{-2}$ s $^{-1}$) which is zero in the absence of seaice and salinity relaxation (see Sect. 3.5).

With the non-linear free-surface, the water column thickness varies as the free-surface goes up and down (as apparent in Eqs. 7–9). With the z^* coordinate, this variation is distributed vertically over all grid-cells⁶. The fact that η enters the continuity equation (Eq. 7)

⁶Each $z^* = -\alpha H$ level is a moving $z = z^* + (1 - \alpha)\eta z$ surface; $z = z^* + (1 - \alpha)\eta z = \eta$ at $z^* = -\alpha H$ 0; z = -H at $z^* = -H$.

also through $\int_{-H}^{\eta} dz$ renders the free-surface non-linear; furthermore, time dependent gridcell thickness introduces many more non-linearities which required code modifications to ensure efficient adjoint code generation via AD (Sect. 4.2).

Earlier ECCO configurations relied on the linear free-surface method (LFS), where column thickness and grid-cell thickness are fixed in time. The LFS version of Eqs. (7) and (9) is:

$$\frac{\partial \eta}{\partial t} + \nabla \cdot \int_{-H}^{0} v \, dz = \epsilon_{FW}(PmE)/\rho_{c}$$
 (10)

$$\frac{\partial}{\partial t}(H\overline{S}) + (\mathsf{PmE})/\rho_{\mathsf{c}}\,\tilde{S} + \nabla \cdot \int\limits_{-H}^{0} S\,\boldsymbol{v}_{\mathsf{res}}\,\mathsf{d}z = S_{\mathsf{flux}}/\rho_{\mathsf{c}} + \int\limits_{-H}^{0} D_{\sigma,S}\,\mathsf{d}z \tag{11}$$

The Goldsbrough-Stommel circulation (Stommel, 1984) can be accounted for by setting $\epsilon_{\rm FW}=1$ (*virtual fresh-water*) or ignored ($\epsilon_{\rm FW}=0$). However, since grid-cell thickness is held fixed with LFS, the dilution effect due to surface freshwater flux needs to be represented explicitly as a virtual salt flux (2nd second term in Eq. 11) using either the local surface salinity S or a constant S_o as \tilde{S} , with drawbacks in both cases (see, e.g., Campin et al., 2008). By contrast, the non-linear free-surface formulation incorporates the dilution effect very naturally, within the time derivative of the water-column salt content (first term in Eq. 9).

The symmetry between continuity (Eq. 7) and tracer (Eqs. 8 and 9) equations allows for strict tracer conservation (Campin et al., 2004) when discretized consistently (Appendix B). In contrast, in the LFS case, this symmetry is lacking $(\partial \eta/\partial t)$ in Eq. 10 has no counter part in Eq. 11) resulting in artificial tracer loss or gain (unless a global correction is added).

Tracer transports 3.3

Ocean tracers are advected by the residual mean velocity $v^{\rm res}, w^{\rm res}$ (Eqs. 4 and 5). The present ECCO v4 uses the 3rd third order DST scheme in the horizontal, and the implicit 3rd

third order upwind scheme in the vertical. Previous ECCO configurations used the explicit 3rd third order upwind scheme in all directions. Flux limited advection schemes are also available in forward mode, although they are not used in the state estimate (Sect. 5), since they are not yet in the body of adjointed codes (Sect. 4). Choices of advection schemes are a concern to in ocean state estimation, since their structural properties cannot generally be controlled by continuous parameters, and since numerical diffusion and advective overshoots could preclude an adequate fit to observations. Their importance can be gauged from Table 3. Thus, activating flux limiters has a sizable influence over 20 years, which is generally smaller than the impact of activating the C-D scheme (defined in the next section), but exceeds the impact of activating geothermal heating for example (Table 3; see next section). Global mean times series often show an exceptionally high sensitivity to a variety of model settings, and to surface boundary layer settings in particular (Table 3).

Diffusion includes diapycnal and isopycnal components, the GGL mixed layer turbulence closure (Gaspar et al., 1990), and simple convective adjustment. The latter (GGL and convective adjustment) are used instead of the KPP vertical mixing scheme (Large et al., 1994) that was used in earlier ECCO configurations. The rationale for this choice and its impact on the 2020-year solution is further discussed in Sect. 5. Time-invariant three dimensional fields of background diapycnal diffusivity (\mathcal{K}_d), isopycnal diffusivity (\mathcal{K}_σ) and GM intensity (\mathcal{K}_{qm}) are adjusted under observational constraints (the data constraints listed in Sect. 4 starting from constant first guess values (reported in Table 1). The estimated parameter maps for these highly uncertain coefficients become an integral part of the ECCO v4 model setup. In Sect. 5, the sensitivity to these parameters parameter adjustments is evaluated, and compared with the results in Table 3. The geography of \mathcal{K}_{qm} , \mathcal{K}_{σ} and \mathcal{K}_{d} , their impact on stratification, and their observability by means of Argo are further assessed in Forget et al. (2015).

Momentum discretization 3.4

Parameters of the momentum Eq. (1) currently used in ECCO v4 are provided in Table 1. Lateral eddy viscosity is harmonic and dependent on grid spacing, with coefficient given by $0.25 \times \mu L^2/\Delta t$, where $\mu = 2 \times 10^{-2}$ (viscAhGrid in Table 1) is a non-dimensional scaling number, L^2 is the spatially varying grid spacing squared (Fig. 2 shows L) and $\Delta t = 3600 \, \mathrm{s}$ (deltaTmom in Table 1). The resulting viscosity varies from $\approx 10^3$ to $1.6 \times 10^4 \text{m}^2 \, \text{s}^{-1}$, depending on location. The other dissipation contributions used in ECCO v4 are harmonic vertical viscosity and quadratic bottom drag (with parameters in Table 1) plus contributions from GGL.

Previous ECCO configurations used the C-D scheme (Adcroft et al., 1999) that interpolates the Coriolis term from the Arakawa C grid to a D grid and back. This scheme acts to reduce grid scale noise that is otherwise seen in the vertical velocity fields at all time scales, and particularly in the deep ocean (Fig. 4). Large vertical velocities have adverse effects on adjoint model stability, which ECCO originally resolved by means of the C-D scheme. The C-D scheme does however have a large impact on the large scale ocean circulation (Fig. 4) and hydrography (Table 3).

A comparable damping of the barotropic circulation could be obtained through a large increase in viscosity (not shown). Also vertical velocity noise is most intense near the ocean floor, which led us to the inference that adding viscosity more selectively near topography could suffice to damp the vertical velocity noise (Fig. 4, top panels) and, along with the use of vertical implicit advection, could stabilize the adjoint. Because the impact of this approach on the circulation and hydrography (Fig. 4, bottom panels) and hydrography (Table 3) is more muted than that of the C-D scheme, the latter was abandoned in ECCO v4. Targeted viscosity increase near topography remains needed to stabilize adjoint solutions (Sect. 4), but it can be omitted in forward solutions, as done in the state estimate (Sect. 5).

Surface boundary conditions 3.5

Upward buoyancy, radiative and mass fluxes (latent, sensible and radiative contributions to \mathcal{F}_{θ} ; evaporation as part of \mathcal{F}) through the free surface are computed using the bulk formulae of Large and Yeager (2004), and 6 hourly ERA-Interim re-analysis fields (Dee et al., 2011) for the near surface atmospheric state (temperature, humidity, downward radiation, precipitation). State estimation accounts for atmospheric re-analysis field uncertainties (Sect. 4).

Downward shortwave radiation is allowed to penetrate, with exponential decay, to a depth of 200 m as part of \mathcal{F}_{θ} (Eq. 4). A seasonal climatology of runoff, from Fekete et al. (2002), is added as part of \mathcal{F} (Eq. 3).

Earlier ECCO configurations using the *virtual salt flux* approach with $\epsilon_{FW} = 0$ (Sect. 3.2) could only account for the dynamical impact of precipitation, evaporation and runoff as they affect buoyancy (see Ponte, 2006). Accordingly, they could only include seaice as a levitating layer without any direct effect on η (Campin et al., 2008). In contrast, ECCO v4 uses the real freshwater flux approach (Sect. 3.2) and thus further accounts for the dynamical effects of material exchanges through the free surface (either with the atmosphere, land or seaice) as shown in Campin et al. (2008).

Open ocean rain, evaporation and runoff simply carry (advect through the free surface) the local SST and zero salinity in the model. When seaice is present, buoyancy and mass fluxes⁷ are recomputed based upon the thermodynamic balance of a fully interactive seaice model (Losch et al., 2010). In this model as configured in ECCO v4, seaice carries 0 °C and 4 g kg⁻¹ salinity, while snow carries 0 °C and zero salinity.

The implementation of mass, buoyancy and momentum exchanges through the seaiceocean interface in the rescaled z^* coordinate framework is presented in detail in Campin et al. (2008). A further correction was added in ECCO v4 to ensure conservation of heat for the combined ocean+seaice+snow system. While the ocean model is configured to exchange freshwater at the local SST, the seaice model operates at constant internal heat, so it cannot freeze and melt at variable temperature. The added correction simply puts the heat differential back into the ocean. Ocean+seaice+snow budgets (as well as separate ocean, seaice, snow budgets) of mass, heat and salt are then closed to machine precision and readily diagnosed (Appendix C).

In centennial ocean model simulations, it is customary to add a Newtonian relaxation of surface salinity to an observation-based climatological map a gridded observational product (e.g., Danabasoglu et al., 2014) as part of \mathcal{F}_S (Eq. 5). While this method has no clear physical basis, it generally adds stability to centennial simulations. In contrast, the state estimate

 $^{7\}mathcal{F}_{\theta}$, \mathcal{F}_{S} , \mathcal{F} in Eqs. (3)–(5); PmE, Q_{net} , S_{flux} in Eqs. (7)–(9).

(Sect. 5) has no salinity relaxation term, so that $\mathcal{F}_S \neq 0$ only occurs when seaice (which salinity is set to 4 g kg⁻¹) melts or freezes. Salt rejected by seaice formation is distributed in the vertical using the parameterization of Duffy et al. (1999) and Nguyen et al. (2009) as part of \mathcal{F}_S .

Wind stress, also from ERA-Interim, is applied directly as part of \mathcal{F}_v (Eq. 1) in ECCO v4. A common alternative is to compute wind stress also through bulk formulae, which is available as an option of the model. This approach could be used to account for wind stress modifications by surface currents that are neglected in ERA-Interim. However computing wind stress through bulk formulae using atmospheric re-analysis fields typically requires backing out adequate drag coefficients - so that the results would approximately match surface stresses that, in atmospheric models, follow from a momentum balance rather than bulk formulae - or ad-hoc adjustments of atmospheric variables (see, e.g. Large and Yeager, 2004; Risien and Chelton, 2008). In the context of state estimation, the direct specification of wind stress further allows for a clear distinction between momentum controls on the one hand, and buoyancy and mass controls on the other hand (see, e.g., Large and Yeager, 2004; Risien and Chelton, 2008). Instead state estimation accounts for re-analysis wind stress uncertainty directly (Sect. 4).

Estimation framework

The state estimation problem is defined here by a distance to observations squared model-data distance (J) to be minimized under the constraint of a dynamical model. Section 4.1 formulates the state estimation problem in more detail. Section 4.2 provides an overview of the MITgcm adjoint, which is instrumental in solving the state estimation problem, and its recent developments in the context of ECCO v4. Aside from the dynamical model (Sects. 2 and 3) the defining ingredients of state estimation are model-data data constraints and control parameters. Their ECCO v4 implementation and specifications are covered in Sects. 4.3 and 4.4.

The state estimate (Sect. 5) is a solution of the forward model (Sects. 2 and 3) at an approximate minimum of J. The process of finding such solutions, typically through an iterative optimization process and using the adjoint model, is not a focus of this paper. A number of well known optimization methods, with third party implementations freely available online, can be used to this end (see, e.g., Heimbach et al., 2005, and references therein) (see, e.g., Heimbach et al., 2005, and references therein)

Note that the existence of a unique global minimum of J is only rigorously established for linear least squares, when it can be solved for in matrix form to machine precision. In contrast, for non-linear inverse problems⁸ one can only aim to find at least one approximate minimum of J that is an *acceptable* fit to the data (i.e. a fit within specified errors).

4.1 **Problem formulation**

State estimation consists in minimizing a least squares squared distance, $J(\mathfrak{u})$, that is defined as

$$J(\mathfrak{u}) = \sum_{i} \alpha_{i} \times \left(d_{i}^{T} \mathbf{R}_{i}^{-1} d_{i} \right) + \sum_{j} \beta_{j} \times \left(\mathfrak{u}_{j}^{T} \mathfrak{u}_{j} \right)$$

$$\tag{12}$$

$$d_i = \mathcal{P}(m_i - o_i) \tag{13}$$

$$m_i = \mathcal{SDM}(\mathfrak{v}) \tag{14}$$

$$\mathfrak{v} = \mathcal{Q}(\mathfrak{u}) \tag{15}$$

$$\mathfrak{u} = \mathcal{R}(\mathfrak{u}') \tag{16}$$

where d_i denotes a set of model-data differences misfits, α_i the corresponding multiplier, \mathbf{R}_i^{-1} the corresponding weights, \mathfrak{u}_i a set of non-dimensional controls, and β_i the corresponding multiplier. Additional symbols appearing in Eqs. (13)-(16) are defined below. The implementation of Eqs. (12)-(16) and the adjoint interface within the MITgcm is charted in Fig. 5.

⁸The degree of non-linearity may depend on the process of interest and increases substantially upon inclusion of meso-scale eddies.

Model counterparts (m_i) to ebservational data (o_i) derive from a set of adjustable model parameters (v) through the model dynamics (\mathcal{M}) , diagnostic computations (\mathcal{D}) , and subsampling or averaging in space and time (\mathcal{S}) , performed as the forward model steps through time (Eq. 14). Model-data misfits are then computed, upon completion of the forward model simulation, in order to evaluate J(u) and provide the adjoint model forcing (Sect. 4.2). Raw model-data misfits (m_i-o_i) can be penalized directly (i.e. used in Eq. 12 in place of d_i). More generally though, as formulated in Eq. (13), misfits being penalized $(d_i$ in Eq. 12) derive from m_i-o_i through the generic post-processor \mathcal{P} (Sect. 4.3).

The control problem, as implemented in ECCO v4, is non-dimensional, as reflected by the omission of weights in control penalties $(u_j^T u_j, \text{Eq. 12})$. Non-dimensional controls are scaled to physical units through multiplication by their respective uncertainty fields, as part of the generic pre-processor \mathcal{Q} (Eq. 15; Sect. 4.4). Pre-conditioner \mathcal{R} (Eq. 16) does not appear in the estimation problem itself (Eq. 12), as it only serves to push an optimization process preferentially towards certain directions of the control space.

The specification of (always approximate) error covariances (e.g., \mathbb{R}_i) is a key ingredient of ocean state estimation, and least squares in general. ECCO has contributed a large body of work in this respect (e.g. Forget and Wunsch, 2007; Ponte et al., 2007; Quinn and Ponte, 2008, 2010; Chaudhuri et al., 2007; Quinn and Ponte, 2008, 2010; Chaudhuri et al., 2007; Quinn and Ponte, 2008, 2010; Chaudhuri et al., 2007; Quinn and So-forth.

For problems as massive as ECCO v4 (see Tables 5–7), full error covariance matrices are impractical value in this context. For example, the method of Weaver and Courtier (2001) is used in ECCO v4 to specify control parameter adjustment scales (Sect. 4.4) and penalize large-scale model-data misfits (Forget and Ponte, 201

however, adequate in practice as a means to partly compensate for approximations in error covariances error covariance approximations, and the neglect of \mathbf{R}_i non-diagonal terms in particular. They also provide a practical means to accelerate the optimization of data sets fit to data introduced in J during later stages of optimization. Furthermore, $\mathfrak{u}_i^T\mathfrak{u}_i$ (in Eq. 12) essentially are regularization terms included to limit control parameters parameter adjustments, and the β_i multipliers provide the corresponding trade-off parameters (Hansen, 1992).

4.2 Adjoint modeling

The method of Lagrange multipliers (i.e. the adjoint method) and its application to numerical models being stepped forward in time is well documented elsewhere. In particular, the interested reader is referred to Thacker and Long (1988) for a succinct presentation, with application to the case of a simple wave equation. The fitting of model sea level variability to altimetry through forcing adjustments estimated by the adjoint method (see, e.g. Forget and Ponte, 2015) (e.g., Forget and Ponte, 2015) is analogous to the simple case treated in Thacker and Long (1988). A crucial advantage of this method, as used in ECCO, is that it avoids adding source/sink terms of unknown nature to the model equations⁹. Adjoint models have many useful applications in their own right, and we shall list a few that are particularly relevant to ECCO.

Integrating adjoint models over extended periods of time allows diagnosis of the sensitivity of model dynamics to various parameters. Two examples are provided in Fig. 6 pertaining to the tracer (left panels) and momentum (right panels) equations that were computed using the "autodiff" (Fig. 5; this section), "profiles", "ctrl" and "smooth" (Fig. 5; subsequent sections) MITgcm packages. Figure 6 illustrates that the sensitivity of model-data misfits (here they cover 2008-2010) extend far back in time (here to 1992). The ability to use information contained in observations backward in time

⁹Note that this desirable property does not hold in the case of incremental (or sequential) data assimilation schemes (whether or not using an adjoint model) but this is not a case of interest here. In particular, it does not hold in 4DVar as practiced in numerical weather prediction.

is a powerful advantage of the adjoint method over sequential/filtering conventional sequential assimilation methods. Such adjoint sensitivities provide a practical means to reduce spurious model drifts and biases, through inversion of uncertain model parameters (see, e.g. Ferreira et al., 2005) (e.g., Ferreira et al., 2005). In cases that are sufficiently linear, adjoint sensitivities to, e.g., wind stress can further be convolved with forcing anomalies to reconstruct and attribute variability in the ocean circulation (see, e.g. Fukumori et al., 2015) (e.g., Fukumori et al., 2015).

Unlike the simple case treated in Thacker and Long (1988), hand-coding the adjoint of the MITgcm would be a very tedious and daunting task. Algorithmic differentiation, through a source-to-source code transformation tool, is a powerful alternative (see Griewank and Walther, 2008). Computational aspects of algorithmic differentiation applied to the MITgcm are described in Heimbach et al. (2005). Since its origin, ECCO has relied on TAMC (Tangent Linear and Adjoint Model Compiler Giering and Kaminski, 1998) and its commercial successor TAF (Transformation of Algorithms in Fortran; Giering et al., 2005). Open source tools such as OpenAD (Utke et al., 2008) and Tapenade (Hascoët and Pascual, 2013) are on their way to provide providing alternatives for massive problems such as ECCO (Heimbach et al., 2011).

During the early development stages of ECCO v4, the adjoint handling of exchanges and storage was extended (partly hand-coded) to allow for elaborate grids such as CS and LLC (Fig. 1). The balancing of storage vs. recomputation via the checkpointing method is essential to computational efficiency (Griewank, 1992; Heimbach et al., 2005). This is particularly true for ECCO v4 since the non-linear free surface (see Sect. 3) expectedly increases storage requirements.

During the early development stages of ECCO v4, the adjoint handling of exchanges and storage was extended (partly hand-coded) to allow for elaborate grids such as CS and LLC (Fig. 1). More generally, development of efficient adjoint code using TAF largely consists in accommodating non-linearities of added forward model features.

Overwhelmingly expensive recomputations of non-linear terms in the adjoint are treated by adding TAF storage directives 10. These directives take the form of fortran Fortran comments (starting with "CADJ") embedded in the forward model code, which TAF transforms into sure code for storage operations (for details, see Heimbach et al., 2005). The ECCO v4 set-up involves 1458 such comments, which were all inserted manually in carefully chosen locations. Once all of the needed storage directives are in place, then "algorithmic differentiation" becomes the "automatic differentiation" that an ECCO v4 user holding a TAF license will experience.

The non-linear free surface, the Adams-Bashforth 3 AB-3 time stepping scheme, and implicit vertical advection were thus added as adjoint capabilities as part of ECCO v4. Including the non-linear free surface, along with the real freshwater flux boundary condition, in the ocean state estimate is regarded as a major improvement in physical realism. The Adams—Bashforth 3 AB-3 and implicit vertical advection schemes have a minor impact on the forward model solution but provide additional stability also in adjoint mode.

Exactness completeness of the the and adjoint is general goal of the MITgcm adjoint development. Exactness can be of particular imporanalyses tance to carry in carrying out quantitative of adjoint (e.g., Verdy et al., 2014; Fukumori et al., 2015) (e.g., Verdy et al., 2014; Fukumori et al., 2015) For state estimation purposes, however, it is often advantageous, or simply convenient, to use an approximated adjoint (see, e.g. Jiang et al., 2002) (see, e.g., Jiang et al., 2002). The most basic approximation consists in switching off forward model features in the adjoint, which allows postponing the development of a stable adjoint.

In ECCO v4, the Gaspar et al. (1990), Nguyen et al. (2009), and Losch et al. (2010) components parameterizations are thus omitted in the adjoint. Note that the approximated adjoint does take into account, e.g., the diffusivities and viscosities computed by GGL (Gaspar et al., 1990). It is only the parametric dependency of these diffusivities and viscosities on the ocean state that is omitted. Until 2008 applications of the MITgcm adjoint were also omitting the Redi (1982) and Gent and Mcwilliams (1990) components, which pre-

¹⁰TAF adopts a "recompute-all" strategy by default; OpenAD in contrast uses "store-all" by default.

cluded optimal control of their parameters. This situation was resolved by using a simple clipping scheme for large isopycnal slopes, and by omitting only the parametric dependency of isopycnal slopes on the ocean density field in the adjoint, following a reasoning similar to that of Jiang et al. (2002). Thus, the parametric dependency of turbulent transports on \mathcal{K}_{qm} , \mathcal{K}_{σ} and \mathcal{K}_{d} is retained in the adjoint, so that they these parameters can be optimally controlled.

Beyond the removal of unstable adjoint dependencies, other alterations of the adjoint are of practical value for optimization purposes. In particular, it is common practice to increase viscosity parameters to add stability to MITgcm adjoint simulations (Hoteit et al., 2005). Despite successful adjoint simulations with particular versions of the sea ice model (Heimbach et al., 2010; Fenty and Heimbach, 2013), the seaice adjoint is omitted in ECCO v4 due to persisting issues. A pseudo-seaice adjoint is introduced instead to account at least for the most basic effect of seaice – the shielding of sea water from the atmosphere. The adjoint pseudo-component is obtained by AD of a forward pseudo-component. The forward pseudo-component merely tapers air—sea fluxes to zero according to (1-a) where a is the seaice fraction computed by the actual forward seaice model. This gross, local approximation omits the thermodynamics and dynamics of seaice, and is never used in forward mode. In the adjoint, it masks out open ocean adjoint sensitivities that do not apply where ice cover is present. A fraction of open ocean sensitivity is preserved at the ice edge, which is physically reasonable and avoids a discontinuity in adjoint fields. The pseudo-seaice adjoint approach has been extended in the context of Arctic ice—ocean state estimation (A. Nguyen, personal communication, 2014).

4.3 Observational Data constraints

Ocean state estimation involves imposing data constraints upon ocean models constraining ocean model solutions to data. Model-data comparison (i.e. computing Eq. 12) becomes an integral part of numerical modeling. In forward mode, "ecco" and "profiles" are diagnostic packages that can be used in any MITgcm run to perform model-data comparisons and to

compute Eqs. (12)–(14). In adjoint mode, they take the role of providing the adjoint model forcing (see Fig. 6).

In situ data constraints In-situ data are handled by the "profiles" package. Model-data comparison A model profile is computed at the time-step and grid point nearest to each observed profile (see Appendix D). Aside from the primary goal of carrying out state estimation, the "profiles" output permits direct and rigorous assessments of modeled and observed statistics (and how they may differ) based upon a near identical and instantaneous sampling (e.g., see Forget et al., 2011). To this end, it alleviates the need to output global fields at full temporal resolution, which becomes overwhelming at high spatial resolution.

Gridded dataconstraints¹¹ are commonly based upon monthly or daily averaged fields and handled by the "ecco" package. Many features have been added to "ecco" over the course of the ECCO v4 development. In preparation for this paper, these features were generalized so they can immediately be applied, when adequate, to any gridded observational constraints data set. As of MITgcm's checkpoint65h, the generic "ecco" capabilities are those listed in Table 4.

In general, observable quantities (m_i in Eq. 13) Model counterparts to observed variables are diagnosed from model state variables (via operator \mathcal{D} in Eq. 14). For potential temperature and salinity ("theta" and "salt" in Table 4) the corresponding model state variables (θ and S in Eqs. 4 and 5) are simply time averaged readily available, and \mathcal{D} then simply denotes the identity operator. In contrast, sea surface height ("eta" in Table 4) is diagnosed as $\eta + \eta_{\text{ips}} + \overline{\eta}_{\text{nbs}}$ where η is the model free surface (see Sect. 3.1), η_{ips} is the weight of sea ice plus snow per unit area divided by ρ_c (see Campin et al., 2008), and $\overline{\eta}_{nbs}$ is a global steric sea level correction to the Boussinesq model (see Griffies and Greatbatch, 2012). Furthermore, for comparison of sea surface height with altimetry, the time mean of $m_i - o_i$ computed at each grid point, and the time variable global mean of $m_i - o_i$, are further subtracted via post-processor \mathcal{P} in Eq. (13) (see Forget and Ponte, 2015).

¹¹By "gridded" we mean either interpolated (e.g., for monthly sea surface temperature) or simply bin averaged (e.g., for along track altimetry).

The basic steps in imposing e.g. a gridded data constraint constraining a model solution to data using the "ecco" package are:

- 1. Mapping observational data (whether along satellite tracks, gridded, or interpolated) to the model grid, which is easily done, e.g., in Matlab using gcmfaces (Appendix C).
- 2. Specifying the error covariances $(\mathsf{R}_i$ in Eq. 12) of model-data To accommodate the great ocean heteroscedasticity fits $(d_i$ in Eq. 12). (e.g. see Forget and Wunsch, 2007) (e.g., see Forget and Wunsch, 2007), spatially varying uncertainties are generally needed.
- 3. Carrying optimization until convergence to an approximate minimum of $J(\mathfrak{u})$.

It should be stressed that all three steps are required to claim that an observational constraint has effectively been imposed on a state estimatea model solution has been constrained to data, and that the specification of errors is the central scientific problem. This is also true for "profiles" although the first step is limited to a vertical interpolation to standard levels in this case. Table 6 provides the list of gridded observational constraints that, along with the in situ data constraints. The state estimate (Sect. 5) has thus been constrained to in-situ data listed in Table 5 and gridded data listed in Table 5, have been imposed on the ECCO-Production, release 1 state estimate (Sect. 5). 6.

Control parameters

Within the MITgcm, the "ctrl" package (Fig. 5) handles adjustable control parameters (u in Eq. 15). In forward mode, "ctrl" is a package that influences the ocean state evolution (Eq. 14). Activating a new control parameter only requires a few lines of codes to map it to corresponding model parameters (Eq. 15). In adjoint mode, "ctrl" takes the diagnostic role of collecting adjoint variables and evaluating derivatives of Eq. (12) (see Fig. 6). A penalty can further be added to $J(\mathfrak{u})$ by setting $\beta_i > 0$ accordingly (Eq. 12), which will act as an adjoint forcing, to constrain the magnitude of control parameter adjustments.

Most features in "ctrl" were recently generalized so they can readily be applied, when adequate, to any set of controls. The generic pre-processor Q (Eq. 15) may thus include the Weaver and Courtier (2001) spatial correlation model (Appendix E), the cyclic application of climatological mean controls and/or a rotation of (zonal, meridional) vectors to the model C grid. Control parameters used in the state estimate are reported in Table 7.

Most generally, complete and accurate error covariance estimates are lacking for control parameters. For all controls used in the state estimate (Table 7) the error correlation scale was simply specified as 3 times the grid scale using the "smooth" package (as part of Q; Appendix E). The estimation of an initial state that pre-dates Argo and of its uncertainty, given the sparsity of the ship-based ocean sampling, is a difficult problem in itself that is proposed for further, dedicated investigation (e.g., see Forget, 2010; Lyman and Johnson, 2014).

For atmospheric re-analyses fields, in the absence of formal error estimates, ad-hoc specifications of Q are based upon the spread of available atmospheric variable estimates Chaudhuri et al. (2013) (Chaudhuri et al., 2013). Here the squared sum of time mean and seasonal differences between NCEP and ERA-Interim fields was computed, then capped to a maximum, and used as an ad-hoc estimate of error variances in atmospheric controls.

For \mathcal{K}_{gm} , \mathcal{K}_{σ} and \mathcal{K}_{d} , the first guess values were 10^3 , 10^3 and 10^{-5} m² s⁻¹, respectively. The corresponding uncertainties were set to 500., 500. and 10^{-4} m² s⁻¹. The adjusted parameters were further imposed to stay within $10^2 < \mathcal{K}_{\text{gm}} < 10^4$, $10^2 < \mathcal{K}_{\sigma} < 10^4$, and $10^{-6} < \mathcal{K}_d < 5 \times 10^{-4} \, \text{m}^2 \, \text{s}^{-1}$. The \mathcal{K}_{gm} , \mathcal{K}_{σ} and \mathcal{K}_d adjustments within the state estimate are assessed more specifically in Forget et al. (2015) . In summary: the estimated \mathcal{K}_{om} , \mathcal{K}_{σ} and \mathcal{K}_{d} adjustments have a strong impact on ocean stratification and mixed layer depth; these ocean characteristics are now well observed by the Argo program; their estimated and observed maps are in close agreement. These results are evidence that regional turbulent transport parameter inversions have an observational basis in Argo data.

State estimate

The ECCO-Production ECCO v4, release 1 state estimate covers the period from 1992 to 2011 and is the baseline solution of the ECCO v4 forward model setup (Sects. 2 and 3), including the parameter adjustments derived from observational using control parameter adjustments guided by data constraints (Sect. 4). Its monthly mean output and model-data misfits are publicly available online. Several recent publications (Speer and Forget, 2013; Wunsch and Heimbach, 2013b, 2014; Buckley et al., 2014; Forget and earlier iterations (see Appendix G). The solution fits altimetry (Forget and Ponte, 2015), SST (Buckley et al., 2014) and subsurface hydrography data (Sect. 5.2) at or close to the specified noise level. Many characteristics of the solution have been analyzed in some detail and found physically plausible, which warranted its public release. The reader is further referred to the extensive documentation (the "standard analysis" provided as Supplement) An extensive documentation of model-data misfits and physical characteristics of the state estimate that is also is publicly available online (the "standard analysis"; Appendix C) and provided as Supplement to this paper.

5.1 **Select characteristics**

The characteristics in Table 2 are a small subset that is representative of the Ocean state estimation is by definition a multi-faceted nature problem, as reflected by the selection of ocean state estimationcharacteristics in Table 2. To shed light on the observational and climate problems, this section assesses the sensitivity of these characteristics, and correlations amongst characteristics, ocean state characteristics as measured within Table 3 (model settingsdiscrete model setting choices) and within Table 8 (adjusted controls). The different levels of sensitivity seen in Table 8 vs. Table 3 is addressed in Sect. 5.3, and pertains to controllability rather than observability control parameter adjustments). In particular, the correlation (or lack thereof) between columns of Tables 3 and 8 (the two tables being considered jointly in this case) indicates whether different ocean state characteristics are tied to each other. Given the limited sample size (i.e. number of lines in Tables 3 and 8)

bootstrap distributions are shown in Fig. 8 to reflect the level of uncertainty in the presented analysis of correlations.

The various observational constraints

The various squared model-data distances (the first seven characteristics) show contrasting levels of sensitivity to control parameter adjustments (Table 8) . The same is true for discrete model settings as well as to discrete model setting choices (Table 3). This behavior may reflect different contrasting levels of random errors amongst the different types of observations in the different data types. In particular, the subsurface hydrography, as constrained by iT and iS, appears as the most sensitive squared model-data distance (Tables 3) -and 8). Another noteworthy result is that global mean time series show more spread than do time averaged meridional transports (Tables 3-8 reporting normalized differences). The main exception to this behavior is for the meridional salt transport, whose time average is small in the state estimate (High correlations amongst squared model-data distances (Fig. 7).

The correlation (or lack thereof) between columns of Tables 3-8 also yields salient conclusions (Fig. 8). High correlations between observational constraints (8 bottom panels) is are suggestive of some redundancy between data sets (i.e. consistency amongst observations).

High correlations between meridional transports and observational constraints squared model-data distances (top and middle right panels) provides provide evidence that Argo and altimetry may efficiently constrain heat and freshwater transports (see also, e.g. Forget et al., 2008a, b).

(see also, e.g., Forget et al., 2008a, b). In contrast, low correlations between global mean time series and distances to observations squared model-data distances is striking (Fig. 8, top and middle left panels). Given that the time variable global mean model-data difference misfit is omitted in computing jHa, the low correlation between mH and jHa indicates that a given global mean sea level time series could be associated with many regional solutions with equal uncertainty. The low correlation between jT and mT may further reflect

that regional variations can be much larger than, and not necessarily related to, temporal changes in global mean properties.

Beyond the present study, the extent to which Argo and altimetry, amongst others, constrain temporal changes in global mean properties remains unclear.

A related concern is that global mean properties are the most sensitive to discrete choices in model numerics and physics amongst the selected characteristics (see time series show outstanding sensitivity not only to atmospheric and oceanic control parameters (Table 8) but also to discrete model setting choices (Table 3). Meridional heat and freshwater transports, in particular, appear much less sensitive than corresponding global mean time series (Fig. 7). It is tempting to attribute this behavior the outstanding sensitivity in global mean time series to the omission of atmospheric, continental, etc. hydrology modeling in ECCO v4, although this (e.g., it does not currently include any explicit constraint of the limited freshwater storage capacity of the atmosphere and continents) although this is merely a working hypothesis that remains to be proventested. Whether and how the large sensitivity of global mean properties seen behavior illustrated in Fig. 7 translates into simpler models used to quantify climate change from observations (as in, e.g. Purkey and Johnson, 2010; Llovel et al., 2014) (as in, e.g., Purkey and Johnson, 2010). as a question of direct relevance to climate change monitoring.

5.2 Improved hydrography fit

In developing and producing the ECCO v4 state estimate, a primary goal was to improve the fit to observed in situ profiles (in-situ profiles of T and S)—as compared with earlier ECCO estimates (see Forget, 2010). As already apparent in Table 3, the inclusion of parameterized physics as controls (i.e. adjustable model parameters) was instrumental in achieving that goal. The present section focuses on this defining characteristic of the baseline ECCO v4 solution.

¹²Note that mT, mS (top to bottom global means) and mH may react to any change in ocean model controls and settings, since oceanic heat and freshwater uptake is determined by bulk formulae.

The fit to in situ profiles of temperature and salinity solutions (see Forget, 2010). This fit is depicted in Fig. 9 as a function of time, for ECCO v4 and earlier MITgcm the various solutions. For ECCO v4 the squared model-data distance for in situ profiles (see Sect. 4.3) is $|T| \approx 1.5$ for potential temperature and $|S| \approx 1.5$ for salinity (on average over all depths, locations and times). Average values of 1 would be ideal if the error estimate (see Forget and Wunsch, 2007) was perfect and the state estimate was devoid of large scale errors (neither of which is true). It is suspected that jT and jS could be further reduced. Values of 1.5, however, are regarded as sufficiently low to justify analysis of the state estimate water masses (Speer and Forget, 2013) and stratification (Forget et al., 2015). Furthermore, jT and jS are already much reduced (by a factor of 2 to 10) compared with earlier ECCO estimates (Fig. 9) throughout the period from 1992 to 2011. Amongst earlier ECCO estimates, the ECCO v3 solution comes the closest to the observed hydrography with a typical distance to observations typical values of 3(Fig. 9).

The contrasts in iT and iS amongst solutions (Fig. 9) reflect large scale misfits as illustrated in Fig. 10. This is equally true for ECCO2 eddying solutions (bottom panels) and for coarser model solutions (top and middle panels). Such broad misfit patterns typically denote spurious model drifts and biases, which are common symptoms of model deficiencies (Stammer, 2005; Ferreira et al., 2005). Similarities in misfit patterns amongst ECCO2 eddying solutions (using a common model set-up, under different sets of forcing)for example , for example, suggest internal ocean model deficiencies. So do similarities in misfit patterns (aside from differences in amplitudes) amongst the four adjoint optimized solutions of comparable resolution that use different adjusted forcing fields (ECCO v2, v3, v4 and GECCO2).

The contrast in misfit amplitude between ECCO v4 and earlier solutions (Figs. 9 and 10) tends to be reduced near the sea surface (not shown), which is encouraging but not entirely surprising since surface forcing fields were already adjustable control parameters in earlier solutions. Conversely the contrast in misfit amplitude tends to increase with depth (not shown), where internal model error sources may predominate.

Within ECCO v4, jT and jS are particularly sensitive to estimated turbulent transport parameter adjustments and generally less sensitive to estimated surface forcing atmospheric control adjustments, with the exception of expectedly high salinity sensitivity to precipitation adjustments (see Table 8, first two columns). This result is in contrast with the analysis of Liu et al. (2012) who suggest that parameterized physics are only marginally important in this regard, a suggestion consistent with the relative weakness of their turbulent transport parameter adjustments (see Forget et al., 2015). A plausible explanation for this contrast lies in the fact that Liu et al. (2012) only estimate the period 1992–2001, whereas ECCO v4 covers 1992–2011. This difference has two important implications: (1) argo Argo largely increased the volume amount of in-situ constraints data, (2) slow models model drifts are more prominent in longer unconstrained solutions. One should expect larger turbulent transport parameter adjustments on both counts.

Amongst turbulent transport control parameters in ECCO v4, jT and jS are most sensitive to the \mathcal{K}_{qm} adjustments (this result is in agreement with Liu et al., 2012). A caveat should be noted though: parameterized surface and interior fluxes are all interactive so that any control vector parameter adjustment can potentially affect any surface or interior flux. Hence Table 8 should not be mistaken for a precise ranking of the importance of the various controls. It clearly shows, however, that turbulent flux transport parameter adjustments were instrumental in fitting observed hydrographic profiles in ECCO v4.

The \mathcal{K}_{qm} , \mathcal{K}_{σ} and \mathcal{K}_{d} adjustments within the state estimate are assessed more specifically in Forget et al. (2015) . In summary: the estimated \mathcal{K}_{am} , \mathcal{K}_{σ} and \mathcal{K}_{d} adjustments have a strong impact on ocean stratification; ocean stratification is now well observed by the Argo program; estimated and observed maps of stratification and mixed layer depths are in close agreement; the \mathcal{K}_{am} , \mathcal{K}_{σ} and \mathcal{K}_{d} adjustments geography is physically plausible and exhibits close connections with ocean stratification. These results are evidence that regional turbulent transport parameter inversions have an observational basis in Argo data.

Comparison of Tables 3 and 8 furthermore reveals that estimated turbulent transport parameter adjustments have a larger impact on model-data distances (see Table 8) than,

for example, choices of advection, mixed layer and momentum schemes (see Table 3). Thus the estimated parameter adjustments (while in the range of values typically used in general circulation models) exceed what may be expected to compensate for model errors unrelated to turbulent tracer transports. The estimated parameter map details, however, should be interpreted with caution, as further discussed in Forget et al. (2015).

5.3 Parametric and structural model error

In this section, the focus is on model uncertainty and controllability, which directly impacts the possibility of fitting a model to observed data. Random data errors and model representation errors are left out of the discussion, which are comparatively well studied (e.g. Forget and Wunsch, 2007; Ponte et al., 2007; Quinn and Ponte, 2008, 2010; Chaudhuri errors associated with computing environment changes (top three rows in Table 3) are generally small enough to be neglected when using the MITgcm.

The interplay of external, structural and parametric ocean model errors has never been tackled in any systematic and quantitative manner. To distinguish amongst model uncertainties associated with ECCO v4 settings, we propose the simple, practical category definitions in Table 9. Clearly the separation between these three categories leaves room for ambiguities. For example, selecting one of the available atmospheric re-analysis products to force the model may fall under "structural", while tuning bulk formulae coefficients may fall under "parametric" and adjusting re-analyzed fields may fall under "external". Nevertheless, as a starting point, the above definitions provide a useful frame of reference. A related discussion can be found in Marzocchi and Jordan (2014), although the focus here is on curve fitting (i.e. interpolation within a time period) rather than on forecasting (i.e. extrapolation forward in time). Relevant discussion discussions can also be found in Danabasoglu et al. (2014) and Balmaseda et al. (2015).

A first assessment of the rela

(Table 3). Solutions perturbed by this much are sufficiently distinct from the state estimate to prompt further optimization leading to a different state estimate. The most important result, however, may be that adjusted control parameters generally have a much larger impact (Table 8) than switching amongst numerical schemes (Table 3).

A ratio \mathcal{C} of model uncertainty controlled by continuous parameters (external or parametric) to structural model uncertainty is introduced to better illustrate this result (Fig. 11). The adjoint method allows for reduction of parametric and external errors, but it does not lend itself to reduction of structural errors that are fundamentally discontinuous. Hence, $\mathcal C$ is an index of model controllability, which can be interpreted as a signal to noise ratio of sorts, but for model simulations rather than observations. Large values of \mathcal{C} are a priori favorable to state estimation.

It is therefore encouraging that $\log_{10}(\mathcal{C}) > 0$ for all variables considered (Fig. 11), showing that controlled model uncertainty exceed exceeds the noise level set by structural model uncertainty. Certain ocean characteristics are particularly prone to structural model uncertainty, whereas others are highly controllable. On the one hand, squared model-data distances for regional sea level variability and in situ in-situ hydrography appear most controllable with $\log_{10}(\mathcal{C}) > 1.5$ (top panels). On the other hand, global mean temperature and sea surface salinity appear most prone to structural model uncertainty with $\log_{10}(\mathcal{C}) < 0.5$. The high level of structural uncertainty seen in global mean heat uptake (i.e. mT) is cause for concern in the context of climate change monitoring (see also Sect. 5.1).

Increasing model controllability is a priori favorable to state estimation. To this end, one may seek to replace discrete choices and switches with continuous parameter specifications that enable smooth state transitions¹³, or simply add adjustable parameters¹⁴. The replacement of the C-D scheme by optional targeted viscosity, and the replacement of KPP with

¹³ At this point it is assumed, for the sake of a simple preliminary discussion, that an expert consensus could be reached to exclude certain discrete numerical schemes (see Marzocchi and Jordan, 2014).

¹⁴If algorithmic differentiation is the method of choice to this end, then schemes that have fewer discrete switches are preferable over other comparable schemes.

GGL (Sect. 3.3) thus aim at increasing model controllability. For example, KPP is a very complex and non-linear parameterization that involves many discrete switches and thousands of code lines. GGL yields broadly similar results to KPP over 20 years (Table 3) and is in contrast a very simple code, so that a practical adjoint may be within reach. It is also noteworthy that activating the C-D scheme generally trumps the impact of switching between mixed layer schemes, albeit with the notable exception of global mean characteristics (see Table 3). This result highlights the potential benefits of further extending the inversion problem to viscosity parameters.

5.4 **Known issues**

State estimation should aim towards universality and completeness (see Wunsch and Heimbach, 2013a, for a review). Thus, its practice always warrants continuous improvement in many respects. In ECCO v4, without trying to be exhaustive, one can distinguish at least three types of issues.

Firstly, the ECCO-Production, release 1 state estimate would benefit from further optimization, with additional datasets, controls, and refined error covariance specifications. The addition Remaining misfits seen in the top left panel of Fig. 10, for example, may point to the need for further optimization. The adjustment of turbulent transport parameters is a step forwardhas largely reduced these misfits, but their specified covariances remain very imprecise. Parametric error in the momentum equations also deserves further attention, since it may limit model controllability. Error covariances between adjustable control parameters (e.g., atmospheric variables) are also neglected. A permanent issue is the need for additional data constraints observations to further constrain models, particularly in the abyss (Wunsch and Heimbach, 2014). Amongst available data that is not yet in ECCO v4, the growing bio-geochemistry data base is becoming a priority.

Secondly, the lack of "posterior" error estimates is regarded as the most outstanding issue with ECCO-Production ECCO v4, release 1. Producing formal error estimates, at a reasonable computational expense and with acceptable precision, for the full, evolving ocean state would be another major breakthrough. In principle, a number of methods are available to this end. In practice, however, most of them are intractable for problems of size $> 10^8$ (sizes are reported in Tables 5–7). One approach that is being pursued is the use of second derivative (Hessian) information that, under the assumption of Gaussian distribution, can be readily related to the posterior error covariance (see Kalmikov and Heimbach, 2014). Also a possibly useful estimate of uncertainty in ECCO v4 may follow from computing the spread amongst available ocean data syntheses, although it is unclear how such ensemble spreads should be interpreted (Balmaseda et al., 2015).

Thirdly, the ECCO v4 model setup could be extended and improved, with possibly important implications for the state estimeestimate. The lack of atmospheric, land, and biogeochemistry components is an obvious limitation of ECCO v4 at this stage. The surface boundary conditions and seaice model settings require further assessment. Issues such as the use of the Boussinesq approximation (in Eqs. 1–5), the omission of geothermal heating (Piecuch et al., 2015), the omission of tides, and the lack of a coastal wetting/drying mechanism are matters for further MITgcm development that are also of importance to state estimation.

Conclusion and perspectives

This paper emphasizes the synergy between ocean modeling and data analysis. The entanglement of models and observations is nothing new – Ekman (1905), Sverdrup (1947), Munk (1966) and Wunsch (1977) are just a few historical examples. The synergy of ocean modeling and data analysis is further becoming a reality as a growing community engages in ocean state estimation, which in essence is the hybridization of ocean modeling and data analysis. What is different now merely is the level of (in)completeness, complexity, and diversity of the models and observations being employed in modern oceanographic and climate science. The scope and size of the ocean state estimation problem tackled in ECCO v4 requires collaborative research and production activities. This unescapable conclusion leads to this attempt at offering ECCO v4 as a fully integrated framework for non-linear inverse modeling and global ocean state estimation. Along with the MITgcm and its adjoint capability, the ECCO v4 framework currently includes the components listed in Table 10.

Each component of the framework is being (re)designed to be modular and of general applicability, as they all are thought to provide valuable stand-alone pieces to different degrees. Standardized in-situ data sets in particular, while a by-product of carrying out ECCO v4, allow for a variety of scientific analyses in their own right. For example they are used for analyses of observed variance that is never fully represented in numerical model solutions (Forget and Wunsch, 2007; Forget, 2015), of water masses volumetric census (Forget et al., 2011; Speer and Forget, 2013), and of macro turbulence (McCaffrey et al., 2015) and mixing (Forget et al., 2015). A complementary description of the standardized in situ in-situ observations and related ECCO v4 components is provided in Appendix D, directed towards users of in-situ observations.

As another example, the gcmfaces Matlab framework (Appendix C) is suitable for the analysis of gridded earth variables (whether observational or modeled) beyond the ECCO v4 model setup and state estimate. At this stage it has already been applied to analyze MITgcm simulations on various grids, and to a variety of observational data sets observations. Interfacing gcmfaces with output from models other than MITgcm would allow for rigorous model intercomparisons without the need to introduce errors through interpolation. As a final example, any interested modeling group should be able to take advantage of the global grids.

The state estimate and the MITgcm are highly integrated with each other. Beyond the few aspects of the solution that have been investigated in some detail, the MITgcm provides numerous prognostic and diagnostic capabilities that remain to be applied to, or employed within, ECCO v4. The "ctrl", "ecco" and "profiles" packages, are just examples of the many MITgcm packages. The last two diagnose model-data misfits and statistics. In contrast, the "ctrl" package defines control parameters that act upon the forward prognostic equations. It also lends itself to development of new parameterizations. Note that the roles of these packages (diagnosing or acting on the solution) are reversed in the adjoint. Amongst forward prognostic MITgcm packages not yet used in ECCO v4, biogeochemistry and simplified

atmospheres (Dutkiewicz et al., 2005; Follows et al., 2007; Marshall et al., 2007a; Ferreira et al., 2011) are worth singling out, as they offer a great potential for extending ocean state estimation. The adjoint capabilities of MITgcm further allow for computations of sensitivity, Green functions, singular value decomposition, mechanistic attribution of variability, and optimal observation design (Marotzke et al., 1999; Köhl and Stammer, 2004; Fukumori et al., 2007, 2015; Heimbach et al., 2011; Zanna et al., 2011). Furthermore, the MITgcm provides a convenient platform for parallel computing and variational estimation that allows for, but is not limited to, ocean data synthesis and analysis (Hoteit et al., 2013; Goldberg and Heimbach, 2013). Optimal interpolation (OI) of an individual variable, for instance, can readily be carried out using Eq. (12) and its adjoint with $\mathcal{M}=I$ (i.e. the identity operator) as illustrated by Forget (2010). In between OI and full ocean state estimation, and beyond, lie many interesting stages and possibilities. For instance, stand alone bulk formulae configurations (available at mitgcm.org, with or without seaice) could readily allow for assessment and optimization of air–sea fluxes (along the lines of, e.g., Yu and Weller, 2007; Maze et al., 2009). The (re)implementation of Eq. (12) within MITgcm provides a versatile environment for such projects, and for variational estimation purposes most generally (and is complementary to, e.g. Barth et al., 2014; Wilson et al., 2014; Hoppe et al., 2014) (and is lis expected that any of the ECCO v4 components listed in Table 10 will eventually be replaced. Most immediately, the specifics of the ocean state estimation problem (grid, forcing, ocean and seaice model settings, control parameters, observational data constraints) can all be refined or substituted for improved components. Our continued commitment is to make every updated component freely and fully available online as soon as possible. All of the Fortran and Matlab components are

web interfacing – and is for now instead made available upon email request (Sect. "Code availability").

Furthermore, at At the present time, taking full advantage of the ECCO v4 framework (Table 10) requires two third party commercial tools that are neither free nor open source: Matlab and TAF. The ability to successfully generate efficient adjoint code using alternative open-source tools, such as OpenAD or Tapenade is gaining increasing priority. Despite its limitations, Matlab is one of the most portable, integrated and popular analysis framework, and it is expected to remain as such for the foreseeable future. However, a Python analysis framework similar to gcmfaces is in planning and should better handle massive output from high resolution models (R. Abernathey, personal communication, 2014).

Gridded observational products (such as hydrography climatologies, ocean state estimates, etc.) are commonly used as a practical shorthand to observations data. It should be stressed that a gridded field in itself does not provide any information about its errors. Therefore, and since direct observational constraints are unevenly distributed data coverage is uneven and restricted to a few variables, users of the state estimate state estimate users are strongly encouraged to consider the underlying observational data base. This being said, and despite the need for continued improvement, the usefulness and scientific value of the ECCO v4 solution is by now largely documented in a number of papers (Speer and Forget, 2013; Wunsch and Heimbach, 2013b, 2014; Buckley et al., 2014, 2015; Forget and Ponte, 2015; Forget, 2015; Forget et al., 2015; Liang et al., 2015; Fukumori et al., 2015; Balmaseda et al., 2015).

As compared with earlier ECCO solutions, the ECCO-Production, release 1 state estimate (i.e. the baseline ECCO v4 solution) state estimate benefits from an extensive revisit of model settings. The improved fit to in situ hydrography in situ observations (Argo profiles of T and S in particular) as compared with earlier ECCO solutions may be the defining characteristic of ECCO-ProductionECCO v4, release 1. The inclusion of turbulent transport parameters in the set of adjustable control parameters was instrumental in achieving that goal – their inversion from hydrography guided by in-situ observations is further assessed in Forget et al. (2015). Nevertheless, it should not be assumed that broad scale misfits to observations model-data misfits are completely absent (e.g., see Fig. 10). Users of the state estimate are expected to question its realism, while being provided with capabilities to assess model-data misfits for themselves. More generally, it should not be assumed that all ocean state variables are fully constrained by available observations. Integrated transports, global averages, etc. are not directly observed, and it is a priori unclear how well they can be constrained by available observations (see Forget et al., 2008a, b; Heimbach et al., 2009; Forget et al., 2015).

Looking to the future, the need for associating formal error estimates with the full, evolving ocean state remains of utmost importance. Aside from this aspect, extensions of the state estimation framework to include other climate components (atmosphere, land, cryosphere) and different variables (biology, chemistry) would be desirable (see, e.g., Blessing et al., 2014; Prinn et al., 2011) (see, e.g., Blessing et al., 2014; Prinn et al. By providing ECCO v4 as a fully integrated framework along with a useful baseline solution that any interested investigator should be able to reproduce for the foreseeable future, the authors aim to stimulate independent research along those lines. The very modest computational requirement of ECCO v4 (Appendix F) is favorable to scientific experimentation, multi-centennial simulations and extensions to biochemistry for example (see Forget and Ponte, 2015; Forget et al., 2015).

The overarching scientific problem (set aside technicalities) to data-model combination lies in the attribution of errors amongst the various elements of Eq. (12). We make no claim to having achieved the proper attribution of errors, but experience gathered in developing ECCO v4 suggests that a paradigm shift, as compared with earlier ECCO publications, is in order. Our results indeed indicate that internal parameters are of first order importance to state estimation, and to fitting the observed hydrography in particular (Table 8). Our assessment is in contrast with that of Liu et al. (2012) who suggest that the importance of internal parameters is of order 10–20% depending on the model variable of interest. Furthermore the inversion of parameters in the momentum equations, which has received comparatively little attention, emerges as a topic of importance as one gets closer to observed data, and is expected to gain further importance as resolution increases. To provide a frame of reference for future research along those lines, a first attempt at defining and gauging various categories of model uncertainty has been presented.

Alleviating structural model errors is a prerequisite to improved dynamical interpolation of observations. In this regard, the main improvement compared with previous ECCO estimates may be the extension of the gridded domain to the Arctic, the addition of the nonlinear free surface, and the switch to real freshwater flux (Sect. 3). These specific expert choices (Marzocchi and Jordan, 2014) should not be controversial. For many other model settings, the situation is not so clear but structural model errors are generally regarded as a more difficult issue than parametric model errors. Indeed, structural model errors by definition consist of fundamentally discontinuous modeling choices that cannot be optimally controlled. Thus, structural model errors fundamentally are a matter of expert choices (Marzocchi and Jordan, 2014). In contrast, sensitivity to continuous parameters can readily be probed in adjoint mode (Sect. 4.2) so that they can be estimated objectively under the constraint of fitting observations (Sect. 5.2).

Parametric and external model uncertainty (Table 8) generally appear to dominate over structural model uncertainty (Table 3) as illustrated by Fig. 11. Such a conclusion most likely depends on spatial resolution, the chosen 2020-year duration, and the necessarily limited array of model settings being considered in Tables 3 -and 8. In particular, we expect that the choice of momentum schemes would be more important in eddy-resolving models, as kinetic energy overcomes potential energy at the meso-scale. Examples of large structural uncertainty in eddy permitting models can be found in Barnier et al. (2006) and subsequent studies. Here, however, the estimated control parameter adjustments appear to determine the solution beyond the level of structural model uncertainty (Sect. Sects. 5.2 and 5.3).

Parametric model uncertainty (associated here with interior turbulent transports) and external model uncertainty (associated here with surface forcing fields) appear to be of comparable magnitude (Table 8). Depending on the characteristic of interest, one predominates over the other. Hence, the importance of including turbulent transport parameters , which are highly uncertain, in the control vector cannot be overstated. Much remains to be understood regarding these highly uncertain parameters and their inference from data

though (see Forget et al., 2015). ECCO v4 will hopefully prove a useful stepping stone in that direction and stimulate further parameter inversion experiments.

Appendix A: Grid generation method

At high-latitude, the LLC mesh is generated numerically by adapting the two dimensional conformal mapping algorithm developed by Zacharias and Ives in the 1980s (see Ives and Zacharias, 1989; Trefethen, 1989; Wilkin and Hedström, 1998) to spherical geometry. The approach is similar to that used in the SeaGRID package (Denham, 2000), except that here spherical polar coordinate geometry defines sub-domain boundaries. The numerical mesh is generated separately for the Arctic Cap and the transition sector. Each quarter of the transition sector is bounded by: the 57° N parallel (southern edge), two 90° spaced meridians (eastern and western edges), and a small-circle arc that crosses the eastern and western edges at 67° N (northern edge). The four northern edges of the transition sector bound the Arctic cap.

To numerically mesh each sub-domain it is first conformally projected onto a plane, using a polar stereographic transformation. The result is then conformally mapped to a rectangular shape by iteratively applying the so-called "hinge-point" or "power" transformation to each of the four arc segments that make up the sub-domain edges. The transformation works with points (x,y) in the complex plane x+iy and applies the mapping $\omega=(x+iy)^P$. The transformation is applied iteratively to adjacent pairs of discrete line segments that define the sub-domain edges. The transformation adjusts P at each iteration for successive line segment pairs, so that the angle between adjacent segments is adjusted to be $\frac{\pi}{2}$ at corners and π for all intermediate segments.

The result of the transformation is a rectangular shape in a new coordinate space denoted by coordinates ζ and η . The rectangular shape has two edges that are line segments of constant ζ and two edges that are lines of constant η . The points that define the line segments have corresponding mappings to the line segment points in the original (x,y)coordinate system. A set of x and y locations that describe orthogonal grid lines in the

sub-domain interior can then be generated numerically ; by solving two Laplace equations (Ryskin and Leal, 1983) of the form

$$\frac{\partial^2 X}{\partial \zeta^2} + \frac{\partial^2 X}{\partial \eta^2} = 0$$
$$\frac{\partial^2 Y}{\partial \zeta^2} + \frac{\partial^2 Y}{\partial \eta^2} = 0$$

over the (ζ,η) rectangular shape and subject to the respective boundary conditions X=xand Y = y on the respective $\zeta = \text{constant}$ and $\eta = \text{constant}$ rectangular shape edges.

Appendix B: Time stepping

The time-discretized version of Eqs. (1)-(5) and (7) calculate the updated state $(v^{n+1}, w^{n+1}, \eta^{n+1}, \theta^{n+3/2}, S^{n+3/2})$ at time $t + \Delta t$ from the current state at time t $(v^n, w^n, \eta^n, \theta^{n+1/2}, S^{n+1/2})$ following:

$$(\Phi')^{n+1/2} = \frac{g}{\rho_{\rm c}} \int_{z}^{\eta^{n}} (\rho')^{n+1/2} dz \quad \text{with:} \quad (\rho')^{n+1/2} = \rho(\theta^{n+1/2}, S^{n+1/2}, -\rho_{\rm c} gz^{*}) - \rho_{\rm c}$$
 (B1)

$$\frac{\boldsymbol{v}^{n+1} - \boldsymbol{v}^n}{\Delta t} - [\mathbf{G}_{\boldsymbol{v}}^n]^{\mathsf{AB}} + g\nabla_{z^*}\eta^{n+1} + \nabla_h\Phi'^{(n+1/2)} = \mathbf{D}_{z^*,\boldsymbol{v}}^n + \mathbf{D}_{\perp,\boldsymbol{v}}^{n+1} + \mathcal{F}_{\boldsymbol{v}}^{n+1/2}$$
(B2)

$$\frac{\eta^{n+1} - \eta^n}{\Delta t} + \nabla \cdot \int_{-H}^{\eta^n} \boldsymbol{v}^{n+1} dz = \mathcal{F}^{n+1/2}$$
 (B3)

$$\frac{1}{H} \frac{\eta^{n+1} - \eta^n}{\Delta t} + \nabla_{z^*} (s^{*n} v^{n+1}) + \frac{\partial w^{n+1}}{\partial z^*} = s^{*n} \mathcal{F}^{n+1/2}$$
(B4)

$$\frac{s^{*n+1}\theta^{n+3/2} - s^{*n}\theta^{n+1/2}}{\Delta t} - \mathcal{A}\left(\theta, \boldsymbol{u}^{n+1} + \boldsymbol{u}_{b}\right) = s^{*n}\left(\mathcal{F}_{\theta}^{n+1} + D_{\sigma,\theta}^{n+1/2} + D_{\perp,\theta}^{n+3/2}\right)$$
(B5)

$$\frac{s^{*n+1}S^{n+3/2} - s^{*n}S^{n+1/2}}{\Delta t} - \mathcal{A}\left(S, \boldsymbol{u}^{n+1} + \boldsymbol{u}_{\mathsf{b}}\right) = s^{*n}\left(\mathcal{F}_{S}^{n+1} + D_{\sigma,S}^{n+1/2} + D_{\perp,S}^{n+3/2}\right) \tag{B6}$$

where u represents the three component velocity vector (u, v, w), u_b the bolus velocity and $\mathcal{A}(\)$ denotes the advection term.

Momentum advection and the Coriolis term are evaluated at time t from ${m v}^n, w^n$ in ${m G}^n_{{m v}}=$ $-(f+\zeta)\hat{k}\times v - \nabla_{z^*}\mathsf{KE} - w \frac{\partial v}{\partial z}$ and the resulting tendency (\mathbf{G}^n_v) is extrapolated forward in time to $t + \Delta t/2$ using the Adams–Bashforth 3 (AB-3) scheme:

$$\mathbf{G}_{\boldsymbol{v}}^{n+1/2} = \left[\mathbf{G}_{\boldsymbol{v}}^{n}\right]^{\mathsf{AB}} = \left(1 + \alpha_{\mathsf{AB}} + \beta_{\mathsf{AB}}\right)\mathbf{G}_{\boldsymbol{v}}^{n} - \left(\alpha_{\mathsf{AB}} + 2\beta_{\mathsf{AB}}\right)\mathbf{G}_{\boldsymbol{v}}^{n-1} + \beta_{\mathsf{AB}}\mathbf{G}_{\boldsymbol{v}}^{n-2}$$

Here we use $(\alpha_{AB}, \beta_{AB}) = (1/2, 0.281105)$ to improve the stability (Shchepetkin and McWilliams, 2005) compared to the true 3rd third order in time Adams-Bashforth $(\alpha_{AB}, \beta_{AB}) = (1/2, 5/12)$. The precision of the scheme drops to just 2nd second order accuracy with little consequences here since most of the other terms are also 2nd second order in time (tracer time-stepping, internal-waves internal-wave dynamics). Note that the precision is still improved compared to the quasi-AB-2 used in previous ECCO configurations which become only 1rst order accurate with stabilization factor ($\epsilon_{AB} \sim 0.1$).

Simple eulerian time stepping (1st order, forward in time) is used in $\mathbf{D}_{z^*}^n$ for horizontal dissipation (harmonic and bi-harmonic viscosity) and quadratic bottom drag. Using a quasi-AB-2 scheme instead (as in previous ECCO configurations) would reduce the stability limit from 1 to 0.9 (for pure damping term, with $\epsilon_{AB} = 0.1$). AB-3 would reduce it even further to 0.55 and therefore was not considered here. For stability reasonalso Also for stability reason, a backward time stepping is used for the other dissipation term in Eq. (B2) (i.e. $\mathbf{D}_{\perp,v}^{n+1}$)that, which represents vertical viscosity effects in the interior, except for bottom friction:

$$\mathbf{D}_{\perp,\boldsymbol{v}}^{n+1} = -\partial/\partial z \left(-\nu_\perp \partial/\partial z (\boldsymbol{v}^{n+1})\right)$$

This vertical shear term is independent of the vertically integrated pressure gradient contribution $(g\nabla_{z^*}\eta^{n+1})$, so that these two operations commute. This allows to find $\mathbf{D}_{\perp,\boldsymbol{v}^{n+1}}$ even before knowing η^{n+1} by solving a tri-diagonal system in each water column.

The updated η^{n+1} is found by combining Eqs. (B2) and (B3) to form a 2-D elliptic Poisson equation for surface pressure (pressure method) which is solved iteratively using the conjugate-gradient method (Marshall et al., 1997). Solver The solver matrix and preconditioner are updated at each time-step as the water column height changes due to the non-linear free-surface (Campin et al., 2004).

The tracer Eqs. (B5) and (B6) contain several subgrid-scale (SGS) terms within D_{\perp}, D_{σ} that can use different time-stepping methods. They represent small scale vertical mixing (K_{\perp}) due to a time-invariant background diffusivity field (\mathcal{K}_d ; Sect. 3.3) and time-variable contributions from GGL (Gaspar et al., 1990), as well as isopycnal diffusion (\mathcal{K}_{σ} ; Sect. 3.3). The effect of unresolved eddies parameterized as a bolus velocity (v_b) advecting tracers (Gent and Mcwilliams, 1990) is included in $\mathcal{A}(\theta, v + v_b)$. All SGS parameters, including v_b , isopycnal slope (α_x, α_y) and vertical diffusivity and viscosity (K_\perp, ν_\perp) are computed at the beginning of the time-step from the current state.

Isopycnal diffusivity (\mathcal{K}_{σ}) is discretized as a tensor (Redi, 1982) where all the terms are treated explicitly (i.e., as a function of $\theta^{n+1/2}$ gradient) except for the pure vertical component $\frac{\partial}{\partial z}(|\alpha|^2\mathcal{K}_\sigma\frac{\partial(\theta)}{\partial z})$ where $|\alpha|=(\alpha_x^2+\alpha_y^2)^{1/2}$ denotes the magnitude of the isopycnal slope. The pure vertical component is combined with K_{\perp} and applied to the future tracer field $(\theta^{n+3/2})$ using a backward time-stepping, leading to:

$$s^{*n} \left(D_{\sigma,\theta}^{n+1/2} + D_{\perp,\theta}^{n+3/2} \right) = -\nabla_{\sigma} \left(-\mathcal{K}_{\sigma} \nabla_{\sigma} \theta^{n+1/2} \right) - \frac{\partial}{\partial z^{*}} \left(-(K_{\perp} + |\alpha|^{2} \mathcal{K}_{\sigma}) \frac{\partial \theta^{n+3/2}}{\partial z} \right)$$

Rather than to evaluate evaluating bolus advection $\mathcal{A}(\theta, u_b)$ separately from the eulerian advection, the $rac{3}{components}$ three component residual mean velocity is formed $u_{
m res}^{n+1} =$ $u_{\mathsf{b}} + u^{n+1}$ and is used to advect tracers, per:

$$\frac{s^{*n+1}\theta^{n+3/2} - s^{*n}\theta^{n+1/2}}{\Delta t} + \nabla_{z^*} \left(s^{*n}\theta^{n+m/2} \boldsymbol{v}_{\mathsf{res}}^{n+1}\right) + \frac{\partial(\theta^{n+3/2} \boldsymbol{w}_{\mathsf{res}}^{n+1})}{\partial z^*} =$$

$$s^{*n}\mathcal{F}_{\theta}^{n+1} - \nabla_{\sigma} \left(-\mathcal{K}_{\sigma} \nabla_{\sigma}\theta^{n+1/2}\right) - \frac{\partial}{\partial z^*} \left(-(K_{\perp} + |\alpha|^2 \mathcal{K}_{\sigma}) \frac{\partial \theta^{n+3/2}}{\partial z}\right)$$

$$A3$$

Horizontal advection (second term in Eq. B7) uses the 3rd third order direct space and time (DST-3) advection scheme (MITgcm Group, 2002; Adcroft et al., 2004b) with the direction splitting method (also called multi-dimensional advection) as described in Adcroft et al. (2004b). The tracer field (m=2) obtained after applying 1-D advection (in X or Y direction) on current tracer (m = 1) is used to compute the advective fluxes in the other direction (Y or X) and ensures 2nd second order accuracy in space and time. Regarding vertical advection, the backward time stepping (unconditionally stable) is applied with 3rd third order advection scheme; this involves solving a penta-diagonal system (with some additional contributions from vertical mixing to the 3 main diagonals) for each column. In particular, this choice This choice in particular alleviates adjoint stability restrictions.

Appendix C: Diagnostics

The MITgcm "diagnostics" package is generally used to generate binary output for offline analysis of the solutions. In the case of the LLC90 grid, a two-dimensional field is thus output as an array of size 90×1170 . It can easily be re-organized according to Table 11 to match the MITgcm layout of the LLC90 grid (Fig. 12). The state estimate output is made available online in a tiled netcdf format (nctiles) where each tile is a 90×90 subdivision of a face (i.e. of f1, f2, f3, f4 or f5 in Table 11) and is written to an individual netcdf file.

The need for notiles files stems from the fact that there is no simple, robust and general way to re-arrange global model output in a single two-dimensional arraymap. For LLC fields, it is only the LL sector that can readily be re-assembled as a single two-dimensional array. ATo this end a simple Matlab script is provided to this end (eccov4 lonlat.m; see Sect. "Code availability"). It is mainly intended for users of earlier non-global ECCO estimates that may want to re-use their old analysis codes. ECCO v4 users are generally advised against interpolating, which introduces errors, and often precludes accurate transport computations. Instead, mimicking the gridded earth decomposition of general circulation models is regarded as the most convenient, robust and general way to carry out offline analyses of the solutions.

This approach is readily implemented in Matlab by the *gcmfaces* toolbox. It defines a class of objects (the gcmfaces class depicted in Table 11) that is a natural extension to the common array class. Basic operators (such as "+") are readily overloaded (i.e. re-defined) for the gcmfaces class. Thus, for For example, the addition of two gcmfaces objects can simply be written in the compact and general "fld1 + fld2" form - exactly as if fld1 and fld2 were two array objects. Note that the grid-specific organization of the binary data internal organization of gcmfaces objects (e.g., Table 11) does not appear in "fld1 + fld2", which reflects so that this compact code is immediately applicable to all supported grids (Fig. 1).

Transport and budget computations are coded with the same degree of generality within gcmfaces. Hard-coding array sizes or exploiting specific grid symmetries (e.g., the zonal symmetry of the LL grid) is excluded, in order to avoid having to re-code the same diagnostics on different grids. Two basic elements are instrumental to the generality of gcmfaces codes, which are worth noting here. Firstly First, any transport is computed following a grid line path, as illustrated in Fig. 13. Three types of paths are readily treated in a general fashion: small circles of constant latitude, great circles defined by two points (as shown in Fig. 13), and the edge of a specified subdomain. Secondly Second, the familiar mechanism¹⁵ by which rows and columns of neighboring faces are appended at the edges of an array (e.g., to f1, f2, f3, f4 or f5 in Table 11) is readily implemented. This yields general codes for gradient, rotational, divergence code to compute gradients, rotationals, divergences, etc. computations that are that is immediately applicable to all supported grids (Fig. 1).

From the state estimate output made available online, users can readily re-compute the gcmfaces standard analysis. The standard analysis document serves as a general documentation of the state estimate, and allows for a direct comparison with other MITgcm simulations regardless of the grid-specifics. It proceeds in two steps:

```
diags_driver('release1/','release1/mat/',1992:2011);
diags_driver_tex('release1/mat/',{},'release1/tex/standardAnalysis');
```

¹⁵It is commonly called *exchanges* in the parallel computing terminology.

The computational loop (i.e. diags driver.m) uses model output in "release1/nctiles/" , which and results are stored to files in "release1/mat/". The display phase (i.e. diags driver tex.m) then generates "release1/tex/standardAnalysis.tex".

Diagnosing heat, and salt budgets requires snapshots the mass. of ocean + seaice + snow model state (to compute the tendency terms), as well as time averaged fluxes between snapshots (to match the tendency terms). The MITgcm flux output accounts for variations of layer thicknesses in z^* coordinate. Tendency terms are computed after the fact using snapshots of, e.g., η and θ (Sect. 3.1). The assembled mass, heat and salt budgets are provided online in the extensive form (in kg s⁻¹, J s⁻¹, g s⁻¹ respectively) and in nctiles format (monthly, three-dimensional). The budgets residuals are less than 10^{-6} times the budget magnitude (a Euclidean norm is used). Here "mass budget" simply denotes the constant Boussinesq density $ho_{\rm c}$ times volume – in contrast with the hydrostatic pressure budget that is most directly relevant to diagnosis of sea level variability (Forget and Ponte, 2015).

The full specification of the MITgcm "diagnostics" package ("data.diagnostics") are available online for ECCO v4, along with the gmfaces (Matlab) codes that assemble the budgets and compute the standard analysis. They can be readily applied to re-runs of the state estimates, or to most perturbation experiments. Re-running the state estimate after editing "data.diagnostics" is the re-commended method for users that desire output that is not readily online.

Appendix D: Profiles

The MITgcm "profiles" package subsamples the model solution, while it is being computed, at the locations and times of observed in situ profiles, in-situ profiles. It uses input files in the "MITprof" format described below. At model initialization, observed profiles dates and locations are read from MITprof files (see below) file and each profile is allocated to the processor corresponding to its sub-domain tile. The latter is generally facilitated by a preprocessing step: observed profiles are collocated with grid points using gcmfaces (see Ap-

pendix C) and grid locations added to the MITgcm input files. During model integration, profiles are sampled at time steps and locations closest to observations, vertically interpolated to the MITprof depth levels, and written to file. At the end of the forward model integration, these profiles are re-read from file along with observed and weight profiles, and the normalized squared distance between modeled and observed profiles is computed (see Sect. 4).

MITprof files contain in situ in situ profiles (prof_T and prof_S) as well as corresponding state estimate profiles (prof Testim and prof Sestim) and least square weights (prof Tweight and prof Sweight) as illustrated in Fig. 15. Weights are set according to the method of Forget and Wunsch (2007) albeit with updated variance fields. The normalized distance to observations squared model-data distance (Eq. 12; Sect. 4.3) is thus readily computed as

$$jT = (prof_Testim-prof_T)^2 \cdot prof_Tweight$$

$$jS = (prof_Sestim-prof_S)^2 \cdot prof_Sweight$$
 (D1)

from the content of any MITprof file. The intention is to eventually distribute all observed data constraints used in ECCO (e.g., altimetry and SST) in a similarly self sufficient and practical format (i.e. observations, model values data, model counterparts and weights all together).

The MITprof format contains a limited amount of ancillary information: profile locations, dates, and an identifying code (prof_descr). This choice, along with the use of standard depth levels, yields data sets that are both more compact and simpler than most data center formats (e.g., the Argo format), providing easy access to vast collections of profiles of various origins (Table 5). The identifying code may be a cruise ID (e.g., for shipboard CTDs) or an instrument ID (e.g., for Argo profiles). They are informative of the data origin, and used for analyses of transects or time series.

As part of the MITprof Matlab toolbox, the pre-processing of in situ in-situ profiles consists of four basic steps: (1) applying relevant data quality flags, if provided by data center, (2) converting in-situ to potential temperature or pressure to depth, if needed, (3) interpolating to standard depth levels 16, (4) resetting weights to 0 for standard levels that are not closest neighbors to observed levels, for S outside the 25–42 range, and when jT (resp. jS) exceeds 50 (i.e. 7 standard errors) when computed for an Argo-based atlas (Forget, 2010). Zero weights thus indicate suspicious data points that users are advised to discard.

Appendix E: Smooth

The MITgcm "smooth" package is an implementation of recipes presented in detail by Weaver and Courtier (2001). At the core of the this method, a diffusion equation is time integrated to smooth a field. Applying the smoother directly (without additional factors) to model-data misfits (as part of \mathcal{P} in Eq. 13) yields a practical method to omit scales at which observations and models data and model are not expected to be consistent with each other. This approach is useful, for example, to constrain eddying models to coarse grained climatological fields, or to constrain models with along-track altimetric data (Forget and Ponte, 2015).

When the smoother is applied to uncorrelated grid scale noise, the resulting fields have a Gaussian correlation (Fig. 14) with a e-folding scale L determined by the joint specification of integration time and diffusivity. The noise amplitude reduction by the smoother (Fig. 14, color scale) can be computed exactly or approximately (Weaver and Courtier, 2001). Normalizing the smoother to account for this effect yields a spatial correlation operator that conserves variance (in the case of uncorrelated noise). A spatial covariance operator is then immediately obtained by further multiplying the normalized smoother with a specified error field, and grid cell areas or volumes are used as a preconditioner (in twoand three-dimensional cases respectively), following Weaver and Courtier (2001).

This method is used for all control parameter covariances (see Sect. 4.4; Q in Eq. 15). Key advantages of this method are that it is matrix free, naturally handles coast lines, and

¹⁶An option also exists to interpolate to standard density levels, which was used in McCaffrey et al. (2015), although the corresponding option is lacking in MITgcm.

easily accommodates a variety of grids. In practice, "smooth" also damps grid scale noise that can arise from the adjoint model, and it thus facilitates optimization.

Appendix F: BenchmarkingRegression tests

While MITgcm evolves continuously its results are tested against benchmarks subjected to regression testing (Myers et al., 2011) on a daily basis, with a variety of compilers, on a variety of computing platforms. These tests are carried The tests not-only evaluate strict bit-wise reproducibility, but also examine the magnitude of the deviation in numerical metrics from reference calculations and compare it to acceptable limits. This allows partially automated testing in the context of numerical innovations and computer platform variations.

Automated daily regression tests are carried out using the "CVS" and "testreport" capabilities for short runs (a few time steps), on a small number of processors (or just one), and exclude optimization by compilers. This design is suited to detect mistakes in code revisions and distinguish them from false positives (associated with truncation errors) truncation errors. The ECCO v4 model setup (Sects. 2 and 3) takes full advantage of that framework, which makes it both portable and stable (Sect. "Code availability").

Advanced usage of ECCO v4 may include re-running forward model solutions (the state estimate in particular) or its adjoint. Computational requirements are modest - the 2020-year forward model integration typically takes between 6 and 12h on 96 processors. ECCO v4 users can thus easily re-run the state estimate solution to generate additional output and carry out analyses that may not already be covered by the publicly distributed material. Running the adjoint model allows for analyses of processes and mechanisms (e.g. see Fukumori et al., 2015) (e.g., Fukumori et al., 2015) as well for the possibility of further optimization of the state estimate.

While the "testreport" tool is very useful and practical, it does not directly apply to the state estimate, but rather to the underlying model code and setup. An extension to the benchmarking regression testing framework is therefore proposed that is suited for the full state estimate solution. The benchmarking tool It is implemented as a self-contained Matlab routine (testreport ecco.m). It relies upon distances to observations squared model-data distances and monthly mean model output (Table 2). It provides a simple mechanism that allows users to verify that their 20 year solution is acceptably close to the released state estimate. The first three lines of Table 3 are reflective of small differences that user should expect when re-running the state estimate using a different computer or an updated MITgcm code. Such slight changes typically result form compiler optimization of slightly different codes and slightly different arithmetic and MPI libraries.

For any given model run, squared model-data distances are simply read from a summary text file (typically named cost function0011) that MITgcm generates at the end of the model integration. Benchmark Reference values are then read from a Matlab file (typically name testreport release1.mat) and relative differences are reported as shown in Table 3. The other tests are slightly more computationally intensive as they read binary output of model fields – a subset of the fields that are distributed online as notiles files (Appendix C). It was chosen to focus on integrated quantities (global means and transports) that are known to be model sensitive (e.g., see Table 3) and of common interest to ECCO users. Computations of monthly global mean free surface height, temperature and salinity illustrate usage of grid cell surfaces and volumes. If gcmfaces is activated in Matlab (see Appendix C and Sect. "Code availability") then a benchmarking of integrated transports can also be performedtested.

Appendix G: Solution history

The ECCO-Production ECCO v4, release 1 state estimate was produced in several phases over the course of the ECCO v4 development. In total, 45 iterations were performed, and a summary of the different phases is provided below. We should stress that the documented solution history reflects the progressive development of ECCO v4 – as opposed to a systematic or advocated approach to the optimization of model solutions.

The first series of 14 adjoint iterations was carried (with the MITgcm's checkpoint62k) using a non-synchronous time step (3 h for tracers, and 20 min for momentum), sea surface salinity relaxation to climatological values, and the linear free surface method. Revision 1 was the switch to the one hour time step (for both tracers and momentum) and to the non linear free surface, followed by 14 adjoint iterations (with checkpoint62y).

In revision 2, the Duffy et al. (1999) parameterization as implemented for the MITgcm by Nguyen et al. (2009) was added, the solution was extended through 2011, and 13 more adjoint iterations were carried out (with checkpoint63g). In revision 3, the surface salinity relaxation was removed and its effect replaced by an adjustment of precipitation controls, followed by 3 adjoint iterations (with checkpoint63g). The resulting solution is used in Speer and Forget (2013); Wunsch and Heimbach (2013a, b); Buckley et al. (2014); Balmased Wunsch and Heimbach (2013a). Wunsch and Heimbach (2013b). Buckley et al. (2014); and Balmaseda et al. (2015). In revision 4, the adjustment of precipitation from revision 3 was removed, followed by 8 adjoint iterations (with checkpoint64f).

Up to this point (revision 4, iteration 8) time-variable global mean sea level had been omitted from the attimetric constraints attimetry constraint — letting the other data constraints (from in situ, primarily from in-situ hydrography, SST and regional attimetryprimarily), determine the solution variability. Then, revision 4 iteration 9 consisted in estimating a time variable global mean precipitation adjustment under the sole constraint of fitting the timevariable global mean precipitation adjustment under the sole constraint of fitting the timevariable global mean precipitation adjustment under the sole constraint of fitting the timevariable global mean attimetry. This operation had very little influence on the rest of model-data misfits — consistent with the analysis presented in Sect. 5.1. This solution is used in

of vertical viscosity to $5 \times 10^{-5} \text{m}^2 \text{s}^{-1}$ to reduce a low bias in the Equatorial Undercurrent velocity, albeit with little impact on model-data misfits.

Revision 4 iteration 11 is the ECCO-Production ECCO v4, release 1 state estimate, which originally ran with MITgcm's checkpoint64t. For benchmarking regression testing purposes (Appendix F) the 2020-year solution is re-run once a month with the up-to-date MITgcm. As of MITgcm's checkpoint65i, it matches the original solution within the precision seen in Table 3 (top three rows).

Code availability

The MITgcm is developed and maintained within Concurrent Versions System (CVS). This framework allows users to download frozen versions of the model code (checkoint65i at the time of writing) or to maintain their local copy up to date. The evolving code is benchmarked subjected to regression tests on a daily basis using the "testreport" capability (Appendix F). Documentation for the MITgcm itself, the CVS framework, and the "testreport" capability can respectively be found at:

- http://mitgcm.org/public/r2_manual/latest/online_documents/manual.pdf
- http://mitgcm.org/public/using_cvs.html
- http://mitgcm.org/public/devel HOWTO/devel HOWTO.pdf

The ECCO v4 model setup (Sects. 2 and 3) exploits the MITgcm CVS and testreport capabilities, to allow any interested user to obtain the up-to-date setup and re-run the short ECCO v4 benchmark (Appendix F). Results of the automated daily benchmarking regression tests are reported at:

http://mitgcm.org/public/testing.html

The Matlab analysis framework (gcmfaces and MITprof; see Appendices C and D) is also developed and maintained within CVS. The ECCO v4 model setup, gcmfaces, and MITprof can be found, along with their respective documentations, at:

- http://mitgcm.org/viewvc/MITgcm/MITgcm contrib/gael/verification/
- http://mitgcm.org/viewvc/MITgcm/MITgcm contrib/gael/matlab class/
- http://mitgcm.org/viewvc/MITgcm/MITgcm_contrib/gael/profilesMatlabProcessing/

The state estimate monthly output, profiles output, budget output, and the standard analysis (see Appendices C and D) can be found at

http://mit.ecco-group.org/opendap/ecco for las/version 4/release1/

that also provides ancillary data (e.g., grid files), and the stand-alone Matlab routine (eccov4 lonlat.m) that extracts the LL sector out of global LLC fields. The eccosupport@mit.edu mailing list provides for collaborative user support (analogous to mitgcmsupport@mitgcm.org).

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Table 1. Interior Select interior and boundary model parameters (as of MITgcm's checkpoint65h; see Appendix G). File names where run time model parameters are set are given in square brackets under "MITgcm parameter name". A more exhaustive list of model parameter settings is available within the model standard output (text file). For each group of parameters, the file where it is defined at run-time is indicated in square brackets in the last column. Parameters reported as 'first guess' are further adjusted as part of state estimation (see Sects. 4 and 5).

description	value	MITgcm parameter name
[momentum equation] time step harmonic vertical viscosity harmonic horizontal viscosity (see text)	$\begin{array}{c} 3600\text{s} \\ 5\times 10^{-5}\text{m}^2\text{s}^{-1} \\ 2\times 10^{-2} \end{array}$	[data] deltaTmom viscAr viscAhGrid
[tracer equations] time step first guess GM intensity first guess diapycnal diffusivity first guess isopycnal diffusivity	$3600 s$ $10^3 m^2 s^{-1}$ $10^{-5} m^2 s^{-1}$ $10^3 m^2 s^{-1}$	[data, data.gmredi] deltaTracer GM_background_K diffKrT,diffKrS GM_isopycK
[sea floor boundary] quadratic bottom drag	10 ⁻³	[data] bottomDragQuadratic
[open-ocean surface boundary] ocean albedo	0.10	[data.exf] exf_albedo
[ice-covered surface boundary] ice albedo (α_i) snow albedo (α_s) maximum ice concentration	$0.66 < lpha_{ m i} < 0.84 \ 0.70 < lpha_{ m i} < 0.90 \ 0.95$	$ \begin{array}{l} [{\rm data.seaice}] \\ \alpha_{\rm i} = {\rm SEAICE_*IceAlb*} \\ \alpha_{\rm i} = {\rm SEAICE_*SnowAlb*} \\ {\rm SEAICE_area_max} \end{array} $

Table 2. Ocean state characteristics (model-data distances defined in Sect. 4, global mean time series, and averaged meridional transports) used to benchmark 2020-year model solutions (Appendix F) and gauge their sensitivity (Tables 3 and 8, Figs. 7, 8 and 11). The first top seven rows denote list squared model-data distances defined in Sect. 4. The corresponding observational estimates data sets are listed indicated under "description" where T, S, SST, SSS, SLA, and MDT respectively stand for potential temperature, salinity, sea surface temperature, sea surface salinity, sea level anomaly, and mean dynamic topography. The last bottom six rows are list model diagnostics : θ where T, S, and $\eta + \eta_{ips}$ denotes model, and V respectively stand for potential temperature, salinity and , free surface height (including η_{ips} ; the weight of sea ice plus snow per unit area divided by ρ_c ; see Campin et al. 2008), and $\frac{V}{denotes}$ volume. The governing equations for θ Global averages and meridional transports of T, S, and ηV are provided in Sect computed over the entire water column. 3.1.

variable_name	description
jT	2008–2010 Argo T
jS	2008–2010 Argo S
jTs	1992–2011 Reynolds-SST
jSs	1992–2011 climatological-SSS
jls	1992–2011 ice-cover fraction
jHa	1992–2011 large scale SLA
jHm	1992–2011 MDT
mH	Monthly global mean $\eta + \eta_{ips}$
mT	Monthly global mean θT
mS	Monthly global mean S
tV	2008–2010 meridional V transport
tT	2008–2010 meridional θ transport
tS	2008–2010 meridional S transport

Table 3. Benchmarking Regression testing of (first top three rows; Appendix F) and sensitivity experiments conducted with (subsequent rows) the model configuration that produces the 20-year state estimate(Sect. 5) being used here as the baseline 20solution. The sensitivity experiments pertain to discrete switches in tracer advectionschemes, momentumequation settings, and boundary layers layer schemes (details are reported in Sect. 3). Ocean state characteristics that are used to gauged the sensitivity of ocean simulations are listed in Table 2. Departures in each characteristic are computed relative to the state estimate, and normalized by the standard deviation of the state estimate baseline result (for mHjT, ..., tSjHm) or the state estimate data distance its standard deviation (for iTmH, ..., iHmtS). Positive numbers denote percentages (for differences above 1%) whereas parenthesized negative numbers are powers of ten (for differences below 1%). The DST-3 and other advection schemes are discussed in the text.

jΤ	jS	jTs	jSs	jls	jHa	jHm	mΗ	mΤ	mS	tV	tΤ	tS
(-6)	(-6)	(-7)	(-6)	(-5)	(-6)	(-7)	(-5)	(-5)	(-5)	(-6)	(-6)	(-5)
(-7)	(-6)	(-6)	(-5)	(-6)	(-4)	(-4)	(-5)	(-5)	(-5)	(-6)	(-6)	(-5)
(-6)	(-8)	(-6)	(-5)	(-5)	(-4)	(-4)	(-4)	(-5)	(-5)	(-6)	(-6)	(-5)
(-3)	(-2)	(-3)	(-2)	(-3)	(-3)	(-2)	60	50	37	(-3)	(-2)	4
(-4)	(-3)	(-3)	(-3)	(-4)	(-4)	(-3)	(-2)	(-2)	(-2)	(-4)	(-3)	(-3)
3	6	1	(-2)	(-3)	(-2)	13	98	93	62	1	3	22
40	52	17	7	2	25	64	69	13	56	2	5	53
6	7	2	6	(-2)	3	6	40	28	31	(-2)	1	22
4	5	1	6	(-2)	2	3	18	11	16	(-2)	1	17
4	11	7	10	11	4	3	148	149	95	(-2)	(-2)	22
(-3)	(-3)	(-3)	(-3)	(-4)	(-3)	(-3)	(-2)	47	(-2)	(-3)	(-2)	1
	(-6) (-7) (-6) (-3) (-4) 3 40 6 4	(-6) (-6) (-7) (-6) (-6) (-8) (-3) (-2) (-4) (-3) 3 6 40 52 6 7 4 5 4 11	(-6) (-6) (-7) (-7) (-6) (-6) (-6) (-8) (-6) (-3) (-2) (-3) (-4) (-3) (-3) 3 6 1 40 52 17 6 7 2 4 5 1 4 11 7	(-6) (-6) (-7) (-6) (-7) (-6) (-6) (-5) (-6) (-8) (-6) (-5) (-3) (-2) (-3) (-2) (-4) (-3) (-3) (-3) 3 6 1 (-2) 40 52 17 7 6 7 2 6 4 5 1 6 4 11 7 10	(-6) (-6) (-7) (-6) (-5) (-7) (-6) (-6) (-8) (-6) (-5) (-5) (-6) (-6) (-8) (-6) (-5) (-5) (-5) (-6) (-7) (-7) (-7) (-7) (-7) (-7) (-7) (-7	(-6) (-6) (-7) (-6) (-5) (-6) (-7) (-6) (-6) (-5) (-6) (-4) (-6) (-8) (-6) (-5) (-5) (-4) (-3) (-2) (-3) (-2) (-3) (-3) (-4) (-3) (-3) (-3) (-4) (-4) 3 6 1 (-2) (-3) (-2) 40 52 17 7 2 25 6 7 2 6 (-2) 3 4 5 1 6 (-2) 2 4 11 7 10 11 4	(-6) (-6) (-7) (-6) (-5) (-6) (-7) (-7) (-6) (-6) (-5) (-6) (-4) (-4) (-6) (-8) (-6) (-5) (-5) (-4) (-4) (-3) (-2) (-3) (-2) (-3) (-2) (-4) (-3) (-3) (-4) (-4) (-3) 3 6 1 (-2) (-3) (-2) 13 40 52 17 7 2 25 64 6 7 2 6 (-2) 3 6 4 5 1 6 (-2) 2 3 4 11 7 10 11 4 3	(-6) (-6) (-7) (-6) (-5) (-6) (-7) (-5) (-7) (-6) (-6) (-5) (-6) (-4) (-4) (-5) (-6) (-8) (-6) (-5) (-5) (-4) (-4) (-4) (-3) (-2) (-3) (-2) (-3) (-2) 60 (-4) (-3) (-3) (-4) (-4) (-3) (-2) 3 6 1 (-2) (-3) (-2) 13 98 40 52 17 7 2 25 64 69 6 7 2 6 (-2) 3 6 40 4 5 1 6 (-2) 2 3 18	(-6) (-6) (-7) (-6) (-5) (-6) (-7) (-5) (-5) (-7) (-6) (-6) (-5) (-6) (-4) (-4) (-5) (-5) (-6) (-8) (-6) (-5) (-5) (-4) (-4) (-4) (-5) (-3) (-2) (-3) (-2) (-3) (-2) 60 50 (-4) (-3) (-3) (-4) (-4) (-3) (-2) (-2) 3 6 1 (-2) (-3) (-2) 13 98 93 40 52 17 7 2 25 64 69 13 6 7 2 6 (-2) 3 6 40 28 4 5 1 6 (-2) 2 3 18 11 4 11 7 10 11 4 3 148 149	(-6) (-6) (-7) (-6) (-5) (-6) (-7) (-5) (-5) (-5) (-7) (-6) (-6) (-5) (-6) (-4) (-4) (-5) (-5) (-5) (-6) (-8) (-6) (-5) (-5) (-4) (-4) (-4) (-5) (-5) (-3) (-2) (-3) (-2) (-3) (-2) 60 50 37 (-4) (-3) (-3) (-4) (-4) (-3) (-2) (-2) (-2) 3 6 1 (-2) (-3) (-2) 13 98 93 62 40 52 17 7 2 25 64 69 13 56 6 7 2 6 (-2) 3 6 40 28 31 4 5 1 6 (-2) 2 3 18 11 16 4 11 7 10 11 4 3 148 149 95	(-6) (-6) (-7) (-6) (-5) (-6) (-7) (-5) (-5) (-6) (-7) (-6) (-6) (-5) (-6) (-4) (-4) (-5) (-5) (-6) (-6) (-8) (-6) (-5) (-5) (-4) (-4) (-4) (-5) (-5) (-6) (-3) (-2) (-3) (-2) (-3) (-2) 60 50 37 (-3) (-4) (-3) (-3) (-4) (-4) (-3) (-2) (-2) (-2) (-4) 3 6 1 (-2) (-3) (-2) 13 98 93 62 1 40 52 17 7 2 25 64 69 13 56 2 6 7 2 6 (-2) 3 6 40 28 31 (-2) 4 11 7 10 11 4 3 148 149 95 (-2)	(-6) (-6) (-7) (-6) (-5) (-6) (-7) (-5) (-5) (-6) (-7) (-6) (-7) (-7) <td< td=""></td<>

Table 4. Generic model-data comparison capabilities provided by the "ecco" package , as of MITgcm's checkpoint65h(Sect. 4.3). The corresponding terms in Eqs. (12)–(14) $(m_i, o_i, \mathcal{D}, \mathcal{S}, \mathcal{P},$ \mathbf{W}_i) are reported here in parentheses, and defined in the text.

generic capability	MITgcm parameter	usage
variable choice (m_i, \mathcal{D})	gencost_barfile gencost_is3d	"thetamon", "saltmon", "etaday", etc. for potential temperature ("theta"), salinity ("salt"), see surface height ("eta"), etc. .TRUE. or.FALSE.
time average (m_i, \mathcal{S})	gencost_avgperiod	"month", "day", or "step" to form monthly, daily, and time step averages, respectively
input data files (o_i)	gencost_datafile	file name root (e.g., "some_sst") for files that may be yearly (e.g., "some_sst_1992" etc.) or otherwise
time average (\mathcal{P})	gencost_preproc gencost_preproc_i	"clim" to form a climatological average misifts e.g., 12 for monthly mean climatologies
spatial smoother (\mathcal{P})	gencost_posproc_c gencost_posproc_i	"smooth" to apply diffusive smoother to misifts e.g., "some_scale.bin" for the smoothing scale e.g., 10 for the diffusive smoother time stepping
weighing (\mathbf{W}_i)	gencost_errfile	squared inverse is used in squared model-data distance, except in places where a zero value is specified
masking (\mathbf{W}_i)	gencost_spzero	data points set to specified value will be omitted
diagnostics	gencost_outputlevel	> 0 to output model data misfits maps to disk

Table 5. Sets of in-situ profiles that have been imposed as constraints on In-situ data to which the state estimate (ECCO-Production, release 1) for the period from 1992 to 2011. has been constrained. XBT, CTD and ITP stand for expendable bathythermograph, Conductivity-Temperature-Depth sensors, and Ice-tethered Profiler respectively. SEaOS is data collected by Southern Ocean elephant seals. The CLIMODE field campaign focused on the North Atlantic subtropical gyre (Marshall et al., 2009). A grand total of 1911983 T profiles (resp. 1 239 247 S profiles) were used. Note however that only CTD profiles extend below 2000 m (26 285 for T, 26 220 for S).

Data Set	T profiles	S profiles	origin
Argo	833 033	800 269	IFREMER
CTD	379 012	333 266	NODC, WOA09
XBT	597 009	0	NODC, WOA09
ITP	18 033	17745	Toole et al. (2011)
SEaOS	103 117	87806	Roquet et al. (2011)
bobbers	7894	0	D. Fratantoni, CLIMODE
CTD	161	161	L. Talley, CLIMODE

Table 6. Gridded observational data sets that have been imposed as constraints on to which the state estimate (ECCO-Production, release 1) for the period from 1992 to 2011. has been constrained, T, S, SST, SLA, MDT, and ICF respectively stand for potential temperature, sea surface temperature, sea surface salinity, sea level anomaly, mean dynamic topography, and ice cover fraction.

variable	description	period	size	origin
MDT	DNSC08 mean SSH minus EGM2008 geoid model	1993–2004	6.2×10^{4}	Andersen and Knudsen (2009), Pavlis et al. (2012)
T, S	blended monthly climatology OCCA WOA 2005 PHC 3.0	2004–2006 unclear unclear	$2\times5.7\times10^{8}$	Forget (2010) Locarnini et al. (2006) updated Steele et al. (2001)
SLA	daily bin average of along-track altimetry	1992–2011	7.7×10^7	Scharroo et al. (2004)
SST	monthly maps	1992–2011	1.5×10^7	Reynolds et al. (2002)
ICF	monthly maps	1992–2010	1.4×10^7	Comiso (1999)

Table 7. Control parameters that have been adjusted as part of the state estimate (ECCO-Production, release 1) for the period from 1992 to 2011.estimation.

description	frequency	size
Initial condition for temperature Initial condition for salinity	N/A N/A	$\begin{array}{c} 2.4 \times 10^{6} \\ 2.4 \times 10^{6} \end{array}$
Diapycnal diffusivity Isopycnal diffusivity GM intensity	time mean time mean time mean	$\begin{array}{c} 2.4 \times 10^6 \\ 2.4 \times 10^6 \\ 2.4 \times 10^6 \end{array}$
Atmospheric temperature at 2 m Specific humidity at 2 m Precipitation Downward longwave radiation Downward shortwave radiation Zonal wind stress Meridional wind stress	bi-weekly bi-weekly bi-weekly bi-weekly bi-weekly bi-weekly	3.2×10^{7} 3.1×10^{7} 3.1×10^{7}

Table 8. Sensitivity of ocean state characteristics (Table 2) to various sets of control parameters. In each sensitivity experiment one subset of the control vector parameter adjustments (Table 7)is omitted. Departures are computed relative to the state estimate, and normalized by the standard deviation of the state estimate (for mH, ..., tS) or the state estimate model-data distance (for jT, ..., iHm). Positive numbers denote percentages (for differences above 1%) whereas parenthesized negative numbers are powers of ten (for differences below 1%). In each sensitivity experiment one subset of the control vector adjustments adjustment subset is reset to zero. "Parameterized oceanInternal parameters" denotes GM intensity, isopycnal and diapycnal diffusivity jointly. "Sea surface External forcing fields" denotes freshwater flux, wind stress and buoyancy flux controls jointly. "Buoyancy flux" denotes atmospheric temperature and humidity, as well as downward shortwave and longwave flux controls jointly. Departures in each characteristic are computed relative to the state estimate, and normalized by the baseline result (for jT, ..., jHm) or its standard deviation (for mH, ..., tS). Positive numbers denote percentages (for differences above 1%) whereas parenthesized negative numbers are powers of ten (for differences below 1%).

experiment	jΤ	jS	jTs	jSs	jls	jHa	jHm	mH	mΤ	mS	tV	tΤ	tS
all controls	369	1027	160	56	17	242	313	7925	99	5295	46	29	396
Internal parameters	212	317	56	15	12	72	163	329	272	233	4	15	96
External forcing fields	63	437	87	27	17	117	112	7665	252	5114	44	12	234
GM intensity	121	136	31	6	14	44	116	42	27	26	2	8	70
isopycnal mixing	44	66	6	(-2)	3	9	17	58	62	36	2	6	28
diapycnal mixing	23	44	13	4	(-2)	6	6	437	360	292	2	5	30
freshwater flux	14	182	(-3)	12	3	40	43	5140	68	3418	38	6	163
wind stress	13	22	11	(-4)	(-2)	32	26	21	28	16	2	5	24
buoyancy flux	9	30	69	5	13	9	16	2553	167	1712	5	6	50

Table 9. Model error categories as discussed in this paper.

- structural: settings that are controlled by discrete choices and switches.
- external: initial conditions, boundary conditions, and external forcing fields.
- parametric: other settings that are controlled by continuous parameters.

Table 10. List of the ECCO v4 framework components, which are fully integrated with(in) the MITgcm and its adjoint.

- the 2 km CS and LLC grids, as well as descending resolution grids
- the MITgcm estimation framework implementation charted in Fig. 5
- the model setup subjected to forward and adjoint daily regression tests
- the state estimate output, including model-data misfits
- the observational data input, including weights, to the state estimate
- the forward model input needed to re-compute the 1992–2011 solution
- the testreport ecco.m benchmarking tool to verify re-runs of the 1992-2011 solution
- the gcmfaces Matlab framework to analyze global, gridded solutions
- the MITprof Matlab framework to process and analyze in situ in situ profiles
- the solution's standard analysis produced by gcmfaces and MITprof

Table 11. Gridded earth variable (two dimensional) represented in Matlab as a gcmfaces object (a set of connected arrays) when the LLC90 grid is used. See also Fig. 12.

$fld \! = \!$		
	nFaces:	5
	f1:	$[90 \times 270 \text{ double}]$
	f2:	$[90 \times 270 \text{ double}]$
	f3:	$[90 \times 90 \text{ double}]$
	f4:	$[270 \times 90 \text{ double}]$
	f5:	$[270 \times 90 \text{ double}]$



Figure 1. Three possible approaches to gridding the Globe. Left: LL maps the earth to a single rectangular array (one face). Center: CS (six faces). Right: LLC (five faces). The faces of CS and LLC are color-coded; LL is only split four ways for rendering. Acronyms are defined in Sect. 2.

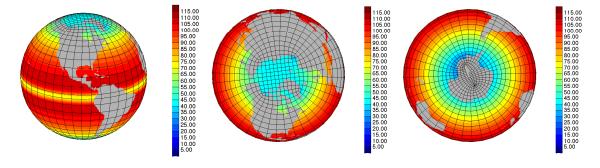


Figure 2. Average grid spacing for LLC90 (in km) computed as the square root of grid cell area. LLC90 denotes the LLC grid with 90 grid points as the common face dimension (i.e. along one quarter of earth circumference at the equator).

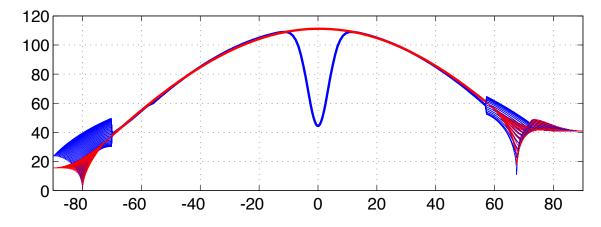


Figure 3. Grid spacing details for LLC90 as function of latitude, in km. Between 70° S and 57° N sector, blue and red curves show meridional and zonal grid spacing, respectively. Poleward of 70° S and 57° N, grid lines deviate from meridians and parallels, and LLC becomes zonally asymmetric (see Fig. 2), leading to the depicted grid spacing ranges.

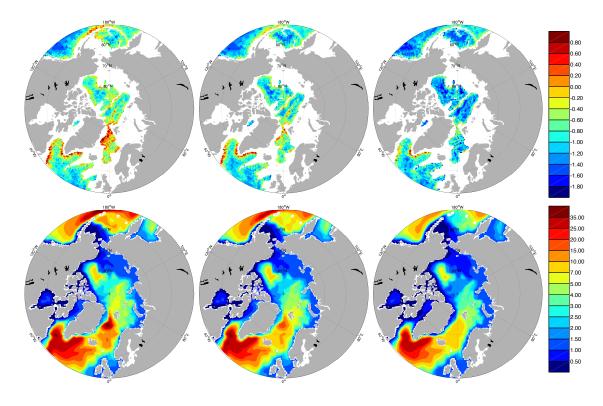


Figure 4. Root mean squared vertical velocity at 2000 m depth (top, in mm day⁻¹ log scale) and in mean horizontal streamfunction for the vertically integrated flow (bottom, in Sv) in three solutions. Left panels: ECCO-Production, release 1. baseline solution. Middle panels: same as left panels, but with increased horizontal viscosity near the ocean floor. Right panels: same as left panels, but with addition of the C-D scheme.

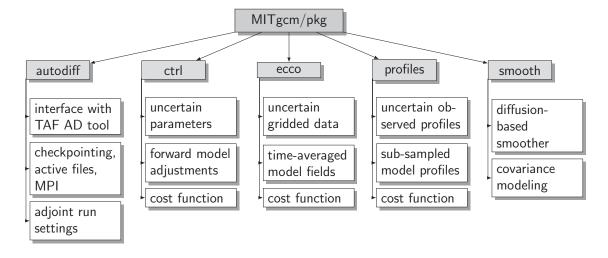


Figure 5. Organization and roles of MITgcm estimation modulespackages. A more complete presentation of MITgcm modules (or packages) can be found in the manual. The algorithmic differentiation (AD) tool being currently used is TAF. The handling of checkpoints and active files is described in Heimbach et al. (2005). The roles of ctrl, ecco, profiles and smooth in forward mode (as reported here) and in adjoint mode are further described in the text Sect. 4. In preparation for this paper, much redundancy was eliminated through generalization of "ecco" and "ctrl" features (see, e.g., Table 4). This process reduced by about 30 % the overall volume of adjointed code in ECCO v4 (counting the entire ocean-seaice model).

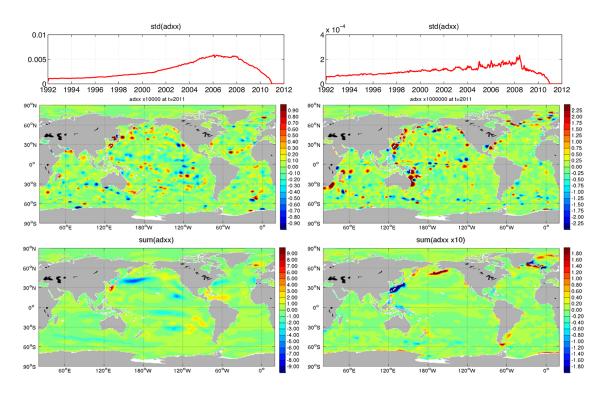


Figure 6. Non-dimensional adjoint sensitivity ($\frac{\partial J}{\partial \mathfrak{u}}$ per Eq. 12 with $\alpha_{\mathsf{i}}=1$, $\beta_{\mathsf{j}}=0$) of the Argo penalty over 2008–2010 (jT + jS) to biweekly GM intensity (left) and Laplacian horizontal viscosity (right) at 300 m. Computations are carried out with added bottom viscosity (as done in Table 3) to improve stability of the adjoint. Top panels show the standard deviation (over all ocean grid points) of biweekly adjoint sensitivities, reflecting their forcing by model-data misfits over 2008-2010 and their propagation backward to 1992 (propagation here may involve persistence, advection, waves, dissipation, etc.). Middle panels shows the first biweekly period of adjoint forcing (in late 2010) and reflects the most patchy, short term sensitivity to model parameters. The patches smoothness is mostly set by the Weaver and Courtier (2001) spatial correlation model, with a specified scale of 3 times the grid scale. Bottom panel show shows the total sensitivity to time mean model parameters, obtained by summing over all biweekly period periods. Their broad patterns primarily reflect the aggregation of adjoint sensitivities due to the 20year 20-year integration of Eqs. (1)–(5).

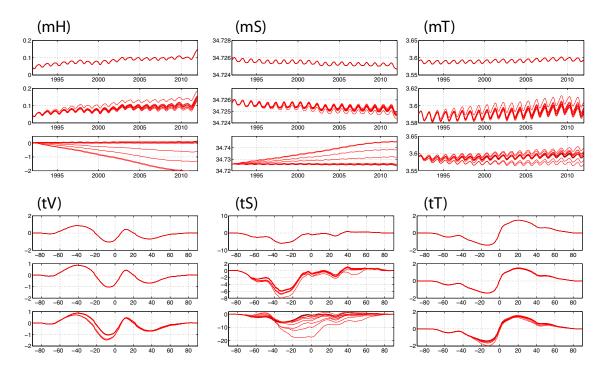


Figure 7. Depiction of Select ocean state characteristics (defined in Table Tab. 2) that reflect for the 20solution sensitivity to various model settings (experiments runs in Tables 3 and 8). The respective units are: m (mH), g kg⁻¹ (mS), °C (mT), Sv (tV), g kg⁻¹ Sv (tS) and PW (tT). For each variable characteristic, the top, middle and bottom panel respectively depict results of regression tests test results (top three rows of Table Tab. 3), structural model sensitivity (bottom eight rows of Table Tab. 3), and external and parametric model sensitivity (Table Tab. 8). The state estimate itself is shown as a thick black curve. All other model runs, which are only discussed collectively, are shown as thin red curves. Note that mH,mS, and mT are global mean time series, whereas tV, tS, and tT are 2008–2010 averages and are functions of latitude.

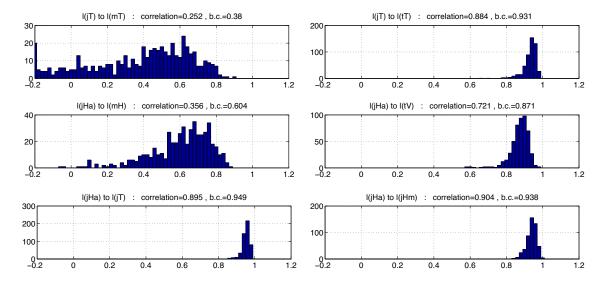


Figure 8. Bootstrap distribution of a cosensitivity an index of cosensitivity between ocean state characteristics. For two-each pair of characteristics a and b, the cosensitivity index is defined as the correlation between $\frac{\log_{10}(a)}{\log_{10}(\delta_a)}$ and $\frac{\log_{10}(b)}{\log_{10}(b)}$ and is computed for $\log_{10}(\delta_b)$ where δ indicates a perturbation. Values reported as negative integers in, e.g., Tab. set 3 are examples of 15 elements $\{\log_{10}(\delta).\ \text{Perturbations reported in the last 9 rows of } \text{Table} \text{Tab. 3 and the last 6 rows of } \text{Table} \text{Tab. 8}$ values). Here $\log_{10}(a)$ and $\log_{10}(b)$ denotes the \log_{10} are used jointly (providing sets of the distance between model solutions for characteristic a and b16 δ_a , respectively δ_b pairs). Values reported in Table 3 as negative integers are examples of $\log_{10}(a)$ and $\log_{10}(b)$. Bootstrap resampling (500 members) gives yields the displayed distributions.

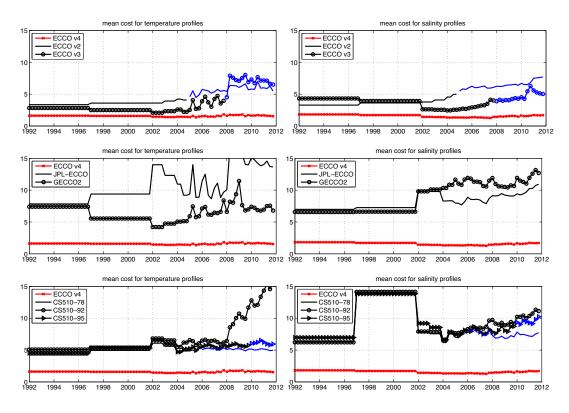


Figure 9. Distance Mean squared distance to in situ in-situ observations (Table 5; Sect. 4; Appendix D) for various MITgem solutions; for temperature (left; jT) and salinity (right; jS); as a function of year. The red line with star symbols (in In each panel) the red curve shows the baseline ECCO v4 solution (the "ECCO-Production, release 1" state estimate). Also shown in top panels: ECCO v2 (Wunsch and Heimbach, 2007, 1992–2004) and ECCO v3 (Wunsch and Heimbach, 2009, 1992–2007); middle panels: JPL-ECCO (Fukumori, 2002, 1992–Present) and GECCO2 (Köhl, 2014, 1948–2011); bottom panels: three ECCO2 eddying solutions using different forcing fields (courtesy of H. Zhang). For each solution, monthly mean output was subsampled at data locations. For solutions that do not extend through 2011, the state of the last full year was replicated afterwards (shown in blue). Temporal resolution in jT, jS is reduced in years before 2005, when the until Argo array reached near-global deployment (i.e. before 2005). The pre-2005 values, while still a useful indication of skill, may be characteristic of limited regions. The Argo period values are mostly representative of the upper 2000 m of the global ocean.

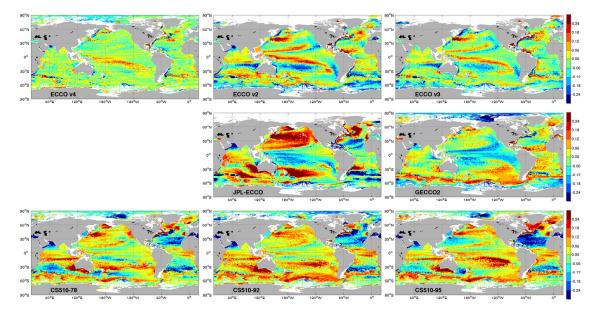


Figure 10. Model-data misfits for salinity at 300 m depth (sample average over all times) for ECCO v4 (top left panel), ECCO v2 (top center), ECCO v3 (top right), JPL-ECCO (middle center), GECCO2 (middle right) and three ECCO2 simulations (bottom panels). Additional computational details are reported in the Fig. 9 caption, along with references for the various solutions.

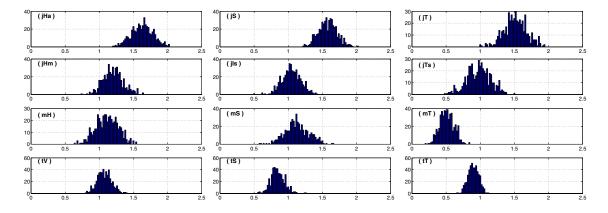


Figure 11. Bootstrap distribution for the of a controllability index (defined as \mathcal{C} hereafter) of 1992–2011 for select ocean state characteristics. For a characteristics b, the quantity $\mathcal{C} = \log_{10}(b_i/b_j)$ \mathcal{C} is computed for adefined as $\log_{10}(\delta_{b,i}/\delta_{b,i})$ where $\delta_{b,i}$ and $\delta_{b,j}$ denote perturbations in one ocean state characteristic b. Values reported as positive integers in Tables 3 and 8 are examples of $\delta_{b,i}$ and $\delta_{b,i}$, respectively. A set of 54 experiment values of $\mathcal C$ is computed from $\delta_{b,i}$, $\delta_{b,j}$ pairs formed from the last 9 rows of Table Tab. 3 values ($\frac{b_i}{1}$ providing a set of 9 $\delta_{b,i}$) values) and the last 6 rows of Table Tab 8 values (b_i providing a set of 6 $\delta_{b,j}$ values). Values reported in Table 3 as positive integers and parenthesized negative integers are examples of b_i and $\log_{10}(b_i)$, respectively. Bootstrap resampling (500 members) gives yields the displayed distributions.

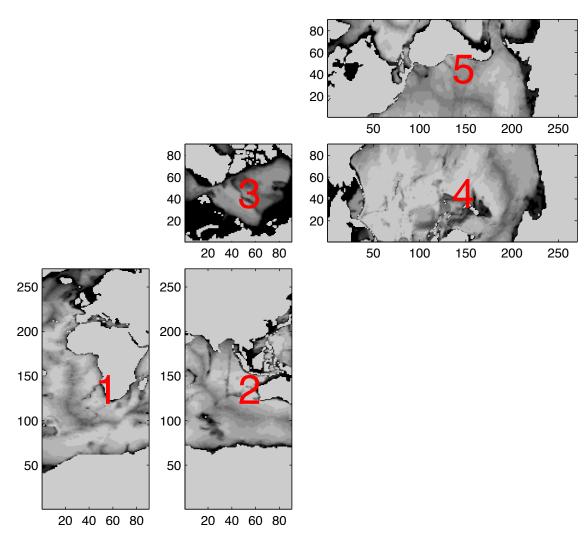


Figure 12. Example of a field (ocean bathymetry) mapped to the LLC90 grid and (Fig. 1, right panel) displayed in a way that reflects the MITgcm layout of the LLC90grid (Fig. 1, right panel). The five grid "faces" number are indicated in red, and their dimensions are shown in black. See also Table 11.

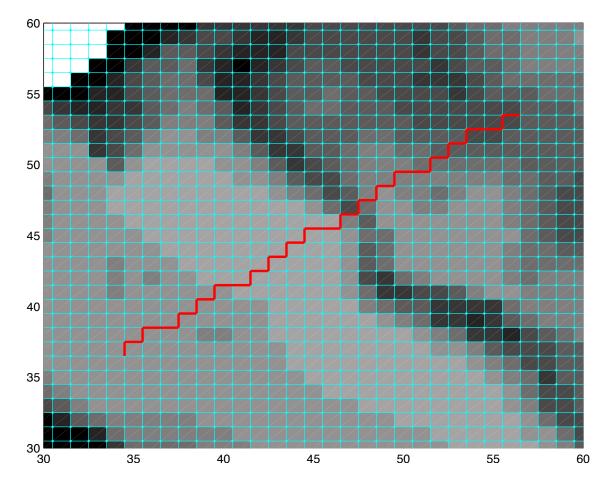


Figure 13. Example of a grid line path (in red) that approximates a great circle between 45° E, 85° N and 135° W, 85° N (a meridian crossing the north pole North Pole). Location: in the central part of face 3 from (see Fig. 12). Shading: ocean bottom depth. Blue lines: grid cell edges.

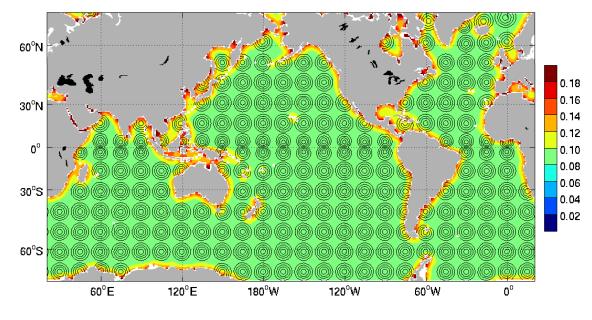


Figure 14. Diffusion applied to grid scale noise (set to unit variance) introduces correlation (contours, drawn for select points) and yields a reduced noise variance (color shading). The smoothing scale was set to three grid points.

```
netcdf argo_feb2013_2008_to_2010 {
. . .
        double prof_T(iPROF, iDEPTH) ;
               prof_T:long_name = "potential temperature" ;
                prof_T:units = "degree C" ;
        double prof_Tweight(iPROF, iDEPTH);
                prof_Tweight:long_name = "least-square weight";
                prof_Tweight:units = "(degree C)^-2";
        double prof_Testim(iPROF, iDEPTH) ;
                prof_Testim:long_name = "pot. temp. estimate";
                prof_Testim:units = "degree C";
. . .
        double prof_depth(iDEPTH) ;
        double prof_YYYYMMDD(iPROF) ;
        double prof_HHMMSS(iPROF) ;
        double prof_lon(iPROF) ;
        double prof_lat(iPROF) ;
        char prof_descr(iPROF, lTXT) ;
                prof_descr:long_name = "profile description" ;
}
```

Figure 15. Netcdf file header illustrating the MITprof format used in MITgcm/pkg/profiles.