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Verifications of the nonlinear numerical model and polarization relations of atmospheric acoustic-gravity waves

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Abstract

Comparisons of amplitudes of wave variations of atmospheric characteristics simulated using direct numerical simulation models with polarization relations given by conventional theories of linear acoustic-gravity waves (AGWs) could be helpful for testing these numerical models. In this study, we performed high-resolution numerical simulations of nonlinear AGW propagation at altitudes 0–500 km from a plane wave forcing at the Earth's surface and compared them with analytical polarization relations of linear AGW theory. After some transition time t_e (increasing with altitude) subsequent to triggering the wave source, initial wave pulse disappear and the main spectral components of the wave source dominate. The numbers of numerically simulated and analytical pairs of AGW parameters, which are equal with confidence 95 %, are largest at altitudes 30–60 km at $t > t_e$. At low and high altitudes and at $t < t_e$ numbers of equal pairs are smaller, because of influence of the lower boundary conditions, strong dissipation and AGW transience making substantial inclinations from conditions, assumed in conventional theories of linear nondissipative stationary AGWs in the free atmosphere. Reasonable agreements between simulated and analytical wave parameters satisfying the scope the limitations of the AGW theory proof adequacy of the used nonlinear numerical model. Significant differences between numerical and analytical AGW parameters reveal circumstances, when analytical theories give substantial errors and numerical simulations of wave fields are required. In addition, direct numerical AGW simulations may be useful tools for testing simplified parameterizations of wave effects in the atmosphere.

1 Introduction

Observations show frequent presence of acoustic-gravity waves (AGWs) generating at tropospheric heights and propagating to the middle and upper atmosphere (e.g., Fritts and Alexander, 2003). These AGWs can break and produce turbulence and perturba-

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substantial mean heating in the upper atmosphere. Dissipating nonlinear AGWs can also create accelerations of the mean flows in the middle atmosphere (e.g., Fritts and Alexander, 2003). However, details of the mean heating and mean flows created by non-stationary nonlinear AGWs in the atmosphere need further studies.

5 Numerical models of atmospheric AGWs require verifications. For plane stationary wave components with small amplitudes conventional linear theories (e.g., Gossard and Hooke, 1975) give the dispersion equation and polarization relations, which connect wave frequency, vertical and horizontal wave numbers and ratios of amplitudes of different wave field variations. One can expect that such relations could exist between corresponding parameters of the numerical model solutions. Therefore, theoretical polarization relations could be useful for verifications of direct simulation models of atmospheric AGWs.

15 In this paper, using the high-resolution numerical three-dimensional model by Gavrilov and Kshevetskii (2014a, b), we made comparisons of calculated ratios of amplitudes of different wave fields with polarization relations given by the conventional linear AGW theory. We considered simple AGW forcing by plane wave oscillations of vertical velocity at the surface, which is similar to the assumptions made in analytical wave theory. We found height regions of the atmosphere, where numerical results agree with analytical ones, and regions of their substantial disagreement.

20 Theoretical dispersion equation and polarization relations are widely used for developing simplified parameterizations of AGW dynamical and thermal effects in the general circulation models of the middle atmosphere. Therefore, comparisons of numerically modeled and analytical polarization relations are useful for both verifications of numerical models, and obtaining limits of analytical relation applicability and for verifications of AGW parameterizations.

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2 Numerical model

The three-dimensional numerical AGW model calculates velocity components u , v , and w along horizontal (x , y) and vertical, z , axes, respectively. The model also calculates departures of pressure p' , temperature T' , and density ρ' from background hydrostatic stationary fields p_0, T_0 and ρ_0 , respectively. Gavrilov and Kshevetskii (2014a) described the set of hydrodynamic nonlinear equations used in the model. The set includes equations of continuity, motion and heat balance. At the upper boundary $z = 500$ km, the conditions involve zero vertical gradients of perturbations of temperature, pressure, density and horizontal velocity, also zero vertical velocity. At the Earth's surface, the lower boundary conditions consist of zero perturbations of temperature, pressure, density and horizontal velocity (see Gavrilov and Kshevetskii, 2013, 2014a, b). In this study, we assume horizontal periodicity of wave solutions:

$$r(x, y, z, t) = r(x + L_x, y + L_y, z, t), \quad (1)$$

where r denotes any of the calculated variables, and $L_x = m\lambda_x$, $L_y = n\lambda_y$ are the horizontal dimensions of the considered atmospheric region, m and n are integer constants, λ_x and λ_y are wavelengths along horizontal axes x and y , respectively. Variations of vertical velocity $w_0 = w(x, y)$ at the ground $z = 0$ generate AGWs in the model.

The used numerical scheme is analogous to the two-dimensional algorithm described by Kshevetskii and Gavrilov (2005). It is a modification of the method by Lax and Wendroff (1960). This algorithm involves the conservation laws of momentum, density and energy. The main difference of our scheme from the classical Lax and Wendroff (1960) algorithm is the implicit approximating equations of hydrodynamic at first half step in time, which diminish errors of description of acoustic waves (Kshevetskii, 2001a, b, c). In the model we utilize a staggered grid, in which temperature, density and pressure are specified at the same nodes, but mesh points for the components of velocity u , v , w are displaced half grid step along axes x , y , z , respectively.

In this study, we employ vertical profiles of background T_0 , ρ_0 , and p_0 given by the model of standard atmosphere MSIS-90 (Hedin, 1991) for average geomagnetic ac-

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tivity in January. The average spacing of height grid is about 170 m, but it is varying from 12 m near the ground to about 1.2 km at altitudes about 500 km depending on inhomogeneities of vertical temperature profiles. The horizontal grids spacing is 1/60 of horizontal wavelengths taken in the wave source Eq. (2). Time spacing is automatically determined to guarantee stability of the numerical algorithm and is equal to 0.14 and 0.24 s for analyzed in this study AGWs having period $\tau = 2 \times 10^3$ s and horizontal phase speeds 30 and 100 m s^{-1} , respectively.

The numerical model involves molecular heat conductivity and viscosity increasing vs. altitude inversely proportional to the background density. We also include background turbulent heat conductivity and viscosity taking their vertical profiles with the maxima of $10 \text{ m}^2 \text{ s}^{-1}$ near the ground and at altitude of 100 km and the minimum of $\sim 0.1 \text{ m}^2 \text{ s}^{-1}$ in the stratosphere. The model does not include some effects, for example, wave dissipation caused by ion drag and radiative heat exchange, which are less important for modeling high-frequency AGWs.

3 AGW polarization relations

The comparisons considered in this paper used relations obtained from a theoretical model of monochromatic AGWs in the plain rotating atmosphere. Convention linear theories suppose that wave components v' , p' , ρ' , and T' are small deviations from stationary background values v_0, p_0, ρ_0 , and T_0 . In agreement with Hines (1960), Beer (1974), and Matsuno and Shimazaki (1981), we can look for solutions to atmospheric wave equations for AGW spectral components in the following form

$$\frac{u'}{U} = \frac{v'}{V} = \frac{w'}{W} = \frac{p'}{\rho_0 P} = \frac{\rho'}{\rho_0 R} = \frac{T'}{T_0 \Theta} = \sqrt{\frac{\rho_{0s}}{\rho_0}} e^{i(\sigma t + \varphi)}, \quad \varphi = -kx - mz, \quad (2)$$

where ρ_{0s} is the surface pressure; axis x is directed along horizontal wave phase velocity; σ , k and m are frequency, horizontal and vertical wave numbers; U , V , W ,

P , R and Θ are complex amplitudes of respective values. Assuming homogeneity of v_0 and T_0 , one can obtain (see Hines, 1960; Beer, 1974) a dispersion equation relating frequency and wave numbers, which can be written in the form of:

$$m^2 = \frac{N^2 - \omega^2}{\omega^2 - f^2} k^2 - \frac{\omega_a^2 - \omega^2}{c^2}, \quad (3)$$

5 where f is the Coriolis parameter, N is the isothermal Brunt–Väisälä frequency, c is the sound velocity, ω_a is highest frequency of acoustic waves, $\omega = \sigma - ku_0$. Beer (1974) found that Eq. (3) could be appropriate approximation for slowly varying background temperature and wind if one use the following expressions:

$$N^2 = \frac{g}{T_0} \left(\frac{\partial T_0}{\partial z} + \gamma_a \right); \omega_a^2 = \frac{c^2}{4H^2} \left(1 + 2 \frac{\partial H}{\partial z} \right), \quad (4)$$

10 where $\gamma_a = g/c_p$, g is the acceleration by gravity, H is the atmospheric scale height, c_p is the heat capacity at constant pressure. Applying technique by Beer (1974) we can get the following polarization relations

$$\begin{aligned} U &\propto \omega k c^2 (m - i\Gamma), & W &\propto \omega (\omega^2 - f^2 - k^2 c^2), \\ V &\propto i f k c^2 (m - i\Gamma), & P &\propto \gamma (\omega^2 - f^2) (m - i\Gamma), \\ R &\propto (\omega^2 - f^2) (m - i\alpha) + i k^2 c^2 N^2 / g, \\ \Theta &\propto (\gamma - 1) (\omega^2 - f^2) (m + i\alpha) - i k^2 c^2 N^2 / g, \end{aligned} \quad (5)$$

15 where $\Gamma = (2 - \gamma)/(2\gamma H)$, $\gamma = c_p/c_v$. Equation (5) does not allow calculating wave amplitudes, but gives opportunity to find their ratios. At $f = 0$ Eq. (5) are equivalent to the polarization relations obtained by Hines (1960). In nondissipative atmosphere, according to Eq. (2), AGW amplitudes should grow with altitude, so that

$$W = W_0 \sqrt{\rho_{0s} / \rho_0} \quad (6)$$

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An important AGW characteristic is the wave momentum flux, vertical component of which, F_{mz} , is as follows

$$F_{mz} = \rho_0 \langle u' w' \rangle = \rho_0 Re(UW)/2, \quad (7)$$

where sign $\langle \cdot \rangle$ denotes averaging over the wave period.

4 Comparisons of the numerical model and polarization relations

In this study, using the high-resolution nonlinear numerical model described in Sect. 2, we simulated hydrodynamic fields produced by spectral AGW components and compared ratios of their amplitudes with those predicted by the analytical polarization relations Eqs. (4) and (5). To make calculations close to assumptions of Eq. (2) of conventional AGW theory, we model nonlinear AGWs having forms of plane waves and suppose horizontally periodical distributions of vertical velocity at the Earth's surface moving along axis x of the form of

$$(w)_{z=0} = W_0 \cos[k(x - c_x t)], \quad (8)$$

where $k = 2\pi/\lambda_x$ and c_x are horizontal wavenumber and phase speed along the horizontal axis x in the direction of the wave propagation; W_0 is amplitude. Equation (8) represents plane wave of vertical velocity at the lower boundary, which may correspond to spectral components of convective and turbulent AGW sources (Townsend, 1965, 1966). Medvedev and Gavrilov (1995) studied AGW generation caused by nonlinear interactions in meteorological and turbulent atmospheric processes. They found variety of wavelengths, amplitudes and other parameters of created AGWs. In this paper, we describe simulations for wave modes having $c_x = 30 \text{ ms}^{-1}$ and $c_x = 100 \text{ ms}^{-1}$ with unchanged period $\tau = 2 \times 10^3 \text{ s}$ and amplitudes $W_0 = 0.3 \text{ cm s}^{-1}$. The modeling was performed beginning from the MSIS initial state (zero wave fields) at $t = 0$, when the wave source Eq. (8) was triggered at the lower boundary.

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c_x . These lengths grow with altitude and may be longer than ten wave periods at height of 100 km.

Table 1 represents SDs at different altitudes calculated with the numerical model and with analytical polarization relations and their ratios for AGW with $c_x = 30 \text{ ms}^{-1}$. The numerically modeled SDs at each altitude calculated periodically and averaged over n values during the initial transient interval $t < t_e$ (bottom part of Table 1) and for quasi-stationary waves $t > t_e$ (upper part of Table 1). Respective data numbers n for each altitude are presented in Table 1. Respective values obtained from analytical linear AGW theory (see Sect. 3) are calculated using average background values and are placed to the columns labeled as “Lin” at each altitude in Table 1. Consideration of Fig. 5 of the paper by Gavrilov and Kshevetskii (2014b) shows that SDs of wave fields simulated with the numerical model vary in time due to definite variations and irregular perturbations. SDs of each average numerically simulated parameter are given in Table 1.

For comparisons of numerically simulated values with analytical ones in Table 1, we use standard t test giving probability of the null hypothesis about equity of averages of two irregular quantities (Rice, 2006). Approximately, the probability of equity of two respective average values in Table 1 is larger 95 %, if difference between them is less than 1.96 multiplied by the SD of the average value (Rice, 2006). In this study, we considered only cases, when the SDs in Table 1 are smaller than 0.15 of respective average values. Pairs of AGW parameters, which we can consider equal with confidence larger than 95 %, are marked with bold font in Table 1. The numbers of those pairs are largest in the upper part of Table 1 at altitudes 30 and 60 km, which correspond to quasi-stationary AGWs in the free atmosphere considered in conventional AGW theory described in Sect. 3. Reasonable agreements between simulated and analytical wave parameters in atmospheric regions, which correspond to the scope the limitations of the nondissipative linear AGW theory, may be considered as evidences of adequate descriptions of wave processes by the used nonlinear numerical model.

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Many numerically simulated AGW parameters do not match to the respective analytical values in Table 1. No matches are in the bottom part of Table 1, which corresponds to the initial transition time interval. Gavrilov and Kshevetskii (2014b) showed that vertical structures of transient waves are different from those predicted by the linear AGW theory during the transition interval after activating the surface wave source Eq. (8). Bottom part of Table 1 shows that numerically simulated wave amplitude W is smaller than that predicted by AGW theory at high altitudes, because these values refer to small $t < t_e$, when energy of the main wave component does not yet reach considered altitude. Numerical and analytical amplitude ratios are also substantially different in the bottom part of Table 1 for $t < t_e$.

In the upper part of Table 1 for quasi-stationary AGWs at $t > t_e$, the numerically simulated AGW amplitudes W are slightly smaller than the analytical values at altitudes up to 60 km. This can be caused by small AGW dissipation at low altitudes and by partial reflections of the wave energy from inhomogeneities of background atmospheric fields in the numerical model. Wave dissipation becomes larger at altitude 100 km due to grows in kinematic viscosity and heat conductivity, therefore simulated amplitude W in the upper part of Table 1 become much smaller than that predicted by nondissipative AGW theory. In addition, one can see substantial differences in numerically simulated and analytical ratios of some AGW amplitudes, which can be due to influences of dissipative effects. At low altitudes, differences in simulated and analytical ratios of AGW amplitudes can reflect the influence of lower boundary conditions. In particular, the condition $u = 0$ at the Earth's surface makes AGW amplitudes of horizontal velocity at low altitudes smaller than that predicted by the AGW theory for free atmosphere. The upper part of Table 1 for $t > t_e$, shows that the best agreements exists between numerical and analytical values of the ratio $R/\Theta \approx 1$ at all altitudes.

Table 1 reveals numerically simulated AGW momentum fluxes F_{mz} Eq. (7) calculated as $\rho_0 u' w'$ averaged over horizontal planes at fixed altitudes and over respective time intervals. For comparisons, Table 1 gives also F_{mz} calculated using the right formula of Eq. (7) from numerically calculated amplitudes W and U . The upper part of Table 1

shows that at $t > t_e$ wave momentum flux F_{mz} is almost constant at altitudes 10–60 km due to relatively small dissipation and reflection of wave energy. At altitude of 100 km wave dissipation increases and F_{mz} decreases producing strong wave accelerations of the mean flow, which are proportional to the vertical gradient of F_{mz} . In the bottom part of Table 1 for $t < t_e$, values of F_{mz} are much smaller than respective F_{mz} values for $t > t_e$, because during initial transition interval, energy of the main AGW modes of the wave source (Eq. 8) does not yet reach high altitudes.

Table 2 is the same as Table 1, but for AGW components with $c_x = 100 \text{ ms}^{-1}$, which has longer vertical wavelength. In the upper part of Table 2 for $t > t_e$, we have smaller number of pairs equal with confidence 95 % (marked with bold font), than that in the upper part of Table 1. This may be connected with stronger influence of vertical inhomogeneities of background temperature profile on faster AGWs with longer vertical wavenumber and with larger partial reflection of faster AGW energy. Stronger reflections lead to smaller amplitudes W at altitudes below 100 km in the upper part of Table 2 compared to that in Table 1. On the other hand, W at altitude 100 km in the upper part of Table 2 is larger than that in Table 1 due to smaller dissipation of longer AGWs. Therefore, waves with longer vertical wavelengths can better penetrate to the upper atmosphere, where they can produce larger dynamical and thermal effects than those with shorter vertical wavelengths (see Gavrilov and Kshevetskii, 2014b). Similar to Table 1, we have larger amounts of equal (with 95 % confidence) numerically simulated and analytical AGW parameters at altitudes 30 and 60 km. At low and high altitudes and at $t < t_e$ (in the bottom part of Table 2) numbers of equal pairs are smaller due to influence of the lower boundary conditions, larger dissipation and AGW transience, respectively.

In atmospheric regions, where numerical and analytical AGW parameters are close, one can use analytical formulae for descriptions and estimations of the wave fields. Opposite to that, areas of substantial differences between numerical and analytical AGW parameters in Tables 1 and 2 reveal regions, where analytical theories give substantial errors and numerical simulations of wave fields are required.

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Relations of linear AGW theory are frequently used for simplified parameterizations of AGW dynamical and thermal effects for their use in the numerical models of atmospheric general circulation (e.g., Lindzen, 1981; Holton, 1983; Gavrilov, 1997; etc.). Similar parameterizations are also developing for highly dissipative AGWs in the upper atmosphere (e.g., Vadas and Fritts, 2005; Yigit et al., 2008). Sometimes, different parameterizations give different results. Direct numerical simulation models of atmospheric AGWs may be useful tools for testing and verifications of simplified parameterizations of wave effects.

5 Conclusions

In this study, we performed high-resolution numerical simulations of nonlinear AGW propagation to the middle and upper atmosphere from a plane wave forcing at the Earth's surface and compared them with analytical polarization relations of linear AGW theory. Such comparisons may be used for verifications of numerical models of atmospheric AGWs. Numerical simulations show that after triggering the wave source Eq. (8) at $t = 0$, fast acoustic and very long gravity wave modes would quickly reach very high heights. After some transition time t_e (increasing with altitude), initial AGW wave modes disappear and wave vertical structure matches to the main spectral component of the wave source Eq. (8) having horizontal wave number k and phase speed c_x . The numbers of numerically simulated and analytical pairs of AGW parameters, which are equal with confidence 95 %, are largest at altitudes 30 and 60 km at $t > t_e$. At low and high altitudes and at $t < t_e$ numbers of equal pairs are smaller, because of influence of the lower boundary conditions, larger dissipation and AGW transience, which can produce substantial inclinations from conditions, assumed in conventional theories of linear nondissipative stationary AGWs in the free atmosphere.

Reasonable agreements between numerically simulated and analytical wave parameters in atmospheric regions, which correspond to the scope the limitations of the AGW theory, may be considered as evidences of adequate descriptions of wave processes

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by the used nonlinear numerical model. Areas of substantial differences between numerical and analytical AGW parameters reveal atmospheric regions, where analytical theories give substantial errors and numerical simulation of wave fields is required. Direct numerical simulation models of atmospheric AGWs may be useful tools for testing and verifications of simplified parameterizations of wave effects.

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Verifications of the nonlinear numerical model

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Table 1. SDs and their ratios for AGW with $c_x = 30 \text{ ms}^{-1}$ calculated with the numerical model and with analytical polarization relations (labeled as Lin) at different altitudes averaged over the initial transient interval $t < t_e$ and for quasi-stationary waves $t > t_e$. Bold font shows the data pairs equal with probabilities larger than 95 %.

Altitude	0.012 km		10 km		30 km		60 km		100 km	
	$t > 0.25\tau$	Lin	$t > t_e$	Lin	$t > t_e$	Lin	$t > t_e$	Lin	$t > t_e$	Lin
n	51		28		23		16		8	
$W, 10^{-3} \text{ ms}^{-1}$	2.982 ± 0.001	3.00	4.7 ± 0.1	5.18	18.4 ± 0.5	24.4	170 ± 6	190	1730 ± 140	4470
U/W	0.78 ± 0.02	3.17	5.1 ± 0.1	4.48	7.1 ± 0.2	6.83	5.0 ± 0.1	5.04	10.3 ± 1.3	7.51
$\Theta/W, 10^{-3} \text{ sm}^{-1}$	5.1 ± 0.2	3.56	7.2 ± 0.1	6.78	15.7 ± 0.2	15.4	8.4 ± 0.1	8.56	26.2 ± 3.3	18.9
$R/W, 10^{-3} \text{ sm}^{-1}$	5.2 ± 0.3	3.55	7.2 ± 0.1	6.77	15.4 ± 0.2	15.4	8.6 ± 0.2	8.56	27.0 ± 3.4	18.8
$P/W, 10^{-3} \text{ sm}^{-1}$	1.8 ± 0.1	1.15	2.6 ± 0.2	2.10	3.5 ± 0.2	3.16	2.3 ± 0.1	2.13	4.0 ± 0.1	4.03
R/Θ	1.01 ± 0.03	1.00	1.00 ± 0.02	1.00	0.98 ± 0.01	1.00	1.03 ± 0.02	1.00	1.03 ± 0.02	1.00
R/P	3.4 ± 0.4	3.08	3.0 ± 0.2	3.23	4.7 ± 0.2	4.86	3.9 ± 0.1	4.01	7.0 ± 1.2	4.68
$R/U, 10^{-3} \text{ sm}^{-1}$	6.7 ± 0.4	1.12	1.41 ± 0.03	1.51	2.16 ± 0.03	2.22	1.71 ± 0.02	1.7	2.63 ± 0.03	2.51
$P/U, 10^{-3} \text{ sm}^{-1}$	2.4 ± 0.1	0.36	0.51 ± 0.03	0.47	0.48 ± 0.02	0.46	0.45 ± 0.02	0.42	0.42 ± 0.05	0.536
$F_{mz}, 10^{-5} \text{ kgm}^{-2} \text{ s}^{-1}$	0.29 ± 0.02	0.42	2.2 ± 0.1	2.29	2.2 ± 0.1	2.20	2.2 ± 0.2	2.17	0.8 ± 0.1	0.84
	$t < 0.25\tau$	Lin	$t < t_e$	Lin	$t < t_e$	Lin	$t < t_e$	Lin	$t < t_e$	Lin
n	7		16		20		26		32	
$W, 10^{-3} \text{ ms}^{-1}$	2.983 ± 0.001	3.00	1.3 ± 0.2	5.18	2.9 ± 0.4	24.4	24 ± 4	190	512 ± 60	4470
U/W	0.60 ± 0.07	3.17	4.1 ± 0.5	4.48	4.3 ± 0.7	6.83	2.9 ± 0.4	5.04	3.8 ± 0.5	7.51
$\Theta/W, 10^{-3} \text{ sm}^{-1}$	3.0 ± 0.7	3.56	5.5 ± 0.8	6.78	7.8 ± 1.3	15.4	4.1 ± 0.7	8.56	9.1 ± 1.5	18.9
$R/W, 10^{-3} \text{ sm}^{-1}$	3.9 ± 0.7	3.55	6.6 ± 0.8	6.77	10.3 ± 1.6	15.4	6.8 ± 1.2	8.56	11.4 ± 1.9	18.8
$P/W, 10^{-3} \text{ sm}^{-1}$	1.8 ± 0.3	1.15	7.1 ± 1.0	2.1	8.9 ± 1.7	3.16	6.6 ± 1.5	2.13	8.3 ± 1.9	4.03
R/Θ	3.1 ± 2.0	1.00	2.0 ± 0.5	1.00	1.97 ± 0.5	1.00	4.4 ± 2.0	1.00	3.5 ± 1.3	1.00
R/P	2.5 ± 0.5	3.08	1.1 ± 0.1	3.23	2.1 ± 0.6	4.86	1.7 ± 0.2	4.01	2.0 ± 0.3	4.68
$R/U, 10^{-3} \text{ sm}^{-1}$	6.6 ± 1.0	1.12	1.9 ± 0.3	1.51	3.6 ± 0.7	2.22	7.1 ± 3.9	1.7	10.1 ± 5.1	2.51
$P/U, 10^{-3} \text{ sm}^{-1}$	3.1 ± 0.4	0.36	2.0 ± 0.3	0.47	3.6 ± 0.9	0.46	9.0 ± 5.4	0.42	12.6 ± 7.0	0.536
$F_{mz}, 10^{-5} \text{ kgm}^{-2} \text{ s}^{-1}$	0.07 ± 0.04	0.32	0.12 ± 0.03	0.14	0.03 ± 0.01	0.03	0.05 ± 0.02	0.03	0.04 ± 0.01	0.03

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Table 2. Same as Table 1, but for AGW with $c_x = 100 \text{ ms}^{-1}$.

Altitude	0.012 km		10 km		30 km		60 km		100 km	
	$t > 0.25\tau$	Lin	$t > t_e$	Lin	$t > t_e$	Lin	$t > t_e$	Lin	$t > t_e$	Lin
n	51		28		23		16		8	
$W, 10^{-3} \text{ ms}^{-1}$	2.982 ± 0.001	3.00	3.7 ± 0.3	5.18	18.2 ± 1.7	24.4	161 ± 14	190	3000 ± 120	4470
U/W	0.79 ± 0.05	2.96	6.4 ± 0.5	4.42	5.8 ± 0.4	7.22	3.9 ± 0.3	5.25	7.1 ± 0.3	12
$\Theta/W, 10^{-3} \text{ sm}^{-1}$	6.4 ± 0.3	3.34	8.4 ± 0.5	6.69	13.6 ± 0.7	16.3	8.5 ± 0.4	8.78	19.0 ± 0.3	30
$R/W, 10^{-3} \text{ sm}^{-1}$	5.9 ± 0.4	3.24	9.4 ± 0.9	6.6	12.4 ± 0.9	16.2	7.9 ± 0.4	8.77	15.0 ± 0.8	30
$P/W, 10^{-3} \text{ sm}^{-1}$	7.0 ± 0.5	3.59	13.1 ± 1.4	6.89	8.5 ± 0.5	11.1	6.5 ± 0.9	7.4	11.9 ± 0.4	13.8
R/Θ	1.1 ± 0.1	0.97	1.2 ± 0.1	0.99	0.91 ± 0.04	1.00	0.93 ± 0.04	1.00	0.78 ± 0.04	1.00
R/P	1.2 ± 0.2	0.9	0.94 ± 0.1	0.96	1.6 ± 0.2	1.46	1.5 ± 0.1	1.19	1.3 ± 0.1	2.17
$R/U, 10^{-3} \text{ sm}^{-1}$	11.1 ± 2.6	1.09	1.6 ± 0.1	1.49	2.2 ± 0.1	2.25	2.2 ± 0.1	1.67	2.2 ± 0.1	2.5
$P/U, 10^{-3} \text{ sm}^{-1}$	10.4 ± 1.4	1.21	2.0 ± 0.1	1.56	1.6 ± 0.1	1.54	1.6 ± 0.2	1.41	1.7 ± 0.1	1.15
$F_{mz}, 10^{-5} \text{ kgm}^{-2} \text{ s}^{-1}$	0.01 ± 0.04	0.43	1.03 ± 0.05	1.78	1.03 ± 0.1	1.76	0.90 ± 0.09	1.52	0.79 ± 0.09	1.74
	$t < 0.25\tau$	Lin	$t < t_e$	Lin	$t < t_e$	Lin	$t < t_e$	Lin	$t < t_e$	Lin
n	7		16		20		26		32	
$W, 10^{-3} \text{ ms}^{-1}$	2.983 ± 0.001	3.00	2.3 ± 0.4	5.18	5.9 ± 0.7	24.4	112 ± 4	190	600 ± 110	4470
U/W	1.0 ± 0.1	2.96	7.0 ± 1.5	4.42	5.8 ± 0.7	7.22	4.5 ± 1.0	5.25	4.1 ± 1.1	12
$\Theta/W, 10^{-3} \text{ sm}^{-1}$	3.6 ± 1.1	3.34	5.9 ± 1.8	6.69	9.5 ± 1.3	16.3	7.3 ± 1.0	8.78	8.8 ± 1.7	30
$R/W, 10^{-3} \text{ sm}^{-1}$	8.6 ± 0.6	3.24	17.9 ± 2.4	6.6	17.5 ± 1.5	16.2	9.8 ± 1.7	8.77	15.5 ± 3	30
$P/W, 10^{-3} \text{ sm}^{-1}$	10.5 ± 0.8	3.59	21.2 ± 2.9	6.89	16.7 ± 1.7	11.1	10.1 ± 2	7.4	14.3 ± 2.8	13.8
R/Θ	4.5 ± 1.4	0.97	6.2 ± 2.1	0.99	3.3 ± 0.9	1.00	2.2 ± 0.8	1.00	2.8 ± 0.7	1.00
R/P	0.84 ± 0.05	0.9	0.86 ± 0.06	0.96	1.2 ± 0.1	1.46	1.3 ± 0.1	1.19	1.2 ± 0.2	2.17
$R/U, 10^{-3} \text{ sm}^{-1}$	9.6 ± 1.7	1.09	4.6 ± 1.8	1.49	4.3 ± 0.8	2.25	9.4 ± 14	1.67	39 ± 22	2.5
$P/U, 10^{-3} \text{ sm}^{-1}$	11.8 ± 2.1	1.21	5.5 ± 2.1	1.56	4.4 ± 0.9	1.54	11.8 ± 19	1.41	45 ± 29	1.15
$F_{mz}, 10^{-5} \text{ kgm}^{-2} \text{ s}^{-1}$	0.12 ± 0.06	0.54	0.44 ± 0.11	0.75	0.31 ± 0.09	0.15	0.59 ± 0.01	0.85	0.06 ± 0.03	0.04

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