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### Supplement of

# V2Karst V1.1: a parsimonious large-scale integrated vegetation—recharge model to simulate the impact of climate and land cover change in karst regions

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## S1. Challenges for modelling ET and representing land cover properties explicitly at large-scales

Representing explicitly land cover properties for ET estimation requires the specification of vegetation properties, such as leaf area index, vegetation height, stomatal resistance, canopy interception storage capacity, and the availability of time series of climate variables such as air temperature, net radiation, humidity and wind speed. Modelling ET at large-scales faces a range of challenges: (1) a lack of ET observations to compare with model simulations, (2) a lack of observations of vegetation properties, and (3) uncertainty in large-scale forcing weather variables.

Firstly, on the ground, measurements of actual ET (e.g. FLUXNET network, Baldocchi et al., 2001) are limited in number and are only representative of plot scale ET. Their footprint can extend to a few hundred metres or possibly to a few kilometres (Baldocchi and Ryu, 2011), which is much smaller than the extent of typical large-scale model simulation units that are mostly between 9 km (5' grid) and 111 km (1° grid) (Bierkens, 2015). Moreover, ground measurements of the partitioning of ET among its main components (transpiration, evaporation from interception and soil evaporation) are lacking as reported in Miralles et al. (2016) and in Fatichi and Pappas (2017) or are affected by large uncertainty (see e.g. Van Dijk et al., 2015 regarding evaporation from canopy interception), and the ET partitioning assessed using isotope techniques has large uncertainties and limited spatial coverage (Coenders-Gerrits et al., 2014; Sutanto et al., 2014). Additionally, global gridded ET products are available. Yet, these products do not provide direct observations of actual ET, but they are estimates of actual ET assessed using models that assimilate remote-sensed variables and either solve the energy balance or use potential ET (PET) equations as discussed e.g. in MacCabe (2016) and in Miralles et al. (2016). Jung et al. (2011) created a global gridded ET products based on model tree ensembles, which are trained using observations from the FLUXNET network.

A second issue is that observations of large-scale vegetation properties are limited. Large-scale gridded land cover databases provide spatially distributed information about the type of vegetation present around the world. We refer to Smith (2016) for a review of land cover databases. Large-scale gridded measurements of vegetation characteristics are obtained using remote-sensing techniques. Remote sensing techniques permit to retrieve vegetation leaf area index (LAI) (e.g. Fang et al., 2013) and other vegetation indices that can be only used as proxy for actual vegetation properties such as density or state of health, e.g. Vegetation Optical Depth (VOD), Normalized Difference Vegetation Index (NDVI) or Enhanced Vegetation Index (EVI) (see a review in Xue and Su, 2017). Moreover, such products suffer from a number of uncertainties, among which cloud contamination as reported e.g. in Fang et al. (2013) regarding LAI, and do not allow to assess critical vegetation properties such as rooting depth, stomatal resistance or canopy interception capacity. Ground measurements of vegetation properties are sparse and only few studies report collected values for specific variables or regions, these include Breuer et al. (2003) for a range of vegetation properties in temperate climates, Körner (1995) for stomatal resistance and Schenk and Jackson (2002) for rooting depth. Since ground measurements are limited,

they do not allow to capture the variability in vegetation characteristics, as discussed in Wang-Erlandsson et al. (2016) regarding rooting depth measurements. In particular, stomatal resistance presents a high temporal variability because it is determined by weather conditions and therefore its measurements are particularly difficult to interpret (Breuer et al., 2003) and to use in modelling applications.

Thirdly, large-scale databases of historical weather data used to force model simulations are affected by large uncertainties because they have to rely on measurements with incomplete spatial coverage, in particular wind speed measurements (New et al., 2002). Moreover, the height from the ground at which these weather data are provided is uncertain. Measurements are assumed to be provided at standard heights, typically 10 m for wind speed and 2 m for temperature and humidity (see e.g. Rodell et al., 2004; Weedon et al., 2010), which may not be representative of the specific location.

#### S2. Parameters used for ET estimation in large-scale models

We reviewed the different approaches currently used to represent land cover properties explicitly in large-scale models, to assess their consistency with our three criteria for model development (Sect. 2.1) and to determine whether we could directly adopt some of these ET representations in the new version of the VarKarst model. In this section, we provide a detailed list of all parameters involved in the representation of ET in the large-scale hydrological models we reviewed. These models are further described in Tables A1-A3.

Parameter	Description	Module a	Category	Unit	Reference
$Z_r$	Rooting depth	Stress	Vegetation	[m]	(Vörösmarty et al., 1989)
AWC	Soil available water capacity	Stress	Soil	$[m^3 m^{-3}]$	(Vörösmarty et al., 1989)
α	Empirical coefficient of the drying curve (set to 5)	Stress	Constant	[-]	(Vörösmarty et al., 1998)

**Table S1**. Parameters used for ET estimation in the WBM model. The model includes a minimum of 3 parameters (reported in the table), and additional parameters depending on the PET formulation which is used (namely the Thornthwaite equation (Thornthwaite, 1948) in (Vörösmarty et al., 1996), the Shuttleworth-Wallace (Shuttleworth and Wallace, 1985) equation in (Federer et al., 2003), and a range of different PET equations in (Vörösmarty et al., 1998)).

<sup>&</sup>lt;sup>a</sup> Stress: Stress model for actual ET calculation

Parameter	Description	Module a	Category	Unit	Reference
$eta_{28}$	Aspect correction factor of PET	PET	Terrain	[-]	(Kumar et al., 2013; Samaniego et al., 2010)
$eta_1$	Effective maximum capacity storage	Interception/ Seasonality	Vegetation	[mm]	(Kumar et al., 2013; Samaniego et al., 2010)
$Exp_{can}$	Exponent to assess the wet canopy fraction (set to 2/3)	Interception	Constant	[-]	(Samaniego et al., 2010)
$eta_{15}$	Permanent wilting point	Stress	Vegetation and soil	[-]	(Samaniego et al., 2010)
$eta_{16}$	Soil moisture limit above which the actual transpiration is equal to PET	Stress Vegetation and soil		[-]	(Samaniego et al., 2010)
$eta_{17}^1$	Fraction of roots in soil layer 1	Stress	Vegetation		(Rakovec et al., 2016; Samaniego et al., 2010)
$eta_{17}^2$	Fraction of roots in soil layer 2	Stress	Vegetation		(Rakovec et al., 2016; Samaniego et al., 2010)
$d_1$	depth soil layer 1 (set to 0.05 m)	Soil layers	Constant	[m]	(Rakovec et al., 2016)
$d_2$	depth soil layer 2 (set to 0.25 m)	Soil layers	Constant	[m]	(Rakovec et al., 2016)
$d_3$	depth soil layer 3 (set to 1 m)	Soil layers	Constant	[m]	(Rakovec et al., 2016)

Table S2. Parameters used for ET estimation in the mHM model.

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<sup>&</sup>lt;sup>a</sup> PET: potential evapotranspiration equation; Stress: Stress model for actual ET calculation from PET.

Parameter	Description	Module a	Category	Unit	Reference
$\alpha_{PT}$	Priestley-Taylor empirical coefficient (1.26 in semiarid and arid areas and 1.74 in humid areas)	PET	Climate	[-]	(Döll et al., 2003)
$E_{pot,max}$	Maximum potential evapotranspiration (20 mmd <sup>-1</sup> in semiarid and arid areas and 10 mmd <sup>-1</sup> in humid areas)	Stress	Climate	[mm d <sup>-1</sup> ]	(Müller Schmied et al., 2014)
$Z_r$	Rooting depth	Stress	Vegetation	[m]	(Müller Schmied et al., 2014)
AWC	Soil available water capacity	Stress	Soil	$[m^3 m^{-3}]$	(Döll et al., 2003)
$V_{can}$	Interception storage capacity per unit of <i>LAI</i> (set to 0.3 mm LAI)	Interception	Constant	[mm LAI]	(Döll et al., 2003)
$Exp_{can}$	Exponent to assess the wet canopy fraction (set to 2/3)	Interception	Constant	[-]	(Deardorff, 1978; Döll et al., 2003)
$LAI_{max}$	Maximum leaf area index	Interception	Vegetation	$[m^2 m^{-2}]$	(Müller Schmied et al., 2014)
$f_{d,lc}$	Fraction of deciduous plants in LAI growth model	Seasonality	Vegetation	[-]	(Müller Schmied et al., 2014)
$C_{e,lc}$	Reduction factor for evergreen plants in LAI growth model	Seasonality	Vegetation	[-]	(Müller Schmied et al., 2014)
$t_{min}$	Initial days to start/end with growing season in LAI growth model	Seasonality	Vegetation	[d]	(Müller Schmied et al., 2014)
$\mathit{LAI}_{min}$	Minimum leaf area index for deciduous plants in LAI growth model (set to 0.1 m <sup>2</sup> .m <sup>-2</sup> )	Seasonality	Constant	$[m^2  m^{-2}]$	(Müller Schmied et al., 2014)
$T_{min}$	Daily temperature threshold to initiate the growing season in LAI growth model (set to 8°C)	Seasonality	Constant	[°C]	(Müller Schmied et al., 2014)
$P_{min,cum}$	Cumulative precipitation threshold to initiate the growing season in LAI growth model (set to 40mm)	Seasonality	Constant	[mm]	(Müller Schmied et al., 2014)
$P_{min,daily}$	Minimum daily precipitation to keep growing season growing in semi-arid and arid regions in LAI growth model (set to 0.5mm)	Seasonality	Constant	[mm d <sup>-1</sup> ]	(Müller Schmied et al., 2014)
$t_{growth}$	Number of days for <i>LAI</i> to increase from its minimum to its maximum value or to decrease from its maximum to its minimum value in LAI growth model (set to 30 d)	Seasonality	Constant	[d]	(Müller Schmied et al., 2014)

Table S3. Parameters used for ET estimation in the WaterGap V2.2 model.

<sup>&</sup>lt;sup>a</sup> PET: potential evapotranspiration equation; Stress: Stress model for actual ET calculation from PET.

Parameter	Description	Module a	Category	Unit	Reference
$g_{min}$	Minimum canopy conductance	PET	Vegetation	[mm s <sup>-1</sup> ]	(Gerten et al., 2004; Sitch et al., 2003)
$g_m$	Scaling conductance in the evaporative demand function (set to 3.26 mm.s <sup>-1</sup> )	PET	Constant	[mm s <sup>-1</sup> ]	(Gerten et al., 2004)
$\alpha_m$	Priestley-Taylor empirical coefficient (set to 1.391)	PET	Constant	[-]	(Gerten et al., 2004)
$\alpha_{PT}$	Priestley-Taylor empirical coefficient (set to 1.32)	PET	Constant	[-]	(Gerten et al., 2004)
i	Empirical coefficient for calculation of interception (same formulation as (Kergoat, 1998))	Interception	Vegetation	[-]	(Gerten et al., 2004)
LAI	Leaf area index (determined as a function of daily phenomenology)	Interception	Vegetation	$[m^2 m^{-2}]$	(Gerten et al., 2004)
$E_{pot,max}$	Maximum potential evapotranspiration (5-7 mm.d <sup>-1</sup> )	Stress	Vegetation	[mm d <sup>-1</sup> ]	(Gerten et al., 2004)
AWC	Soil available water capacity	Stress	Soil	$[m^3 m^{-3}]$	(Gerten et al., 2004)
$f_{root,0}$	Weighting constant to determine fraction of roots in evaporation layer (set to 1.3)	Stress	Constant	[-]	(Gerten et al., 2004)
$f_{root,1}$	fraction of roots in soil layer 1	Stress	Vegetation	[-]	(Gerten et al., 2004; Sitch et al., 2003)
$d_1$	depth soil layer 1 (set to 0.5 m)	Soil layers	Constant	[m]	(Gerten et al., 2004)
$d_2$	depth soil layer 2 (set to 1 m)	Soil layers	Constant	[m]	(Gerten et al., 2004)
$d_0$	depth evaporation layer (set to 0.2 m)	Soil layers	Constant	[m]	(Gerten et al., 2004)
$f_c$	Vegetation cover fraction (determined as a function of daily phenomenology)	Sparse vegetation	Vegetation	[-]	(Gerten et al., 2004)

**Table S4**. Parameters used for ET estimation in the LPJ model.

<sup>&</sup>lt;sup>a</sup> PET: potential evapotranspiration equation; Stress: Stress model for actual ET calculation from PET.

Parameter	Description	Module a	Category	Unit	Reference
$r_{a,veg}$	Vegetation aerodynamic resistance	PET	Vegetation	[s m <sup>-1</sup> ]	(Kergoat, 1998)
$r_{st}$	Minimum stomatal resistance	PET	Vegetation	[s m <sup>-1</sup> ]	(Kergoat, 1998)
$r_{a,soi}$	Soil aerodynamic resistance (set to 100 s.m <sup>-1</sup> )	PET	Constant	[s m <sup>-1</sup> ]	(Kergoat, 1998)
$r_{s,soi}$	Soil surface resistance (set to 50 s.m <sup>-1</sup> )	PET	Constant	[s m <sup>-1</sup> ]	(Kergoat, 1998)
LAI	Leaf area index	PET and interception	Vegetation	$[m^2 m^{-2}]$	(Kergoat, 1998)
β	Empirical coefficient for calculation of interception	Interception	Vegetation	[-]	(Kergoat, 1998)
$S_1$	Constant in radiation term in stomatal resistance parameterization (set to 10 W PAR.m <sup>-2)</sup>	PET (surface resistance)	Constant	[W PAR m <sup>-2</sup> ]	(Kergoat, 1998)
$f_s$	Fraction of photosynthetically active solar radiation (set to 0.48)	PET (surface resistance)	Constant	[-]	(Kergoat, 1998)
$D_1$	First coefficient of the vapour pressure deficit term in stomatal resistance parameterization (set to 3000 Pa)	PET (surface resistance)	Constant	[Pa]	(Kergoat, 1998)
$D_2$	Second coefficient of the vapour pressure deficit term in stomatal resistance parameterization (set to 3500 Pa)	PET (surface resistance)	Constant	[Pa]	(Kergoat, 1998)
k	Beer- Lambert extinction coefficient (set to 0.5)	PET (surface resistance) and Sparse vegetation	Constant	[-]	(Kergoat, 1998)
$Z_r$	Rooting depth	Stress	Vegetation	[m]	(Kergoat, 1998)
AWC	Soil available water capacity	Stress	Soil	$[m^3 m^{-3}]$	(Kergoat, 1998)
$W_1$	Soil water constant for stomatal closure as a fraction of soil water storage (set to 0.4)	Stress	Constant	[-]	(Kergoat, 1998)
$W_2$	Soil water constant for soil evaporation reduction (set to 0.6)	Stress	Constant	[-]	(Kergoat, 1998)

**Table S5**. Parameters used for ET estimation in the model proposed by (Kergoat, 1998). We did not review the light limitation sub-model of the model, which is used to calculate an equilibrium value of LAI.

<sup>&</sup>lt;sup>a</sup> PET: potential evapotranspiration equation; Stress: Stress model for actual ET calculation from PET.

Parameter	Description	Module a	Category	Unit	Reference
$K_c$	Crop factor (monthly values estimated as a function of land cover and climatology)	PET (and seasonality)	Vegetation	[-]	(Van Beek, 2008)
$K_{c,min}$	Minimum crop factor for bare soil (set to 0.2)	PET	Constant	[-]	(Van Beek, 2008; Sperna Weiland et al., 2015)
LAI	Leaf area index (monthly values estimated as a function of land cover and climatology)	Interception (and seasonality)	Vegetation	$[m^2 m^{-2}]$	(Van Beek, 2008; Sutanudjaja et al., 2011)
$V_{can}$	Interception storage capacity (set to 0.3 mm LAI)	Interception	Constant	[mm LAI]	(Sutanudjaja et al., 2011) (Van Beek, 2008; Sperna Weiland
$f_{root,1}$	Root fraction in soil layer 1	Stress	Vegetation	[-]	et al., 2015; Sutanudjaja et al., 2011)
$eta_1$	Coefficient of the soil water retention curve in soil layer 1	Stress	Soil	[-]	(Van Beek, 2008; Sutanudjaja et al., 2011)
$eta_2$	Coefficient of the soil water retention curve in soil layer 2	Stress	Soil	[-]	(Van Beek, 2008; Sutanudjaja et al., 2011)
$W_{sat,1}$	Saturated volumetric moisture content in soil layer 1	Stress	Soil	$[m^3 m^{-3}]$	(Van Beek and Bierkens, 2008; Sperna Weiland et al., 2015)
$W_{sat,2}$	Saturated volumetric moisture content in soil layer 2	Stress	Soil	$[m^3 m^{-3}]$	(Van Beek and Bierkens, 2008; Sperna Weiland et al., 2015)
$k_{sat,1}$	Saturated hydraulic conductivity in soil layer 1	Stress (soil evaporation)	Soil	[m d <sup>-1</sup> ]	(Van Beek, 2008; Sutanudjaja et al., 2011)
$\Psi_{sat,1}$	Matric soil suction at saturation in soil layer 1	Stress (transpiration)	Soil	[m]	(Sutanudjaja et al., 2011)
$\Psi_{sat,2}$	Matric soil suction at saturation in soil layer 2	Stress (transpiration)	Soil	[m]	(Sutanudjaja et al., 2011)
$\Psi_{50\%}$	Matric soil suction at which transpiration is halved (set for instance equal to 3.33m)	Stress (transpiration)	Constant	[m]	(Sutanudjaja et al., 2011)
$d_1$	Depth of soil layer 1 (set to 0.3 m)	Stress	Constant	[m]	(Van Beek and Bierkens, 2008)
$d_2$	Depth of soil layer 2 (set to 1.2 m)	Stress	Constant	[m]	(Van Beek and Bierkens, 2008)

 Table S6. Parameters used for ET estimation in the PCR-GLOBWB model.

<sup>&</sup>lt;sup>a</sup> PET: potential evapotranspiration equation; Stress: Stress model for actual ET calculation from PET.

Parameter	Description	Module a	Category	Unit	Reference
$h_{veg,over}$	Overstory vegetation height	PET	Overstory vegetation	[m]	(Gosling and Arnell, 2011; Smith, 2016)
$r_{st,over}$	Overstory vegetation stomatal resistance	PET	Overstory vegetation	[s m <sup>-1</sup> ]	(Gosling and Arnell, 2011; Smith, 2016)
$\mathit{LAI}_{over}$	Overstory leaf area index	PET	Overstory vegetation	$[\mathrm{m}^2\mathrm{m}^{\text{-}2}]$	(Gosling and Arnell, 2011; Smith, 2016)
$h_{veg,over}$	Understory vegetation height (set to value for grass)	PET	Understory vegetation	[m]	(Gosling and Arnell, 2011; Smith, 2016)
$r_{st,under}$	Understory vegetation stomatal resistance (set to value for grass)	PET	Understory vegetation	[s m <sup>-1</sup> ]	(Gosling and Arnell, 2011; Smith, 2016)
$\mathit{LAI}_{under}$	Understory leaf area index (set to value for grass)	PET	Understory vegetation	$[m^2 m^{-2}]$	(Gosling and Arnell, 2011; Smith, 2016)
K	Radiation coefficient to calculate canopy surface resistance (set to 0.7)	PET	Constant	[-]	(Smith, 2016)
$r_{s,soi}$	(Soil) resistance to calculate canopy surface resistance (set to 100 s.m <sup>-1</sup> )	PET	Constant	[s m <sup>-1</sup> ]	(Smith, 2016)
$Z_{r,over}$	Overstory rooting depth	Stress	Overstory vegetation	[m]	(Gosling and Arnell, 2011; Smith, 2016)
$Z_{r,under}$	Understory rooting depth (set to value for grass)	Stress	Understory vegetation	[m]	(Gosling and Arnell, 2011; Smith, 2016)
FC	Soil field capacity	Stress	Soil	$[m^3 m^{-3}]$	(Gosling and Arnell, 2011; Smith, 2016)
$S_{max}$	Soil saturation capacity	Stress	Soil	$[m^3 m^{-3}]$	(Gosling and Arnell, 2011; Smith, 2016)
$\gamma_{over}$	Overstory interception capacity	Interception	Overstory vegetation	[mm]	(Gosling and Arnell, 2011; Smith, 2016)
$\gamma_{under}$	Understory interception capacity (set to value for grass)	Interception	Understory vegetation	[mm]	(Gosling and Arnell, 2011; Smith, 2016)
δ	Empirical parameter of interception model (set to 0.75)	Interception	Constant	[-]	(Arnell, 1999; Smith, 2016)
Percov	Percent overstory cover	Sparse vegetation	Overstory vegetation	[%]	(Gosling and Arnell, 2011; Smith, 2016)

 Table S7. Parameters used for ET estimation in the Mac-PDM model.

<sup>&</sup>lt;sup>a</sup> PET: potential evapotranspiration equation; Stress: Stress model for actual ET calculation from PET.

Parameter	Description	Module a	Category	Unit	Reference
$z_0$	Surface roughness length	PET	Vegetation	[m]	(Noilhan and Planton, 1989)
$r_{st}$	Minimum stomatal resistance	PET	Vegetation	[s m <sup>-1</sup> ]	(Noilhan and Planton, 1989)
LAI	Leaf area index (average monthly values)	PET and interception	Vegetation	$[m^2 m^{-2}]$	(Noilhan and Planton, 1989)
$V_{can}$	Interception storage capacity per unit of <i>LAI</i> (set to 0.2 mm LAI)	Interception	Constant	[mm LAI]	(Noilhan and Planton, 1989)
$Exp_{can}$	Exponent to assess the wet canopy fraction (set to 2/3)	Interception	Constant	[-]	(Deardorff, 1978; Noilhan and Planton, 1989)
$R_{GL}$	Limit value of incoming solar radiation (set to 30 W m <sup>-2</sup> for forest and 100 W m <sup>-2</sup> for crop)	PET (surface resistance)	Vegetation	[W m <sup>-2</sup> ]	(Noilhan and Planton, 1989)
$r_{st,max}$	Maximum surface resistance (set to 5000 s.m <sup>-1</sup> )	PET (surface resistance)	Constant	[s m <sup>-1</sup> ]	(Noilhan and Planton, 1989)
$f_s$	Fraction of photosynthetically active solar radiation (set to 0.55)	PET (surface resistance)	Constant	[-]	(Noilhan and Planton, 1989)
g	Coefficient of the vapour pressure term (set to 0.025 hPa <sup>-1</sup> )	PET (surface resistance)	Constant	[hPa <sup>-1</sup> ]	(Noilhan and Planton, 1989)
$k_T$	Coefficient of the temperature term (set to $0.0016\ K^{-2}$ )	PET (surface resistance)	Constant	[K <sup>-2</sup> ]	(Noilhan and Planton, 1989)
WP	Wilting point volumetric water content	Stress	Soil	$[m^3 m^{-3}]$	(Noilhan and Planton, 1989)
$W_{sat}$	Saturated volumetric moisture content	Stress	Soil	$[m^3 m^{-3}]$	(Noilhan and Planton, 1989)
$W_{crit}$	Critical soil moisture (set to 0.75)	Stress	Constant	[-]	(Noilhan and Planton, 1989)
$d_1$	Depth of the evaporation soil layer (set to $0.01m$ ))	Stress	Constant	[m]	(Noilhan and Planton, 1989)
$d_2$	Rooting depth	Stress	Vegetation	[m]	(Noilhan and Planton, 1989)
$d_3$	Total soil depth	Stress	Vegetation and soil	[m]	(Boone et al., 1999)
$f_c$	Vegetation cover fraction	Sparse vegetation	Vegetation	[-]	(Noilhan and Planton, 1989)

 Table S8. Parameters used for ET estimation in the ISBA model.

<sup>&</sup>lt;sup>a</sup> PET: potential evapotranspiration equation; Stress: Stress model for actual ET calculation from PET.

Parameter	Description	Module a	Category	Unit	Reference
$lpha_{PT}$	Priestley-Taylor empirical coefficient	PET	Vegetation	[-]	(Miralles et al., 2011)
$f_G$	Ground heat as a fraction of net radiation	PET	Vegetation	[-]	(Miralles et al., 2011)
β	Correction factor for transpiration to account for hours with wet canopy (set to 0.07)	PET (tall vegetation)	Constant	[-]	(Miralles et al., 2011)
VOD	Vegetation optical depth (remotely sensed)	Stress and seasonality	Vegetation	[-]	(Martens et al., 2017; Miralles et al., 2011)
$VOD_{max}$	Maximum vegetation optical depth	Stress	Vegetation	[-]	(Martens et al., 2017)
$Z_r$	Rooting depth	Stress	Vegetation	[m]	(Miralles et al., 2011)
WP	Wilting point	Stress	Soil	$[m^3 m^{-3}]$	(Martens et al., 2017)
FC	Field capacity	Stress	Soil	$[m^3 m^{-3}]$	(Martens et al., 2017)
$S_c$	Canopy storage for tall vegetation (set to 1.2 mm)	Interception (tall vegetation)	Constant	[mm]	(Miralles et al., 2010)
$\overline{E_c}$	Mean evaporation rate for interception for tall vegetation (set to 0.3 mm.h <sup>-1</sup> )	Interception (tall vegetation)	Constant	[mm h <sup>-1</sup> ]	(Miralles et al., 2010)
$\overline{R_s}$	Mean (synoptic) rainfall rate for tall vegetation (set to 1.5 mm.h <sup>-1</sup> )	Interception (tall vegetation)	Constant	[mm h <sup>-1</sup> ]	(Miralles et al., 2010)
$\overline{R_c}$	Mean (convective) rainfall rate for tall vegetation (set to 5.6 mm.h <sup>-1</sup> )	Interception (tall vegetation)	Constant)	[mm h <sup>-1</sup> ]	(Miralles et al., 2010)
$p_d$	Fraction of rain to trunks for tall vegetation (set to 0.02)	Interception (tall vegetation)	Constant	[-]	(Miralles et al., 2010)
e	Fraction of trunk evaporation for tall vegetation (set to 0.02)	Interception (tall vegetation)	Constant	[-]	(Miralles et al., 2010)
$S_t$	Trunk capacity for tall vegetation (set to 0.02 mm)	Interception (tall vegetation)	Constant	[mm]	(Miralles et al., 2010)
$d_1$	Depth at the bottom of the first soil layer (set to 0.05m)	Soil layers	Constant	[m]	(Miralles et al., 2011)
$d_2$	Depth at the bottom of the second soil layer (set to 1 m)	Soil layers	Constant	[m]	(Miralles et al., 2011)
$d_3$	Depth at the bottom of the third soil layer (set to 2.5 m)	Soil layers	Constant	[m]	(Miralles et al., 2011)

**Table S9**. Parameters used for ET estimation in the GLEAM V3 model.

<sup>&</sup>lt;sup>a</sup> PET: potential evapotranspiration equation; Stress model for actual ET calculation from PET.

Parameter	Description Module <sup>a</sup>		Category	Unit	Reference	
$z_0$	Surface roughness length	PET	Vegetation	[m]	(Liang et al., 1994)	
$r_{st}$	Minimum stomatal resistance	PET	Vegetation	[s m <sup>-1</sup> ]	(Bohn and Vivoni, 2016; Liang et al., 1994)	
$r_{arc}$	Vegetation architectural resistance (boundary layer resistance)	PET	Vegetation	[s m <sup>-1</sup> ]	(Bohn and Vivoni, 2016; Liang et al., 1994)	
$d_0$	Vegetation zero plane displacement height	PET	Vegetation	[m]	(Liang et al., 1994)	
$r_{s,soi}$	Soil surface resistance (set to 0 s.m <sup>-1</sup> )	PET	Constant	[s m <sup>-1</sup> ]	(Bohn and Vivoni, 2016)	
$r_{arc,soi}$	Soil architectural resistance (set to 0 s.m <sup>-1</sup> )	PET	Constant	[s m <sup>-1</sup> ]	(Bohn and Vivoni, 2016) (Bohn and	
LAI	Leaf area index (average monthly values)	PET and interception	Vegetation	$[m^2 m^{-2}]$	Vivoni, 2016; Liang et al., 1994)	
$V_{can}$	Interception storage capacity per unit of <i>LAI</i> (set to 0.2 mm LAI)	Interception	Constant	[mm LAI]	(Liang et al., 1994)	
$Exp_{can}$	Exponent to assess the wet canopy fraction (set to 2/3)	Interception	Constant	[-]	(Deardorff, 1978; Liang et al., 1994)	
$R_{GL}$	Limit value of incoming solar radiation	PET (surface resistance)	Vegetation	[W m <sup>-2</sup> ]	(Bohn and Vivoni, 2016)	
$r_{st,max}$	Maximum surface resistance	PET (surface resistance)	Constant	[s m <sup>-1</sup> ]	(Bohn and Vivoni, 2016)	
$f_s$	Fraction of photosynthetically active solar radiation	PET (surface resistance)	Constant	[-]	(Bohn and Vivoni, 2016)	
g	Coefficient of the vapour pressure deficit term	PET (surface resistance)	Constant	[hPa <sup>-1</sup> ]	(Bohn and Vivoni, 2016)	
$k_T$	Coefficient of the temperature term	PET (surface resistance)	Constant	[K <sup>-2</sup> ]	(Bohn and Vivoni, 2016)	
$f_{root,1}$	Root fraction in first soil layer	Stress	Vegetation	[-]	(Liang et al., 1994)	
$W_{crit}$	Critical soil moisture in stomatal resistance parameterization as a fraction of soil saturation	Stress	Soil	$[m^3 m^{-3}]$	(Bohn and Vivoni, 2016; Liang et al., 1994)	
WP	Wilting point	Stress	Soil	$[m^3 m^{-3}]$	(Bohn and Vivoni, 2016; Liang et al., 1994)	
$d_1$	Depth of soil layer 1 (e.g. set to 0.3 m)	Stress	Constant	[m]	(Liang et al., 1994)	
$d_2$	Depth of soil layer 2 (e.g. set to 0.7 m)	Stress	Constant	[m]	(Liang et al., 1994)	
NDVI	Normalized Difference Vegetation Index (remotely sensed daily values)	Sparse vegetation and	Vegetation	[-]	(Bohn and Vivoni, 2016)	
$NDVI_{min}$	Minimum Normalized Difference Vegetation Index (set to 0.1)	seasonality Sparse vegetation	Constant	[-]	(Bohn and Vivoni, 2016)	

MDM	Maximum Normalized Difference	Sparse	Constant	ГЛ	(Bohn and
$NDVI_{max}$	Vegetation Index (set to 0.8)	vegetation	Constant	[-]	Vivoni, 2016)

 $\textbf{Table S10}. \ \ Parameters \ used \ for \ ET \ estimation \ in \ the \ VIC \ V4.2 \ model. \ Additional \ information \ on \ model \ parameters \ was found \ in the GLDAS \ project \ (https://ldas.gsfc.nasa.gov/gldas/GLDAS mapveg.php).$ 

<sup>&</sup>lt;sup>a</sup> PET: potential evapotranspiration equation; Stress: Stress model for actual ET calculation from PET.

### S3. Additional information on the determination of parameter ranges

In this section, Tables S11 and S12 are extended versions of Tables 1 and 3 respectively that present the model parameters and the ranges used for application of V2Karst at FLUXNET sites. We added explanations and references for the determination of the parameter ranges.

Parameter	Description	unit	Lower limit	Upper limit	Category	Note and references for parameter range
$h_{veg}$	Vegetation height	[m]	0.2	Site specific	vegetation	The upper bound is set for each site specifically so that it is lower than the measurement heights reported in Table B1.
$r_{st}$	Stomatal resistance	[s m <sup>-1</sup> ]	20	600	vegetation	The range includes the 70th percentiles of the values for the different vegetation types in temperate climate (Breuer et al., 2003).
$LAI_{min}$	Reduction in leaf area index during the dormant season	[%]	5	100	vegetation	Best guess estimate.
$LAI_{max}$	Annual maximum leaf area index	$[m^2 m^{-2}]$	0.5	8	vegetation	The range includes the 70th percentiles calculated for the different vegetation types in temperate climate (Breuer et al., 2003).
$V_r$	Maximum storage capacity of the root zone	[mm]	20	500	vegetation	The range includes the 70th percentiles of the values of rooting depth (provided in [m]) for the different vegetation types in temperate climate (Breuer et al., 2003) multiplied by an average value of soil available water capacity of 0.2 m <sup>3</sup> m <sup>-3</sup> (Bonan, 2015; Miralles et al., 2011; Salter and Williams, 1965).
$V_{can}$	Canopy storage capacity per unit of <i>LAI</i>	[mm LAI]	0.1	0.5	vegetation	The range includes the value used in WaterGap (Döll et al., 2003) for daily application (0.3 mm LAI); in VIC (Liang et al., 1994) and ISBA (Noilhan and Planton, 1989) for subdaily applications as proposed in (Dickinson, 1984) (0.2 mm LAI); in the Distributed Hydrology-Soil-Vegetation model (Wigmosta et al., 1994) for subdaily applications (0.1 mm LAI); the maximum value used in Mac-PDM [Gosling and Arnell, 2011] (0.5 mm LAI for open shrublands).
k	Beer-Lambert's law extinction coefficient	[-]	0.4	0.7	vegetation	The range includes the value reported in (Van Dijk and Bruijnzeel, 2001; Granier et al., 1999; Kergoat, 1998; Ruiz et al., 2010) (0.5); in (Shuttleworth and Wallace, 1985) (0.7).
$f_{red}$	Reduction factor for transpiration below the root zone	[-]	0	0.15	soil	The range includes the value reported in (Penman, 1950; Wagener et al., 2003) (1/12).
$z_0$	Soil roughness length	[m]	0.0003	0.013	soil	The range includes the value used in MOSES (Essery et al., 2001) (0.0003m); in Hydrus (Šimůnek et al., 2009) (0.001 m); in NOAH (Yang et al., 2011) and the Community Land model (Oleson et al., 2010) (0.01 m); in (Masson et al., 2003) (0.013 m).
$r_{s,soi}$	Soil surface resistance	[s m <sup>-1</sup> ]	0	100	soil	The range includes the value used in VIC (Bohn and Vivoni, 2016) and SWAP (Kroes et al., 2008) (0 m s <sup>-1</sup> ); in (Kergoat, 1998) (50 m s <sup>-1</sup> ); in MacPDM (Smith, 2016) (100 m s <sup>-1</sup> ); in (Van de Griend and Owe, 1994) (10 m s <sup>-1</sup> ).
$V_e$	Maximum storage capacity of the first soil layer	[mm]	5	45	soil	Range includes the average depth of 0.1-0.15 m recommended in (Allen et al., 1998) multiplied by a large value of the soil water capacity of 0.3 m <sup>3</sup> m <sup>-3</sup> ((Bonan, 2015; Salter and Williams, 1965)).
а	Spatial variability coefficient	[-]	0	6	soil and epikarst	(Hartmann et al., 2015)
$V_{soil}$	Mean soil storage capacity	[mm]	20	800	soil	Best guess estimate.
$V_{epi}$	Mean epikarst storage capacity	[mm]	200	700	epikarst	(Hartmann et al., 2015)
$K_{epi}$	Mean epikarst outflow coefficient	[d]	0	50	epikarst	(Hartmann et al., 2015)

**Table S11**. Description of V2Karst parameters, unconstrained ranges used in the application at the four FLUXNET sites to capture the variability across soil, epikarst and vegetation types, category of the parameters (which indicated whether the parameters depend on soil, epikarst or vegetation properties) and references for the determination of parameter ranges. Parameters a,  $V_{soil}$ ,  $V_{epi}$  and  $K_{epi}$  were already present in the previous version of the model (VarKarst).

Parameter	Unit	German site (deciduous forest)		Spanish site (shrubland)		French 1 site (evergreen forest)		French 2 site (evergreen forest)		Note and reference for parameter ranges
		Lower limit	Upper limit	Lower limit	Upper limit	Lower limit	Upper limit	Lower limit	Upper limit	
$h_{veg}$	[m]	23.1	42.9	0.35	0.85	7.1	13.3	3.9	7.2	The range corresponds to the average value reported in Table B1 for the site $\pm 30$ %. At the Spanish site, the upper bound is set higher due to the presence of a few plants taller than average.
$r_{st}$	[s m <sup>-1</sup> ]	275	400	195	350	320	455	320	455	40 <sup>th</sup> and 60 <sup>th</sup> percentile values reported in (Breuer et al., 2003) for the specific land cover at the site.
$\mathit{LAI}_{min}$	[%]	5	20	34	63	80	100	80	100	At the Spanish site, the range corresponds to the value reported in Table B1 for the site $\pm 30$ %, and it is a best guess estimates for the other sites.
$LAI_{max}$	$[m^2 m^{-2}]$	3.5	6.5	1.9	3.5	1.5	2.9	2.0	3.8	The range corresponds to the value reported in Table B1 for the site $\pm 30$ %.
$V_r$	[mm]	60	300	30	200	30	200	30	200	The range includes the average value of the soil available water capacity for the German, Spanish and French 2 sites, and the value of the available water capacity of the root zone for the French 2 site. The upper bound is set to a high value to include uncertainty and to account for the fact that at the German, Spanish and French 1 sites, roots could extend below the soil because the soil is quite shallow.
$V_{soi}$	[mm]	60	400	30	300	30	300	30	300	Best guess estimates.

**Table S12.** Site-specific constrained parameter ranges at the four FLUXNET sites for the vegetation parameters  $(h_{veg}, r_{st}, LAI_{min}, LAI_{max}, V_r)$  and for the soil storage capacity  $(V_{soi})$  and references for the determination of parameter ranges.

#### S4. Data processing and analysis at FLUXNET sites

This section provides details on the processing of the data measured at the FLUXNET site to force and test the V2Karst model and to perform the virtual experiments (this section complements Sect. 3.2 and Sect. 4.3).

#### 5 S4.1 Processing of forcing data

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Measurements of precipitation, air temperature, net radiation, relative humidity and wind speed were gap-filled and then aggregated from 30 min to daily time scale. Missing precipitation data were filled with zero values for short gaps only (less or equal to 3 hours). For all other variables, we used the following procedure for gap-filling:

- short gaps (less or equal to 3 hours) were filled using linear interpolation;
- medium gaps (from 3.5 hours to 15 days) were filled using moving window averaging, i.e. the values corresponding to same time of the day for the previous and following days were averaged. For each gap we expanded progressively the width of the moving window until a minimum of four values to calculate the average were found. The maximum width of the moving window was 30 days.
- long gaps (from 15 to 80 days) were filled using long term averaging, i.e. for each month, we derived an average value for each time of the day by calculating the average over the entire time series.

We could then extract for each site a simulation period for which no gaps remained. We identified the 'poor' months for which the forcing data contained many gaps, and therefore for which the impact of the gap-filling on the simulation results is likely to be significant. 'Poor' months were defined as the months that had more than 20 % of the days that contained gap-filled data. In addition, after each period of months that contained many gaps, we also discarded (added to the list of 'poor' months') a period of the same length because we assumed that the impact of the gap-filling is still significant over this subsequent period. During the 'poor' months we did not compare model simulations with latent heat flux and soil moisture observations when applying the soft rules for parameter estimation (Sect. 4.1).

#### 25 S4.2 Processing and analysis of the uncertainty in observed ET

#### Processing of latent heat flux measurements

Observations of latent heat flux were aggregated from 30 min to monthly time scale and we discarded the months when more than 20 % of 30 min data were missing. We also removed monthly aggregated latent heat flux measurements when the mismatch in the energy balance closure was higher than 50 % similar to Miralles et al. (2011). We also derived two corrected estimates of actual ET, obtained by forcing the closure in the energy balance following Twine et al. (2000) and Foken et al. (2012):

1. a corrected value that assumes that latent heat flux (LE [M] m<sup>-2</sup> month<sup>-1</sup>]) and sensible heat flux (H [MJ m<sup>-2</sup> month<sup>-1</sup>]) have similar errors (referred to as Bowen ratio estimate,  $E_{act.cor}$  [mm month<sup>-1</sup>]):

$$E_{act,cor} = \frac{R_n - G}{\lambda(1 + \frac{H}{LE})},\tag{S1}$$

where  $R_n$  [MJ m<sup>-2</sup> month<sup>-1</sup>] is the net radiation, G [MJ m<sup>-2</sup> month<sup>-1</sup>] is the ground heat flux and  $\lambda$  [MJ kg<sup>-1</sup>] is the latent heat of vaporization of water;

2. a second corrected value that assumes errors in latent heat flux only (referred to as residual estimate,  $E_{act,cor2}$  [mm month<sup>-1</sup>]):

$$E_{act,cor2} = \frac{R_n - G - H}{\lambda}.$$
 (S2)

#### 5 Impact of neglecting the ground heat flux in Eq. (S1-S2)

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We note that measurements of G are not available for the French 1 site and contain many gaps for the French 2 site. Therefore, the tested the impact of neglecting the ground heat flux G in Eq. (S1-S2), i.e. of setting G = 0. We assessed the closure in the energy balance and the two correct estimates of ET (Eq. (S1-S2)) in two cases, a first case in which we included the measurements of G and a second case in which we neglected them. We conducted this analysis at the FLUXNET sites for which measurements of G are available (German, Spanish and French 2 site). The monthly time series of the two corrected estimates of ET of Eq. (S1-S2) obtained are reported in Fig. S1.

We then assessed the bias  $Bias_1$  [%] and the monthly Pearson correlation coefficient  $\rho_1$  [-] between the corrected estimate of Eq. (S1) processed with and without measurements of G:

$$Bias_1 = 100 \frac{\sum_{t \in M_{ET}} (E_{act,cor}^{no\ G}(t) - E_{act,cor}^G(t))}{\sum_{t \in M_{ET}} E_{act,cor}^G(t)}$$
(S3)

where  $E_{act,cor}^{no\ G}$  is the estimate of Eq. (S1) assessed neglecting G,  $E_{act,cor}^{G}$  is the estimate of Eq. (S1) assessed using G measurements and  $M_{ET}$  is the set of months for which latent heat flux measurements are available and for which the simulations can be compared to the observations because the forcing data contain few gaps (blue areas in Fig. S1).

Table S13 shows the values of  $Bias_1$  and  $\rho_1$  at the German, Spanish and French 2 sites. We see that  $\rho_1$  is close to 1, and therefore neglecting G does not impact the dynamic of the ET estimate.  $Bias_1$  is generally very small (< 2 %) apart from the Spanish site where it is equal to -8.3 %. This is due to the fact that a small number of observations can be used at the Spanish site and that  $Bias_1$  is therefore largely impacted by some differences between  $E_{act,cor}^{no\,G}$  and  $E_{act,cor}^{G}$  at the end of year 2010 (Fig. S1).

Our analysis shows that it is reasonable to neglect the ground heat flux (i.e. to assume G = 0) when assessing the corrected estimates of ET. This allows to use the French 1 site to test the model and to use a longer time series of ET measurements to test the model at the French 2 site.

Site	Number of monthly values used to assess $Bias_1$ and $\rho_1$	Bias <sub>1</sub> [%]	$\rho_1[-]$
German site	61	1.5	1
Spanish site	12	-8.3	0.99
French 2 site	22	0.2	1

Table S13. Bias  $Bias_1$  and monthly correlation coefficient  $\rho_1$  between the monthly Bowen ratio estimate of Eq. (S1) assessed when neglecting or using the ground heat flux.

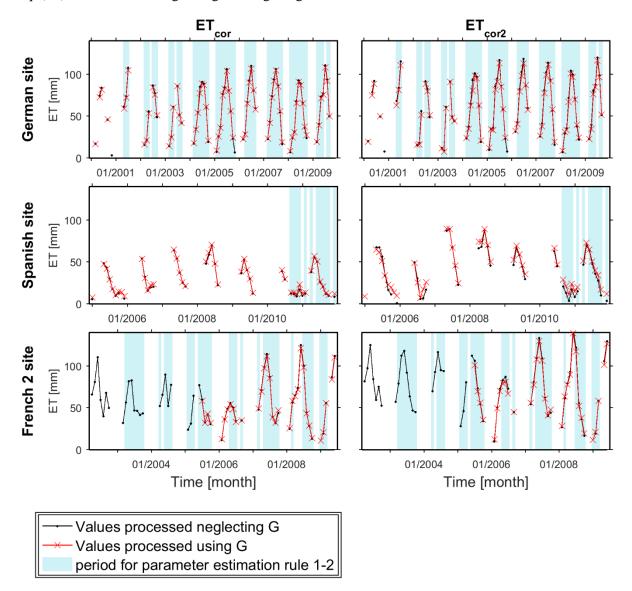


Figure S1. Time series of monthly corrected estimates of actual ET at the German, Spanish and French 2. Reported values were processed for two cases, i.e. neglecting G (ground heat flux) in black and using G in red. The two correct estimates  $E_{act,cor}$  and  $E_{act,cor2}$  are defined in Eq. (S1-S2). The blue shaded areas indicate the time period for which ET measurements were used to estimate the model parameters (Sect. 4.1) because the forcing data have a sufficient quality (few gaps) so that we can sensibly compare simulations and observations.

#### Analysis of the uncertainty in observed actual ET

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We then analysed the uncertainty in observed ET. We calculated the bias  $Bias_2$  [%] and the monthly correlation coefficient  $\rho_2$  [-] between the uncorrected actual ET estimate and the corrected estimates  $E_{act,cor}$  and  $E_{act,cor2}$  (assessed neglecting the ground heat flux since we have previously shown that it is a reasonable assumption) at the four FLUXNET sites. For instance, for  $E_{act,cor}$ ,  $Bias_2$  was calculated as follows:

$$Bias_2 = 100 \frac{\sum_{t \in M_{ET}} (E_{act,cor}(t) - E_{act,obs}(t))}{\sum_{t \in M_{ET}} E_{act,obs}(t)}$$
(S4)

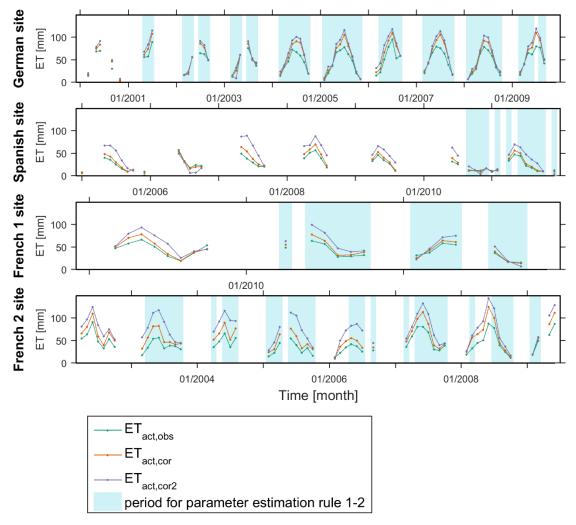
Where  $E_{act,obs}$  [mm month<sup>-1</sup>] is the uncorrected observed actual ET equal to  $\frac{LE}{\lambda}$ .

Figure S2 reports the monthly time series of  $E_{act,obs}$ ,  $E_{act,cor}$  and  $E_{act,cor2}$  and values of  $Bias_2$  and  $\rho_2$  are reported in Table S14. We observe that  $Bias_2$  can be quite large, especially for  $E_{act,cor2}$ , since the relative difference can be as high as 77 % for the French 2 site. We see that  $E_{act,cor}$  provides an intermediate value, between the uncorrected and the residual corrected estimate. The correlation coefficient  $\rho_2$  was always high at all sites (above 0.86), which means that all three estimated have similar temporal dynamics.

Therefore, the magnitude of observed actual ET has large uncertainties at the FLUXNET sites, while we can have a much higher confidence regarding the temporal dynamics of observed actual ET.

Site	Bias	· [%]	$ ho_2[-]$		
Site	$E_{act,cor}$	$E_{act,cor2}$	$E_{act,cor}$	$E_{act,cor2}$	
German	16	23	0.97	0.94	
Spanish	17	76	0.99	0.87	
French 1	10	30	0.97	0.91	
French 2	34	77	0.97	0.86	

**Table S14.** Bias  $Bias_2$  and monthly correlation coefficient  $\rho_2$  between monthly measured actual evapotranspiration ( $E_{act,obs}$ ) and monthly actual evapotranspiration estimate corrected using the Bowen method ( $E_{act,cor}$ ) or the energy residual method ( $E_{act,cor2}$ ) at the four FLUXNET sites.



**Figure S2**. Time series of monthly uncorrected estimate of actual ET ( $E_{act,obs}$ ) and corrected estimates ( $E_{act,cor}$ ) and ( $E_{act,cor2}$ ) (Eq. (S1-S2)) for the four FLUXNET sites. The blue shaded areas indicate the time period for which ET measurements were used to estimate the model parameters (Sect. 4.1) because the forcing data have a sufficient quality (few gaps) so that we can sensibly compare simulations and observations

#### S4.3 Estimation of wind speed at 43.5 m high at the Spanish site for the virtual experiments

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To set up the virtual experiments, we transformed the wind speed measurements at the Spanish site to estimate their value at the same height as measured at the German site (43.5 m). In fact, at the Spanish site wind speed is measured at a low height (2.5 m), since the vegetation is short. Therefore, to simulate the impact of a change to tall vegetation (forest) at the shrub virtual site, wind speed should be estimated at a height which is above canopy level, as required by the Penman Monteith equation. We assumed a logarithmic wind profile as e.g. in Lhomme et al. (2014). We note that we modified Eq. (6) in Lhomme et al. (2014), which is valid when the vegetation is fully covering the ground, to account for sparse vegetation. We calculated the value of wind speed at 43.5 m over vegetated and non-vegetated fraction separately using Eq. (6) in Lhomme et al. (2014) and we estimated the overall wind speed at 43.5 m for the site as the area weighted value over both fractions. The other weather variables (air temperature and humidity) are assumed to be the same at 43.5 m and 2.5 m. We deemed that these assumptions were reasonable, since the objective of the virtual experiments is to understand recharge sensitivity and not to predict recharge.

#### S5. Analysis of the impact of the warm-up period on predictions at FLUXNET sites

The analyses reported in this section aim to identify an appropriate value of the warm-up period (denoted as  $H_w$  [month]), to evaluate V2Karst at the four FLUXNET sites. The warm-up period corresponds to the initial time period which is discarded to reduce the impact of the choice of the value of the model initial states on the simulations.

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We assessed the sensitivity of the fluxes simulated with V2Karst to  $H_w$  by running the model for a range of values of  $H_w$ . For a given FLUXNET site, the date of the first day following the warm-up period is kept constant across the simulations (1 January 2001 at the German site, 1 January 2006 at the Spanish site, 1 January 2010 at the French 1 site and 1 April 2003 at the French 2 site). Instead, the date of the first day of the warm-up period is varied following the value of  $H_w$ . In this way, simulated fluxes are assessed over the same time horizon for all values of  $H_w$  and therefore simulations using different values of  $H_w$  can be compared among each other. We varied  $H_w$  between 2 and 12 months and we assessed the sensitivity of the total simulated recharge  $(Q_{epi})$  and actual ET  $(E_{act})$  to  $H_w$ , because we are interested in these two variables in our study. We estimated the metrics  $\Delta Q_{epi}$  [mm] and  $\Delta E_{act}$  [mm] defined as follows:

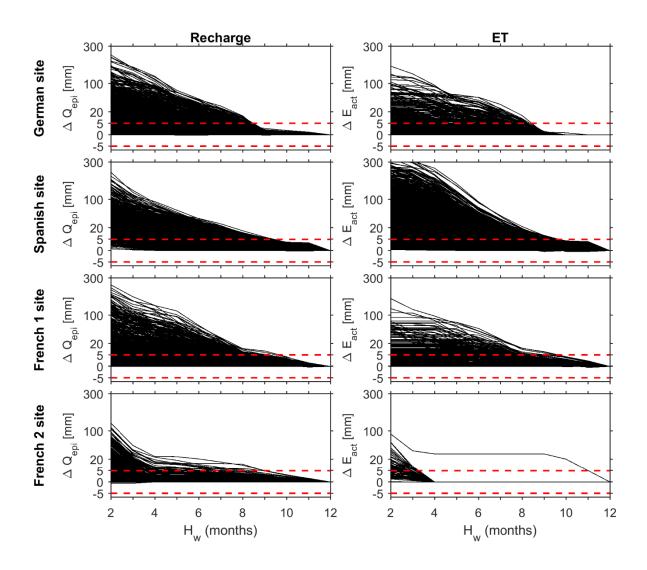
$$\Delta Q_{epi}(H_w = h_w) = Q_{epi}(H_w = h_w) - Q_{epi}(H_w = 12)$$

$$\Delta E_{act}(H_w = h_w) = E_{act}(H_w = h_w) - E_{act}(H_w = 12)$$
where  $h_w = 2, ..., 11$  months (S5)

The two metrics of Eq. (S5) measure the difference in  $Q_{epi}$  and  $E_{act}$  when  $H_w$  is set to 12 months compared to when  $H_w$  is set to lower values. A large value of  $\Delta Q_{epi}$  or  $\Delta E_{act}$  means that the choice of  $H_w$  has an impact on simulated recharge and actual ET, while a small value of  $\Delta Q_{epi}$  or  $\Delta E_{act}$  means that  $H_w$  has little effect on the simulation results. Initially, we assumed that the soil and epikarst stores for all model vertical compartments of V2Karst are saturated. For each of the 11 values of  $H_w$  that were tested, we repeated the simulations over 1,000 parameter sets sampled using latin hypercube sampling and the ranges reported in Table 1 of the main paper. Therefore, for each site, we performed a total number of 11,000 model executions.

Figure S3 reports  $\Delta Q_{epi}$  (left panels) and  $\Delta E_{act}$  (right panels) against  $H_w$  for the 1,000 parameter sets for each FLUXNET site. We see that when  $H_w$  increases, the width of the simulation ensemble decreases, which means that the impact of  $H_w$  on the simulations decreases. In general, the value of  $\Delta Q_{epi}$  and  $\Delta E_{act}$  becomes very small (-5  $mm < \Delta Q_{epi} < 5mm$  and -5  $mm < \Delta E_{act} < 5mm$ ) when  $H_w$  is equal to or larger than 10 months, apart from one parameterisation at the Spanish site for which  $\Delta Q_{epi}$  and  $\Delta E_{act}$  becomes very small when  $H_w$  is equal to 11 months. Therefore, the simulated fluxes show generally little changes in response to changes in  $H_w$  when  $H_w$  is higher than 10 months.

Consequently, we deemed reasonable to set the warm-up period equal to 12 months at all FLUXNET sites to perform the parameter estimation and the sensitivity analysis in this study (Sect. 4.1 and 4.2).

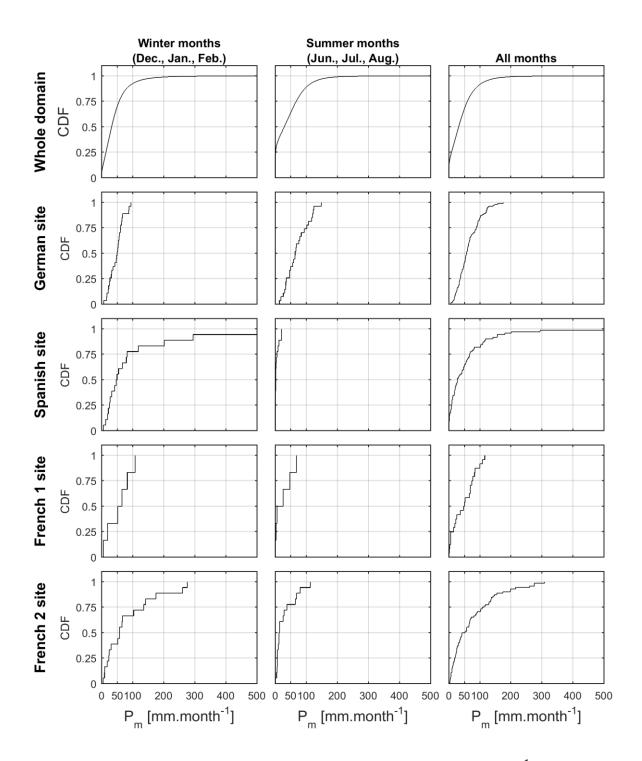


**Figure S3**. Difference in simulated recharge  $\Delta Q_{epi}$  and actual ET  $\Delta E_{act}$  (defined in Eq. (S5)) against the length warm-up period  $(H_w)$ .

# S6. Analysis of the range of variation of the precipitation characteristics to inform the setup of the virtual experiments

This section aims to inform the choice of the ranges of the monthly precipitation  $P_m$  [mm month<sup>-1</sup>], the precipitation intensity  $I_p$  [mm d<sup>-1</sup>] and the interval between rainy days  $H_p$  [d] to derive the synthetic precipitation inputs used in the virtual experiment (Sect. 4.3). This section reports the cumulative distribution function of  $P_m$  (Fig. S4),  $I_p$  (Fig. S5) and  $H_p$  (Fig. S6) for:

- the whole domain, which is all European and Mediterranean carbonate rock areas reported in the carbonate rock map of Williams and Ford (2006) presented in Fig.1 in the main paper. For this, precipitation from the GLDAS database is used (Rodell et al., 2004);
- the four carbonate rock sites of the FLUXNET network (Baldocchi et al., 2001) analysed in this study and presented in Fig. 1 and Table B1.



**Figure S4**. Cumulative distribution function of monthly precipitation  $P_m$  [mm month<sup>-1</sup>] over winter months (Dec., Jan. Feb.), summer months (Jun., Jul., Aug.) and all months of the year estimated for the whole domain (all European and Mediterranean carbonate rock areas) over the period 1 October 2002–30 September 2012, at the German FLUXNET site over the period 1 January 2001–17 December 2009, at the Spanish FLUXNET site over the period 1 January 2010–30 December 2011, at the French 1 FLUXNET site over the period 1 January 2010–30 December 2011 and at the French 2 FLUXNET site over the period 1 April 2003–31 March 2009.

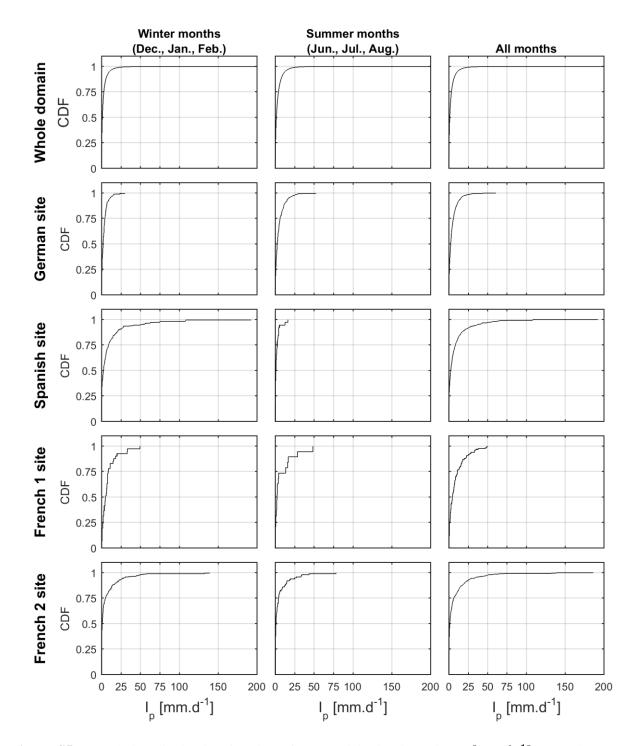
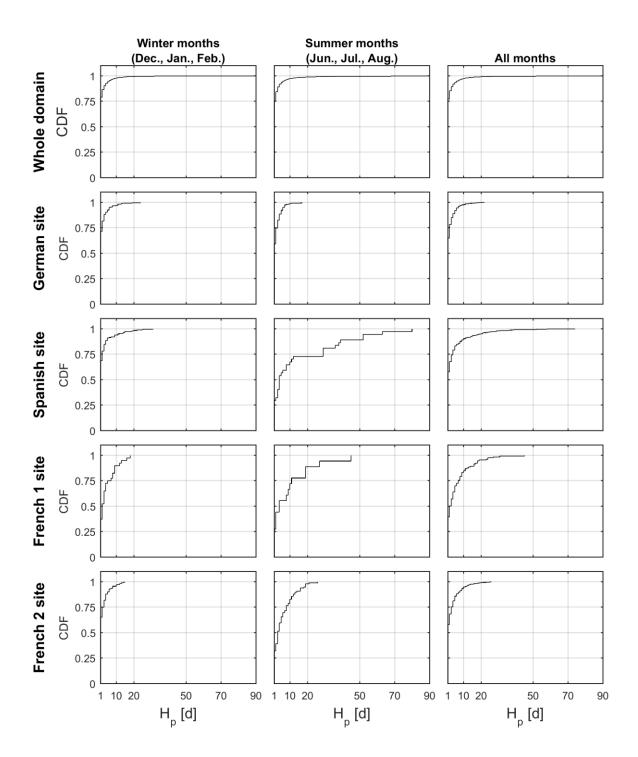


Figure S5. Cumulative distribution function of the precipitation intensity  $I_p$  [mm d<sup>-1</sup>] over winter months (Dec., Jan. Feb.), summer months (Jun., Jul., Aug.) and all months of the year estimated for the whole domain (all European and Mediterranean carbonate rock areas) over the period 1 October 2002–30 September 2012, at the German FLUXNET site over the period 1 January 2001–17 December 2009, at the Spanish FLUXNET site over the period 1 January 2010–30 December 2011, at the French 1 FLUXNET site over the period 1 January 2010–30 December 2011 and at the French 2 FLUXNET site over the period 1 April 2003–31 March 2009. Only days that had a precipitation amount above 0.1 mm were included in the calculation.



**Figure S6**. Cumulative distribution function of the interval between wet days  $H_p[d]$  over winter months (Dec., Jan. Feb.), summer months (Jun., Jul., Aug.) and all months of the year estimated for the whole domain (all European and Mediterranean carbonate rock areas) over the period 1 October 2002–30 September 2012, at the German FLUXNET site over the period 1 January 2001–17 December 2009, at the Spanish FLUXNET site over the period 1 January 2006–30 December 2011, at the French 1 FLUXNET site over the period 1 January 2010–30 December 2011 and at the French 2 FLUXNET site over the period 1 April 2003–31 March 2009. A wet day is defined as a day with more than 0.1 mm of precipitation.

### S7. Global sensitivity analysis of V2Karst parameters for the standard deviation of monthly simulated recharge and for simulated actual transpiration

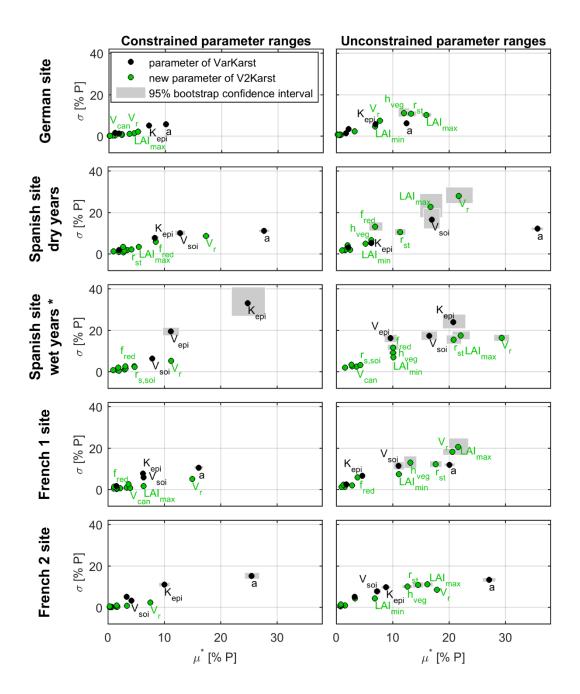
This section reports additional results for the global sensitivity analysis of the V2Karst parameters (Sect. 4.2). While in Sect. 5.2 and Fig. 7 we present the results for total recharge, here Fig. S7 and S8 report the results for the standard deviation of monthly recharge and for actual transpiration respectively. Figure 7 shows that some parameters that have a very small effect on total recharge at all sites and for both range choices (left and right panels in Fig. 7). The additional sensitivity analyses presented in this section reveal that some of these parameters have an influence on other aspects of the model simulations.

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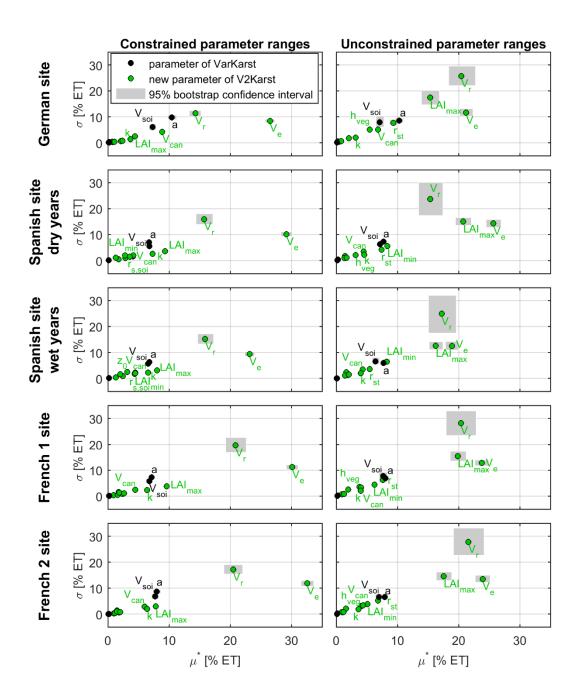
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For example, we find that parameters  $K_{epi}$  and  $V_{epi}$  have a small impact on total recharge ( $\mu^* < 3\%$  in all plots in Fig. 7), while they have an effect on the standard deviation of the recharge (Fig. S7). The same holds for parameter  $f_{red}$ , which also has a small impact on total recharge but a significantly higher importance on the standard deviation of the recharge, in particular at the Spanish and French 1 site (Fig. 7). Given that the standard deviation of recharge is a proxy metric for recharge dynamics, we infer that parameters  $K_{epi}$ ,  $V_{epi}$  and  $f_{red}$  have a significant effect on how recharge is distributed in time, but a limited effect on its total amount.

Furthermore, parameters  $V_e$  and k have little effect on total recharge ( $\mu^* < 3$  % in all plots in Fig. 7), while they are influential with respect to the percentage of actual transpiration in total ET (Fig. S8). Therefore, both parameters have an impact on the partitioning of ET among its three components.



**Figure S7**. Sensitivity indices of the V2Karst parameters ( $\mu^*$  is the mean of the absolute Elementary Effects and  $\sigma$  is the standard deviation of the Elementary Effects) for the standard deviation of simulated monthly recharge (expressed as a percentage of mean monthly precipitation) at the four FLUXNET sites when constrained (site-specific) parameter ranges are used (ranges of Table 3 in the main paper) and when unconstrained ranges are used (ranges of Table 1 in the main paper). Sensitivity indices were computed over the period 1 January 2001–17 December 2009 for the German site, 1 January 2006–31 December 2008 for the Spanish site (dry years), 1 January 2009–30 December 2011 for the Spanish site (wet years), 1 January 2010–30 December 2011 for the French 1 site and 1 April 2003-31 March 2009 for the French 2 site.\* Sensitivity indices for parameter a are not reported in the plots for the Spanish site wet years because they are significantly higher than the other parameters ( $\mu_a^* = 68 \%$  and  $\sigma_a = 51 \%$  for constrained ranges and  $\mu_a^* = 68 \%$  and  $\sigma_a = 38 \%$  for unconstrained ranges).



**Figure S8**. Sensitivity indices of the V2Karst parameters ( $\mu^*$  is the mean of the absolute Elementary Effects and  $\sigma$  is the standard deviation of the Elementary Effects) for simulated actual transpiration (expressed as a percentage of total ET) at the four FLUXNET sites when constrained (site-specific) parameter ranges are used (ranges of Table 3 in the main paper) and when unconstrained ranges are used (ranges of Table 1 in the main paper). Sensitivity indices were computed over the period 1 January 2001–17 December 2009 for the German site, 1 January 2006–31 December 2008 for the Spanish site (dry years), 1 January 2009–30 December 2011 for the Spanish site (wet years), 1 January 2010–30 December 2011 for the French 1 site and 1 April 2003–31 March 2009 for the French 2 site.

## S8. Comparison between V2Karst results obtained using daily and hourly simulation time step

The V2Karst model (version V1.1) can be run at both daily and sub-daily time step. This section presents a comparison of simulation results obtained using a daily and an hour time step (Fig. S9-S17). We tested the model predictions by estimating the model parameters using the soft rules presented in Sect. 4.1 for both daily and hourly time step. We did not observe significant differences between the results for daily and hourly time step in terms of parameter constraining (Fig. S9-S12) and in terms of model predictions (Fig. S13-S17). This means that the simulation time step has little effect on recharge at monthly and annual time scale, which is the focus of our study. Therefore, it is reasonable to apply the model at daily time step for our application, which significantly reduces the computational requirements.

#### **Description of the experiment setup**

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For hourly simulations, we forced V2Karst using measurements of P, T,  $R_n$ , RH, WS and G at the carbonate rock FLUXNET sites, while G was neglected for daily simulations (as explained in Sect. 2.3.3). We did not run the model at hourly time step at the French 1 site since no measurements of G are available. Forcing and calibration data were processed as explained in Sect. 3.2, S4.1 and S4.2

Table S15 reports the simulation period and the number of monthly latent heat flux and soil moisture observations that were used to estimate the model parameters at the three FLUXNET sites. We note that the simulation period for the French 2 site is reduced compared to the simulation period used to perform the daily analyses presented in the main paper (Table 2). This is because the time series of *G* contained many gaps for this site and we therefore had to discard part of it to perform hourly simulations.

We run V2Karst against the same sample of the model parameter of size 100,000 and within the ranges of Tables 1 and 3, for both hourly and daily time step (as explained in Sect. 4.1). We note that we applied a conversion factor to parameter  $K_{epi}$  for hourly simulation compared to daily simulations to run the model ( $K_{epi}$  is expressed in hours for hourly simulations, while it is expressed in days for daily simulations). All model runs were performed using a 1-year warmup period, which we found to be sufficient to remove the impact of the initial conditions on the simulation results in the case of daily time step (Sect. S5). We applied the soft rules to both hourly and daily simulation results, as explained in Sect. 4.1.

Site	Simulation per one-year warm	riod (including a n-up period)	Number of months with latent heat flux measurement for	Number of months with soil moisture	
	Start	End	calibration	measurement for calibration	
German site	1 Jan. 2000	17 Dec. 2009	62	74	
Spanish site	1 Jan. 2005	30 Dec. 2011	12	12	
French 2 site	17 Jul. 2005	29 Jun. 2009	16	Not measured	

**Table S15**. Simulation period at the three FLUXNET sites, and number of months where latent heat flux measurements and soil moisture measurements are available to calibrate the model. Soil moisture measurements is not provided at the French 2 site.

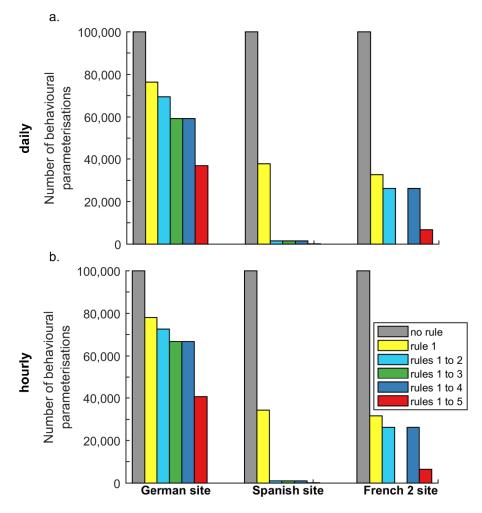
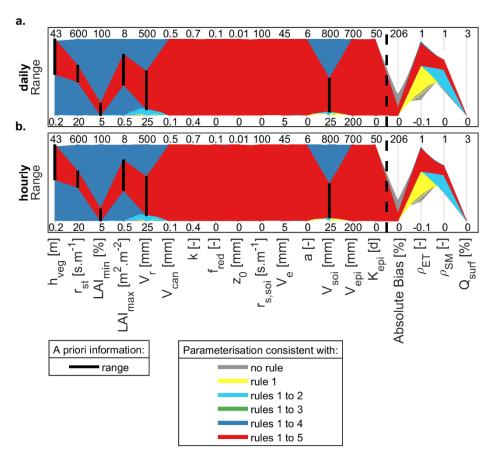
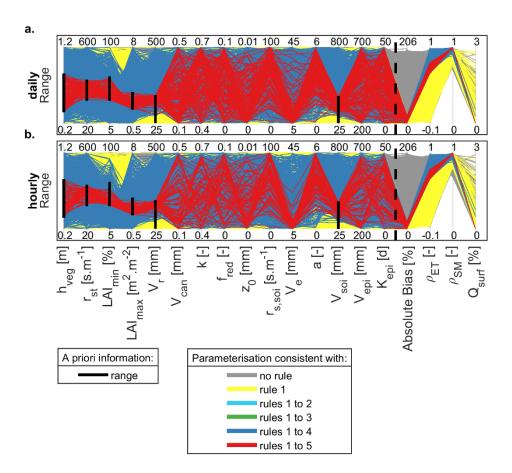


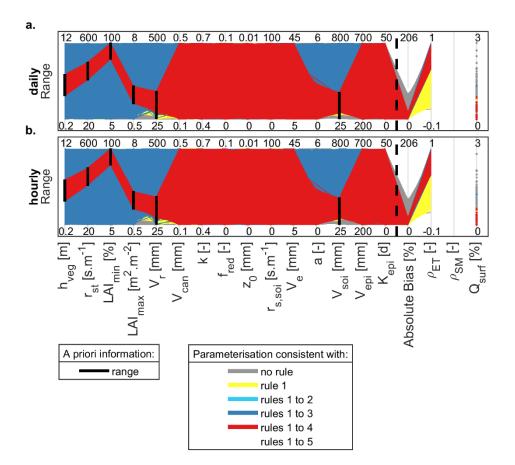
Figure S9. Reduction in the number of behavioural parameterisations of the V2Karst model at FLUXNET sites when applying sequentially the five soft rules defined in Sect. 4.1 (no rule: initial sample; rule 1: ET bias; rule 2: ET correlation; rule 3: soil moisture correlation; rule 4: runoff; rule 5: a priori information). Rule 3 could not be applied to the French 2 site where soil moisture observations are not available. (a) results for daily time step and (b) results for hourly time step.



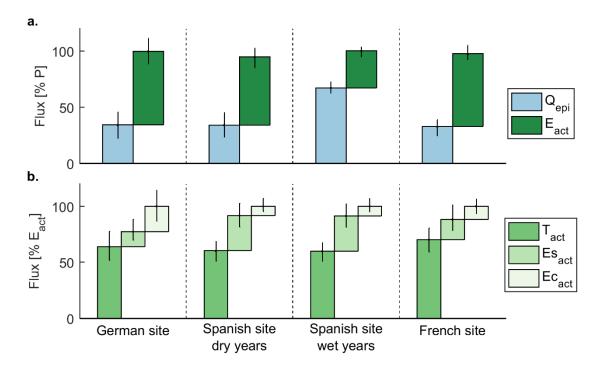
**Figure S10**. Parallel coordinate plots representing V2Karst behavioural parameterisations and their corresponding simulated output values, identified when sequentially applying the five soft rules defined in Sect. 4.1 at the German site for (a) daily time step and (b) hourly time step. Parameters are defined in Tables 1 and S11. *BIAS* absolute mean error between observed and simulated total actual ET (rule 1),  $\rho_{ET}$  correlation coefficient between observed and simulated total actual ET (rule 2),  $\rho_{SM}$  correlation coefficient between observed and simulated soil moisture (rule 3),  $Q_{surf}$  surface runoff (rule 4). Rule 5 corresponds to application of a priori information on parameter ranges (black vertical bars, Tables 3 and S12).



**Figure S11**. Parallel coordinate plots representing V2Karst behavioural parameterisations and their corresponding simulated output values, identified when sequentially applying the five soft rules defined in Sect. 4.1 **at the Spanish site** for (a) daily time step and (b) hourly time step. Parameters are defined in Table 1. *BIAS* absolute mean error between observed and simulated total actual ET (rule 1),  $\rho_{ET}$  correlation coefficient between observed and simulated total actual ET (rule 2),  $\rho_{SM}$  correlation coefficient between observed and simulated soil moisture (rule 3),  $Q_{surf}$  surface runoff (rule 4). Rule 5 corresponds to application of a priori information on parameter ranges (black vertical bars, Tables 3 and S12).



**Figure S12.** Parallel coordinate plots representing V2Karst behavioural parameterisations and their corresponding simulated output values, identified when sequentially applying the five soft rules defined in Sect. 4.1 **at the French 2 site** for (a) daily time step and (b) hourly time step. Parameters are defined in Tables 1 and S11. *BIAS* absolute mean error between observed and simulated total actual ET (rule 1),  $\rho_{ET}$  correlation coefficient between observed and simulated total actual ET (rule 2),  $\rho_{SM}$  correlation coefficient between observed and simulated soil moisture (rule 3),  $Q_{surf}$  surface runoff (rule 4). Rule 5 corresponds to application of a priori information on parameter ranges (black vertical bars, Tables 3 and S12).



**Figure S13**. Model outputs assessed using a <u>daily time step</u>: (a) Simulated recharge  $(Q_{epi})$  and actual ET  $(E_{act})$  expressed as a percentage of total precipitation and (b) simulated actual transpiration  $(T_{act})$ , actual soil evaporation  $(Es_{act})$  and actual evaporation from interception  $(Ec_{act})$  expressed as a percentage of  $E_{act}$ . The figure reports the ensemble mean and 95 % confidence intervals calculated over the behavioural simulation ensemble of the V2Karst model at the four FLUXNET sites. Simulated fluxes were evaluated over the period 1 January 2001–17 December 2009 for the German site, 1 January 2006–31 December 2008 for the Spanish site (dry years), 1 January 2009–30 December 2011 for the Spanish site (wet years), 1 January 2010–30 December 2011 for the French 1 site and 1 April 2003–31 March 2009 for the French 2 site. Mean annual water balance for behavioural set.

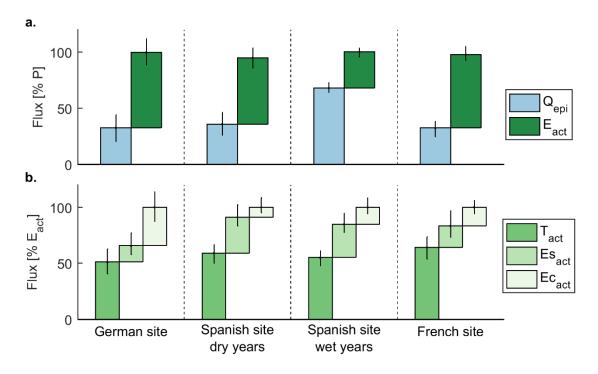
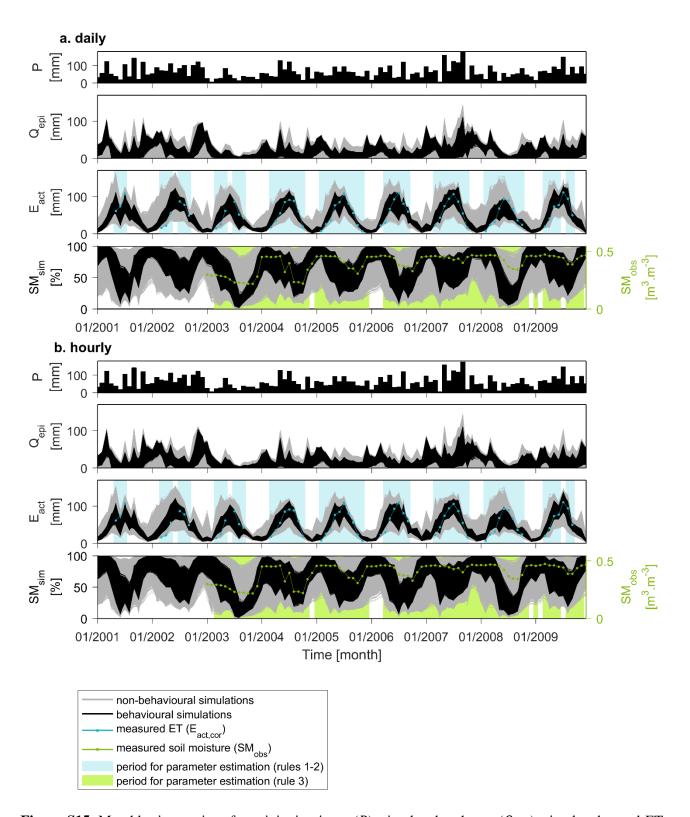
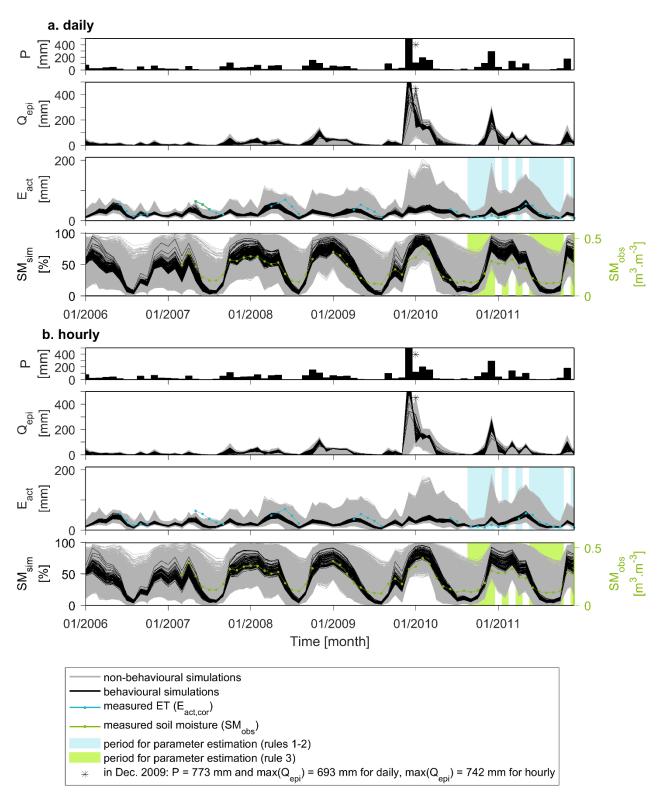


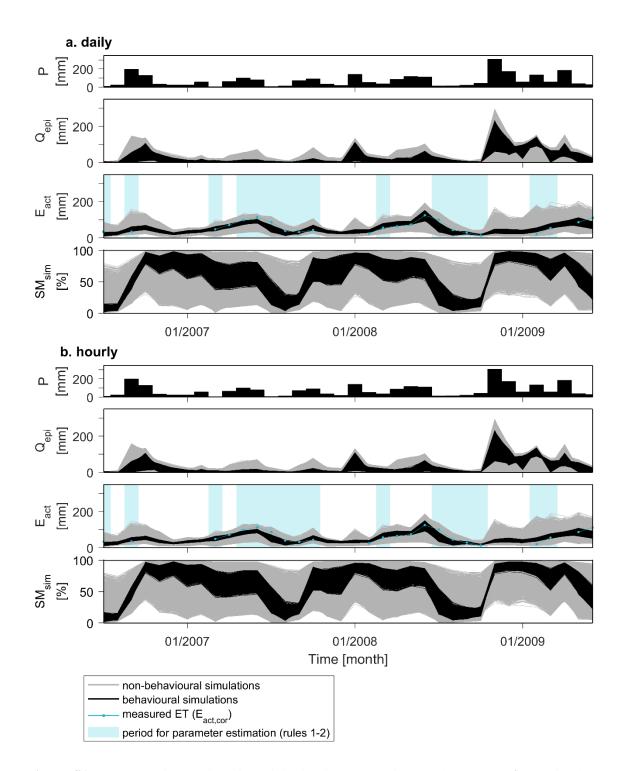
Figure S14. Same as Figure S13 but using an hourly time step.



**Figure S15**. Monthly time series of precipitation input (P), simulated recharge  $(Q_{epi})$ , simulated actual ET  $(E_{act})$ , which is the sum of evaporation from canopy interception, transpiration and soil evaporation), simulated soil moisture within the root zone  $(SM_{sim})$ , and monthly observations of actual ET and soil moisture at the **German site** for (a) daily time step, (b) hourly time step. Blue and green shaded areas correspond to the periods in which observation of ET and soil moisture respectively were selected to apply the soft rules of Sect. 4.1 (further details on data processing in Sect. 3.2, S4.1 and S4.2).



**Figure S16**. Monthly time series of precipitation input (P), simulated recharge  $(Q_{epi})$ , simulated actual ET  $(E_{act})$ , which is the sum of evaporation from canopy interception, transpiration and soil evaporation), simulated soil moisture within the root zone  $(SM_{sim})$ , and monthly observations of actual ET and soil moisture at the **Spanish site** for (a) daily time step, (b) hourly time step. Blue and green shaded areas correspond to the periods in which observation of ET and soil moisture respectively were selected to apply the soft rules of Sect. 4.1 (further details on data processing in Sect. 3.2, S4.1 and S4.2).



**Figure S17**. Monthly time series of precipitation input (P), simulated recharge  $(Q_{epi})$ , simulated actual ET  $(E_{act})$ , which is the sum of evaporation from canopy interception, transpiration and soil evaporation), simulated soil moisture within the root zone  $(SM_{sim})$ , and monthly observations of actual ET and soil moisture at the **German site** for (a) daily time step, (b) hourly time step. Blue and green shaded areas correspond to the periods in which observation of ET and soil moisture respectively were selected to apply the soft rules of Sect. 4.1 (further details on data processing in Sect. 3.2, S4.1 and S4.2).

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