



*Supplement of*

**Description and evaluation of the Multiscale Online Nonhydrostatic AtmospheRe CHemistry model (NMMB-MONARCH) version 1.0: gas-phase chemistry at global scale**

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## S1 Statistical Measures

There are several metrics that are used by the modeling community to evaluate performances of AQMs (U.S.EPA, 1991; Cox and Tikvart, 1990; Russell and Dennis, 2000). The statistical indicators selected in this study are: Correlation coefficient ( $r$ : Eq. 1) , Mean Bias (MB: Eq. 2) and Root Mean Square Error (RMSE: Eq.3).

$$r = \frac{1}{N} \frac{\sum_{i=1}^N (O_i - \bar{O})(P_i - \bar{P})}{\sigma_O \Delta \sigma_P} \quad (1)$$

$$MB = \frac{\sum_{i=1}^N (P_i - O_i)}{N} \quad (2)$$

$$RMSE = \sqrt{\frac{1}{N} \sum_{i=1}^N (P_i - O_i)^2} \quad (3)$$

where  $\sigma$  is the standard deviation and  $P$  and  $O$  denote the vector of model output and the vector observations, respectively. No threshold has been applied in the computation of the statistics.

## S2 Figures

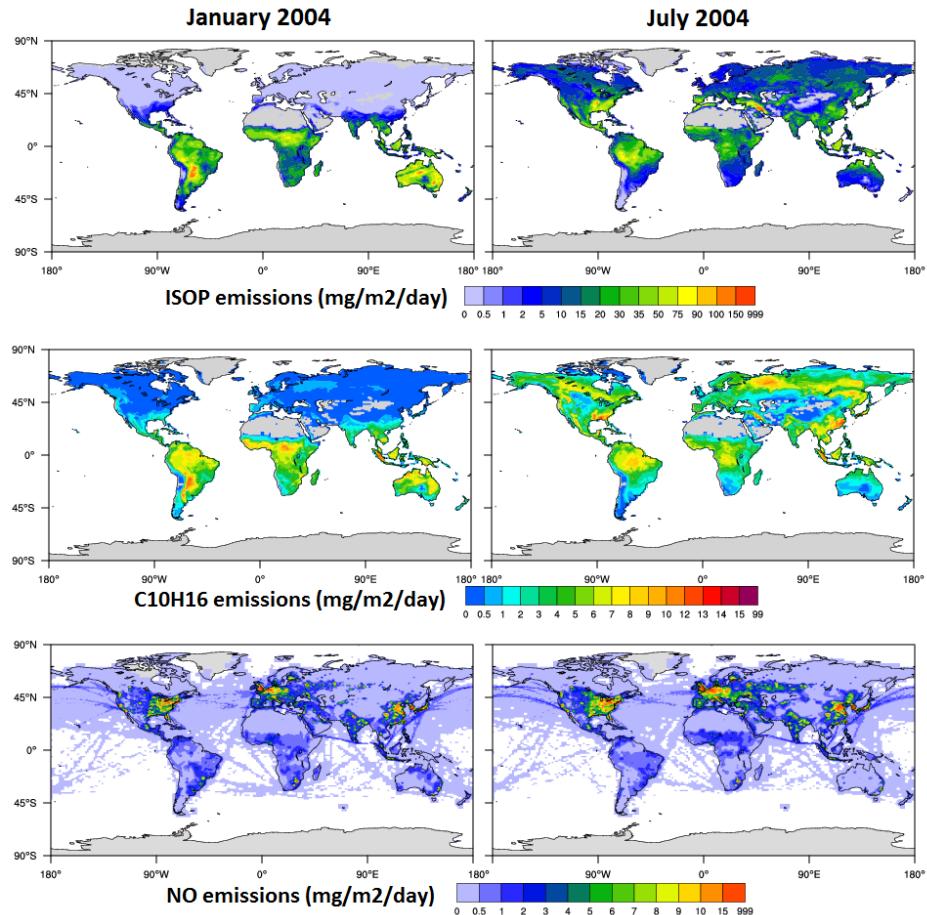


Figure S1: Biogenic emissions of isoprene (upper panel) and monoterpane (middle panel), from the on-line model MEGAN, and anthropogenic emissions of NO (lower panel), from ACCMIP inventory, for January and July 2004 used in this model simulation.

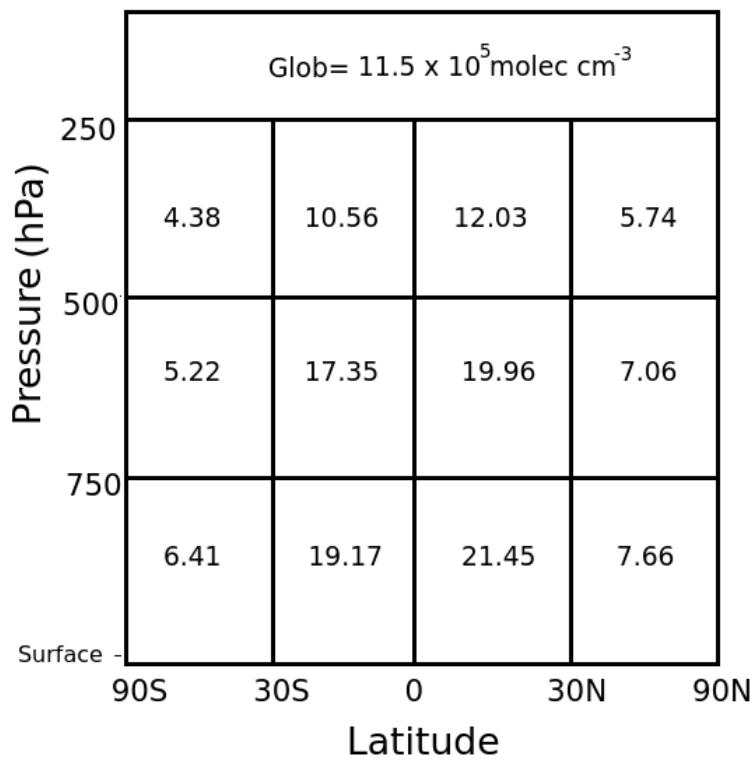


Figure S2: NMMB-MONARCH regional annual mean airmass-weighted OH concentrations (  $\times 10^5$  molecule cm $^{-3}$  ).

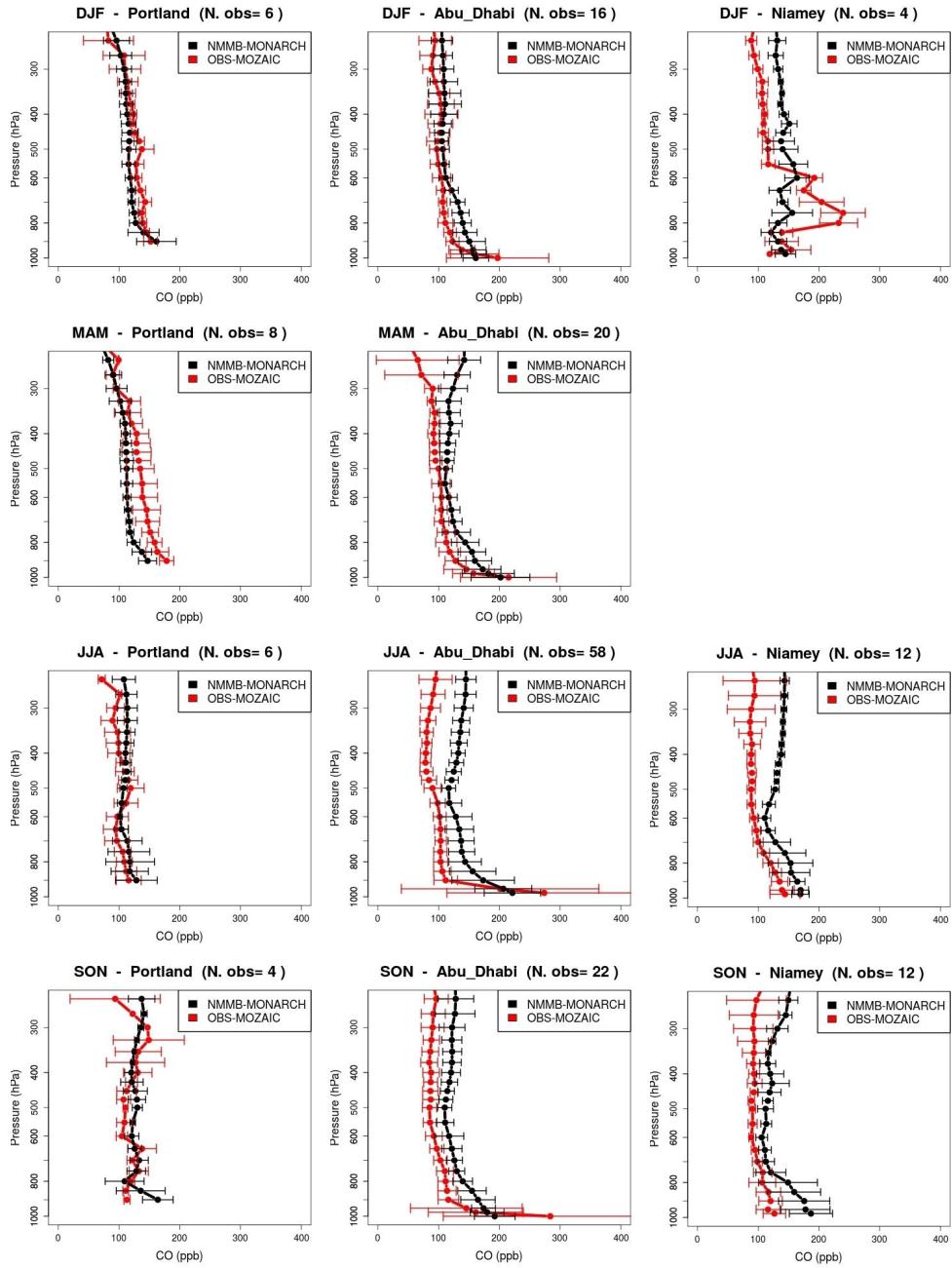


Figure S3: CO vertical profile seasonal averages over Portland, Abu Zabi and Niamey (from left to right) for year 2004. Observations depicted with a solid red line and model with a solid black line. The number of flights is provided on the top of each plot.

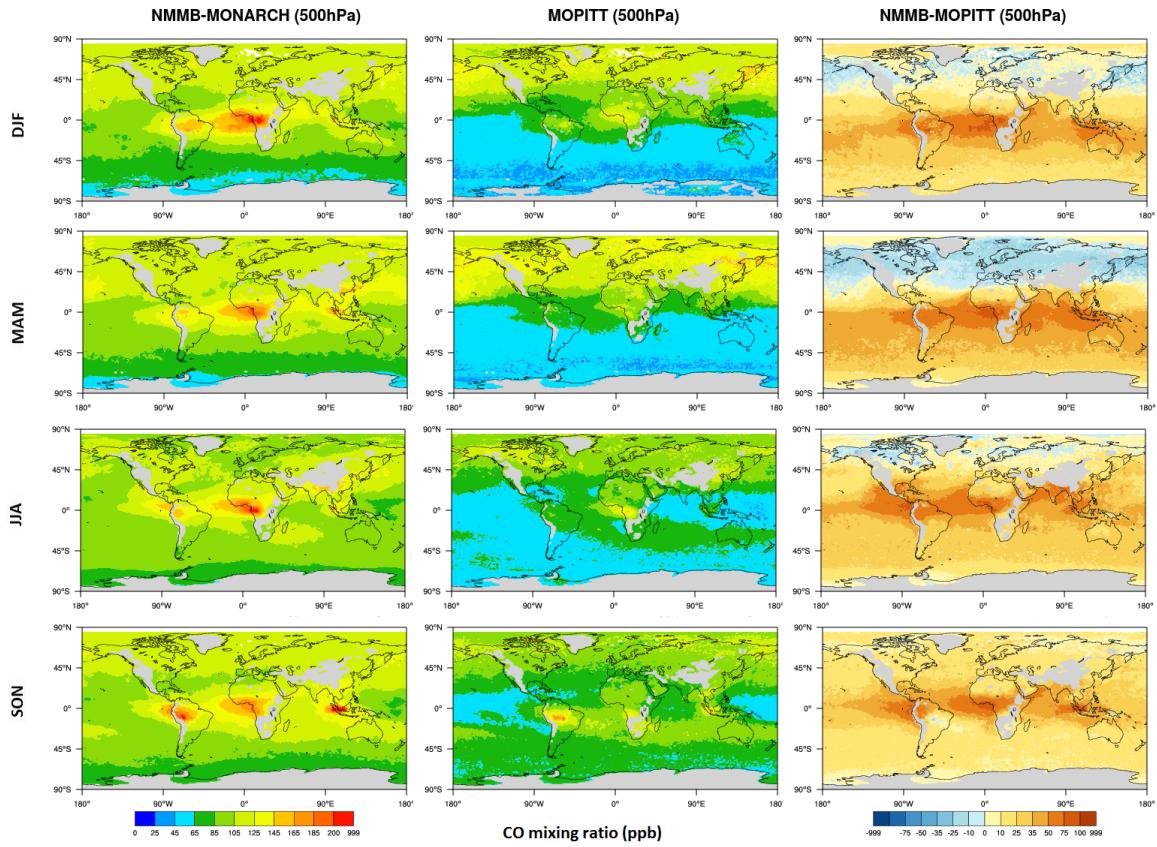


Figure S4: Comparison of modeled CO mixing ratio at 500 hPa against satellite data (MOPITT) in ppb. From top to bottom: DJF for December-January-February, MAM for March-April-May, JJA for June-July-August and SON for September-October-November for year 2004. NMMB-MONARCH data is displayed in the left panel, MOPITT data in the middle panel and the bias in the right panel.

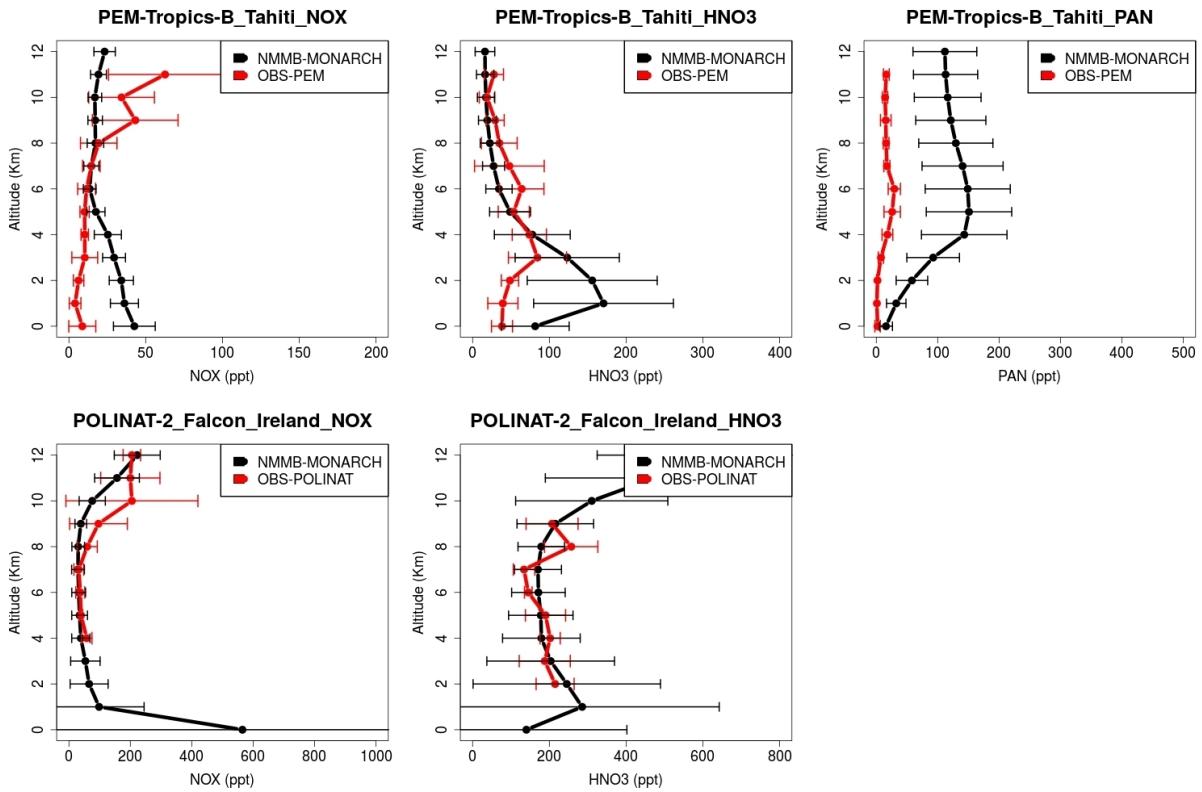


Figure S5: Comparison of modeled (black lines) and observed (red lines) vertical profiles of NO<sub>x</sub> (first column), HNO<sub>3</sub> (second column) and PAN (third column) over Tahiti and Ireland.

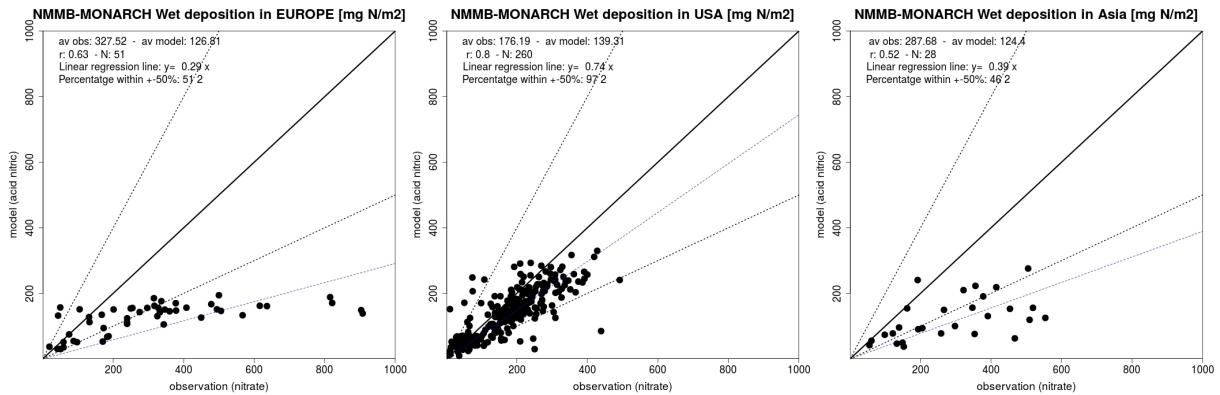


Figure S6: Scatter plots of the simulated  $\text{HNO}_3$  versus nitrate measurements for three networks: Europe (left panel), USA (middle panel) and Asia (right panel). Dashed lines have slopes equal to 2 and 0.5. The dotted line is the result of the linear regression fitting through the origin.

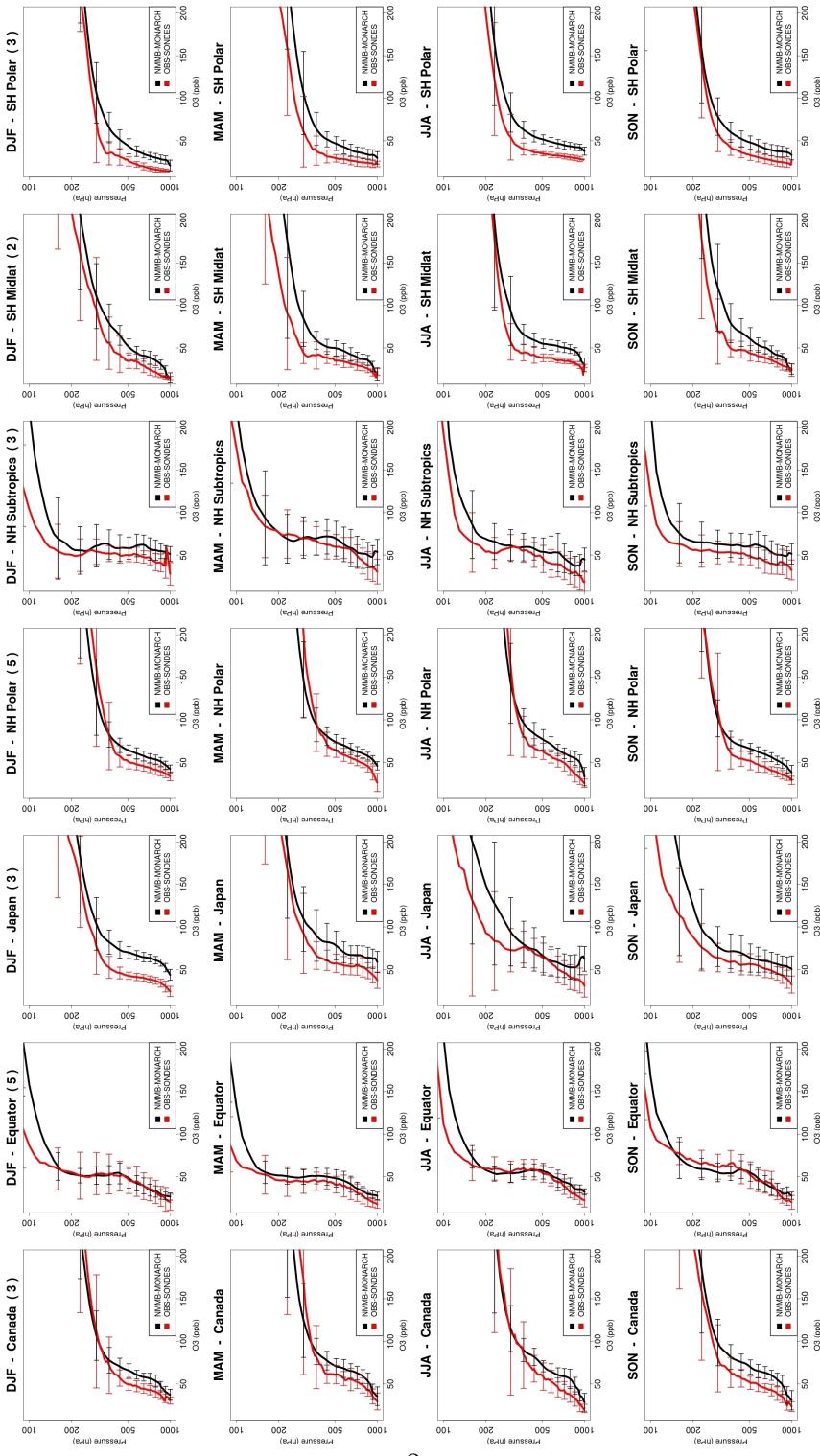


Figure S7: Comparison of ozonesonde measurements (red lines) and simulated (black lines) seasonal vertical profiles of  $O_3$  (ppb) and standard deviations (horizontal lines). The region name and the number of stations are given above each plot between brackets.

## S3 Tables

Table S1: The chemical trace species for the CB05 chemical mechanism included in gas-phase tropospheric chemistry version of NMMB-MONARCH.

Species name	Description	Species name	Description
NO	Nitric oxide	SO <sub>2</sub>	Sulfur dioxide
NO <sub>2</sub>	Nitrogen dioxide	MEO <sub>2</sub>	Methylperoxy radical
O <sub>3</sub>	Ozone	MEOH	Methanol
O	Oxygen atom in the O <sup>3</sup> (P) electronic state	MEPX	Methylhydroperoxide
O <sup>1</sup> D	Oxygen atom in the O <sup>1</sup> (D) electronic state	FACD	Formic acid
OH	Hydroxyl radical	ETHA	Ethane
HO <sub>2</sub>	Hydroperoxy radical	ROOH	Higher organic peroxide
H <sub>2</sub> O <sub>2</sub>	Hydrogen peroxide	AACD	Acetic and higher carboxylic acids
NO <sub>3</sub>	Nitrate radical	PACD	Peroxyacetic and higher peroxycarboxylic acids
N <sub>2</sub> O <sub>5</sub>	Dinitrogen pentoxide	PAR	Paraffin carbon bond (C-C)
HONO	Nitrous acid	ROR	Secondary alkoxy radical
HNO <sub>3</sub>	Nitric acid	ETH	Ethene
PNA	Peroxynitric acid (HNO <sub>4</sub> )	OLE	Terminal olefin carbon bond (R-C=C)
CO	Carbon monoxide	IOLE	Internal olefin carbon bond (R-C=C-R)
FORM	Formaldehyde	ISOP	Isoprene
ALD2	Acetaldehyde	ISPD	Isoprene product (lumped methacrolein, methyl vinyl ketone, etc.)
C <sub>2</sub> O <sub>3</sub>	Acetylperoxy radical	TERP	Terpene
PAN	Peroxyacetyl nitrate	TOL	Toluene and other monoalkyl aromatics
ALDX	Propionaldehyde and higher aldehydes	XYL	Xylene and other polyalkyl aromatics
CXO <sub>3</sub>	C <sub>3</sub> and higher acylperoxy radicals	CRES	Cresol and higher molecular weight phenols
PANX	C <sub>3</sub> and higher peroxyacetyl nitrates	TO <sub>2</sub>	Toluene-hydroxyl radical adduct
XO <sub>2</sub>	NO to NO <sub>2</sub> conversion from alkylperoxy (RO <sub>2</sub> ) radical	OPEN	Aromatic ring opening product
XO <sub>2</sub> N	NO to organic nitrate conversion from alkylperoxy (RO <sub>2</sub> ) radical	CRO	Methylphenoxy radical
NTR	Organic nitrate (RNO <sub>3</sub> )	MGLY	Methylglyoxal and other aromatic products
ETOH	Ethanol		
SULF	Sulfuric acid (gaseous)		

Table S2: The gas-phase CB05 chemical mechanism reactions applied in the NMMB-MONARCH. The first column describes the reactants, the second the products and the third displays the coefficients to compute the full rate expressions for each reaction.

Reactants	Products	Rate expression
O + O <sub>2</sub> + M	→ O <sub>3</sub> + M	6.0E-34*(300/T) <sup>2.4</sup>
O <sub>3</sub> + NO	→ NO <sub>2</sub>	3.0E-12*exp(T/1500)
O + NO <sub>2</sub>	→ NO	5.6E-12*exp(180/T)
O + NO <sub>2</sub>	→ NO <sub>3</sub>	K <sub>0</sub> = 2.5E-31*exp(300/T) <sup>1.8</sup> K <sub>∞</sub> = 2.2E-11*exp(300/T) <sup>0.7</sup>
O + NO	→ NO <sub>2</sub>	K <sub>0</sub> = 9.0E-32*exp(300/T) <sup>1.5</sup> K <sub>∞</sub> = 3.0E-11
NO <sub>2</sub> + O <sub>3</sub>	→ NO <sub>3</sub>	1.2E-13*exp(T/2450)
O( <sup>1</sup> D) + M	→ O + M	2.1E-11*exp(102/T)
O( <sup>1</sup> D) + H <sub>2</sub> O	→ 2.000*OH	2.2E-10
O <sub>3</sub> + OH	→ HO <sub>2</sub>	1.7E-12*exp(T/940)
O <sub>3</sub> + HO <sub>2</sub>	→ OH	1.0E-14*exp(T/490)
NO <sub>3</sub> + NO	→ 2.000*NO <sub>2</sub>	1.5E-11*exp(170/T)
NO <sub>3</sub> + NO <sub>2</sub>	→ NO + NO <sub>2</sub>	4.5E-14*exp(T/1260)
NO <sub>3</sub> + NO <sub>2</sub>	→ N <sub>2</sub> O <sub>5</sub>	K <sub>0</sub> = 2.0E-30 *(300/T) <sup>4.4</sup> K <sub>∞</sub> = 1.4E-12*(300/T) <sup>0.7</sup>
N <sub>2</sub> O <sub>5</sub> + H <sub>2</sub> O	→ 2.000*HNO <sub>3</sub>	2.5E-22
N <sub>2</sub> O <sub>5</sub> + H <sub>2</sub> O + H <sub>2</sub> O	→ 2.000*HNO <sub>3</sub>	1.8E-39
N <sub>2</sub> O <sub>5</sub>	→ NO <sub>3</sub> + NO <sub>2</sub>	K <sub>0</sub> = 1.0E-03*exp(11000/T) <sup>3.5</sup> K <sub>∞</sub> = 9.7E+14*exp(T/11080) <sup>0.1</sup> F <sub>c</sub> = 0.45 n= 1.0
NO + NO + O <sub>2</sub>	→ 2.000*NO <sub>2</sub>	3.3E-39*exp(530/T)
NO + NO <sub>2</sub> + H <sub>2</sub> O	→ 2.000*HONO	5.0E-40
NO + OH	→ HONO	7.0E-31*exp(300/T) <sup>2.6</sup> 3.6E-11*exp(300/T)-0.1
OH + HONO	→ NO <sub>2</sub>	1.8E-11*exp(T/390)
HONO + HONO	→ NO + NO <sub>2</sub>	1.0E-20
NO <sub>2</sub> + OH	→ HNO <sub>3</sub>	K <sub>0</sub> = 2.0E-30*exp(300/T) <sup>3.0</sup> K <sub>∞</sub> = 2.5E-11
OH+ HNO <sub>3</sub>	→ NO <sub>3</sub>	K <sub>0</sub> = 2.4E-14*exp(460/T) K <sub>2</sub> = 2.7E-17*exp(2199/T) K <sub>3</sub> = 6.5E-34*exp(1335/T)
HO <sub>2</sub> + NO	→ OH + NO <sub>2</sub>	K <sub>0</sub> = 3.5E-12*exp(250/T)
HO <sub>2</sub> + NO <sub>2</sub>	→ PNA	K <sub>0</sub> = 1.8E-31*exp(300/T) <sup>3.2</sup> K <sub>∞</sub> = 4.7E-12 F <sub>c</sub> = 0.6
PNA	→ HO <sub>2</sub> +NO <sub>2</sub>	K <sub>0</sub> = 4.1E-5*exp(T/10650) K <sub>∞</sub> = 4.8E15*exp(T/11170) F <sub>c</sub> = 0.6
OH + PNA	→ NO <sub>2</sub>	1.3E-12*exp(380/T)
HO <sub>2</sub> + HO <sub>2</sub>	→ H <sub>2</sub> O <sub>2</sub>	K <sub>1</sub> = 2.3E-13*exp(600/T) K <sub>2</sub> = 1.7E-33*exp(1000/T)
HO <sub>2</sub> +HO <sub>2</sub> +H <sub>2</sub> O	→ H <sub>2</sub> O <sub>2</sub>	K <sub>1</sub> = 3.22E-34*exp(2800/T) K <sub>2</sub> = 2.38E-54*exp(3200/T)

Table S2: Continued from previous page

Reactants	Products	Rate expression
OH + H <sub>2</sub> O <sub>2</sub>	HO <sub>2</sub>	2.9E-12*exp(T/160)
O <sup>1</sup> D + H <sub>2</sub>	OH + HO <sub>2</sub>	1.1E-10
OH + H <sub>2</sub>	HO <sub>2</sub>	5.5E-12*exp(T/2000)
OH + O	HO <sub>2</sub>	2.2E-11*exp(120/T)
OH + OH	O	4.2E-12*exp(T/240)
OH + OH	H <sub>2</sub> O <sub>2</sub>	K <sub>0</sub> =6.9E-31*exp(300/T) <sup>1.0</sup> K <sub>∞</sub> =2.6E-11
OH + HO <sub>2</sub>	→	4.8E-11*exp(250/T)
HO <sub>2</sub> + O	OH	3.0E-11*exp(200/T)
H <sub>2</sub> O <sub>2</sub> + O	OH + HO <sub>2</sub>	1.4E-12*exp(-2000/T)
NO <sub>3</sub> + O	NO <sub>2</sub>	1.0E-11
NO <sub>3</sub> + OH	HO <sub>2</sub> + NO <sub>2</sub>	2.2E-11
NO <sub>3</sub> + HO <sub>2</sub>	HNO <sub>3</sub>	3.5E-12
NO <sub>3</sub> + O <sub>3</sub>	NO <sub>2</sub>	1.0E-17
NO <sub>3</sub> + NO <sub>3</sub>	2.000*NO <sub>2</sub>	8.5E-13*exp(T/2450)
XO <sub>2</sub> + NO	NO <sub>2</sub>	2.6E-12*exp(365/T)
XO <sub>2</sub> N + NO	NTR	2.6E-12*exp(365/T)
XO <sub>2</sub> + HO <sub>2</sub>	ROOH	7.5E-13*exp(700/T)
XO <sub>2</sub> N + HO <sub>2</sub>	ROOH	7.5E-13*exp(700/T)
XO <sub>2</sub> + XO <sub>2</sub>	→	6.8E-14
XO <sub>2</sub> N + XO <sub>2</sub> N	→	6.8E-14
XO <sub>2</sub> + XO <sub>2</sub> N	→	6.8E-14
NTR + OH	HNO <sub>3</sub> + HO <sub>2</sub> + 0.330*FORM+	5.9E-13*exp(360/T)
ROOH + OH	XO <sub>2</sub> + 0.500*ALD2 + 0.500*ALDX	3.01E-12*exp(190/T)
OH + CO	HO <sub>2</sub>	K <sub>1</sub> = 1.44E-13 K <sub>2</sub> =3.43E-33
OH + CH <sub>4</sub>	MEO <sub>2</sub>	2.45E-12*exp(T/1775)
MEO <sub>2</sub> + NO	FORM + HO <sub>2</sub> + NO <sub>2</sub>	2.8E-12*exp(300/T)
MEO <sub>2</sub> + HO <sub>2</sub>	MEPX	4.1E-13*exp(750/T)
MEO <sub>2</sub> + MEO <sub>2</sub>	1.370*FORM+ 0.740*HO <sub>2</sub> + 0.630*MEOH	9.5E-14*exp(390/T)
MEPX + OH	0.700*MEO <sub>2</sub> + 0.300*XO <sub>2</sub> + 0.300*HO <sub>2</sub>	3.8E-12*exp(200/T)
MEOH + OH	FORM + HO <sub>2</sub>	7.3E-12*exp(T/620)
FORM + OH	HO <sub>2</sub> + CO	9.0E-12
FORM + O	OH + HO <sub>2</sub> + CO	3.4E-11*exp(T/1600)
FORM + NO <sub>3</sub>	HNO <sub>3</sub> +HO <sub>2</sub> + CO	5.8E-16
FORM + HO <sub>2</sub>	HCO <sub>3</sub>	9.7E-15*exp(625/T)
HCO <sub>3</sub>	FORM + HO <sub>2</sub>	2.4E+12*exp(T/7000)
HCO <sub>3</sub> + NO	FACD+ NO <sub>2</sub> + HO <sub>2</sub>	5.6E-12
HCO <sub>3</sub> + HO <sub>2</sub>	MEPX	5.6E-15*exp(2300/T)
FACD + OH	HO <sub>2</sub>	4.0E-13
ALD2 + O	C <sub>2</sub> O <sub>3</sub> + OH	1.8E-11*exp(T/1100)
ALD2 + OH	C <sub>2</sub> O <sub>3</sub>	5.6E-12*exp(270/T)
ALD2 + NO <sub>3</sub>	C <sub>2</sub> O <sub>3</sub> + HNO <sub>3</sub>	1.4E-12*exp(T/1900)
C <sub>2</sub> O <sub>3</sub> + NO	MEO <sub>2</sub> + NO <sub>2</sub>	8.1E-12*exp(270/T)
PAN	C <sub>2</sub> O <sub>3</sub> + NO <sub>2</sub>	K <sub>0</sub> = 4.9E-3*exp(12100/T) K <sub>∞</sub> = 5.4E16*exp(T/13830) F <sub>c</sub> =0.3
C <sub>2</sub> O <sub>3</sub> + HO <sub>2</sub>	0.800*PACD+ 0.200*AACD+ 0.200*O <sub>3</sub>	4.3E-13*exp(1040/T)
C <sub>2</sub> O <sub>3</sub> + MEO <sub>2</sub>	0.900*MEO <sub>2</sub> + 0.900*HO <sub>2</sub> + FORM+ 0.100*AACD	2.0E-12*exp(500/T)

Table S2: Continued from previous page

Reactants	Products	Rate expression
$\text{C}_2\text{O}_3 + \text{XO}_2$	$\rightarrow 0.900*\text{MEO}_2 + 0.100*\text{AACD}$	$4.4\text{E}-13*\exp(1070/\text{T})$
$\text{C}_2\text{O}_3 + \text{C}_2\text{O}_3$	$\rightarrow 2.000*\text{MEO}_2$	$2.9\text{E}-12*\exp(500/\text{T})$
$\text{PACD} + \text{OH}$	$\rightarrow \text{C}_2\text{O}_3$	$4.0\text{E}-13*\exp(200/\text{T})$
$\text{AACD} + \text{OH}$	$\rightarrow \text{MEO}_2$	$4.0\text{E}-13*\exp(200/\text{T})$
$\text{ALDX} + \text{O}$	$\rightarrow \text{CXO}_3 + \text{OH}$	$1.3\text{E}-11*\exp(\text{T}/870)$
$\text{ALDX} + \text{OH}$	$\rightarrow \text{CXO}_3$	$5.1\text{E}-12*\exp(405/\text{T})$
$\text{ALDX} + \text{NO}_3$	$\rightarrow \text{CXO}_3 + \text{HNO}_3$	$6.5\text{E}-15$
$\text{CXO}_3 + \text{NO}$	$\rightarrow \text{ALD2} + \text{NO}_2 + \text{HO}_2 + \text{XO}_2$	$6.7\text{E}-12*\exp(340/\text{T})$
$\text{CXO}_3 + \text{NO}_2$	$\rightarrow \text{PANX}$	$K_0=2.7\text{E}-28*\exp(300/\text{T})^{7.1}$ $K_\infty=1.2\text{E}-11*\exp(300/\text{T})^{0.9}$ $F_c=0.3$
$\text{PANX}$	$\rightarrow \text{CXO}_3 + \text{NO}_2$	
$\text{PANX} + \text{OH}$	$\rightarrow \text{ALD2} + \text{NO}_2$	$3.0\text{E}-13$
$\text{CXO}_3 + \text{HO}_2$	$\rightarrow 0.800*\text{PACD} + 0.200*\text{AACD} + 0.200*\text{O}_3$	$4.3\text{E}-13*\exp(1040/\text{T})$
$\text{CXO}_3 + \text{MEO}_2$	$\rightarrow 0.900*\text{ALD2} + 0.900*\text{XO}_2 + \text{HO}_2 +$	$2.0\text{E}-12*\exp(500/\text{T})$
$\text{CXO}_3 + \text{XO}_2$	$\rightarrow 0.100*\text{AACD} + 0.100*\text{FORM}$	
$\text{CXO}_3 + \text{CXO}_3$	$\rightarrow 0.900*\text{ALD2} + 0.100*\text{AACD}$	$4.4\text{E}-13*\exp(1070/\text{T})$
$\text{CXO}_3 + \text{C}_2\text{O}_3$	$\rightarrow 2.000*\text{ALD2} + 2.000*\text{XO}_2 + 2.000*\text{HO}_2$	$2.9\text{E}-12*\exp(500/\text{T})$
$\text{PAR} + \text{OH}$	$\rightarrow \text{MEO}_2 + \text{XO}_2 + \text{HO}_2 + \text{ALD2}$	$2.9\text{E}-12*\exp(500/\text{T})$
	$0.870*\text{XO}_2 + 0.130*\text{XO}_2\text{N} + 0.110*\text{HO}_2 +$	
	$0.060*\text{ALD2} - 0.110*\text{PAR} + 0.760*\text{ROR} +$	$8.1\text{E}-13$
	$0.050*\text{ALDX}$	
	$0.960*\text{XO}_2 + 0.600*\text{ALD2} + 0.940*\text{HO}_2 -$	
$\text{ROR}$	$\rightarrow 2.100*\text{PAR} + 0.040*\text{XO}_2\text{N} + 0.020*\text{ROR} +$	$1.\text{E}+15*\exp(\text{T}/8000)$
	$0.500*\text{ALDX}$	
$\text{ROR}$	$\rightarrow \text{HO}_2$	$1.6\text{E}+3$
$\text{ROR} + \text{NO}_2$	$\rightarrow \text{NTR}$	$1.5\text{E}-11$
	$0.200*\text{ALD2} + 0.300*\text{ALDX} + 0.300*\text{HO}_2 +$	
$\text{O} + \text{OLE}$	$\rightarrow 0.200*\text{XO}_2 + 0.200*\text{CO} + 0.200*\text{FORM} +$	$1.\text{E}-11*\exp(\text{T}/280)$
	$0.010*\text{XO}_2\text{N} + 0.200*\text{PAR} + 0.100*\text{OH}$	
	$0.800*\text{FORM} + 0.330*\text{ALD2} +$	
$\text{OH} + \text{OLE}$	$\rightarrow 0.620*\text{ALDX} + 0.800*\text{XO}_2 + 0.950*\text{HO}_2 -$	$3.2\text{E}-11$
	$0.700*\text{PAR}$	
	$0.180*\text{ALD2} + 0.740*\text{FORM} +$	
$\text{O}_3 + \text{OLE}$	$\rightarrow 0.320*\text{ALDX} + 0.220*\text{XO}_2 + 0.100*\text{OH} +$	$6.5\text{E}-15*\exp(\text{T}/1900)$
	$0.330*\text{CO} + 0.440*\text{HO}_2 - 1.000*\text{PAR}$	
$\text{NO}_3 + \text{OLE}$	$\rightarrow \text{NO}_2 + \text{FORM} + 0.910*\text{XO}_2 + 0.090*\text{XO}_2\text{N} +$	$7.0\text{E}-13*\exp(\text{T}/2160)$
	$0.560*\text{ALDX} + 0.350*\text{ALD2} - 1.000*\text{PAR}$	
$\text{O} + \text{ETH}$	$\rightarrow \text{FORM} + 1.700*\text{HO}_2 + \text{CO} + 0.700*\text{XO}_2 +$	$1.04\text{E}-11*\exp(\text{T}/792)$
$\text{OH} + \text{ETH}$	$\rightarrow \text{XO}_2 + 1.560*\text{FORM} + 0.220*\text{ALDX} + \text{HO}_2$	$K_0=1.0\text{E}-28*\exp(300/\text{T})^{0.8}$ $K_\infty=8.8\text{E}-12$
$\text{O}_3 + \text{ETH}$	$\rightarrow \text{FORM} + 0.630*\text{CO} + 0.130*\text{HO}_2 +$	$1.2\text{E}-14*\exp(\text{T}/2630)$
$\text{NO}_3 + \text{ETH}$	$\rightarrow \text{NO}_2 + \text{XO}_2 + 2.0*\text{FORM}$	$3.3\text{E}-12*\exp(\text{T}/2880)$
$\text{IOLE} + \text{O}$	$\rightarrow 1.240*\text{ALD2} + 0.660*\text{ALDX} + 0.100*\text{HO}_2 +$	$2.3\text{E}-11$
$\text{IOLE} + \text{OH}$	$0.100*\text{XO}_2 + 0.100*\text{CO} + 0.100*\text{PAR}$	
$\text{IOLE} + \text{O}_3$	$\rightarrow 1.300*\text{ALD2} + 0.700*\text{ALDX} + \text{HO}_2 + \text{XO}_2$	$1.0\text{E}-11*\exp(550/\text{T})$
	$0.650*\text{ALD2} + 0.350*\text{ALDX} +$	
	$0.250*\text{FORM} + 0.250*\text{CO} + 0.500*\text{O}$	$8.4\text{E}-15*\exp(\text{T}/1100)$
	$+ 0.500*\text{OH} + 0.500*\text{HO}_2$	

Table S2: Continued from previous page

Reactants	Products	Rate expression
IOLE + NO <sub>3</sub>	$1.180^*\text{ALD2} + 0.640^*\text{ALDX} + \text{HO}_2 + \text{NO}_2$ $0.440^*\text{HO}_2 + 0.080^*\text{XO}_2 + 0.360^*\text{CRES} +$	$9.6\text{E-13}^*\exp(\text{T}/270)$
TOL + OH	$0.560^*\text{TO}_2 + 0.765^*\text{TOLRO}_2$ $0.900^*\text{NO}_2 + 0.900^*\text{HO}_2 + 0.900^*\text{OPEN} +$	$1.8\text{E-12}^*\exp(355/\text{T})$
TO <sub>2</sub> + NO	$0.100^*\text{NTR}$	$8.1\text{E-12}$
TO <sub>2</sub>	CRES + HO <sub>2</sub>	4.2
OH + CRES	$0.400^*\text{CRO} + 0.600^*\text{XO}_2 + 0.600^*\text{HO}_2 +$ $0.300^*\text{OPEN}$	$4.1\text{E-11}$
CRES + NO <sub>3</sub>	CRO + HNO <sub>3</sub>	2.2E-11
CRO + NO <sub>2</sub>	NTR	1.4E-11
CRO + HO <sub>2</sub>	CRES	5.5E-12
OPEN + OH	$\text{XO}_2 + 2.000^*\text{CO} + 2.000^*\text{HO}_2 + \text{C}_2\text{O}_3 +$ FORM $0.030^*\text{ALDX} + 0.620^*\text{C}_2\text{O}_3 +$	$3.0\text{E-11}$
OPEN + O <sub>3</sub>	$0.700^*\text{FORM} + 0.030^*\text{XO}_2 + 0.690^*\text{CO} +$ $0.080^*\text{OH} + 0.760^*\text{HO}_2 + 0.200^*\text{MGLY}$ $0.700^*\text{HO}_2 + 0.500^*\text{XO}_2 + 0.200^*\text{CRES} +$	$5.4\text{E-17}^*\exp(\text{T}/500)$
OH + XYL	$0.800^*\text{MGLY} + 1.100^*\text{PAR} + 0.300^*\text{TO}_2 +$ $0.804^*\text{XYLRO}_2$	$1.7\text{E-11}^*\exp(116/\text{T})$
OH + MGLY	XO <sub>2</sub> + C <sub>2</sub> O <sub>3</sub>	1.8E-11
O + ISOP	$0.750^*\text{ISPD} + 0.500^*\text{FORM} + 0.250^*\text{XO}_2$ $+ 0.250^*\text{HO}_2 + 0.250^*\text{CXO}_3 + 0.250^*\text{PAR}$	3.6E-11
OH + ISOP	$0.912^*\text{ISPD} + 0.629^*\text{FORM} + 0.991^*\text{XO}_2$ $+ 0.912^*\text{HO}_2 + 0.089^*\text{XO}_2\text{N} + \text{ISOPRXN}$ $0.650^*\text{ISPD} + 0.600^*\text{FORM} + 0.200^*\text{XO}_2$	$2.54\text{E-11}^*\exp(407.6/\text{T})$
O <sub>3</sub> + ISOP	$+ 0.066^*\text{HO}_2 + 0.266^*\text{OH} + 0.200^*\text{CXO}_3 +$ $0.150^*\text{ALDX} + 0.350^*\text{PAR} + 0.066^*\text{CO}$ $0.200^*\text{ISPD} + 0.800^*\text{NTR} + \text{XO}_2 +$	$7.86\text{E-15}^*\exp(\text{T}/1912)$
NO <sub>3</sub> + ISOP	$0.800^*\text{HO}_2 + 0.200^*\text{NO}_2 + 0.800^*\text{ALDX} +$ $2.400^*\text{PAR}$ $1.565^*\text{PAR} + 0.167^*\text{FORM} + 0.713^*\text{XO}_2 +$	$3.03\text{E-12}^*\exp(\text{T}/448)$
OH + ISPD	$0.503^*\text{HO}_2 + 0.334^*\text{CO} + 0.168^*\text{MGLY} +$ $0.252^*\text{ALD2} + 0.210^*\text{C}_2\text{O}_3 + 0.250^*\text{CXO}_3$ $+ 0.120^*\text{ALDX}$ $0.114^*\text{C}_2\text{O}_3 + 0.150^*\text{FORM} +$	3.36E-11
O <sub>3</sub> + ISPD	$0.850^*\text{MGLY} + 0.154^*\text{HO}_2 + 0.268^*\text{OH} +$ $0.064^*\text{XO}_2 + 0.020^*\text{ALD2} + 0.360^*\text{PAR} +$ $0.225^*\text{CO}$ $0.357^*\text{ALDX} + 0.282^*\text{FORM} + 1.282^*\text{PAR}$	$7.1\text{E-18}$
NO <sub>3</sub> + ISPD	$+ 0.925^*\text{HO}_2 + 0.643^*\text{CO} + 0.850^*\text{NTR} +$ $0.075^*\text{CXO}_3 + 0.075^*\text{XO}_2 + 0.150^*\text{HNO}_3$	1.0E-15
TERP + O	$0.150^*\text{ALDX} + 5.12^*\text{PAR} + \text{TRPRXN}$ $0.750^*\text{HO}_2 + 1.250^*\text{XO}_2 + 0.250^*\text{XO}_2\text{N} +$	3.6E-11
TERP + OH	$0.280^*\text{FORM} + 1.66^*\text{ PAR} + 0.470^*\text{ALDX}$ + TRPRXN $0.570^*\text{OH} + 0.070^*\text{HO}_2 + 0.760^*\text{XO}_2 +$	$1.5\text{E-11}^*\exp(449/\text{T})$
TERP + O <sub>3</sub>	$0.180^*\text{XO}_2\text{N} + 0.240^*\text{FORM} + 0.001^*\text{CO} +$ $7.000^*\text{PAR} + 0.210^*\text{ALDX} + 0.390^*\text{CXO}_3$ + TRPRXN	$1.2\text{E-15}^*\exp(\text{T}/821)$
TERP + NO <sub>3</sub>	$0.470^*\text{NO}_2 + 0.280^*\text{HO}_2 + 1.030^*\text{XO}_2 +$ $0.250^*\text{XO}_2\text{N} + 0.470^*\text{ALDX} + 0.530^*\text{NTR}$ + TRPRXN	$3.7\text{E-12}^*\exp(175/\text{T})$

Table S2: Continued from previous page

<b>Reactants</b>	<b>Products</b>	<b>Rate expression</b>
SO <sub>2</sub> + OH	→ SULF + HO <sub>2</sub> + SULRXN	K <sub>0</sub> = 3.0E-31*exp(300/T) <sup>3.3</sup> K <sub>∞</sub> = 1.5E-12
OH + ETOH	→ HO <sub>2</sub> + 0.900*ALD2 + 0.050*ALDX + 0.100*FORM + 0.100*XO <sub>2</sub>	6.9E-12*exp(T/230)
OH + ETHA	→ 0.991*ALD2 + 0.991*XO <sub>2</sub> + 0.009*XO <sub>2</sub> N + HO <sub>2</sub> + 0.200*ISPD + 0.800*NTR + XO <sub>2</sub> +	8.7E-12*exp(T/1070)
NO <sub>2</sub> + ISOP	→ 0.800*HO <sub>2</sub> + 0.200*NO + 0.800*ALDX + 2.400*PAR	1.5E-19

Table S3: Photolysis reactions applied in the NMMB-MONARCH.

Reactants	Products
NO <sub>2</sub> +hv	→ NO + O
O <sub>3</sub> +hv	→ O
O <sub>3</sub> +hv	→ O <sup>1</sup> D
NO <sub>3</sub> +hv	→ NO <sub>2</sub> + O
NO <sub>3</sub> +hv	→ NO
HONO +hv	→ NO + OH
H <sub>2</sub> O <sub>2</sub> +hv	→ 2.000*OH
PNA +hv	→ 0.610*HO <sub>2</sub> + 0.610*NO <sub>2</sub> + 0.390*OH+
	0.390*NO <sub>3</sub>
HNO <sub>3</sub> +hv	→ OH + NO <sub>2</sub>
N <sub>2</sub> O <sub>5</sub> +hv	→ NO <sub>2</sub> + NO <sub>3</sub>
NTR +hv	→ NO <sub>2</sub> + HO <sub>2</sub> + 0.330*FORM+ 0.330*ALD2+
	0.330*ALDX- 0.660*PAR
FORM +hv	→ 2.000*HO <sub>2</sub> + CO
FORM +hv	→ CO
ALD2 +hv	→ MEO <sub>2</sub> + CO + HO <sub>2</sub>
PAN +hv	→ C <sub>2</sub> O <sub>3</sub> + NO <sub>2</sub>
PANX +hv	→ CXO <sub>3</sub> + NO <sub>2</sub>
PACD +hv	→ MEO <sub>2</sub> + OH
ALDX +hv	→ MEO <sub>2</sub> + CO+ HO <sub>2</sub>

## References

- W. M. Cox and J. A. Tikvart. A statistical procedure for determining the best performing air quality simulation model . *Atmospheric Environment. Part A. General Topics*, 24(9): 2387 – 2395, 1990. ISSN 0960-1686. doi: [http://dx.doi.org/10.1016/0960-1686\(90\)90331-G](http://dx.doi.org/10.1016/0960-1686(90)90331-G).
- A. Russell and R. Dennis. NARSTO critical review of photochemical models and modeling . *Atmospheric Environment*, 34(12–14):2283 – 2324, 2000. ISSN 1352-2310. doi: [http://dx.doi.org/10.1016/S1352-2310\(99\)00468-9](http://dx.doi.org/10.1016/S1352-2310(99)00468-9).
- U.S.EPA. Guideline for Regulatory Application of the Urban Airshed Model. Technical report, EPA-450/4-91-013. U.S. Environmental Protection Agency, Office of Air Quality Planning and Standards, Research Triangle Park, NC., 1991.